

CITY OF SCOTTSDALE

**DESERT GREENBELT PROJECT  
PIMA ROAD CHANNEL**

**DESIGN HYDROLOGY MEMORANDUM**

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**FINAL  
DRAFT**

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*George V. Sabol Consulting Engineers, Inc.*  
Scottsdale, Arizona

January 1997

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(In separate volume)

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2	DC Ranch on-site watershed map
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4	Watershed delineation per Greiner
5	Soils map
6	Land use map

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A	HEC-1 Option 1 output file (100-year, 6-hour storm)
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## INTRODUCTION

### General

The hydrology for the final design of the Pima Road Channel is presented in this Design Hydrology Memorandum. The hydrology is for the three detention basin concept that is recommended and the preliminary sizing of those detention basins along with the design discharges for the channel are also presented herein.

Two methods were evaluated for the purpose of estimating design hydrology; 1) the method that is used for previous flood hydrology studies in the Scottsdale area north of the CAP Canal (herein referred to as the City of Scottsdale (COS) method), and 2) the method in the Drainage Design Manual for Maricopa County, Volume 1, Hydrology (herein referred to as the Maricopa County (MC) method). Based on the results of that evaluation, the COS method is used to estimate the design hydrology for the Pima Road Channel.

The hydrology is based on the best available topographic mapping of the watershed and the hydrologic modeling represents the most current information on land use and development within the watershed. The hydrologic modeling that was performed by others for the Grayhawk and DC Ranch developments are incorporated into the watershed models.

### Background

The hydrology of the study area has been performed by others for various purposes, including FEMA flood hazard delineation, highway drainage studies, land development, and the Desert Greenbelt Project. Virtually all of that current hydrology (dating to the late 1980s) is based on the modeling by Mr. Robert L. Ward, PE. The previous modeling for the Pima Road Channel was performed by Greiner and PACE by modifying and updating previous models by Mr. Ward. In the process of reviewing the design concepts by Greiner and PACE for the Pima Road Channel, the reviewer for the City of Scottsdale, George V. Sabol Consulting Engineers, Inc. (GVSCE), noted deficiencies in the model (see Concept Review report, November 1996, by GVSCE). As a consequence, the City of Scottsdale requested that GVSCE revise the hydrology. Subsequently, the hydrology was revised and modified for the purpose of defining the design hydrology for the recommended Pima Road Channel concept (see Recommended Design Concept and Construction Cost Estimate report, December 1996, by GVSCE).

### **Purpose and Limitation**

This report presents the design hydrology and preliminary sizing of the three detention basins for the Pima Road Channel. Two options are considered for the Deer Valley basin; 1) that basin receives the combined runoff from the Pima Road Channel that enters the basin from the north plus the runoff from the Deer Valley collector channel that is at the north boundary of DC Ranch, and 2) that basin receives only the runoff from the Pima Road Channel and the Deer Valley collector channel bypasses the Deer Valley basin and discharges directly to the Pima Road Channel south of the Deer Valley basin. Those two options are called Option 1 and 2.

The design hydrology is determined from the 100-year, 6-hour storm. The performance of the basins are evaluated for the 100-year, 24-hour storm. The basins are sized such that the spillways do not operate for the 100-year, 6-hour storm.

The design discharges for the Pima Road Channel are contingent upon the preliminary sizing of the Happy Valley and Deer Valley detention basins and the outlets of those basins. Refinement or modification of those detention basins and/or outlets will have some impact on the design discharges for the channel. The hydrology conceivably will be altered somewhat as the final design of the Pima Road Channel and the detention basins is performed. The hydrology, as presented herein, is intended to represent the ultimate, full build-out condition of the watershed. It is based on the most reliable data and assumptions in regard to land use and drainage design. The hydrologic model can be used by the City of Scottsdale for master drainage planning. The model incorporates the drainage modeling for the DC Ranch and Grayhawk developments as presently available. Changes in the drainage designs for those areas could impact the results of this hydrology and the design discharges for the Pima Road Channel.

## MAPPING

### **Watershed Base Maps**

Previous hydrologic modeling of the study area (those by Ward, Greiner, PACE, etc.) used USGS quadrangle maps for watershed delineation and estimation of hydraulic parameters. The USGS maps are at a scale of 1 inch = 2,000 feet with contour interval of 10- or 20-foot. The present study uses the topographic mapping that is available from the City of Scottsdale's GIS at 1-foot or 2-foot contour interval based on 1993 aerial photography.

The watershed base map is shown in Plate 1 at a scale of 1 inch = 500 feet with 5-foot or 10-foot contour intervals. That map shows the entire contributing watershed from north of Jomax Road to the Pima Freeway alignment. For hydrologic modeling purposes, two additional maps are used to account for the hydrologic modeling of DC Ranch and Grayhawk developments. The DC Ranch on-site development area is shown in Plate 2. The Grayhawk hydrologic modeling area is shown in Plate 3. Plates 2 and 3 are obtained from the drainage engineers for DC Ranch and Grayhawk and are shown without modification.

### **Watershed Delineation**

The watershed delineation and concentration point identification is shown in Plates 1, 2 and 3. The watershed delineation that was used by Greiner is shown in Plate 4, and that map is provided for reference only. The numbering of concentration points that is shown in Plate 1 is the same as that used in previous hydrology studies (Plate 4). The numbering of concentration points used in the DC Ranch and Grayhawk models (Plates 2 and 3) are maintained in the present hydrologic model.

The use of the better mapping that is available from the City of Scottsdale coupled with field reconnaissance of the watershed resulted in the identification of two flow-split areas. Those are identified in Plate 1. The modeling of those flow-splits was by development of rating curves for the discharge capacity at each flow-split. The basins are sized according to the flow-split analyses and the design discharges assume that those flow-splits will continue to exist under future build-out conditions. Since those flow-splits are in presently developed areas, this is a reasonable assumption. For the purpose of checking the performance of the detention basins for the 100-year, 24-hour storm, it was

assumed that the discharge at the flow-splits would be altered such that all the flow took one flowpath or the other. The most severe hydrologic condition was assumed to exist for checking the performance of each basin under the condition of the 100-year, 24-hour storm. For the Deer Valley basin, several combinations of flow-split assumptions were made since it is not possible to predict the most severe condition.

The redelineation of the watershed using the better topographic mapping resulted in some meaningful changes from the previous delineation (comparison of Plates 1 and 4). A comparison of the drainage area changes at key concentration points along the Pima Road Channel is provided in Table 1. The most significant change is for concentration point C34.1I which is at the inflow to the Happy Valley basin. That drainage area increased from 2.38 square miles to 2.90 square miles (increase of 0.52 square miles).

TABLE 1

Comparison of drainage areas at key concentration points along the Pima Road Channel as a result of redelineation of the watershed

Concentration Point	Drainage Area		Comments
	Original <sup>a</sup> sq. miles	Revised sq. miles	
(1)	(2)	(3)	(4)
C30N	0.66	0.65	Jomax Road
C31.1	1.18	0.92	
C34.1I	2.38	2.90	Happy Valley Detention Basin
C36.1	2.61	3.04	
C36R1	4.76	4.64	Pinnacle Peak Road
C36R2	5.06	5.01	
C51.1I	6.28	6.14	Deer Valley Detention Basin
C52A	6.43	6.27	Thompson Peak Parkway
C52	8.01	7.92	Beardsley Road Alignment
C53	8.58	8.09	
C53A	-----	8.42	Union Hills Road
C1I	11.23	11.05	Union Hills Detention Basin
C1A	11.31	11.27	CAP Basin outlet

<sup>a</sup> - as per Greiner and others

## SELECTION OF WATERSHED MODELING METHOD

### Description of Models

Two methods of watershed modeling were compared for the purpose of selecting the recommended hydrologic modeling method. Those methods are generally described as follows:

1. Hydrologic modeling as previously used by Ward, Greiner, PACE and others for the Pima Road Channel and other projects in the area. That modeling generally consists of use of the hypothetical rainfall distribution, CN method for rainfall losses, kinematic wave modeling of runoff from subbasins, and normal depth for channel routing. That is the general modeling methodology that is recommended in the City of Scottsdale Design Standards and Policies Manual, Chapter 2: Drainage. The modeling methodology is referred to herein as the City of Scottsdale (COS) method.
2. Hydrologic modeling as defined in the Drainage Design Manual for Maricopa County, Volume 1, Hydrology. That modeling consists of a 6-hour storm defined by Pattern Number or the SCS distribution for the 24-hour storm, Green and Ampt method for rainfall losses, Clark unit hydrograph, and normal depth for channel routing. The modeling methodology is referred to herein as the Maricopa County (MC) method.

Hydrologically, the two methods represent significantly different technologies and methodologies. Such differences could produce dramatically different results, depending upon assumptions and input parameter selection.

For the purpose of model method comparison and selection, the watershed area north of the Deer Valley basin was modeled by each method. The area south of the Deer Valley basin was not included in the methodology comparison because most of that area will be modeled by adoption of the drainage studies for DC Ranch and Grayhawk. Therefore, that southern watershed area will have little impact on the comparison of results.

Rainfall input is based on the rainfall depth-duration-frequency statistics from the Precipitation-Frequency Atlas for Arizona (NOAA Atlas). Rainfall depth-duration-frequency statistics from the NOAA Atlas, as developed by the PREFRE program, are shown in Table 2. Comparison of rainfall values from other hydrologic models shows that rainfall input often deviates slightly from the values shown in Table 2. Those deviations are not considered to be meaningful. The point rainfalls for the present modeling are adopted from the Greiner models.

A comparison of the 6-hour storm rainfall distributions by the COS method (hypothetical) and the MC method (Pattern Number) is shown in Figure 1. Those distributions are for the watershed area at the Deer Valley basin. Other than the timing of the maximum rainfall intensity portion of the storm, the distributions are very similar.

A comparison of the 24-hour storm rainfall distributions by the COS method (hypothetical) and the MC method (SCS 24-hour dimensionless) is shown in Figure 2. Those distributions are for the watershed area at the Deer Valley basin. The hypothetical distribution has significantly greater rainfall intensity than the SCS dimensionless distribution. For the 24-hour storm, the COS-type model will produce greater peak discharges than the MC-type model, all other input being equal.

Both the COS model and the MC model used the same watershed delineation as shown in Plate 1. The land use and percent impervious area (RTIMP) are the same in both models. A summary of the COS model input for each modeling subbasin and channel routings is shown in Table 3.

The rainfall loss parameters by the Green and Ampt equation for the MC method are summarized in Table 4. Those parameters are based on soils data contained in the SCS Soil Survey of Aguila-Carefree Area and Parts of Maricopa and Pinal Counties. The CN selection for the COS method are based on that same SCS soils data. A soils map of the watershed is shown in Plate 5. A land use map is shown in Plate 6 and that information was used to select the RTIMP for each subbasin as shown in Tables 3 and 4. Rainfall loss parameters by both methods are for future full build-out conditions.

TABLE 2

Rainfall depth-duration-frequency statistics for the Pima Road Channel watershed  
(from PREFRE based on NOAA Atlas input)

1

\*\*\* O U T P U T   D A T A \*\*\*

REVISED JUNE 1988 TO UPDATE COMPUTATION OF SHORT-DURATION VALUES

PRECIPITATION FREQUENCY VALUES FOR Pima Channel Revised Hydrology

PRIMARY ZONE NUMBER= 7

SHORT-DURATION ZONE NUMBER= 8

POINT VALUES

DURATION	RETURN PERIOD							
	2-YR	5-YR	10-YR	25-YR	50-YR	100-YR	500-YR	
5-MIN	.38	.46	.52	.61	.68	.74	.90	5-MIN
10-MIN	.56	.70	.79	.93	1.03	1.14	1.38	10-MIN
15-MIN	.68	.87	1.00	1.18	1.32	1.46	1.79	15-MIN
30-MIN	.91	1.16	1.34	1.59	1.79	1.98	2.43	30-MIN
1-HR	1.10	1.43	1.66	1.98	2.23	2.48	3.05	1-HR
2-HR	1.24	1.60	1.86	2.21	2.49	2.76	3.40	2-HR
3-HR	1.33	1.72	1.99	2.36	2.66	2.95	3.63	3-HR
6-HR	1.50	1.93	2.23	2.65	2.98	3.31	4.07	6-HR
12-HR	1.70	2.19	2.52	3.00	3.37	3.74	4.59	12-HR
24-HR	1.90	2.44	2.82	3.35	3.76	4.17	5.12	24-HR

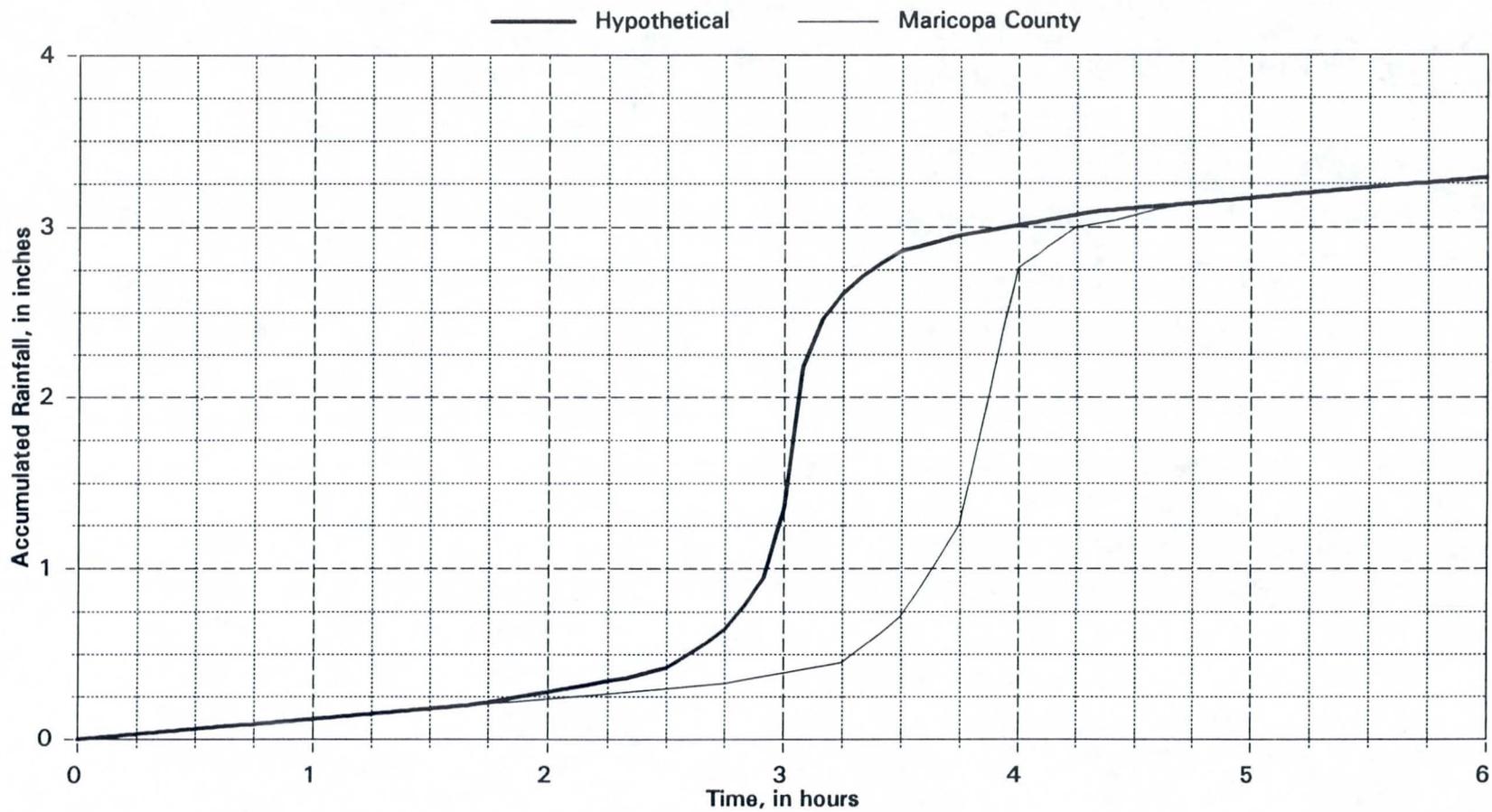
\* IF YOUR SITE IS IN ARIZONA OR NEW MEXICO, PLEASE CONSULT THE FOLLOWING PAPER FOR REVISED DEPTH-AREA VALUES:

DEPTH-AREA RATIOS IN THE SEMI-ARID SOUTHWEST UNITED STATES  
NOAA TECHNICAL MEMORANDUM NWS HYDRO-40  
ZEHR AND MYERS  
AUGUST 1984

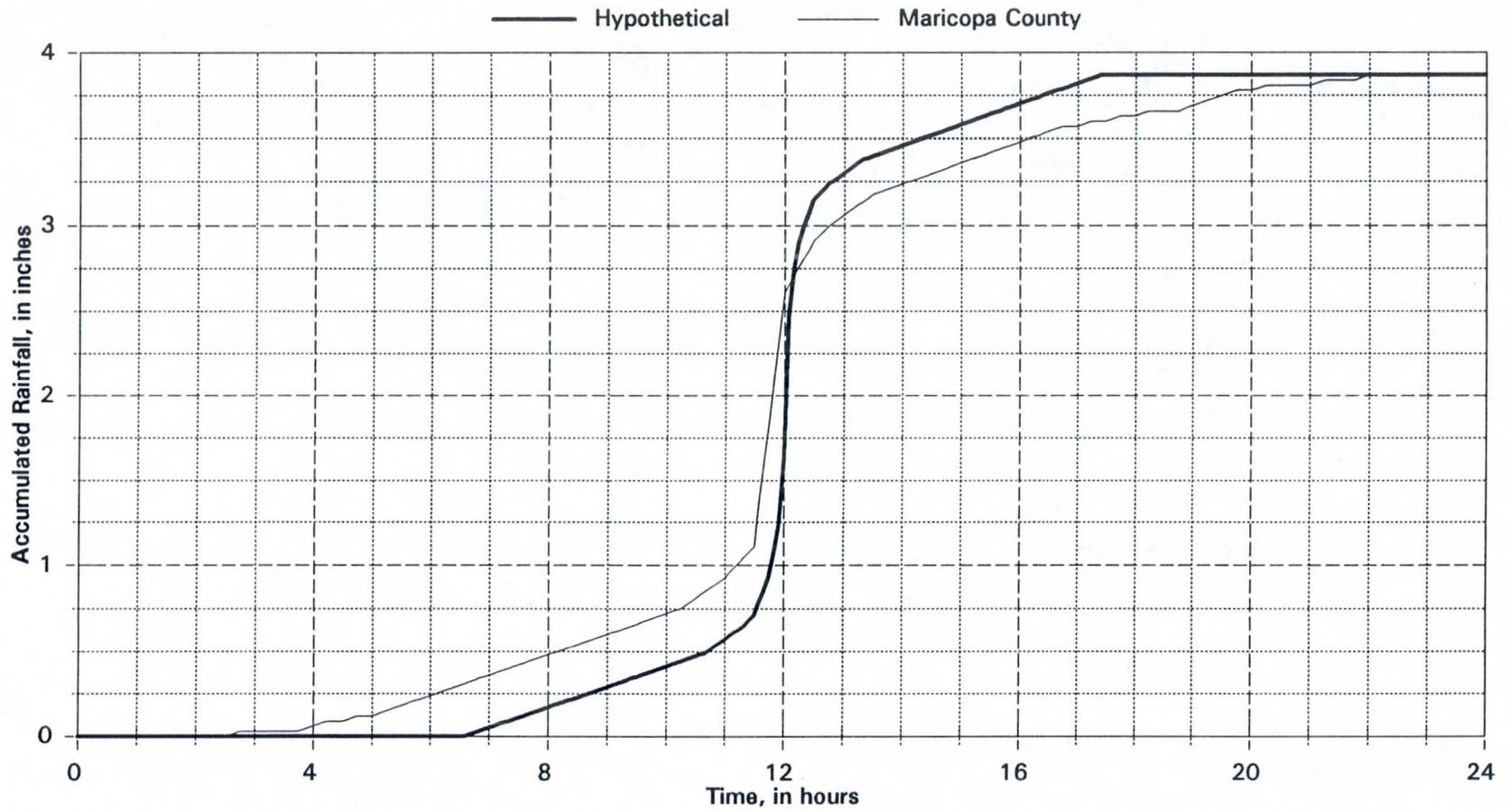
INPUT DATA

PROJECT NAME=Pima Channel Revised Hydrology  
ZONE= 7      SHORT-DURATION ZONE= 8  
LATITUDE= .00      LONGITUDE= 100.00      ELEVATION= 0  
2-YR, 6-HR PCPN= 1.50      100-YR, 6-HR PCPN= 3.31  
2-YR, 24-HR PCPN= 1.90      100-YR, 24-HR PCPN= 4.17

\* \* \* \* E N D   O F   R U N   \* \* \* \*



**FIGURE 1**  
**100-year, 6-hour rainfall comparison**



**FIGURE 2**  
**100-year, 24-hour rainfall comparison**

TABLE 3

Rainfall loss and runoff hydraulic parameters for the COS method  
For model comparison purposes

Subbasin ID	Area sq. mi.	Losses		Overland Flow				Collector Channel							Main Channel					
		CN	RTIMP %	Length feet	Slope ft/ft	n	% Contributing	Length feet	Slope ft/ft	n	Contrib. Area sm	Channel Shape	Bottom Width feet	Side Slope	Length feet	Slope %	n	Channel Shape	Bottom Width feet	Side Slope
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)	(16)	(17)	(18)	(19)	(20)	(21)
S30N	0.6518	82.0	13	300	0.350	0.13	20	1550	0.069	0.045	0.0096	TRAP	0	12	10520	0.038	0.040	TRAP	15	15
		82.0	13	300	0.050	0.13	80													
S31.1	0.2663	76.6	13	300	0.567	0.13	10	1950	0.056	0.045	0.0147	TRAP	0	10	7600	0.035	0.040	TRAP	22	8
		76.6	13	300	0.050	0.13	90													
S35N	0.5482	82.0	13	300	0.491	0.13	15	2700	0.079	0.045	0.0242	TRAP	3	6	5050	0.028	0.040	TRAP	15	15
		82.0	13	300	0.113	0.13	85													
S36.2	0.2087	76.6	13	300	0.580	0.13	5	1800	0.036	0.045	0.0145	TRAP	10	10	3520	0.028	0.040	TRAP	20	6
		76.6	13	300	0.100	0.13	95													
S34.1	1.6076	77.3	12	300	0.590	0.13	25	2570	0.085	0.045	0.0214	TRAP	0	10	9200	0.042	0.040	TRAP	50	9
		77.3	12	300	0.040	0.13	75													
S36.1	0.1394	73.4	11	300	0.042	0.13	100	2330	0.032	0.045	0.0134	TRAP	10	30	3200	0.027	0.040	TRAP	20	30
S36R1	1.2173	74.3	10	300	0.020	0.20	100	1420	0.032	0.045	0.0061	TRAP	0	13	12600	0.033	0.040	TRAP	10	9
S36R2	0.3742	72.0	16	280	0.045	0.10	100	1900	0.032	0.017	0.0150	TRAP	15	7	7360	0.030	0.040	TRAP	30	10
S51.1	1.1300	73.9	12	300	0.037	0.13	100	1800	0.038	0.045	0.0161	TRAP	0	12	14400	0.032	0.040	TRAP	40	15

TABLE 4

Green and Ampt rainfall loss parameters for the MC method  
For model comparison purposes

Sub-basin ID (1)	Area sq. mi. (2)	IA inches (3)	RTIMP % (4)	Vegetation Cover % (5)	XKSAT		DTHETA normal (8)	XKSAT Corrected for Veg. in/hr (9)
					Bare Ground in/hr (6)	PSIF inches (7)		
S30N	0.6518	0.25	13	20	0.13	6.40	0.21	0.14
S31.1	0.2663	0.25	13	20	0.18	5.60	0.25	0.20
S35N	0.5482	0.25	13	20	0.16	5.80	0.25	0.18
S36.2	0.2087	0.25	13	20	0.23	5.00	0.25	0.26
S34.1	1.6076	0.25	12	20	0.26	4.70	0.25	0.29
S36.1	0.1394	0.25	11	20	0.33	4.35	0.25	0.37
S36R1	1.2173	0.25	10	20	0.17	5.70	0.25	0.19
S36R2	0.3742	0.25	16	20	0.35	4.25	0.25	0.39
S51.1	1.1300	0.25	12	20	0.20	5.30	0.25	0.22

The Clark unit hydrograph parameters for the MC method are summarized in Table 5. Those parameters are based on topographic data as shown in Plate 1 and land use as shown in Plate 6. The procedures for calculating the unit hydrograph parameters (Tc and R) are as presented in the Maricopa County manual.

Routing in the Pima Road Channel is by the normal depth method and is the same in both the COS and MC models.

#### **Model Comparison Results and Selection of Model**

The COS and MC methods, with input as previously described, were used to model the watershed that contributes to the Deer Valley basin. For comparison purposes, neither the Happy Valley nor the Deer Valley basins are incorporated into the models. Peak discharges at key concentration points in the Pima Road Channel are shown in Table 6. The peak discharges that were used by Greiner for its Concept 1 design are also shown for comparison. Results are shown for both the 100-year, 6-hour and 24-hour storms.

For the 6-hour storm, almost identical peak discharges are obtained by both the COS and MC methods. For the 24-hour storm, the MC model produces peak discharges that are 20 to 38 percent less than the COS model. This is because of the differences in rainfall distribution and the methods in estimating rainfall losses. Of most significance is that using the MC method, the peak discharges for the 24-hour storm are less than those for the 6-hour storm. The consequence of this is that the 6-hour storm dictates the design discharge. This is expected for a small drainage area such as that for the Pima Road Channel.

Runoff volumes at the Happy Valley (C34.11) and Deer Valley (C51.11) basin sites are shown in Table 7. For the 6-hour storm, the MC method gives about 10 percent more runoff volume than the COS method. For the 24-hour storm, the COS method gives about 25 percent more runoff volume than the MC method. Of significant consequence is that using the MC method, the runoff volumes for both the 6-hour and 24-hour storms are about equivalent.

TABLE 5

Clark unit hydrograph parameters for the MC method  
For model comparison purposes

Subbasin ID (1)	Area sq. mi. (2)	Hydrograph Type (3)	Flow Path miles (4)	Slope ft/mile (5)	Adjusted Slope ft/mile (6)	Surface Roughness Type (7)	Kb (9)	Time-Area Relation (10)	Tc hrs (11)	R hrs (12)
S30N	0.6518	Clark	2.33	251.1	238.5	B	0.04	B	0.367	0.305
S31.1	0.2663	Clark	1.96	350.4	283.1	B	0.05	B	0.321	0.381
S35N	0.5482	Clark	1.20	388.5	296.9	B	0.05	B	0.163	0.080
S36.2	0.2087	Clark	0.91	569.9	315.9	B	0.05	B	0.179	0.124
S34.1	1.6076	Clark	2.17	426.3	298.0	B	0.04	B	0.350	0.164
S36.1	0.1394	Clark	1.10	168.5	168.5	B	0.05	B	0.200	0.205
S36R1	1.2173	Clark	2.68	174.2	174.2	B/C	0.06	B	0.317	0.203
S36R2	0.3742	Clark	1.39	158.8	158.8	A	0.03	A	0.217	0.155
S51.1	1.1300	Clark	2.78	169.0	169.0	B	0.04	B	0.329	0.228

TABLE 6

Comparison of 100-year, 6-hour and 100-year, 24-hour peak discharges  
at key concentration points along Pima Road Channel for COS and MC methods

Concentration Point	Drainage Area		100-year, 6-hour Peak			100-year, 24-hour Peak		
	Original sq. miles	Revised sq. miles	Discharges			Discharges		
			Original	Present Study		Original	Present Study	
	(1)	(2)	(3)	Original cfs	COS cfs	MC cfs	Original cfs	COS cfs
C30N	0.66	0.65	820	1,230	1,180	910	1,260	780
C31.1	1.18	0.92	1,410	1,470	1,460	1,610	1,650	1,020
C34.1I	2.38	2.90	2,880	3,670	3,490	3,450	4,280	3,280
C36.1	2.61	3.04	3,120	3,710	3,610	3,730	4,470	3,370
C36R1	4.76	4.64	5,070	4,940	4,940	6,080	6,020	4,750
C36R2	5.06	5.01	5,326	5,030	5,110	6,280	6,160	4,960
C51.1I	6.28	6.14	5,703	5,900	6,050	6,950	7,460	5,990

Note:

Original refers to the Greiner hydrology model - PIMA53R, dated March 96  
Revised refers to the hydrology performed by GVSCE

TABLE 7

Comparison of 100-year, 6-hour and 100-year, 24-hour runoff volumes at the Happy Valley and Deer Valley detention basins for COS and MC methods

Concentration Point	Drainage Area		100-year, 6-hour Runoff Volumes			100-year, 24-hour Runoff Volumes		
	Original	Revised	Original	Present Study		Original	Present Study	
	sq. miles	sq. miles	acre-ft	COS	MC	acre-ft	COS	MC
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)
C34.1I	2.38	2.90	198	249	272	282	354	261
C51.1I	6.28	6.14	493	480	529	717	700	536

Based on these comparisons, it is recommended that the COS method be used for design hydrology for the Pima Road Channel project. This recommendation is based on the following:

- The peak discharges for the 6-hour storm are about identical for both the COS and MC methods.
- The peak discharges for the 24-hour storm are larger for the COS method than the MC method.
- The runoff volumes for the 6-hour storm are about the same by both methods.
- The runoff volumes for the 24-hour storm are larger for the COS method.
- Overall, using the 100-year, 6-hour storm as the design event will result in nearly the same design regardless of which method is used.
- Using the 100-year, 24-hour storm and the COS method to check the design for performance during a general storm will result in a conservative analysis.
- The COS method is used for the DC Ranch and Grayhawk hydrology which is incorporated into this project hydrology.
- The COS method is used on other Desert Greenbelt, FEMA and other regional hydrologic studies, and use of that method for the Pima Road Channel will result in a consistent methodology.

## WATERSHED MODEL

Subbasin model input by the COS method for the design hydrology is summarized in Table 8. Refer to Plates 1, 2 and 3 for location of subbasins and concentration points. A schematic diagram of the watershed and hydrologic model is shown in Figure 3 (provided in jacket of this report). Input for DC Ranch and Grayhawk are as per models provided by Wood/Patel Associates and DEI, respectively. Certain small subbasins south of DC Ranch and Grayhawk were added to "fill-in" the model. The model is used to size each of the three detention basins and to set design discharges for the channel. The design hydrology is for the 100-year, 6-hour storm. Two Options (1 and 2) are considered for the Deer Valley Basin and the design hydrology is provided for each Option. The HEC-1 output files for each Option are provided in Appendices A and B. A diskette is provided for those input and output files. Table 9 summarizes peak discharges from the subbasins. Table 10 summarizes peak discharges at key concentration points for both Options. The performance of the basins, including spillway discharge, is evaluated based on the 100-year, 24-hour storm. Various information is provided for the detention basins in Appendix C, and this includes area-capacity curves, outlet rating curves, stage hydrographs, and inflow and outflow hydrographs for both Options under different flow-split assumptions.

TABLE 8

Subbasin input parameters for the Pima Road Channel design hydrology  
Future full build-out conditions

Subbasin ID	Drainage Area sq. mi.	Rainfall Losses		Overland Flow Element				Collector Channel Element							Main Channel Element					
		Curve No.	RTIMP %	Length feet	Slope ft/ft	n	% Contributing	Length feet	Slope ft/ft	n	Contrib. Area sm	Shape	Bottom Width	Side Slopes	Length feet	Slope ft/ft	n	Shape	Bottom Width	Side Slopes
		(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)	(16)	(17)	(18)	(19)	(20)	(21)
S30N	0.6518	82.0	13	300	0.350	0.13	20	1550	0.069	0.045	0.0096	TRAP	0	12	10520	0.038	0.040	TRAP	15	15
		82.0	13	300	0.050	0.13	80													
S31.1	0.2663	76.6	13	300	0.567	0.13	10	1950	0.056	0.045	0.0147	TRAP	0	10	7600	0.035	0.040	TRAP	22	8
		76.6	13	300	0.050	0.13	90													
S35N	0.5482	82.0	13	300	0.491	0.13	15	2700	0.079	0.045	0.0242	TRAP	3	6	5050	0.028	0.040	TRAP	15	15
		82.0	13	300	0.113	0.13	85													
S36.2	0.2087	76.6	13	300	0.580	0.13	5	1800	0.036	0.045	0.0145	TRAP	10	10	3520	0.028	0.040	TRAP	20	6
		76.6	13	300	0.100	0.13	95													
S34.1	1.6076	77.3	12	300	0.590	0.13	25	2570	0.085	0.045	0.0214	TRAP	0	10	9200	0.042	0.040	TRAP	50	9
		77.3	12	300	0.040	0.13	75													
S36.1	0.1394	73.4	11	300	0.042	0.13	100	2330	0.032	0.045	0.0134	TRAP	10	30	3200	0.027	0.040	TRAP	20	30
S36R1	1.2173	74.3	10	300	0.020	0.20	100	1420	0.032	0.045	0.0061	TRAP	0	13	12600	0.033	0.040	TRAP	10	9
S36R2	0.3742	72.0	16	280	0.045	0.10	100	1900	0.032	0.017	0.0150	TRAP	15	7	7360	0.030	0.040	TRAP	30	10
S51.1	1.1300	73.9	12	300	0.037	0.13	100	1800	0.038	0.045	0.0161	TRAP	0	12	14400	0.032	0.040	TRAP	40	15
*** BEGIN DC RANCH WATERSHED ***																				
52D4	0.0700	75	14.5	120	0.01	0.15	100	---	---	---	---	---	---	---	3100	0.035	0.045	TRAP	30	10
52D4B	0.0220	75	63	120	0.01	0.15	100	---	---	---	---	---	---	---	2200	0.033	0.045	TRAP	30	10
52D5A	0.0232	75	63	120	0.01	0.15	100	---	---	---	---	---	---	---	1300	0.032	0.045	TRAP	30	10
52C3	0.0060	75	65	100	0.02	0.1	100	---	---	---	---	---	---	---	800	0.033	0.045	TRAP	30	10
52C3B	0.0160	75	60	100	0.02	0.1	100	---	---	---	---	---	---	---	1400	0.034	0.045	TRAP	30	10
51C	0.0972	74	15	100	0.0213	0.1	100	---	---	---	---	---	---	---	3900	0.0375	0.045	TRAP	30	10
52C1	0.0290	75	20.5	100	0.02	0.1	100	---	---	---	---	---	---	---	1350	0.021	0.045	TRAP	30	10
52C2A	0.0190	75	2	100	0.02	0.1	100	---	---	---	---	---	---	---	1500	0.033	0.045	TRAP	30	10
52C2B	0.0275	75	11	100	0.02	0.1	100	---	---	---	---	---	---	---	2000	0.03	0.045	TRAP	30	10
52C2C	0.0140	75	62	100	0.02	0.1	100	---	---	---	---	---	---	---	1500	0.04	0.045	TRAP	30	10
52C4	0.0170	75	60	100	0.02	0.1	100	---	---	---	---	---	---	---	1550	0.03	0.045	TRAP	30	10
52C13	0.0230	75	31	100	0.02	0.1	100	---	---	---	---	---	---	---	950	0.04	0.045	TRAP	30	10
52C15	0.0460	75	64.4	100	0.02	0.1	100	---	---	---	---	---	---	---	2050	0.036	0.045	TRAP	30	10
52C14A	0.0410	75	67.7	100	0.02	0.1	100	---	---	---	---	---	---	---	2050	0.031	0.045	TRAP	30	10
52C5	0.0160	75	27	100	0.02	0.1	100	---	---	---	---	---	---	---	1200	0.03	0.045	TRAP	30	10
52C6	0.0360	75	31.4	100	0.02	0.1	100	---	---	---	---	---	---	---	3100	0.035	0.045	TRAP	30	10
51B	0.5711	71.9	13.1	100	0.0213	0.1	100	---	---	---	---	---	---	---	8900	0.03	0.045	TRAP	50	25
52C7	0.0060	75	27	100	0.02	0.1	100	---	---	---	---	---	---	---	550	0.04	0.045	TRAP	30	10
52C8	0.0080	75	27	100	0.02	0.1	100	---	---	---	---	---	---	---	750	0.034	0.045	TRAP	30	10
52C9	0.0690	75	31.85	100	0.02	0.1	100	---	---	---	---	---	---	---	3150	0.036	0.045	TRAP	30	10
52C10	0.0140	75	7.85	100	0.02	0.1	100	---	---	---	---	---	---	---	800	0.032	0.045	TRAP	30	10
52C11	0.0425	75	27	100	0.02	0.1	100	---	---	---	---	---	---	---	2800	0.031	0.045	TRAP	30	10
52C12	0.0230	75	85	100	0.02	0.1	100	---	---	---	---	---	---	---	900	0.03	0.045	TRAP	30	10

TABLE 8

Subbasin input parameters for the Pima Road Channel design hydrology  
Future full build-out conditions

Subbasin ID	Drainage Area sq. mi.	Rainfall Losses		Overland Flow Element				Collector Channel Element							Main Channel Element						
		Curve No.	RTIMP %	Length feet	Slope ft/ft	n	% Contributing	Length feet	Slope ft/ft	n	Contrib. Area sm	Shape	Bottom Width	Side Slopes	Length feet	Slope ft/ft	n	Shape	Bottom Width	Side Slopes	
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)	(16)	(17)	(18)	(19)	(20)	(21)	
52C14B	0.0210	75	60	100	0.02	0.1	100	---	---	---	---	---	---	---	1250	0.029	0.045	TRAP	30	10	
52B1	0.0030	75	27	100	0.02	0.1	100	---	---	---	---	---	---	---	600	0.039	0.045	TRAP	30	10	
52B2	0.0320	75	17	100	0.02	0.1	100	---	---	---	---	---	---	---	2350	0.037	0.045	TRAP	30	10	
52B3	0.0620	75	31.8	100	0.02	0.1	100	---	---	---	---	---	---	---	3450	0.03	0.045	TRAP	30	10	
52B4	0.0260	75	62	100	0.02	0.1	100	---	---	---	---	---	---	---	1700	0.024	0.045	TRAP	30	10	
52B5	0.0210	75	56.9	100	0.02	0.1	100	---	---	---	---	---	---	---	1400	0.03	0.045	TRAP	30	10	
52B6	0.0960	75	13.55	100	0.02	0.1	100	---	---	---	---	---	---	---	3200	0.033	0.045	TRAP	30	10	
52B7	0.0800	75	78.45	100	0.02	0.1	100	---	---	---	---	---	---	---	2750	0.028	0.045	TRAP	30	10	
52A2	0.0650	75	88.8	100	0.02	0.1	100	---	---	---	---	---	---	---	2900	0.023	0.045	TRAP	30	10	
52A1	0.1300	75	32.25	100	0.02	0.1	100	---	---	---	---	---	---	---	3400	0.033	0.045	TRAP	30	10	
*** END DC RANCH WATERSHED ***																					
*** BEGIN GRAYHAWK WATERSHED ***																					
37A	0.6765	74	24.8	61	0.0213	0.1	100	---	---	---	---	---	---	---	4800	0.0237	0.045	TRAP	50	130	
SUB5N	0.0290	77	18	100	0.013	0.15	100	1000	0.005	0.018	0.015	TRAP	50	20	500	0.015	0.025	TRAP	10	4	
SUB6B	0.0320	81	0	200	0.025	0.15	100	---	---	---	---	---	---	---	1300	0.015	0.025	TRAP	10	4	
SUB1N	0.0190	77	18	100	0.013	0.15	100	---	---	---	---	---	---	---	1470	0.0204	0.018	TRAP	50	20	
SUB2NA	0.0150	81	0	150	0.013	0.15	100	---	---	---	---	---	---	---	1050	0.0215	0.025	TRAP	20	6	
SUB2NB	0.0300	77	53	150	0.013	0.15	100	---	---	---	---	---	---	---	1200	0.015	0.025	TRAP	20	50	
SUB6N	0.0490	81	0	200	0.025	0.15	100	---	---	---	---	---	---	---	1300	0.015	0.025	TRAP	10	4	
SUB3N	0.0270	81	0	100	0.02	0.15	100	---	---	---	---	---	---	---	2800	0.0207	0.025	TRAP	10	4	
SUB4N	0.0320	77	18	100	0.015	0.15	100	---	---	---	---	---	---	---	1200	0.007	0.018	TRAP	50	20	
SUB6A	0.0130	83	68	100	0.015	0.12	100	---	---	---	---	---	---	---	800	0.01	0.025	TRAP	2	3	
SUB3C	0.0104	77	68	100	0.025	0.02	100	---	---	---	---	---	---	---	600	0.015	0.035	TRAP	50	20	
GC1018	0.0440	81	0	200	0.025	0.15	100	---	---	---	---	---	---	---	1800	0.0233	0.025	TRAP	10	4	
GC1-9	0.0260	81	0	200	0.025	0.15	100	---	---	---	---	---	---	---	2110	0.022	0.025	TRAP	10	4	
SUB3S	0.0102	77	53	100	0.01	0.15	100	---	---	---	---	---	---	---	930	0.016	0.025	TRAP	50	20	
SUB4S	0.0273	77	53	100	0.01	0.15	100	---	---	---	---	---	---	---	1780	0.018	0.015	TRAP	50	20	
GC2-8	0.0140	81	0	200	0.025	0.15	100	---	---	---	---	---	---	---	980	0.016	0.025	TRAP	10	4	
SUB3D3	0.0140	81	0	50	0.015	0.1	100	---	---	---	---	---	---	---	2450	0.016	0.025	TRAP	5	4	
GC7	0.0134	81	0	200	0.025	0.15	100	---	---	---	---	---	---	---	1380	0.02	0.025	TRAP	10	4	
SUB3D1	0.0088	77	34	SCS dimensionless hydrograph with a lag time of 0.06 hrs.				---	---	---	---	---	---	---	---	---	---	---	---	---	---
SUB3B1	0.0137	77	47	SCS dimensionless hydrograph with a lag time of 0.06 hrs.				---	---	---	---	---	---	---	---	---	---	---	---	---	---
SUB3F	0.0344	77	68	100	0.025	0.15	100	---	---	---	---	---	---	---	1000	0.015	0.025	TRAP	100	20	
SUB3B2	0.0246	77	40	SCS dimensionless hydrograph with a lag time of 0.10 hrs.				---	---	---	---	---	---	---	---	---	---	---	---	---	---
SUB3E1	0.0246	77	40	SCS dimensionless hydrograph with a lag time of 0.10 hrs.				---	---	---	---	---	---	---	---	---	---	---	---	---	---
SUB3D2	0.0220	77	35	SCS dimensionless hydrograph with a lag time of 0.08 hrs.				---	---	---	---	---	---	---	---	---	---	---	---	---	---
SUB3E2	0.0120	77	35	SCS dimensionless hydrograph with a lag time of 0.06 hrs.				---	---	---	---	---	---	---	---	---	---	---	---	---	---
PC3*	0.0434	77	10	100	0.015	0.15	100	---	---	---	---	---	---	---	2200	0.01	0.03	TRAP	30	4	

TABLE 8

Subbasin input parameters for the Pima Road Channel design hydrology  
Future full build-out conditions

Subbasin ID	Drainage Area sq. mi.	Rainfall Losses		Overland Flow Element				Collector Channel Element							Main Channel Element					
		Curve No.	RTIMP %	Length feet	Slope ft/ft	n	% Contributing	Length feet	Slope ft/ft	n	Contrib. Area sm	Shape	Bottom Width	Side Slopes	Length feet	Slope ft/ft	n	Shape	Bottom Width	Side Slopes
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)	(16)	(17)	(18)	(19)	(20)	(21)
SUB3E3	0.0200	77	32	SCS dimensionless hydrograph with a lag time of 0.06 hrs.																
PC4*	0.0217	77	0	100	0.015	0.15	100	---	---	---	---	---	---	---	1100	0.01	0.03	TRAP	30	4
SUB13N	0.0370	77	24	100	0.015	0.15	100	---	---	---	---	---	---	---	2400	0.007	0.018	TRAP	50	20
SUB14N	0.0490	81	0	300	0.025	0.15	100	---	---	---	---	---	---	---	2300	0.01	0.025	TRAP	10	4
SUB20N	0.0240	77	24	200	0.01	0.15	100	---	---	---	---	---	---	---	1400	0.02	0.018	TRAP	50	20
SUB19N	0.0380	77	31	150	0.01	0.15	100	---	---	---	---	---	---	---	1800	0.015	0.018	TRAP	50	20
UB18NC	0.0210	77	42	100	0.01	0.15	100	---	---	---	---	---	---	---	1550	0.02	0.018	TRAP	50	20
UB18NA	0.0220	77	42	100	0.01	0.15	100	---	---	---	---	---	---	---	1450	0.02	0.018	TRAP	50	20
UB18NB	0.0096	77	42	100	0.01	0.15	100	---	---	---	---	---	---	---	800	0.02	0.018	TRAP	50	20
PC1	0.0620	77	10	500	0.015	0.15	100	---	---	---	---	---	---	---	2700	0.01	0.03	TRAP	30	4
UB16NA	0.0139	77	42	100	0.015	0.15	100	---	---	---	---	---	---	---	1500	0.015	0.022	TRAP	50	20
UB16NB	0.0156	77	42	100	0.015	0.15	100	---	---	---	---	---	---	---	1500	0.015	0.022	TRAP	50	20
SUB7N	0.0310	77	18	100	0.015	0.15	100	---	---	---	---	---	---	---	1900	0.01	0.018	TRAP	50	20
SUB8NA	0.0046	81	0	100	0.03	0.15	100	---	---	---	---	---	---	---	450	0.03	0.025	TRAP	20	6
SUB8NB	0.0142	81	0	100	0.03	0.15	100	---	---	---	---	---	---	---	1150	0.025	0.025	TRAP	20	6
SUB8NC	0.0182	81	0	100	0.03	0.15	100	---	---	---	---	---	---	---	900	0.03	0.025	TRAP	20	6
SUB9N	0.0550	77	28	100	0.008	0.15	100	---	---	---	---	---	---	---	1700	0.01	0.018	TRAP	50	20
SUB10B	0.0280	77	42	100	0.015	0.15	100	350	0.008	0.018	0	TRAP	50	20	600	0.008	0.025	TRAP	10	4
UB11NA	0.0076	81	0	100	0.025	0.15	100	---	---	---	---	---	---	---	500	0.03	0.025	TRAP	30	6
UB11NB	0.0078	81	0	100	0.04	0.15	100	---	---	---	---	---	---	---	700	0.025	0.025	TRAP	30	6
UB11NC	0.0069	81	0	100	0.03	0.15	100	---	---	---	---	---	---	---	650	0.028	0.025	TRAP	20	5
SUB10A	0.0300	77	42	100	0.015	0.15	100	350	0.008	0.018	0	TRAP	50	20	800	0.008	0.025	TRAP	10	4
UB12NA	0.0153	81	0	150	0.025	0.15	100	---	---	---	---	---	---	---	650	0.017	0.025	TRAP	30	6
UB12NB	0.0157	81	0	150	0.025	0.15	100	---	---	---	---	---	---	---	650	0.017	0.025	TRAP	30	6
UB16NC	0.0337	77	42	100	0.015	0.15	100	---	---	---	---	---	---	---	1600	0.015	0.022	TRAP	50	20
PC2	0.0540	77	10	100	0.015	0.15	100	---	---	---	---	---	---	---	2700	0.01	0.03	TRAP	50	4
UB17NA	0.0098	81	0	150	0.025	0.05	100	---	---	---	---	---	---	---	960	0.0292	0.025	TRAP	30	50
UB17NB	0.0111	81	0	150	0.025	0.05	100	---	---	---	---	---	---	---	1200	0.0217	0.025	TRAP	30	50
SUB17A	0.0079	77	34	75	0.03	0.05	100	---	---	---	---	---	---	---	1500	0.02	0.025	TRAP	8	4
UB17NC	0.0056	77	12	75	0.03	0.05	100	---	---	---	---	---	---	---	910	0.0187	0.025	TRAP	8	4
SUB15N	0.0391	77	68	100	0.01	0.15	100	400	0.008	0.018	0	TRAP	50	20	1700	0.015	0.025	TRAP	10	4
SUB1-2	0.0558	77	68	200	0.01	0.15	100	---	---	---	---	---	---	---	1370	0.027	0.015	TRAP	50	20
SUB5S	0.0263	77	31	100	0.01	0.15	100	---	---	---	---	---	---	---	1280	0.007	0.015	TRAP	50	20
GC1216	0.0365	81	0	200	0.025	0.15	100	---	---	---	---	---	---	---	2200	0.024	0.025	TRAP	10	4
GC1415	0.0450	81	0	200	0.025	0.15	100	---	---	---	---	---	---	---	1300	0.022	0.025	TRAP	10	4
SUB6S	0.0210	77	42	100	0.01	0.15	100	---	---	---	---	---	---	---	2150	0.013	0.025	TRAP	50	20
SUB7S	0.0270	77	42	100	0.01	0.15	100	---	---	---	---	---	---	---	2080	0.023	0.025	TRAP	50	20
SUB8S	0.0256	77	42	100	0.01	0.15	100	---	---	---	---	---	---	---	1600	0.015	0.025	TRAP	50	20

TABLE 8

Subbasin input parameters for the Pima Road Channel design hydrology  
Future full build-out conditions

Subbasin ID	Drainage Area sq. mi.	Rainfall Losses		Overland Flow Element				Collector Channel Element							Main Channel Element					
		Curve No.	RTIMP %	Length feet	Slope ft/ft	n	% Contributing	Length feet	Slope ft/ft	n	Contrib. Area sm	Shape	Bottom Width	Side Slopes	Length feet	Slope ft/ft	n	Shape	Bottom Width	Side Slopes
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)	(16)	(17)	(18)	(19)	(20)	(21)
GC36	0.0406	81	0	200	0.025	0.15	100	---	---	---	---	---	---	---	2350	0.015	0.035	TRAP	10	4
SUB9S	0.0210	77	53	100	0.01	0.15	100	---	---	---	---	---	---	---	1100	0.013	0.025	TRAP	50	20
SUB7A	0.0092	77	42	100	0.025	0.15	100	---	---	---	---	---	---	---	950	0.015	0.025	TRAP	50	20
SUB10S	0.0248	77	53	100	0.01	0.15	100	---	---	---	---	---	---	---	1150	0.02	0.025	TRAP	50	20
SUB11S	0.0234	77	68	100	0.015	0.018	100	---	---	---	---	---	---	---	1050	0.015	0.025	TRAP	100	20
GC45	0.0127	81	0	200	0.015	0.025	100	---	---	---	---	---	---	---	550	0.015	0.035	TRAP	10	4
PC5*	0.0370	77	0	100	0.015	0.15	100	---	---	---	---	---	---	---	1900	0.01	0.03	TRAP	30	4
*** END GRAYHAWK WATERSHED ***																				
S53A	0.1692	74	11	300	0.022	0.13	100	1475	0.026	0.045	0.0111	TRAP	3	5	2700	0.021	0.040	TRAP	25	5
S53A1	0.3384	74	12	300	0.022	0.13	70	1250	0.023	0.045	0.0087	TRAP	4	5	5650	0.017	0.040	TRAP	35	5
		74	30	150	0.027	0.10	30													
SCN5C	0.2667	74	20	240	0.021	0.13	100	1200	0.018	0.045	0.0067	TRAP	0	45	5600	0.009	0.040	TRAP	15	3
SCN6	0.2597	74	85	180	0.019	0.13	100	1075	0.019	0.045	0.0066	TRAP	5	7	4430	0.013	0.040	TRAP	8	50
SCN6A	0.1335	74	20	300	0.017	0.13	100	1050	0.017	0.045	0.0057	TRAP	8	20	2250	0.012	0.040	TRAP	10	4
S54	0.0853	74	22	300	0.017	0.13	100	---	---	---	---	---	---	---	3460	0.012	0.040	TRAP	5	2

note \*: Subbasins added by GVSCE in order to bring flow previously released to natural channels together, routing the hydrographs down to the Union Hills detention basin.

TABLE 9

Summary of peak discharges from subbasins  
for the Pima Road Channel design hydrology  
Future full build-out conditions

Subbasin ID	Drainage Area  sq. mi.	100-year, 6-hour storm Peak Discharge  cfs
(1)	(2)	(3)
S30N	0.6518	1,227
S31.1	0.2663	395
S35N	0.5482	1,298
S36.2	0.2087	400
S34.1	1.6076	2,491
S36.1	0.1394	159
S36R1	1.2173	1,107
S36R2	0.3742	489/509 <sup>b</sup>
S51.1	1.1300	1,058/998 <sup>b</sup>
52D4	0.0700	116
52D4B	0.0220	70
52D5A	0.0232	79
52C3	0.0060	24
52C3B	0.0160	53
51C	0.0972	166
52C1	0.0290	69
52C2A	0.0190	35
52C2B	0.0275	56
52C2C	0.0140	46
52C4	0.0170	56
52C13	0.0230	69
52C15	0.0460	157
52C14A	0.0410	142
52C5	0.0160	40
52C6	0.0360	82
51B	0.5711	596
52C7	0.0060	18
52C8	0.0080	21
52C9	0.0690	174
52C10	0.0140	28
52C11	0.0425	96
52C12	0.0230	119

TABLE 9

Summary of peak discharges from subbasins  
for the Pima Road Channel design hydrology  
Future full build-out conditions

Subbasin ID	Drainage Area sq. mi.	100-year, 6-hour storm Peak Discharge cfs
(1)	(2)	(3)
52C14B	0.0210	76
52B1	0.0030	8
52B2	0.0320	69
52B3	0.0620	141
52B4	0.0260	87
52B5	0.0210	69
52B6	0.0960	190
52B7	0.0800	303
52A2	0.0650	263
52A1	0.1300	340
37A	0.6765	1,164
SUB5N	0.0290	70
SUB6B	0.0320	74
SUB1N	0.0190	47
SUB2NA	0.0150	34
SUB2NB	0.0300	96
SUB6N	0.0490	114
SUB3N	0.0270	67
SUB4N	0.0320	80
SUB6A	0.0130	64
SUB3C	0.0104	55
GC1018	0.0440	101
GC1-9	0.0260	58
SUB3S	0.0102	33
SUB4S	0.0273	87
GC2-8	0.0140	32
SUB3D3	0.0140	35
GC7	0.0134	31
SUB3D1	0.0088	27
SUB3B1	0.0137	47
SUB3F	0.0344	141
SUB3B2	0.0246	67

TABLE 9

Summary of peak discharges from subbasins  
for the Pima Road Channel design hydrology  
Future full build-out conditions

Subbasin ID	Drainage Area	100-year, 6-hour storm Peak Discharge
(1)	sq. mi. (2)	cfs (3)
SUB3E1	0.0246	67
SUB3D2	0.0220	58
SUB3E2	0.0120	37
PC3	0.0434	82
SUB3E3	0.0200	60
PC4	0.0217	43
SUB13N	0.0370	81
SUB14N	0.0490	88
SUB20N	0.0240	47
SUB19N	0.0380	94
UB18NC	0.0210	62
UB18NA	0.0220	65
UB18NB	0.0096	27
PC1	0.0620	66
UB16NA	0.0139	42
UB16NB	0.0156	48
SUB7N	0.0310	74
SUB8NA	0.0046	13
SUB8NB	0.0142	34
SUB8NC	0.0182	51
SUB9N	0.0550	143
SUB10B	0.0280	87
UB11NA	0.0076	21
UB11NB	0.0078	22
UB11NC	0.0069	19
SUB10A	0.0300	88
UB12NA	0.0153	36
UB12NB	0.0157	37
UB16NC	0.0337	102
PC2	0.0540	93
UB17NA	0.0098	28
UB17NB	0.0111	27

TABLE 9

Summary of peak discharges from subbasins  
for the Pima Road Channel design hydrology  
Future full build-out conditions

Subbasin ID	Drainage Area sq. mi.	100-year, 6-hour storm Peak Discharge cfs
(1)	(2)	(3)
SUB17A	0.0079	30
UB17NC	0.0056	19
SUB15N	0.0391	142
SUB1-2	0.0558	181 32437
GCRB18	0.0120	27
SUB5S	0.0263	72
GC1216	0.0365	83
GC1415	0.0450	104
SUB6S	0.0210	53
SUB7S	0.0270	79
SUB8S	0.0256	76
GC36	0.0406	77
SUB9S	0.0210	68
SUB7A	0.0092	27
SUB10S	0.0248	78
SUB11S	0.0234	118
GC45	0.0127	45
PC5	0.0375	60
SCN5C	0.2667	351
SCN6	0.2597	730 2811
S53A	0.1692	226 1336
S53A1	0.3384	445
S54	0.0853	136
SCN6A	0.1335	198 1483

Note: a. All discharge the same for both Options 1 and 2 except as noted  
b. Option 1/Option 2

TABLE 10

Summary of peak discharges at key concentration points  
for the Pima Road Channel design hydrology  
Future full build-out conditions

Concentration Point	Drainage Area sq. mi.	100-year, 6-hour storm Peak Discharge	
		Option 1 cfs	Option 2 cfs
(1)	(2)	(3)	(4)
30N	0.65	1,227	1,227
C31.1	0.92	1,465	1,465
35N	0.55	1,298	1,298
C36.2	0.54	947	947
C34.1I	2.90	3,668	3,668
C34.1O	2.90	219	219
C36.1	3.04	311	311
C36R1	4.64	1,832	1,832
C36R2	5.01	1,922	1,964
C51.1I	6.14	2,849	1,964
C51.1O	6.14	360	282
C51.1A	6.14	----	1,156
C52A	6.27	385	1,242
C52	7.92	2,201	2,365
CPC5	2.10	1,266	1,266
CN5C	0.27	351	351
CN6	0.26	790	730
C53	8.09	2,321	2,464
C53A	8.42	2,660	2,824
C1I	11.05	4,456	4,639
C1O	11.05	636	704
54	0.09	136	136
C1A	11.27	690	717

1511  
636

## PRELIMINARY SIZING AND DESIGN OF BASINS

The hydrology for the Pima Road Channel is contingent upon the routing of the inflows through the basins. Preliminary sizing of the three detention basins and the outlets, as represented in the hydrology models, are presented in the Recommended Concept Design and Construction Cost Estimate report. Refer to that report for layouts of the basins.

The basins and outlets are sized to evacuate the floodwaters within 36 hours after the end of the design storm. Drain time of the basins is enhanced by excavating a sump area at the headworks of the outlet conduits. The sump enables the outlet to operate under a higher head for the duration of the basin operation. The sump also provides for quicker draining of the majority of the basin floor with only a relatively small area of delayed drainage due to low head on the outlet. All three basins will be effectively drained within 20 hours after the end of the 6-hour design storm.

In the following, the performance of each basin during the 100-year, 6-hour design storm is presented. The basins are all sized such that the spillways do not operate for the 6-hour storm. The basins are checked for performance during a longer duration general storm, and the 100-year, 24-hour storm is used for that check. In checking the performance of the basins, it is assumed that flow-splits that maximize runoff to the respective basins will occur. This checking presents the most severe reasonable conditions for the basins.

## Happy Valley Detention Basin

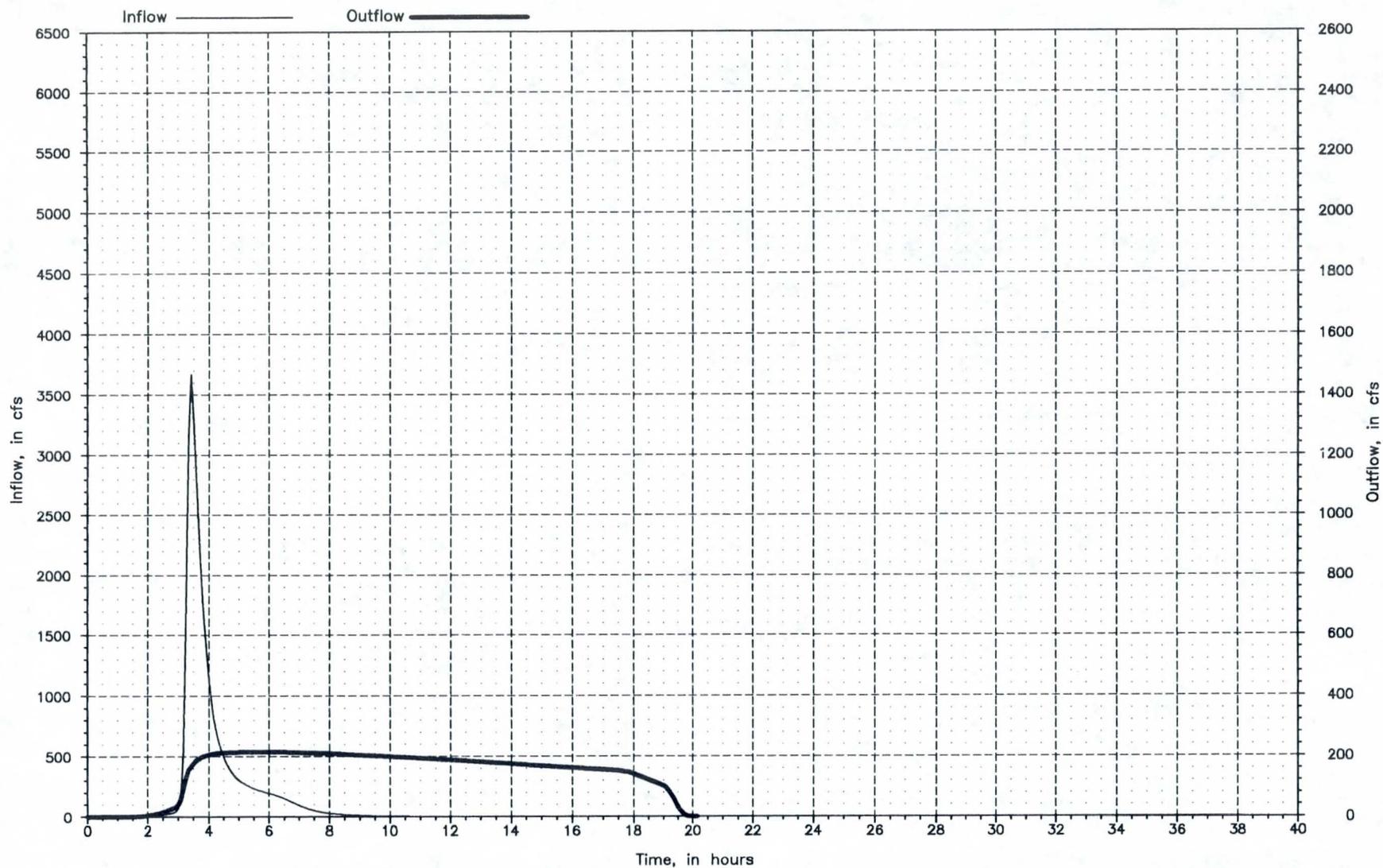
The Happy Valley basin has an inflow design hydrograph (100-year, 6-hour storm) with a peak discharge of 3,670 cfs. The area-capacity curves and outlet rating curve for the preliminary basin sizing are shown in Figures C-1 and C-2, respectively. (Note: All figures denoted with a "C" in the figure number are provided in Appendix C.) Routing the inflow hydrograph through the basin and the 48 inch outlet conduit results in an outlet peak discharge of 220 cfs and a maximum detention volume of 182 acre-feet. The inflow and outflow hydrographs are shown in Figure 4. (The hydrographs for the basins in this report are all shown at the same scale for comparison purposes.) The basin is effectively evacuated within 20 hours after the start of the storm, and within 14 hours after the end of the 6-hour storm. The requirement to evacuate the basin in less than 36 hours after the end of the storm is satisfied.

The performance of the Happy Valley basin is checked for the general storm (100-year, 24-hour). That check also includes taking all the runoff to the Happy Valley basin from the upstream flow-splits (100 percent flow-split to the basin). Under that condition, which is the most severe reasonable assumption for the basin, the spillway has a maximum discharge of 1,275 cfs and spillway operation for about 3.5 hours. The hydrographs for the outlet conduit and the spillway are shown in Figure C-3. The maximum combined release from the spillway and the outlet is 1,475 cfs. The stage hydrographs for the 6-hour and 24-hour storms are shown in Figure C-4. The 24-hour storm results in about a 1.2 feet higher stage than the 6-hour storm.

## Deer Valley Detention Basin

### Option 1

The detention basin at Deer Valley for Option 1 provides for receiving all inflow from the Pima Road Channel entering from the north plus the Deer Valley collector channel along the northern boundary of DC Ranch entering from the east. The total inflow to the basin (100-year, 6-hour) has a peak discharge of 2,850 cfs. The area-capacity curves and outlet rating curve for the preliminary basin sizing are shown in Figures C-5 and C-6, respectively. Routing the inflow hydrograph through the basin and the 60 inch outlet conduit results in an outlet peak discharge of 360 cfs and a maximum detention volume of 177 acre-feet. The inflow and outflow hydrographs are shown in Figure 5. The basin is effectively evacuated within 17 hours after the end of the storm.



**FIGURE 4**  
 Happy Valley Detention Basin hydrographs  
 for the 100-year, 6-hour storm

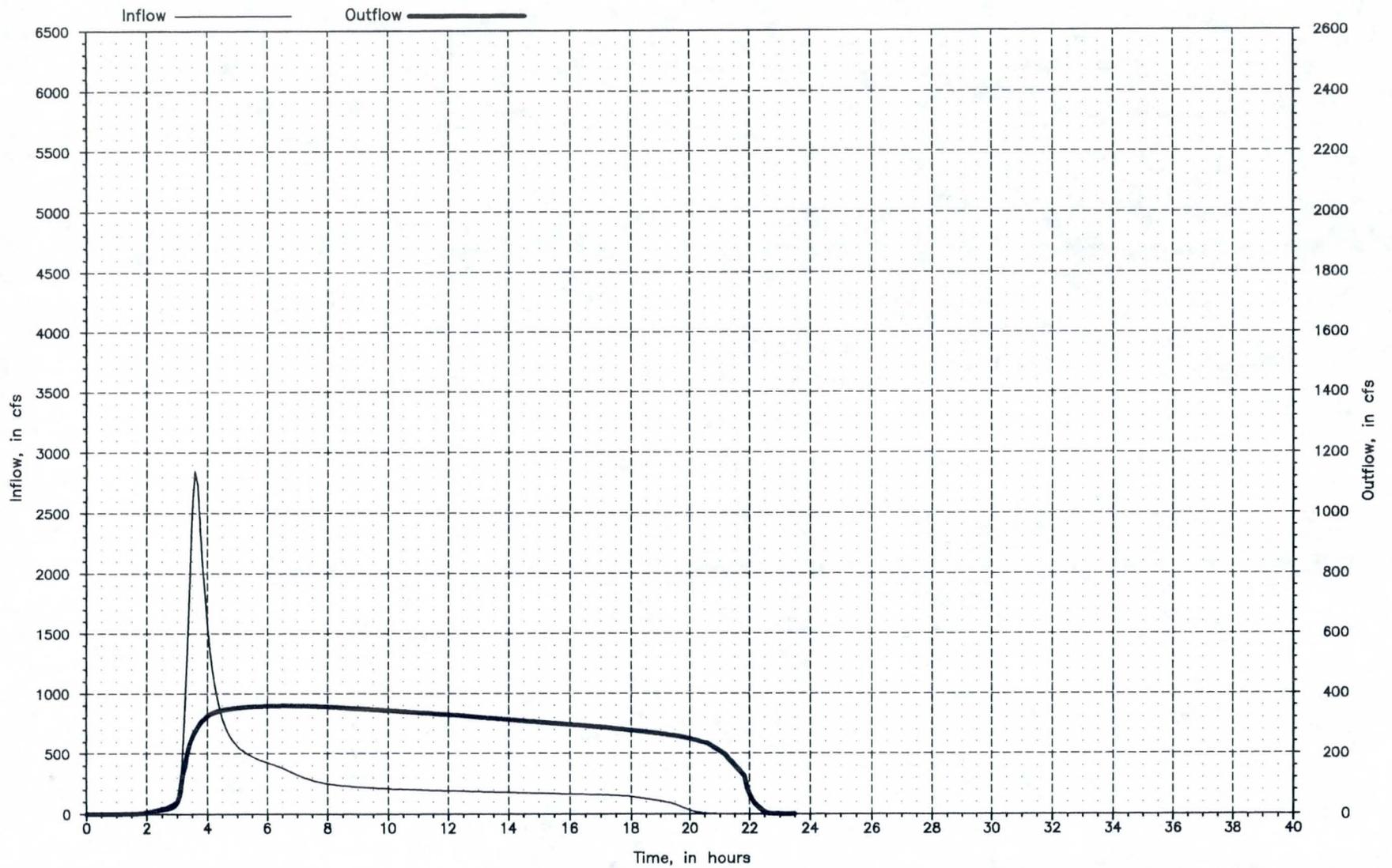


FIGURE 5  
 Deer Valley Detention Basin - Option 1  
 hydrographs for the 100-year, 6-hour storm

The performance of the Deer Valley basin under Option 1 is checked for the general storm (100-year, 24-hour). That check includes two cases for the flow-split that exists upstream of the Happy Valley basin. Case 1 assumes that 100 percent of the flow-split discharge goes to the Happy Valley basin. Case 2 assumes that 100 percent of the flow-split goes to the Deer Valley basin. Both cases are considered because it cannot be determined beforehand which causes the most severe condition at the Deer Valley basin.

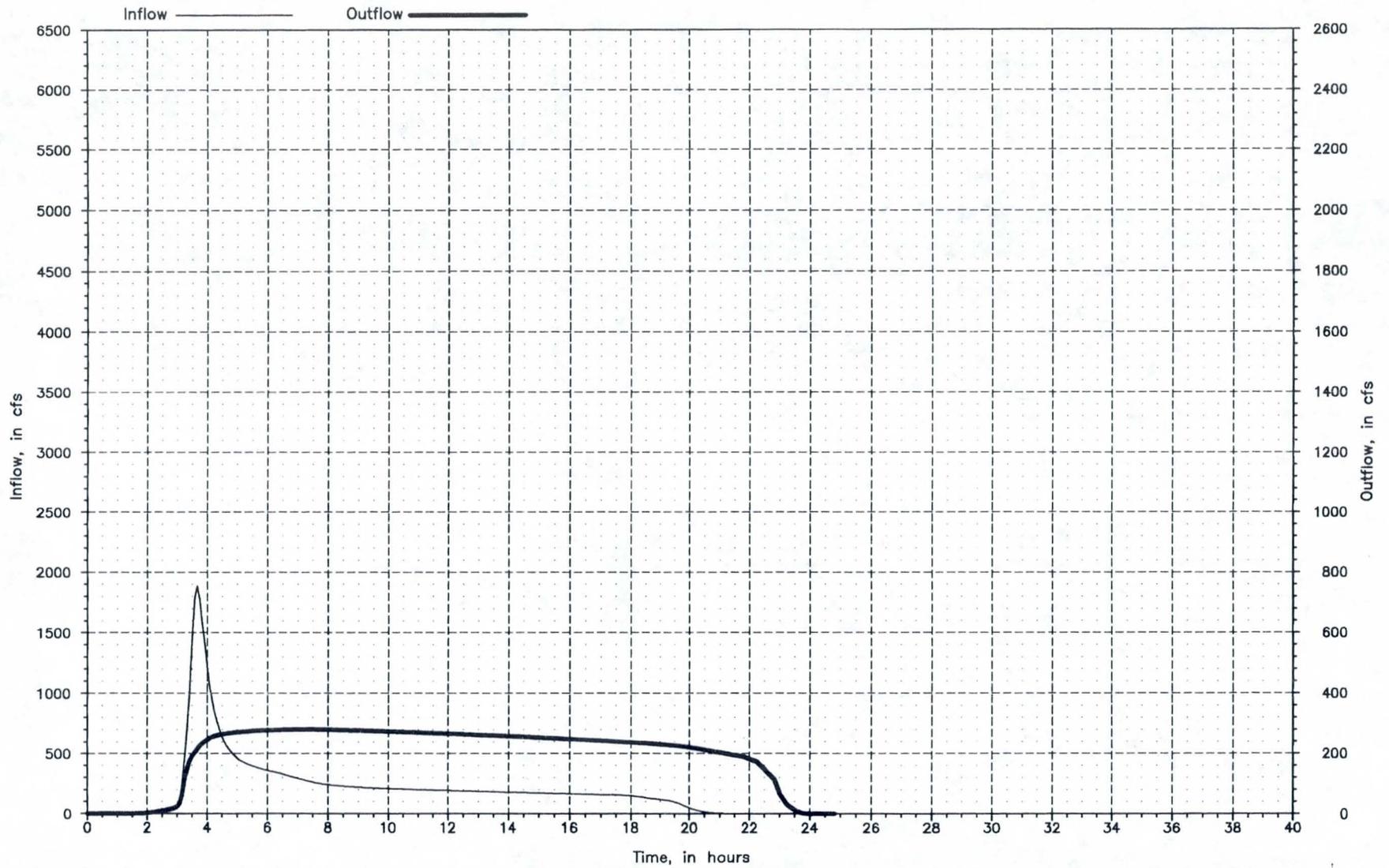
The check of the Option 1 basin under flow-split assumption for Case 1 results in spillway operation with a maximum discharge of 550 cfs and a spillway operation of 4 hours. The hydrographs for the outlet conduit and spillway are shown in Figure C-7. The maximum combined release from the spillway and outlet is 925 cfs. The stage hydrographs for the design storm (100-year, 6-hour) and the Case 1 check condition are shown in Figure C-8. The Case 1 check condition results in about 2.2 feet higher stage than the design storm.

The check of the Option 1 basin under flow-split assumption for Case 2 results in spillway operation with a maximum discharge of 575 cfs and a spillway operation of 4.5 hours. The hydrographs for the outlet conduit and spillway are shown in Figure C-9. The maximum combined release from the spillway and outlet is 950 cfs. The stage hydrographs for the design storm and the Case 2 check condition are shown in Figure C-10. The Case 2 check condition results in about 2.2 feet higher stage than the design storm.

## Option 2

The detention basin at Deer Valley under Option 2 provides for receiving only inflow from the Pima Road Channel entering from the north. Discharge in the Deer Valley collector channel along the northern boundary of DC Ranch bypasses the basin and flows directly to the Pima Road Channel that continues to the south of the Deer Valley basin.

The inflow to the basin from the Pima Road Channel has a peak discharge of 1,960 cfs. The bypass channel has a peak discharge of 1,000 cfs entering the Pima Road Channel directly. The area-capacity curves and outlet rating curve for the preliminary basin sizing are shown in Figures C-11 and C-12, respectively. Routing the inflow hydrograph through the basin and the 54 inch outlet conduit results in an outlet peak discharge of 280 cfs and a maximum detention volume of 130 acre-feet. The inflow and outflow hydrographs are shown in Figure 6. The basin is effectively evacuated within 18 hours after the end of the storm.



**FIGURE 6**  
**Deer Valley Detention Basin - Option 2**  
**hydrographs for the 100-year, 6-hour storm**

The performance of the Deer Valley basin under Option 2 is checked in the same manner as Option 1. For the Option 2 basin under the Case 1 flow-split assumption, the spillway has a maximum discharge of 480 cfs and a spillway operation of 4.5 hours. The hydrographs for the outlet conduit and spillway are shown in Figure C-13. The maximum combined release from the spillway and outlet is 770 cfs. The stage hydrographs for the design storm (100-year, 6-hour) and for the Case 1 check condition are shown in Figure C-14. The Case 1 check condition results in about 2 feet higher stage than the design storm.

For the Option 2 basin under the Case 2 flow-split assumption, the spillway has a maximum discharge of 500 cfs and a spillway operation of 6.5 hours. The hydrographs for the outlet conduit and spillway are shown in Figure C-15. The maximum combined release from the spillway and outlet is 790 cfs. The stage hydrographs for the design storm and for the Case 2 check condition are shown in Figure C-16. The Case 2 check condition results in about 2.3 feet higher stage than the design storm.

### **Union Hills Detention Basin**

#### Option 1

The detention basin at Union Hills for Option 1 corresponds to the Option 1 conditions at the Deer Valley basin. Under Option 1 conditions, the total inflow to the basin (100-year, 6-hour) has a peak discharge of 4,460 cfs. The area-capacity curves and outlet rating curve for the preliminary basin sizing are shown in Figures C-17 and C-18, respectively. Routing the inflow hydrograph through the basin and the 78 inch outlet conduit results in an outlet peak discharge of 640 cfs and a maximum detention volume of 312 acre-feet. The inflow and outflow hydrographs are shown in Figure 7. The basin is effectively evacuated within 19 hours after the end of the storm.

The performance of the Union Hills basin under Option 1 is checked in the same manner as the Deer Valley basin. For the Option 1 basin and the Case 1 flow-split assumption, the spillway has a maximum discharge of 635 cfs and a spillway operation of 5 hours. The hydrographs for the outlet conduit and spillway are shown in Figure C-19. The maximum combined release from the spillway and outlet is 1,300 cfs. The stage hydrographs for the design storm (100-year, 6-hour) and for the Case 1 check condition are shown in Figure C-20. The Case 1 check condition results in about 2.3 feet higher stage than the design storm.

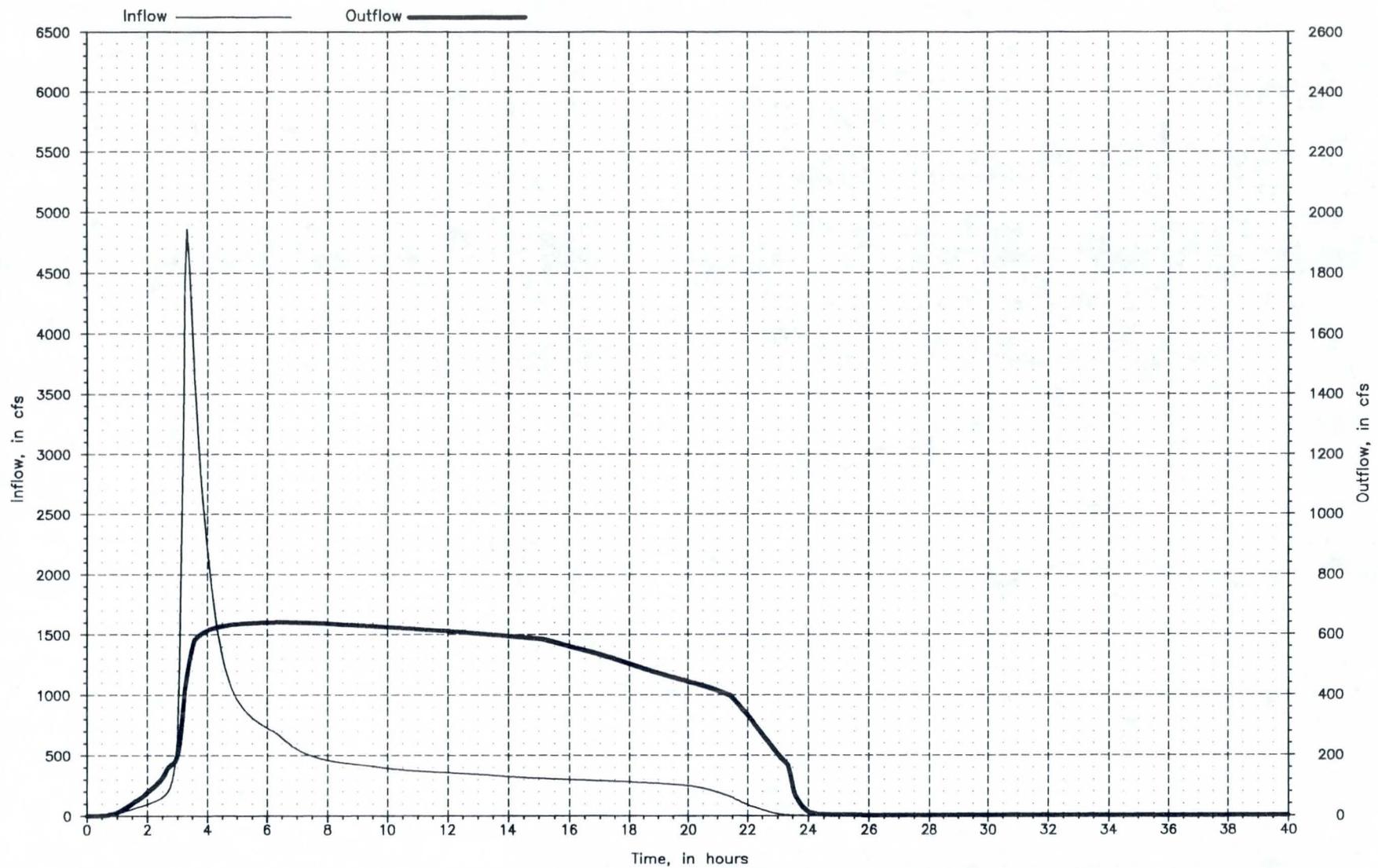


FIGURE 7  
 Union Hills Detention Basin - Option 1  
 hydrographs for the 100-year, 6-hour storm

For the Option 1 basin and the Case 2 flow-split assumption, the spillway has a maximum discharge of 670 cfs and a spillway operation of 5.5 hours. The hydrographs for the outlet conduit and spillway are shown in Figure C-21. The maximum combined release from the spillway and outlet is 1,330 cfs. The stage hydrographs for the design storm and for the Case 2 check condition are shown in Figure C-22. The Case 2 check condition results in about 2.3 feet higher stage than the design storm.

### Option 2

The detention basin at Union Hills for Option 2 corresponds to the Option 2 conditions at the Deer Valley basin. Under Option 2 conditions, the inflow to the basin (100-year, 6-hour) has a total peak discharge of 4,640 cfs. The area-capacity curves and outlet rating curve for the preliminary basin sizing are shown in Figures C-23 and C-24, respectively. Routing the inflow hydrograph through the basin and the 84 inch outlet conduit results in an outlet peak discharge of 770 cfs and a maximum detention volume of 330 acre-feet. The inflow and outflow hydrographs are shown in Figure 8. The basin is effectively evacuated within 19 hours after the end of the storm.

The performance of the Union Hills basin under Option 2 is checked in the same manner as the Deer Valley basin. For the Option 2 basin and the Case 1 flow-split assumption, the spillway has a maximum discharge of 520 cfs and a spillway operation of 3.5 hours. The hydrographs for the outlet conduit and spillway are shown in Figure C-25. The maximum combined release from the spillway and outlet is 1,310 cfs. The stage hydrographs for the design storm (100-year, 6-hour) and for the Case 1 check condition are shown in Figure C-26. The Case 1 check condition results in about 2.4 feet higher stage than the design storm.

For the Option 2 basin and the Case 2 flow-split assumption, the spillway has a maximum discharge of 630 cfs and a spillway operation of 4 hours. The hydrographs for the outlet conduit and spillway are shown in Figure C-27. The maximum combined release from the spillway and outlet is 1,425 cfs. The stage hydrographs for the design storm and the Case 2 check condition are shown in Figure C-28. The Case 2 check condition results in about 2.5 feet higher stage than the design storm.

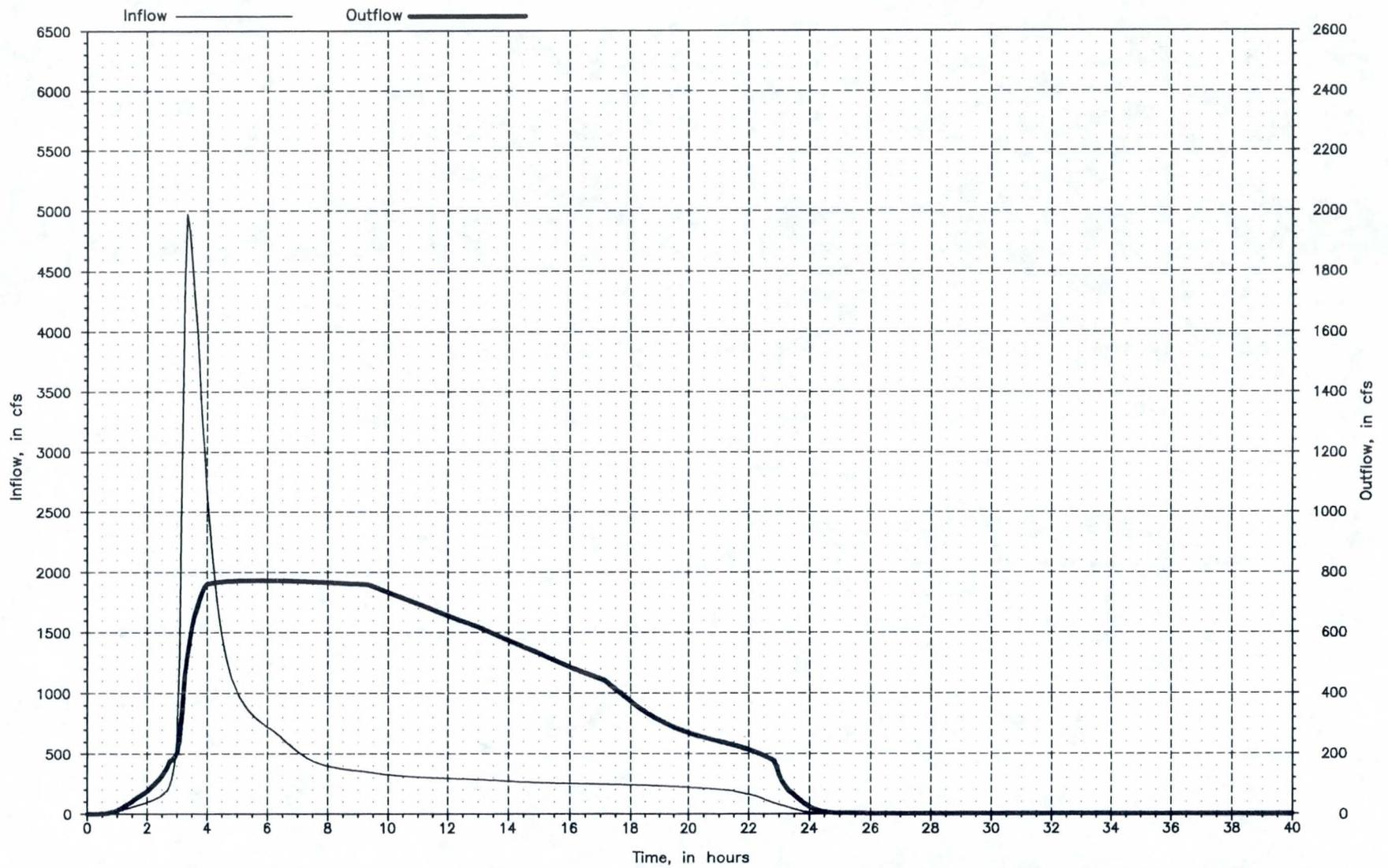


FIGURE 8  
 Union Hills Detention Basin - Option 2  
 hydrographs for the 100-year, 6-hour storm

## CHANNEL DESIGN DISCHARGES

The design discharges for the Pima Road Channel, Options 1 and 2, are listed in Table 11 and illustrated in Figure 9. As shown, the design discharges for the channel north of the Deer Valley basin (above C51.11 in Table 11) are the same under both options. At C36R2 there is a slight difference because of minor deviations in the drainage areas under the two options.

At the Deer Valley basin, the total peak inflow is reduced from 2,849 cfs under Option 1 to 1,964 cfs under Option 2. This allows the Deer Valley basin to be considerably smaller under Option 2 than Option 1, as previously discussed. However, Option 2 results in higher discharges in the Pima Road Channel from the Deer Valley basin south to Beardsley Road. Therefore, the Pima Road Channel for the reach from the Deer Valley basin to Beardsley Road will be larger under Option 2 than under Option 1. Because of the timing of inflows to the channel and routing effects, the design discharges for the channel south of Beardsley Road will be approximately the same under both Options 1 and 2.

The Recommended Design Concept and Construction Cost Estimate report should be used to compare the Deer Valley basins and cost estimates for the two options. As stated in that report, the cost differential between the two options is not meaningful in regard to selecting one option over the other. Environmental, aesthetic and recreational factors should be used to select either Option 1 or Option 2 for the Deer Valley basin.

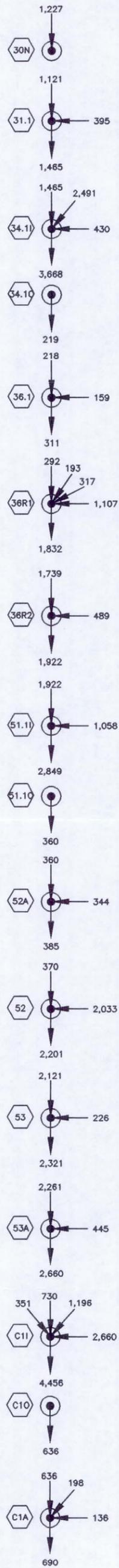
Table 11

Summary of 100-year, 6-hour design discharges at key concentration points along the Pima Road Channel for Options 1 and 2

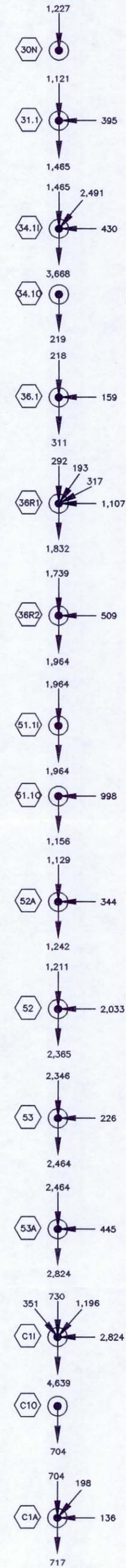
Concentration Point (1)	Design Discharge, in cfs	
	Option 1	Option 2
	(2)	(3)
C30N	1,227	1,227
C31.1	1,465	1,465
C34.1I	3,668	3,668
C314.1O	219	219
C36.1	311	311
C36R1	1,832	1,832
C36R2	1,922	1,964
C51.1I	2,849	1,964
C51.1O	360	282
C51.1A	---	1,156
C52A	385	1,242
C52	2,201	2,365
C53	2,321	2,464
C53A	2,660	2,824
C1I	4,456	4,639
C1O	636	704
C1A	690	717

**OPTION 1**

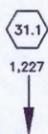
**OPTION 2**



Jomax Road  
Desert Highlands Drive  
Happy Valley Basin Inflow  
Happy Valley Basin Outflow  
Pinnacle Peak Road  
Los Gatos Drive  
Deer Valley Basin Inflow  
Deer Valley Basin Outflow  
Thompson Peak Parkway  
Beardsley Road  
Union Hills Basin Inflow  
Union Hills Basin Outflow  
Pima Road  
CAP Basin



**LEGEND**

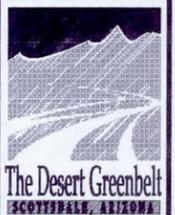


Pima Channel Concentration Point

100-year, 6-hour Peak Discharge In cfs

**Pima Road Channel**

**FIGURE 9**  
Peak Discharges for Option 1  
and Option 2



## SUMMARY

The following is a summary of the design hydrology for the Pima Road Channel:

1. The hydrology is based on the best available topographic maps (1993) and current projections of future land use and drainage plans from City land use planners.
2. The hydrology is for the future, fully built-out condition in the watershed.
3. The hydrology includes two existing flow-split locations upstream of the Happy Valley basin.
4. The HEC-1 model includes the drainage design models for DC Ranch and Grayhawk. Those models were prepared by Wood/Patel Associates and DEI, respectively. Those models were reviewed by the City of Scottsdale and GVSCE prior to incorporation into the design hydrology model. Any changes to those drainage design plans by DC Ranch or Grayhawk could impact the hydrology for the Pima Road Channel.
5. Two methods are compared for performing the flood hydrology; 1) the current City of Scottsdale (COS) method which was used for FEMA mapping, other regional drainage projects and the previous Pima Road Channel of the Desert Greenbelt Project, and 2) the Maricopa County (MC) method. That comparison shows the following:
  - a.) The peak discharges are about the same by both methods for the 100-year, 6-hour storm.
  - b.) The peak discharge for the 100-year, 24-hour storm by the COS method is larger than by the MC method.
  - c.) For the MC method, the peak discharges for the 100-year, 6-hour storm are larger than for the 100-year, 24-hour storm.
  - d.) The runoff volumes are about the same by both methods for the 100-year, 6-hour storm.
  - e.) For the MC method, the runoff volume for the 100-year, 6-hour storm is about the same as for the 100-year, 24-hour storm.

6. Based on the results and comparison of the COS and MC hydrology methods, it is recommended that the COS method be used for design hydrology for the Pima Road Channel. The COS method is used for other regional studies including FEMA flood hazard delineation, highway drainage, local land development, and other aspects of the Desert Greenbelt Project, therefore, use of that method for the Pima Road Channel will result in a consistent regional hydrologic modeling methodology. Also, the COS method is used for the drainage design for the DC Ranch and Grayhawk land developments and it is logical to use those hydrological models for the Pima Road Channel design hydrology.
7. It is recommended that the Pima Road Channel be designed for the 100-year, 6-hour storm. The performance of the basins is to be checked for a longer duration general storm.
8. The Happy Valley basin is preliminarily sized with a 48 inch outlet conduit and 182 acre-feet storage capacity. The inflow and outlet hydrographs are shown in Figure 4. The basin is effectively evacuated within 14 hours after the end of the storm.
9. The Deer Valley basin is preliminarily sized for two options. For Option 1 with the Deer Valley collector channel draining to the basin, a 60 inch outlet conduit and 177 acre-feet storage capacity are determined. The inflow and outlet hydrographs are shown in Figure 5. The basin is effectively evacuated within 17 hours after the end of the storm. For Option 2 with the Deer Valley collector channel bypassing the basin, a 54 inch outlet conduit and 130 acre-feet storage capacity are determined. The inflow and outlet hydrographs are shown in Figure 6. The basin is effectively evacuated within 18 hours after the end of the storm.
10. The Union Hills basin is preliminarily sized for the two Deer Valley basin options. For Option 1, a 78 inch outlet conduit and a 312 acre-feet storage volume are determined. The inflow and outlet hydrographs are shown in Figure 7. The basin is effectively evacuated within 19 hours after the end of the storm. For Option 2, an 84 inch outlet conduit and a storage volume of 330 acre-feet is determined. The inflow and outlet hydrographs are shown in Figure 8. The basin is effectively evacuated within 19 hours after the end of the storm.

11. The spillways at the three detention basins will not operate for the 100-year, 6-hour design storm.
12. The hydraulic performances of the three detention basins are checked for the 100-year, 24-hour storm and the most severe assumptions regarding flow-splits. Under those conditions, the Happy Valley basin has a spillway peak discharge of about 1,275 cfs and operation for about 3.5 hours (see Figure C-3).

The Deer Valley basin for Option 1, Case 1 has a spillway peak discharge of about 550 cfs and operation for about 4 hours (see Figure C-7), and for Option 1, Case 2, the spillway peak discharge is about 575 cfs and operation for about 4.5 hours (see Figure C-9). For Option 2, Case 1, the spillway peak discharge is about 480 cfs and operation for about 4.5 hours (see Figure C-13), and for Option 2, Case 2, the spillway peak discharge is about 500 cfs and operation for about 6.5 hours (see Figure C-15).

The Union Hills basin for Option 1, Case 1 has a spillway peak discharge of about 635 cfs and operation for about 5 hours (see Figure C-19), and for Option 1, Case 2, the spillway peak discharge is about 670 cfs and operation for about 5.5 hours (see Figure C-21). For Option 2, Case 1, the spillway peak discharge is about 520 cfs and operation for about 3.5 hours (see Figure C-25), and for Option 2, Case 2, the spillway peak discharge is about 630 cfs and operation for about 4 hours (see Figure C-27).

13. The design discharges for the Pima Road Channel are shown in Table 11. The maximum channel discharge is about 2,824 cfs at its inflow to the Union Hills basin (Option 2). The channel design discharges are greater under Option 2 for the reach of channel from the Deer Valley basin to Beardsley Road.
14. The selection of Option 1 or Option 2 for the Deer Valley basin will not be based on cost (see the separate Recommended Design Concept and Construction Cost Estimate report). That decision should be based on environmental, aesthetic and recreational factors, and factors related to spillway operation at the Deer Valley basin.

**APPENDIX A**

**HEC-1 Option 1 output file (100-year, 6-hour storm)**

```

*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
* MAY 1991 *
* VERSION 4.0.1E *
* Lahey F77L-EM/32 version 5.01 *
* Dodson & Associates, Inc. *
* RUN DATE 12/30/96 TIME 16:29:28 *
*****

```

```

*****
*
* U.S. ARMY CORPS OF ENGINE
* HYDROLOGIC ENGINEERING CE
* 609 SECOND STREET
* DAVIS, CALIFORNIA 9561
* (916) 551-1748
*
*****

```

*Not the same  
as the diskette  
run.*

*Disregard  
this file*

```

X X XXXXXXXX XXXXX X
X X X X X XX
X X X X X
XXXXXXXX XXXX X XXXXX X
X X X X X
X X X X X
X X XXXXXXXX XXXXX XXX

```

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION. NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE, SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY, DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL, LOSS RATE:GREEN AND AMPT INFILTRATION, KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM.

```

LINE      ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

  1      ID      PIMA ROAD CHANNEL
  2      ID      by GVSCE for the City of Scottsdale
  3      ID      Project: 95
  4      ID
  5      ID      100-YEAR 6-HR HYPOTHETICAL RAINFALL DISTRIBUTION
  6      ID      RAINFALL LOSSES: SCS CURVE NUMBERS
  7      ID      UNIT HYDROGRAPH: KINEMATIC WAVE
  8      ID      ROUTING: MODIFIED PULS - USING NORMAL DEPTH
  9      ID
 10      ID      COLLECTOR CHANNEL LENGTHS ARE AS FOLLOWS:
 11      ID      HAPPY VALLEY ROAD ..... 1.0 MILE
 12      ID      PINNACLE PEAK ROAD ..... 0.5 MILE
 13      ID      DEER VALLEY ROAD ..... 0.25 MILE
 14      ID      BEARDLSEY ROAD ..... 1.0 MILE
 15      ID
 16      ID      DETENTION BASINS AT HAPPY VALLEY, DEER VALLEY AND UNION HILLS ROADS.
 17      ID
 18      IT      5              720
 19      IO      5
 20      JD      .01
 21      JD      .1
 22      JD      .5
 23      JD      1
 24      JD      5
 25      JD      25
 26      *
 26      KK      S30N
 27      KM      RUNOFF FROM SUBBASIN 30N
 28      BA      0.6518
 29      PH      .84      1.53      2.46      2.75      2.94      3.31
 30      LS      82      13      82      13
 31      UK      300      0.350      0.13      20
 32      UK      300      0.050      0.13      80
 33      RK      1550      0.069      0.045      0.0096      TRAP      0      12
 34      RK      10520      0.038      0.040      TRAP      15      15
 35      *
 35      KK      R30N
 36      KM      NORMAL DEPTH CHANNEL ROUTE FROM C30N TO C31.1 THROUGH PIMA CHANNEL
 37      RS      1      FLOW      -1
 38      RC      0.035      0.025      0.035      2685      0.01
 39      RX      1000      1020      1022      1033      1068      1079      1081      1101
 40      RY      110.6      105.6      105.5      100      100      105.5      105.6      110.6
 41      *
 41      KK      S31.1
 42      KM      RUNOFF FROM SUBBASIN 31.1
 43      BA      0.2663
 44      LS      76.6      13      76.6      13
 45      UK      300      0.567      0.13      10
 46      UK      300      0.050      0.13      90
 47      RK      1950      0.056      0.045      0.0147      TRAP      0      10
 48      RK      7600      0.035      0.040      TRAP      22      8
  
```

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

49 KK C31.1  
 50 KM COMBINE ROUTED HYDROGRAPH FROM S30N WITH RUNOFF FROM SUBBASIN 31.1  
 51 HC 2  
 \*

52 KK R31.1  
 53 KM NORMAL DEPTH CHANNEL ROUTE FROM C31.1 TO C34.1 THROUGH PIMA CHANNEL  
 54 RS 1 FLOW -1  
 55 RC 0.035 0.025 0.035 2200 0.01  
 56 RX 1000 1020 1022 1033 1068 1079 1081 1101  
 57 RY 110.6 105.6 105.5 100 100 105.5 105.6 110.6  
 \*

58 KK S35N  
 59 KM RUNOFF FROM SUBBASIN 35N  
 60 BA 0.5482  
 61 LS 82 13 82 13  
 62 UK 300 0.491 0.13 15  
 63 UK 300 0.113 0.13 85  
 64 RK 2700 0.079 0.045 0.0242 TRAP 3 6  
 65 RK 5050 0.028 0.040 TRAP 15 15  
 \*

66 KK D35NR  
 67 KM DIVERT 60% OF FLOW INTO S36.2 - THE REMAINDER ENTERS S36R1  
 68 DT D35NL  
 69 DI 0 2000  
 70 DQ 0 800  
 \*

71 KK R35NR  
 72 KM NORMAL DEPTH CHANNEL ROUTE FROM S35N TO C36.2  
 73 KM SOURCE: 1993 MAPPING (2' CI) PROVIDED BY COS  
 74 RS 1 FLOW -1  
 75 RC 0.06 0.04 0.06 3500 0.0343  
 76 RX 1000 1006 1026 1027 1057 1058 1078 1084  
 77 RY 105 103 101 100 100 101 103 105  
 \*

78 KK S36.2  
 79 KM RUNOFF FROM SUBBASIN 36.2  
 80 BA 0.2087  
 81 LS 76.6 13 76.6 13  
 82 UK 300 0.580 0.13 5  
 83 UK 300 0.100 0.13 95  
 84 RK 1800 0.036 0.045 0.0145 TRAP 10 10  
 85 RK 3520 0.028 0.040 TRAP 20 6  
 \*

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

128 KK R34.1  
 129 KM NORMAL DEPTH CHANNEL ROUTE FROM C34.1 TO C36.1 THROUGH PIMA CHANNEL  
 130 RS 1 FLOW -1  
 131 RC 0.035 0.025 0.035 2300 0.01  
 132 RX 1000 1020 1022 1034 1079 1091 1093 1113  
 133 RY 111 106 105.9 100 100 105.9 106 111  
 \*

134 KK S36.1  
 135 KM RUNOFF FROM SUBBASIN 36.1  
 136 BA 0.1394  
 137 LS 73.4 11  
 138 UK 300 0.0420 0.130 100  
 139 RK 2330 0.0320 0.045 0.0134 TRAP 10 30  
 140 RK 3200 0.0270 0.040 TRAP 20 30  
 \*

141 KK C36.1  
 142 KM COMBINE ROUTED HYDROGRAPH FROM C34.1 WITH RUNOFF FROM SUBBASIN 36.1  
 143 HC 2  
 \*

144 KK R36.1  
 145 KM NORMAL DEPTH CHANNEL ROUTE FROM C36.1 TO C36R1 THROUGH PIMA CHANNEL  
 146 RS 1 FLOW -1  
 147 RC 0.035 0.025 0.035 2980 0.01  
 148 RX 1000 1020 1022 1034 1079 1091 1093 1113  
 149 RY 111 106 105.9 100 100 105.9 106 111  
 \*

*earlier channel considered by hydrograph*

150 KK B35NL  
 151 KM BRING BACK DIVERTED HYDROGRAPH FROM C35N  
 152 DR D35NL  
 \*

153 KK R35NL  
 154 KM NORMAL DEPTH CHANNEL ROUTE FROM S35N TO C36R1  
 155 KM SOURCE: 1993 MAPPING (2' CI) PROVIDED BY COS  
 156 RS 5 FLOW -1  
 157 RC 0.06 0.04 0.06 14480 0.0318  
 158 RX 1000 1040 1080 1086 1091 1097 1137 1174  
 159 RY 105 104 103 100 100 103 104 105  
 \*

160 KK B36.2L  
 161 KM BRING BACK DIVERTED HYDROGRAPH FROM C36.2  
 162 DR D36.2L  
 \*

LINE	ID	.....1	.....2	.....3	.....4	.....5	.....6	.....7	.....8	.....9	.....10	
86	KK	C36.2										
87	KM	COMBINE ROUTED HYDROGRAPH FROM S35N WITH RUNOFF FROM SUBBASIN 36.2										
88	KM	AREA IS AREA OF S36.2 + 60% OF AREA FROM S35N										
89	HC	2	0.5411									
	*											
90	KK	D36.2R										
91	KM	DIVERT 70% OF FLOW INTO S34.1 - THE REMAINDER ENTERS S36R1										
92	DT	D36.2L										
93	DI	0	2000									
94	DQ	0	600									
	*											
95	KK	R36.2R										
96	KM	NORMAL DEPTH CHANNEL ROUTE FROM C36.2 TO C34.1										
97	KM	SOURCE: 1993 MAPPING (2' CI) PROVIDED BY COS										
98	RS	4	FLOW	-1								
99	RC	0.06	0.04	0.06	7800	0.0321						
100	RX	1000	1043	1053	1068	1093	1098	1133	1218			
101	RY	102.6	100.6	100.5	100	100	100.5	100.6	102.6			
	*											
102	KK	S34.1										
103	KM	RUNOFF FROM SUBBASIN 34.1										
104	KM	RAINFALL LOSSES FOR GREINER SUBBASINS 31.2 AND 34.1 ARE WEIGHTED BY AREA										
105	BA	1.6076										
106	LS		77.3	12		77.3	12					
107	UK	300	0.590	0.13	25							
108	UK	300	0.040	0.13	75							
109	RK	2570	0.085	0.045	0.0214	TRAP	0	10				
110	RK	9200	0.042	0.040		TRAP	50	9				
	*											
111	KK	C34.1I										
112	KM	COMBINE ROUTED HYDROGRAPH FROM C31.1 & C36.2 W/RUNOFF FROM SUBBASIN 34.1										
113	KM	AREA IS AREA FROM C31.1 + S34.1 + 70% OF AREA FROM C36.2										
114	HC	3	2.9029									
	*											
115	KK	C34.1O										
116	KM	DETENTION BASIN AT HAPPY VALLEY ROAD - NONREGULATORY STRUCTURE										
117	KM	OUTLET RATING CURVE - USING HY8 FOR A 48" RCP WITH A SLOPE OF 0.5%										
118	KM	13 ACRE-FEET OF STORAGE FOR SEDIMENTAION										
119	RS	1	STOR									
120	SV	0	0.1	0.2	0.5	1.2	2.2	20.5	65.1	116.9	182.1	
121	SV	195										
122	SE	2065	2066	2067	2068	2069	2070	2075	2080	2085	2090	
123	SE	2091										
124	SQ	0	21	42	63	84	105	110	147	168	189	
125	SQ	210	216	244	549	665	811	996	1300	1511		
126	SE	2065.0	2066.82	2067.83	2068.64	2069.47	2070.44	2070.70	2073.43	2078.36	2083.14	
127	SE	2088.3	2090.00	2090.10	2090.50	2090.60	2090.70	2090.80	2090.90	2091.00		
	*											

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

128 KK R34.1  
 129 KM NORMAL DEPTH CHANNEL ROUTE FROM C34.1 TO C36.1 THROUGH PIMA CHANNEL  
 130 RS 1 FLOW -1  
 131 RC 0.035 0.025 0.035 2300 0.01  
 132 RX 1000 1020 1022 1034 1079 1091 1093 1113  
 133 RY 111 106 105.9 100 100 105.9 106 111  
 \*

134 KK S36.1  
 135 KM RUNOFF FROM SUBBASIN 36.1  
 136 BA 0.1394  
 137 LS 73.4 11  
 138 UK 300 0.0420 0.130 100  
 139 RK 2330 0.0320 0.045 0.0134 TRAP 10 30  
 140 RY 3200 0.0270 0.040 TRAP 20 30  
 \*

141 KK C36.1  
 142 KM COMBINE ROUTED HYDROGRAPH FROM C34.1 WITH RUNOFF FROM SUBBASIN 36.1  
 143 HC 2  
 \*

144 KK R36.1  
 145 KM NORMAL DEPTH CHANNEL ROUTE FROM C36.1 TO C36R1 THROUGH PIMA CHANNEL  
 146 RS 1 FLOW -1  
 147 RC 0.035 0.025 0.035 2980 0.01  
 148 RX 1000 1020 1022 1034 1079 1091 1093 1113  
 149 RY 111 106 105.9 100 100 105.9 106 111  
 \*

150 KK B35NL  
 151 KM BRING BACK DIVERTED HYDROGRAPH FROM C35N  
 152 DR D35NL  
 \*

153 KK R35NL  
 154 KM NORMAL DEPTH CHANNEL ROUTE FROM S35N TO C36R1  
 155 KM SOURCE: 1993 MAPPING (2' CI) PROVIDED BY COS  
 156 RS 5 FLOW -1  
 157 RC 0.06 0.04 0.06 14480 0.0318  
 158 RX 1000 1040 1080 1086 1091 1097 1137 1174  
 159 RY 105 104 103 100 100 103 104 105  
 \*

160 KK B36.2L  
 161 KM BRING BACK DIVERTED HYDROGRAPH FROM C36.2  
 162 DR D36.2L  
 \*

HEC-1 INPUT

1

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

163 KK R36.2L  
 164 KM NORMAL DEPTH CHANNEL ROUTE FROM C36.2 TO C36R1  
 165 KM SOURCE: 1993 MAPPING (2' CI) PROVIDED BY COS  
 166 RS 3 FLOW -1  
 167 RC 0.06 0.04 0.06 10160 0.0342  
 168 RX 1000 1030 1060 1066 1076 1082 1112 1142  
 169 RY 103 102.5 102 100 100 102 102.5 103  
 \*

170 KK S36R1  
 171 KM RUNOFF FROM SUBBASIN 36R1  
 172 KM RAINFALL LOSSES FOR GREINER SUBBASINS 36.3, 36R1 AND 35R ARE AREA WEIGHT  
 173 BA 1.2173  
 174 LS 74.3 10  
 175 UK 300 0.020 0.200 100  
 176 RK 1420 0.032 0.045 0.0061 TRAP 0 13  
 177 RY 12600 0.033 0.040 TRAP 10 9  
 \*

178 KK C36R1  
 179 KM COMBINE ROUTED HYDROGRAPH FROM C36.1, D35NL & D36.2L W/RUNOFF FROM S36R1  
 180 KM AREA IS AREA FROM C36.1 + S36R1 + 40% OF AREA FROM S35N + 30% OF AREA  
 181 KM FROM C36.2  
 182 HC 4 4.6393  
 \*

183 KK R36R1  
 184 KM NORMAL DEPTH CHANNEL ROUTE FROM C36R1 TO C36R2 THROUGH PIMA CHANNEL  
 185 RS 1 FLOW -1  
 186 RC 0.035 0.025 0.035 4000 0.01  
 187 RX 1000 1020 1022 1034 1084 1096 1098 1118  
 188 RY 111.4 106.4 106.3 100 100 106.3 106.4 111.4  
 \*

189 KK S36R2  
 190 KM RUNOFF FROM SUBBASIN 36R2  
 191 BA 0.3742  
 192 LS 72 16  
 193 UK 280 0.045 0.100 100  
 194 RK 1900 0.032 0.017 0.015 TRAP 15 7  
 195 RY 7360 0.030 0.040 TRAP 30 10  
 \*

196 KK C36R2  
 197 KM COMBINE ROUTED HYDROGRAPH FROM C36R1 W/RUNOFF FROM SUBBASIN 36R2  
 198 HC 2  
 \*

199 KK S51.1  
 200 KM RUNOFF FROM SUBBASIN 51.1  
 201 KM RAINFALL LOSSES FOR GREINER SUBBASINS 51.1 AND 49.1 ARE AREA WEIGHTED  
 202 BA 1.130

LINE	ID	1	2	3	4	5	6	7	8	9	10
163	KK	R36.2L									
164	KM	NORMAL DEPTH CHANNEL ROUTE FROM C36.2 TO C36R1									
165	KM	SOURCE: 1993 MAPPING (2' CI) PROVIDED BY COS									
166	RS	3	FLOW	-1							
167	RC	0.06	0.04	0.06	10160	0.0342					
168	RX	1000	1030	1060	1066	1076	1082	1112	1142		
169	RY	103	102.5	102	100	100	102	102.5	103		
	*										
170	KK	S36R1									
171	KM	RUNOFF FROM SUBBASIN 36R1									
172	KM	RAINFALL LOSSES FOR GREINER SUBBASINS 36.3, 36R1 AND 35R ARE AREA WEIGHT									
173	BA	1.2173									
174	LS		74.3	10							
175	UK	300	0.020	0.200	100						
176	RK	1420	0.032	0.045	0.0061	TRAP	0	13			
177	RK	12600	0.033	0.040		TRAP	10	9			
	*										
178	KK	C36R1									
179	KM	COMBINE ROUTED HYDROGRAPH FROM C36.1, D35NL & D36.2L W/RUNOFF FROM S36R1									
180	KM	AREA IS AREA FROM C36.1 + S36R1 + 40% OF AREA FROM S35N + 30% OF AREA									
181	KM	FROM C36.2									
182	HC	4	4.6393								
	*										
183	KK	R36R1									
184	KM	NORMAL DEPTH CHANNEL ROUTE FROM C36R1 TO C36R2 THROUGH PIMA CHANNEL									
185	RS	1	FLOW	-1							
186	RC	0.035	0.025	0.035	4000	0.01					
187	RX	1000	1020	1022	1034	1084	1096	1098	1118		
188	RY	111.4	106.4	106.3	100	100	106.3	106.4	111.4		
	*										
189	KK	S36R2									
190	KM	RUNOFF FROM SUBBASIN 36R2									
191	BA	0.3742									
192	LS		72	16							
193	UK	280	0.045	0.100	100						
194	RK	1900	0.032	0.017	0.015	TRAP	15	7			
195	RK	7360	0.030	0.040		TRAP	30	10			
	*										
196	KK	C36R2									
197	KM	COMBINE ROUTED HYDROGRAPH FROM C36R1 W/RUNOFF FROM SUBBASIN 36R2									
198	HC	2									
	*										
199	KK	S51.1									
200	KM	RUNOFF FROM SUBBASIN 51.1									
201	KM	RAINFALL LOSSES FOR GREINER SUBBASINS 51.1 AND 49.1 ARE AREA WEIGHTED									
202	BA	1.130									
203	LS		73.9	12							
204	UK	300	0.037	0.130	100						



LINE	ID	1	2	3	4	5	6	7	8	9	10
240	KK	52D4R									
241	KM	ROUTE 52D4C THROUGH 52D5 TO CP 52D5C									
242	RK	1350	.033	.045			TRAP	10		10	
	*										
243	KK	52D4B									
244	KM	RUNOFF FROM SUBBASIN 52D4B									
245	BA	.022									
246	LS		75	63							
247	UK	120	.010	.15	100						
248	RK	2200	.033	.045			TRAP	30		10	
	*										
249	KK	52D5C1									
250	KM	COMBINE 52D4R AND 52D4B									
251	HC	2									
	*										
252	KK	52D5A									
253	KM	RUNOFF FROM 52D5A									
254	BA	.0232									
255	LS		75	63							
256	UK	120	.010	.15	100						
257	RK	1300	.032	.045			TRAP	30		10	
	*										
258	KK	52D5AR									
259	KM	ROUTE 52D5A THROUGH BEARDSLEY CHANNEL TO CP 52D5C2									
260	RK	400	.0143	.035			TRAP	50		4	
	*										
261	KK	52D5C2									
262	KM	COMBINE 25D5C1 AND 52D5AR									
263	HC	2									
	*										
264	KK	52D5R									
265	KM	ROUTE 52D5C IN BEARDSLEY CHANNEL TO CP 52C3BC2									
266	RK	240	.0143	.035			TRAP	50		4	
	*										
267	KK	52C3									
268	KM	RUNOFF FROM SUBBASIN 52C3									
269	BA	.006									
270	LS		75	65							
271	UK	100	.02	.10	100						
272	RK	800	.033	.045			TRAP	30		10	
	*										





LINE	ID	1	2	3	4	5	6	7	8	9	10
338	KK	52C2C									
339	KM	RUNOFF FROM SUBBASIN 52C2C									
340	BA	.014									
341	LS		75	62							
342	UK	100	.02	.10	100						
343	RK	1500	.04	.045		TRAP	30	10			
	*										
344	KK	52C2CC									
345	KM	COMBINE 52C2C AND 52C2BR									
346	HC	2									
	*										
347	KK	52C2R									
348	KM	ROUTE 52C2CC THROUGH SUBBASIN 52C4 TO CP 52C4C1									
349	RK	1550	.030	.045		TRAP	10	10			
	*										
350	KK	52C4									
351	KM	RUNOFF FROM SUBBASIN 52C4									
352	BA	.017									
353	LS		75	60							
354	UK	100	.02	.10	100						
355	RK	1550	.030	.045		TRAP	30	10			
	*										
356	KK	52C4C1									
357	KM	COMBINE 52C4 AND 52C2R									
358	HC	2									
	*										
359	KK	52C4C2									
360	KM	COMBINE 52C4C1 AND 52C3BR									
361	HC	2									
	*										
362	KK	52C4R									
363	KM	ROUTE 52C4C2 WEST IN BEARDSLEY CHANNEL TO CP 52C15C2									
364	RK	850	.0143	.035		TRAP	50	4			
	*										
365	KK	52C13 ?									
366	KM	RUNOFF FROM SUBBASIN 52C13									
367	BA	.023									
368	LS		75	31							
369	UK	100	.02	.10	100						
370	RK	950	.040	.045		TRAP	30	10			
	*										

LINE	ID	1	2	3	4	5	6	7	8	9	10
371	KK	2C13DV									
372	KM	DIVERT FIRST 40 CFS INTO STORM DRAIN; REMAINDER FLOWS OVER ROAD									
373	DT	STORM									
374	DI	0	40	1000							
375	DQ	0	40	40							
	*										
	*	KK52C13R									
	*	KM ROUTE 52C13 THROUGH SUBBASIN 52C15 TO CP 52C15C1									
	*	RK 1800	.035	.045		TRAP	10		10		
	*										
376	KK	52C15									
377	KM	RUNOFF FROM SUBBASIN 52C15									
378	BA	.046									
379	LS		75	64.4							
380	UK	100	.02	.10	100						
381	RK	2050	.036	.045		TRAP	30		10		
	*										
382	KK	2C15C1									
383	KM	COMBINE 52C15 AND 52C13DV									
384	HC	2	.046								
	*										
385	KK	2C15C2									
386	KM	COMBINE 52C15C1 AND 52C4R									
387	HC	2									
	*										
388	KK	52C15R									
389	KM	ROUTE 52C15C2 IN BEARDSLEY CHANNEL TO CP 52C14C3									
390	RK	750	.0143	.035		TRAP	50		4		
	*										
391	KK	52C14A									
392	KM	RUNOFF FROM SUBBASIN 52C14A									
393	BA	.041									
394	LS		75	67.7							
395	UK	100	.02	.10	100						
396	RK	2050	.031	.045		TRAP	30		10		
	*										
397	KK	2C14AC									
398	KM	COMBINE 52C14A AND 52C15R									
399	HC	2									
	*										
400	KK	2C14AR									
401	KM	ROUTE 52C14AC IN BEARDSLEY CHANNEL TO CP 52C14BC2									
402	RK	380	.0143	.035		TRAP	50		4		
	*										
	*										

*why?*

*no point  
route  
since  
29 cfs remains  
else drain*

LINE	ID	1	2	3	4	5	6	7	8	9	10
403	KK	51C1DV									
404	KM	RETRIEVE DIVERTED FLOW									
405	DR	51C1DV									
	*										
406	KK	51C2D									
407	KM	DIVERT 27 PERCENT OF 51C1DV TO WEST (73 PERCENT TO SOUTH)									
408	DT	51C2DV									
409	DI	0	10000								
410	DQ	0	2700								
	*										
411	KK	51C2R									
412	KM	ROUTE 51C2D THROUGH SUBBASIN 52C5 TO CP 52C5C									
413	RK	700	.030	.045		TRAP	10	10			
	*										
414	KK	52C5									
415	KM	RUNOFF FROM SUBBASIN 52C5									
416	BA	.016									
417	LS		75	27							
418	UK	100	.02	.10	100						
419	RK	1200	.03	.045		TRAP	30	10			
	*										
420	KK	52C5C									
421	KM	COMBINE 51C2R AND 52C5									
422	HC	2	.0635								
	*										
423	KK	52C5R									
424	KM	ROUTE 52C5C THROUGH SUBBASIN 52C6 TO CP 52C6C									
425	RK	3100	.035	.045		TRAP	10	10			
	*										
426	KK	52C6									
427	KM	RUNOFF FROM SUBBASIN 52C6									
428	BA	.036									
429	LS		75	31.4							
430	UK	100	.02	.10	100						
431	RK	3100	.035	.045		TRAP	30	10			
	*										
432	KK	52C6C									
433	KM	COMBINE 52C5R AND 52C6									
434	HC	2									
	*										
435	KK	52C6R									
436	KM	ROUTE 52C6C THROUGH SUBBASIN 52C10 TO CP 52C10C2									
437	RK	450	.032	.045		TRAP	10	10			
	*										

LINE	ID	1	2	3	4	5	6	7	8	9	10
438	KK	51C2DV									
439	KM	RETRIEVE 52C2DV									
440	DR	51C2DV									
	*										
441	KK	51C3R									
442	KM	ROUTE 52C2DV THROUGH SUBBASIN 52C7 TO CP 52C7C									
443	RK	700	.040	.045			TRAP	10		10	
	*										
444	KK	51B	SUB								
445	KM	RUNOFF FROM SUB 51B									
446	BA	.5711									
447	LS	0	71.9	13.1							
448	UK	100	.0213	.10	100						
449	RK	8900	.0300	.045			TRAP	50		25	
	*										
450	KK	51B1D									
451	KM	DIVERT 92 PERCENT OF SUBBASIN 51B TO WEST (8 PERCENT TO SOUTH)									
452	DT	51B1DV									
453	DI	0	10000								
454	DQ	0	9200								
	*										
455	KK	51B1R									
456	KM	ROUTE 51B1D THROUGH SUBBASIN 52C7 TO CP 52C7C									
457	RK	450	.04	.045			TRAP	10		10	
	*										
458	KK	52C7									
459	KM	RUNOFF FROM SUBBASIN 52C7									
460	BA	.006									
461	LS		75	27							
462	UK	100	.02	.10	100						
463	RK	550	.04	.045			TRAP	30		10	
	*										
464	KK	52C7C									
465	KM	COMBINE 51B1R, 51C3R, AND 52C7									
466	HC	3	.0693								
	*										
467	KK	52C7R									
468	KM	ROUTE 52C7C THROUGH SUBBASIN 52C9 TO CP 52C9C1									
469	RK	1550	.036	.045			TRAP	10		10	
	*										
470	KK	51B1DV									
471	KM	RETRIEVE DIVERTED FLOW 51B1DV									
472	DR	51B1DV									
	*										

LINE	ID	1	2	3	4	5	6	7	8	9	10
473	KK	51B2D									
474	KM	DIVERT 84 PERCENT OF 51B1DV TO WEST (16 PERCENT TO SOUTH)									
475	DT	51B2DV									
476	DI	0	10000								
477	DQ	0	8400								
	*										
478	KK	51B2R									
479	KM	ROUTE 51B2D THROUGH SUBBASIN 52C8 TO CP 52C8C									
480	RK	750	.034	.045			TRAP	10	10		
	*										
481	KK	52C8									
482	KM	RUNOFF FROM SUBBASIN 52C8									
483	BA	.008									
484	LS		75	27							
485	UK	100	.02	.10	100						
486	RK	750	.034	.045			TRAP	30	10		
	*										
487	KK	52C8C									
488	KM	COMBINE 51B2R AND 52C8									
489	HC	2	.4493								
	*										
490	KK	52C8R									
491	KM	ROUTE 52C8C THROUGH SUBBASIN 52C9 TO CP 52C9C1									
492	RK	1100	.036	.045			TRAP	10	10		
	*										
493	KK	52C9C1									
494	KM	COMBINE 52C7R AND 52C8R									
495	HC	2									
	*										
496	KK	52C9R1									
497	KM	ROUTE 52C9C1 THROUGH SUBBASIN 52C9 TO CP 52C9C2									
498	RK	1050	.036	.045			TRAP	10	10		
	*										
499	KK	52C9									
500	KM	RUNOFF FROM SUBBASIN 52C9									
501	BA	.069									
502	LS		75	31.85							
503	UK	100	.02	.10	100						
504	RK	3150	.036	.045			TRAP	30	10		
	*										
505	KK	52C9C2									
506	KM	COMBINE 52C9R1 AND 52C9									
507	HC	2									
	*										

LINE	ID	1	2	3	4	5	6	7	8	9	10
508	KK	52C9R2									
509	KM	ROUTE 52C9C2 THROUGH SUBBASIN 52C10 TO CP 52C10C1									
510	RK	500	.032	.045		TRAP	10		10		
	*										
511	KK	2C10C1									
512	KM	COMBINE 52C9R2 AND 52C6R									
513	HC	2									
	*										
514	KK	2C10R1									
515	KM	ROUTE 52C10C1 THROUGH SUBBASIN 52C10 TO CP 52C10C2									
516	RK	300	.032	.045		TRAP	10		10		
	*										
517	KK	52C10									
518	KM	RUNOFF FROM SUBBASIN 52C10									
519	BA	.014									
520	LS		75	7.85							
521	UK	100	.02	.10	100						
522	RK	800	.032	.045		TRAP	30		10		
	*										
523	KK	2C10C2									
524	KM	COMBINE 52C10R1 AND 52C10									
525	HC	2									
	*										
526	KK	52C11									
527	KM	RUNOFF FROM SUBBASIN 52C11									
528	BA	.0425									
529	LS		75	27							
530	UK	100	.02	.10	100						
531	RK	2800	.031	.045		TRAP	30		10		
	*										
532	KK	2C11R1									
533	KM	PIPE ROUTE 52C11 TO CP 52C11C									
534	RK	650	.02	.045		CIRC	3				
	*										
535	KK	52C13D									
536	KM	RETRIEVE DIVERTED FLOW									
537	DR	STORM									
	*										
538	KK	52C11C									
539	KM	COMBINE 52C13D AND 52C11R1									
540	HC	2	.0655								
	*										

LINE	ID	1	2	3	4	5	6	7	8	9	10
541	KK	2C11CR									
542	KM	PIPE ROUTE 52C11C TO CP 52C11C2									
543	RK	750	.02	.045			CIRC		3		
	*										
544	KK	2C11C2									
545	KM	COMBINE 52C11CR AND 52C10C2									
546	HC	2									
	*										
547	KK	2C11R2									
548	KM	ROUTE 52C11C2 THROUGH SUBBASIN 52C12 TO CP 52C12C									
549	RK	700	.03	.045			TRAP	10		10	
	*										
550	KK	52C12									
551	KM	RUNOFF FROM SUBBASIN 52C12									
552	BA	.023									
553	LS		75	85							
554	UK	100	.02	.10	100						
555	RK	900	.03	.045			TRAP	30		10	
	*										
556	KK	52C12C									
557	KM	COMBINE 52C11R2 AND 52C12									
558	HC	2									
	*										
559	KK	52C12R									
560	KM	ROUTE 52C12C THROUGH SUBBASIN 52C14 TO CP 52C14C1									
561	RK	1150	.029	.045			TRAP	10		10	
	*										
562	KK	52C14B									
563	KM	RUNOFF FROM SUBBASIN 52C14B									
564	BA	.021									
565	LS		75	60							
566	UK	100	.02	.10	100						
567	RK	1250	.029	.045			TRAP	30		10	
	*										
568	KK	C14BC1									
569	KM	COMBINE 52C14B AND 52C12R									
570	HC	2									
	*										
571	KK	C14BC2									
572	KM	COMBINE 52C14BC1 AND 52C14AR									
573	HC	2									
	*										

LINE	ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
574	KK 52C14R
575	KM ROUTE 52C14C3 WEST IN BEARDSLEY CHANNEL TO CP 52B5C2
576	RK 600 .0143 .035 TRAP 50 4
	*
577	KK 51B2DV
578	KM RETRIEVE DIVERTED FLOW
579	DR 51B2DV
	*
580	KK 51B3D
581	KM DIVERT 84 PERCENT OF 51B2DV TO WEST (16 PERCENT TO SOUTH)
582	DT 51B3DV
583	DI 0 10000
584	DQ 0 8400
	*
585	KK 51B3R
586	KM ROUTE 51B3D THROUGH SUBBASIN 52B1 TO CP 52B1C
587	RK 600 .039 .045 TRAP 10 10
	*
588	KK 52B1
589	KM RUNOFF FROM SUBBASIN 52B1
590	BA .003
591	LS 75 27
592	UK 100 .02 .10 100
593	RK 600 .039 .045 TRAP 30 10
	*
594	KK 52B1C
595	KM COMBINE 51B3R AND 52B1
596	HC 2 .0736
	*
597	KK 52B1R
598	KM ROUTE 52B1C THROUGH SUBBASIN 52B2 TO CP 52B2C1
599	RK 930 .037 .045 TRAP 10 10
	*
600	KK 51B3DV
601	KM RETRIEVE DIVERTED FLOW 51B3DV
602	DR 51B3DV
	*
603	KK 51B4D
604	KM DIVERT 82 PERCENT OF 51B3DV TO WEST (18 PERCENT TO SOUTH)
605	DT 51B4DV
606	DI 0 10000
607	DQ 0 8200
	*

LINE	ID	1	2	3	4	5	6	7	8	9	10
608	KK	51B4R1									
609	KM	ROUTE 51B4D THROUGH SUBBASIN 52B2 TO CP 52B2C1									
610	RK	1350	.037	.045			TRAP	10		10	
	*										
611	KK	52B2C1									
612	KM	COMBINE 51B4R1 AND 52B1R									
613	HC	2	.1403								
	*										
614	KK	52B2R1									
615	KM	ROUTE 52B2R1 THROUGH SUBBASIN 52B2 TO CP 52B2C2									
616	RK	1000	.037	.045			TRAP	10		10	
	*										
617	KK	52B2									
618	KM	RUNOFF FROM SUBBASIN 52B2									
619	BA	.032									
620	LS		75	17							
621	UK	100	.02	.10	100						
622	RK	2350	.037	.045			TRAP	30		10	
	*										
623	KK	52B2C2									
624	KM	COMBINE 52B2 AND 52B2R1									
625	HC	2									
	*										
626	KK	52B2R2									
627	KM	ROUTE 52B2C2 THROUGH SUBBASIN 52B3 TO CP 52B3C2									
628	RK	850	.026	.045			TRAP	10		10	
	*										
629	KK	52B3R1									
630	KM	ROUTE 52B3C1 THROUGH SUBBASIN 52B3 TO CP 52B3C2									
631	RK	500	.024	.045			TRAP	10		10	
	*										
632	KK	52B3									
633	KM	RUNOFF FROM SUBBASIN 52B3									
634	BA	.062									
635	LS		75	31.8							
636	UK	100	.02	.10	100						
637	RK	3450	.030	.045			TRAP	30		10	
	*										
638	KK	52B3C2									
639	KM	COMBINE 52B3 AND 52B3R1									
640	HC	2									
	*										

LINE	ID	1	2	3	4	5	6	7	8	9	10
641	KK	52B3R2									
642	KM	ROUTE 52B3C2 THROUGH 52B4 TO CP 52B4C									
643	RK	1700	.024	.045			TRAP	10		10	
	*										
644	KK	52B4									
645	KM	RUNOFF FROM SUBBASIN 52B4									
646	BA	.026									
647	LS		75	62							
648	UK	100	.02	.10	100						
649	RK	1700	.024	.045			TRAP	30		10	
	*										
650	KK	52B4C									
651	KM	COMBINE 52B4 AND 52B3R2									
652	HC	2									
	*										
653	KK	52B4R									
654	KM	ROUTE 52B4C THROUGH SUBBASIN 52B5 TO CP 52B5C1									
655	RK	550	.027	.045			TRAP	10		10	
	*										
656	KK	52B5									
657	KM	RUNOFF FROM SUBBASIN 52B5									
658	BA	.021									
659	LS		75	56.9							
660	UK	100	.02	.10	100						
661	RK	1400	.03	.045			TRAP	30		10	
	*										
662	KK	52B5C1									
663	KM	COMBINE 52B5 AND 52B4R									
664	HC	2									
	*										
665	KK	52B5C2									
666	KM	COMBINE 52B5C1 AND 52C14R									
667	HC	2									
	*										
668	KK	52B5R									
669	KM	ROUTE 52B5C2 IN BEARDSLEY CHANNEL TO CP 52B7C2									
670	RK	1100	.0143	.035			TRAP	50		4	
	*										
671	KK	51B4DV									
672	KM	RETRIEVE DIVERTED FLOW 51B4DV									
673	DR	51B4DV									
	*										



LINE	ID	1	2	3	4	5	6	7	8	9	10
707	KK	51B7R2									
708	KM	ROUTE 51B7C THROUGH SUBBASIN 52B6 TO CP 52B6C									
709	RK	2300	.033	.045			TRAP	10		10	
	*										
710	KK	52B6									
711	KM	RUNOFF FROM SUBBASIN 52B6									
712	BA	.096									
713	LS		75	13.55							
714	UK	100	.02	.10	100						
715	RK	3200	.033	.045			TRAP	30		10	
	*										
716	KK	52B6C									
717	KM	COMBINE 51B7R2 AND 52B6									
718	HC	2									
	*										
719	KK	52B6R									
720	KM	ROUTE 52B6C THROUGH SUBBASIN 52B7 TO CP 52B7C1									
721	RK	2750	.028	.045			TRAP	10		10	
	*										
722	KK	52B7									
723	KM	RUNOFF FROM SUBBASIN 52B7									
724	BA	.080									
725	LS		75	78.45							
726	UK	100	.02	.10	100						
727	RK	2750	.028	.045			TRAP	30		10	
	*										
728	KK	52B7C1									
729	KM	COMBINE 52B7 AND 52B6R									
730	HC	2									
	*										
731	KK	52B7C2									
732	KM	COMBINE 52B7C1 AND 52B5R									
733	HC	2									
	*										
734	KK	52A2									
735	KM	RUNOFF FROM SUBBASIN 52A2									
736	BA	.065									
737	LS		75	88.8							
738	UK	100	.02	.10	100						
739	RK	2900	.023	.045			TRAP	30		10	
	*										

LINE	ID	1	2	3	4	5	6	7	8	9	10
740	KK	52A2C2									
741	KM	COMBINE 52B7C2 AND 52A2									
742	HC	2	1.62								
	*										
743	KK	51B7DV									
744	KM	RETRIEVE DIVERTED FLOW 51B7DV									
745	DR	51B7DV									
	*										
746	KK	51B8R									
747	KM	ROUTE 51B7DV THROUGH SUBBASIN 52A1 TO CP 52A1C									
748	RK	3400	.033	.045		TRAP	10	10			
	*										
749	KK	52A1									
750	KM	RUNOFF FROM SUBBASIN 52A1									
751	BA	.130									
752	LS		75	32.25							
753	UK	100	.02	.10	100						
754	RK	3400	.033	.045		TRAP	30	10			
	*										
755	KK	52A1C									
756	KM	COMBINE 52A1 AND 51B8R									
757	HC	2									
	*										
	*										
	*	***** END DC RANCH WATERSHED *****									
	*										
	*	***** BEGIN GVSCE MODIFICATIONS *****									
	*										
758	KK	D51.1									
759	KM	RETRIEVE DIVERTED FLOW									
760	DR	B51.1T									
	*										
761	KK	C52A									
762	KM	COMBINE ROUTED HYDROGRAPH FROM C51.1 WITH HYDROGRAPH FROM C52A1C AT									
763	KM	THOMPSON PEAK PARKWAY									
764	HC	2	6.2735								
	*										
765	KK	R52A									
766	KM	NORMAL DEPTH CHANNEL ROUTE FROM C52A TO C52 THROUGH PIMA CHANNEL									
767	RS	1	FLOW	-1							
768	RC	0.035	0.025	0.035	2700	0.01					
769	RX	1000	1020	1022	1034	1084	1096	1098	1118		
770	RY	111.4	106.4	106.3	100	100	106.3	106.4	111.4		
	*										

LINE	ID	1	2	3	4	5	6	7	8	9	10
771	KK	C52									
772	KM	COMBINE ROUTED HYDROGRAPH FROM C52A WITH HYDROGRAPH FROM C52A2C AT									
773	KM	BEARDSLEY ROAD									
774	HC	2	7.9160								
	*										
775	KK	R52									
776	KM	NORMAL DEPTH CHANNEL ROUTE FROM C52 TO C53 THROUGH PIMA CHANNEL									
777	RS	1	FLOW	-1							
778	RC	0.035	0.025	0.035	3600	0.01					
779	RX	1000	1020	1022	1034	1084	1096	1098	1118		
780	RY	111.4	106.4	106.3	100	100	106.3	106.4	111.4		
	*										
781	KK	D52T									
782	KM	DIVERT 100% OF FLOW TO RETRIEVE JUST U/S OF UNION HILLS DETENTION BASIN									
783	DT	B52T									
784	DI	0	10000								
785	DQ	0	10000								
	*										
786	KK	CLEAR									
787	KM	CLEAR HYDROGRAPHS FROM STACK									
788	HC	2									
	*										
	*	***** BEGIN GREYHAWK WATERSHED *****									
	*										
	*	THE GREYHAWK HEC-1 MODEL (VILLAGES II AND III) WAS DEVELOPED BY DEI									
	*	DEI FILE NAME: GH23FAB.H1I									
	*	MODEL DATE: 21 MAY 96									
	*										
789	KK	37A	SUB								
790	KM	RUNOFF FROM SUB-BASIN 37A									
791	BA	.6765									
792	LS		74	24.8							
793	UK	61	.0213	.10	100						
794	RK	4800	.0237	.045	TRAP	50	130				
	*										
795	KK	37AE	DIV								
796	KM	SPLIT FLOWS AT SOUTH BOUNDARY OF SUB 37A FOR ROUTING TO DETENTION									
797	KM	BASIN 53R & 38R-1. THIS DIVERT OPERATION REFLECTS THE BREAK IN THE									
798	KM	DEER VALLEY ROAD CHANNEL BETWEEN HAYDEN & PIMA ROADS. THIS SPLIT IS									
799	KM	BASED ON NEW CORE NORTH PLAN DEVELOPED BY G.W. LARSON & ASSC., INC.									
800	KM	DATED 6/16/92. DIVERT RATIO IS BASED ON APPROXIMATE D.A. FROM SUB 37A									
801	KM	THAT IS INTERCEPTED BY EACH CHANNEL SEGMENT ALONG DEER VALLEY ROAD.									
802	KM										
803	KM	(THIS SPLIT HAS BEEN UPDATED FROM THE OLP.6 MODEL TO REFLECT A 30% SPLIT									
804	KM	TO THE SOUTH AND A 70% SPLIT TO THE WEST FOR THIS STUDY AND IS BASED ON									
805	KM	UPSTREAM CONTRIBUTING WATERSHED AREA TO THIS CONCENTRATION POINT)									
806	DT	37AW									
807	DI	0	100	500	1000	1500					
808	DQ	0	70	350	700	1050					





LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

883 KK R2NB  
 884 KM ROUTE FLOW FROM CP2NA TO CP2NB  
 885 RS 1 FLOW  
 886 RC .03 .03 .03 1050 .015  
 887 RX 0 8 13 17 22 26 31 39  
 888 RY 4 2 2 0 0 2 2 4  
 \*

889 KK SUB2NB  
 890 KM RUNOFF FROM SUBBASIN 2NB  
 891 BA .03  
 892 LS 77 53  
 893 UK 150 .013 .15 100  
 894 RK 1200 .015 .025 TRAP 20 50  
 \*

895 KK CP2NB  
 896 KM ADD HYDROGRAPHS AT CP2NB  
 897 HC 2  
 \*

898 KK SR2NB  
 899 KM STORAGE ROUTE FLOW THROUGH DETENTION BASIN IN SUB2NB  
 900 RS 1 STOR 0 0  
 901 SV 0 .19 .69 1.66 3.23 4.5  
 902 SQ 0 2 8 12 17 170  
 903 SE 1796 1798 1800 1802 1804 1805  
 \*

904 KK RCP4N  
 905 KM ROUTE FLOW FROM CP2NB TO CP4N  
 906 RS 1 FLOW  
 907 RC .03 .03 .03 740 .018  
 908 RX 0 8 13 17 22 26 31 39  
 909 RY 4 2 2 0 0 2 2 4  
 \*

910 KK SUB6N  
 911 KM RUNOFF FROM SUBBASIN 6 IN NORTH 18 MODEL. TO LAKE NORTH OF CLUBHOUSE.  
 912 BA .049  
 913 LS 81 0  
 914 UK 200 .025 .15 100  
 915 RK 1300 .015 .025 TRAP 10 4  
 \*

916 KK RET6N  
 917 KM RETENTION ROUTING THROUGH LAKE AT HOLE 18, NORTH COURSE.  
 918 RS 1 STOR  
 919 SV 0 3.01 6.64 10.75 13.09 15.90  
 920 SQ 0 0 0 10 26 100  
 921 SE 1782 1784 1786 1788 1789 1790  
 \*

LINE	ID	1	2	3	4	5	6	7	8	9	10
922	KK	RCP4N1									
923	KM	ROUTE FLOW FROM CP6N TO CP4N									
924	RS	1	FLOW								
925	RC	.03	.03	.03	550	.018					
926	RX	0	8	13	17	22	26	31	39		
927	RY	4	2	2	0	0	2	2	4		
	*										
928	KK	CP4N.1									
929	KM	ADD HYDROGRAPHS AT CP4N.1									
930	HC	2									
	*										
931	KK	SUB3N									
932	KM	RUNOFF FROM SUBBASIN 3N, NORTH 18 MODEL									
933	BA	.027									
934	LS		81	0							
935	UK	100	.02	.15	100						
936	RK	2800	0.0207	.025		TRAP	10	4			
	*										
937	KK	RET3N									
938	KM	ROUTE FLOW THROUGH RETENTION BASIN NO. 3. 18" PIPE OUTFLOW WILL									
939	KM	BLEED FLOWS TO DRAIN THE BASIN AFTER THE STORM HAS PASSED.									
940	RS	1	STOR	0	0						
941	SV	0	1.73	8.97	13.32	15.74					
942	SQ	0	4	7	9	11					
943	SE	1793	1795	1800	1803	1804					
	*										
944	KK	R4N									
945	KM	ROUTE FLOW FROM CP3N TO CP4N IN NORTH MODEL									
946	RS	1	FLOW								
947	RC	.035	.035	.035	950	.018					
948	RX	0	8	13	17	22	26	31	39		
949	RY	4	2	2	0	0	2	2	4		
	*										
950	KK	CP4N.2									
951	KM	ADD HYDROGRAPHS AT CPN.2									
952	HC	2									
	*										
953	KK	SUB4N									
954	KM	RUNOFF FROM SUBBASIN 4N.									
955	BA	.032									
956	LS		77	18							
957	UK	100	.015	.15	100						
958	RK	1200	0.007	.018		TRAP	50	20			
	*										

LINE	ID	1	2	3	4	5	6	7	8	9	10
959	KK	CP4N									
960	KM	ADD HYDROGRAPHS AT CP4N									
961	HC	2									
	*										
962	KK	R6N									
963	KM	ROUTE FLOW FROM CP4N TO CP6N ALONG THOMPSON PEAK PKWY AT CLUBHOUSE									
964	RS	1	FLOW								
965	RC	.045	.035	.045	750	.025					
966	RX	0	8	13	17	22	26	31	39		
967	RY	4	2	2	0	0	2	2	4		
	*										
968	KK	SUB6A									
969	KM	RUNOFF FROM SUBBASIN 6A (CLUBHOUSE AREA NORTH OF THOMPSON PEAK PKWY).									
970	BA	.013									
971	LS		83	68							
972	UK	100	.015	.12	100						
973	RK	800	.01	.025		TRAP	2	3			
	*										
974	KK	CP6.2									
975	KM	ADD HYDROGRAPHS AT CP6.2									
976	HC	2									
	*										
977	KK	CP6N									
978	KM	ADD HYDROGRAPHS AT CP6N									
979	HC	2									
	*										
	*	ABOVE DISCHARGE FROM NORTH 18 THROUGH BRIDGE AT TFP STATION 103+45									
	*										
980	KK	RCP6N									
981	KM	ROUTE FLOW FROM CP6N TO CP3C									
982	RS	1	FLOW								
983	RC	.045	.035	.045	300	.015					
984	RX	0	8	13	17	37	45	51	59		
985	RY	4	2	2	0	0	2	2	4		
	*										
986	KK	SUB3C									
987	KM	RUNOFF FROM SUBBASIN 3C, SOUTH COURSE AT MAINTENANCE FACILITY.									
988	BA	.0104									
989	LS		77	68							
990	UK	100	.025	.02	100						
991	RK	600	.015	.035		TRAP	50	20			
	*										

LINE	ID	1	2	3	4	5	6	7	8	9	10
992	KK	CP3C									
993	KM	COMBINE NORTH COURSE HYDROGRAPH WITH FIRST SOUTH COURSE HYDROGRAPH									
994	HC	2									
	*										
995	KK	R3C									
996	KM	ROUTE FLOW FROM SUB3C TO CP3 THROUGH GC1018									
997	KM	ASSUME CHANNEL IS SAME CONFIGURATION AS ABOVE FOR PROPOSED GOLF COURSE									
998	KM	CHANNEL.									
999	RS	1	FLOW								
1000	RC	.055	.045	.055	2050	.025					
1001	RX	0	20	30	40	60	70	80	100		
1002	RY	1650	1746	1744	1742	1742	1744	1746	1750		
	*										
1003	KK	GC1018									
1004	KM	RUNOFF FROM HOLES NO. 10, 18 AND DRIVING RANGE THAT CONTRIBUTE TO WASH									
1005	BA	.044									
1006	LS		81	0							
1007	UK	200	.025	.15	100						
1008	RK	1800	.0233	.025		TRAP	10	4			
	*										
1009	KK	GC1-9									
1010	KM	RUNOFF FROM GOLF COURSE HOLES 1 & 9 CONTRIBUTING TO WASH									
1011	BA	.026									
1012	LS		81	0							
1013	UK	200	.025	.15	100						
1014	RK	2110	.022	.025		TRAP	10	4			
	*										
1015	KK	SUB3S									
1016	KM	RUNOFF FROM SUB BASIN 3 SOUTH COURSE									
1017	BA	.0102									
1018	LS		77	53							
1019	UK	100	.010	.15	100						
1020	RK	930	.016	.025		TRAP	50	20			
	*										
1021	KK	CP3S									
1022	KM	COMBINE HYDROGRAPHS AT CP3 SOUTH COURSE									
1023	HC	4									
	*										
1024	KK	RT3S									
1025	KM	ROUTE FLOW FROM CP3S TO CPGC28									
1026	RS	1	FLOW								
1027	RC	.055	.045	.055	900	.023					
1028	RX	0	20	30	40	60	70	80	100		
1029	RY	1750	1746	1744	1742	1742	1744	1746	1750		
	*										



LINE	ID	1	2	3	4	5	6	7	8	9	10
1066	KK	RT7S									
1067	KM	ROUTE FLOW FROM SRGC28 TO CP7S									
1068	RS	1	STOR	0	0						
1069	RC	.055	.045	.055	1700	.0187					
1070	RX	0	20	30	40	60	70	80	100		
1071	RY	1750	1746	1744	1742	1742	1744	1746	1750		
	*										
1072	KK	GC7									
1073	KM	RUNOFF FROM SOUTH GOLF COURSE HOLE NO. 7									
1074	BA	.0134									
1075	LS		81	0							
1076	UK	200	.025	.15	100						
1077	RK	1380	.020	.025		TRAP	10	4			
	*										
1078	KK	CP7S									
1079	KM	ADD HYDROGRAPHS AT CP7S ON SOUTH COURSE									
1080	HC	2	0.6083								
	*										
1081	KK	D7ST									
1082	KM	D7ST IS A DIVERSION ADDED BY GVSCE IN ORDER TO ROUTE RUNOFF TO THE									
1083	KM	UNION HILLS DETENTION BASIN VIA THE POWER LINE CHANNEL.									
1084	KM										
1085	KM	DIVERT 100% OF FLOW									
1086	DT	B7ST									
1087	DI	0	10000								
1088	DQ	0	10000								
	*										
1089	KK	CLEAR									
1090	KM	CLEAR HYDROGRAPHS FROM THE STACK.									
1091	HC	2									
	*										
	*										
	*	THIS PORTION OF MODEL TAKEN FROM, "DRAINAGE REPORT FOR VILLAGE 3 - PHASE 1",									
	*	APPROVED BY THE CITY OF SCOTTSDALE 7-19-95. MODIFIED TO ACCOUNT FOR ASBUILT									
	*	CONDITION									
	*										
	*										
	*										
	*										
1092	KK	SUB3D1									
1093	KM	RUNOFF FROM SUBBASIN 3D1, PARCEL 3D.									
1094	BA	.0088									
1095	LS		77	34							
1096	UD	.06									
	*										

LINE	ID.....	1.....	2.....	3.....	4.....	5.....	6.....	7.....	8.....	9.....	10
1097	KK	RD1B1									
1098	KM	FOUTE FLOW FROM 3D1 TO 3B1									
1099	RS	1	FLOW	-1							
1100	RC	0.03	0.03	0.03	1250	.015					
1101	RX	0	0.5	1	7	12	19	19.5	20		
1102	RY	3.2	3.1	3.0	1.0	1.0	3.0	3.1	3.2		
	*										
1103	KK	SUB3B1									
1104	KM	RUNOFF FROM SUBBASIN 3B1, PARCEL 3B.									
1105	BA	.0137									
1106	LS		77	47							
1107	UD	.06									
	*										
1108	KK	CP3B1									
1109	KM	ADD HYDROGRAGHS AT CP3B1									
1110	HC	2									
	*										
1111	KK	RB13F									
1112	KM	ROUTE FLOW FROM 3B1 TO SUB3F									
1113	RS	1	FLOW	-1							
1114	RC	0.03	0.03	0.03	2150	.015					
1115	RX	0	0.5	1	7	17	24	24.5	25		
1116	RY	3.2	3.1	3.0	1.0	1.0	3.0	3.1	3.2		
	*										
1117	KK	SUB3F									
1118	KM	RUNOFF FROM SUBBASIN 3F, PARCEL 3F, SOUTH COURSE MODEL.									
1119	BA	.0344									
1120	LS		77	68							
1121	UK	100	.025	.15	100						
1122	RK	1000	.015	.025		TRAP	100	20			
	*										
1123	KK	CP3F									
1124	KM	ESTIMATED PEAK DISCHARGE RATE AT POINT CP3F ALONG THE POWER CORRIDOR									
1125	HC	2									
	*										
1126	KK	SUB3B2									
1127	KM	RUNOFF FROM SUBBASIN 3B2, PARCEL 3B.									
1128	BA	.0246									
1129	LS		77	40							
1130	UD	.10									
	*										
1131	KK	RB2E1									
1132	KM	1/2 OF ENTIRE ROUTING REACH FROM 3B2 TO CP3E1									
1133	RS	1	FLOW	-1							
1134	RC	0.03	0.03	0.03	800	0.02					
1135	RX	0	0.5	1	7	17	24	24.5	25		
1136	RY	3.2	3.1	3.0	1.0	1.0	3.0	3.1	3.2		

LINE	ID	1	2	3	4	5	6	7	8	9	10
1137	KK	RB2E2									
1138	KM	SECOND 1/2 OF ENTIRE ROUTING REACH FROM 3B2 TO CP3E1									
1139	RS	1	FLOW	-1							
1140	RC	0.03	0.03	0.03	600	.015					
1141	RX	0	0.5	1	7	17	24	24.5	25		
1142	RY	3.2	3.1	3.0	1.0	1.0	3.0	3.1	3.2		
	*										
1143	KK	SUB3E1									
1144	KM	RUNOFF FROM SUBBASIN 3E1, PARCEL 3E.									
1145	BA	.0246									
1146	LS		77	40							
1147	UD	.10									
	*										
1148	KK	1CPE31									
1149	KM	ESTIMATED PEAK DISCHARGE RATE AT POINT CP3E1 ALONG THE POWER CORRIDOR									
1150	HC	2									
	*										
1151	KK	SUB3D2									
1152	KM	RUNOFF FROM SUBBASIN 3D2, PARCEL 3D.									
1153	BA	.022									
1154	LS		77	35							
1155	UD	.08									
	*										
1156	KK	RD2E2									
1157	KM	ROUTE EXCESS FROM 3D2 TO CP3E2									
1158	RS	1	FLOW	-1							
1159	RC	0.03	0.03	0.03	1200	.0216					
1160	RX	0	0.5	1	7	17	24	24.5	25		
1161	RY	3.2	3.1	3.0	1.0	1.0	3.0	3.1	3.2		
	*										
1162	KK	SUB3E2									
1163	KM	RUNOFF FROM SUBBASIN 3E2, PARCEL 3E.									
1164	BA	.012									
1165	LS		77	35							
1166	UD	.06									
	*										
1167	KK	CP3E2									
1168	KM	ESTIMATED PEAK DISCHARGE RATE AT POINT CP3E2 ALONG THE POWER CORRIDOR									
1169	HC	2									
	*										
1170	KK	PC3									
1171	KM	PC3 IS A SUBBASIN ADDED BY GVSCE TO ESTIMATE THE SURFACE RUNOFF FROM									
1172	KM	THE POWER LINE CORRIDOR WHICH ENTERS THE POWER LINE CHANNEL									
1173	KM										
1174	KM	RUNOFF FROM SUBBASIN PC3.									
1175	BA	0.0434									
1176	LS		77	10							



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LINE      ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

1220      KK   DPC4T
1221      KM           DPC3T IS A DIVERSION ADDED BY GVSCE IN ORDER TO ROUTE RUNOFF TO THE
1222      KM           UNION HILLS DETENTION BASIN VIA THE POWER LINE CHANNEL.
1223      KM
1224      KM           DIVERT 100% OF FLOW
1225      DT   BPC4T
1226      DI     0   10000
1227      DQ     0   10000
          *

1228      KK   CLEAR
1229      KM           CLEAR HYDROGRAPHS FROM THE STACK.
1230      HC     3
          *
          *
          *   THIS ENDS THE PORTION OF THE MODEL TAKEN FROM DRAINAGE REPORT
          *   FOR VILLAGE 3 - PHASE I HEC-1 MODEL BY GILBERTSON ASSOC. INC.
          *   DATED 7-19-95
          *
          *
          *   RETURN TO NORTH 18\VILLAGE 2\TPP3 MODEL.
          *   THE REMAINDER OF THE SUBBASINS IN THIS MODEL WILL CONTRIBUTE TO THE
          *   PROPOSED CHANNNEL IN THE POWER EASEMENT AS IDENTIFIED IN THE
          *   "COMMUNITY DRAINAGE STUDY - CORE NORTH AND WILL DISCHARGE TO REGIONAL
          *   RETENTION BASIN 38R1.
          *
          *
1231      KK   37AW   RET
1232      KM           RETRIEVE DIVERTED FLOW FROM SOUTH BOUNDARY OF SUB 37A TO REFLECT
1233      KM           BREAK IN DEER VALLEY ROAD CHANNEL BETWEEN HAYDEN & PIMA ROADS
1234      DR   37AW
          *

1235      KK   R14R
1236      KM           ROUTE FLOW FROM DIVERT AT DEER VALLEY ROAD (UPSTREAM OF SUBBAIN 5) TO
1237      KM           RET14.1
1238      RS     1   FLOW
1239      RC   .055 .045 .055 2900 .01
1240      RX     0   16   26   30   50   54   64   80
1241      RY     6    2    2    0    0    2    2    6
          *   RET 141 HAS BEEN REVISED FOLLOWING REFINEMENT OF GRADING PLANS 11-16-94
          *

1242      KK   RET141
1243      KM           ROUTE FLOW THROUGH RETENTION BASIN NO. 14.1. 18" PIPE OUTFLOW WILL
1244      KM           BLEED FLOWS TO DRAIN THE BASIN AFTER THE STORM HAS PASSED.
1245      RS     1   STOR     0     0
1246      SV     0   .46   2.79   4.56   5.71   6.92   8.24
1247      SQ     0    11    15    22    147   463   968
1248      SE   1778  1785  1790  1792  1793  1794  1795
          *
    
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LINE	ID	.....1	.....2	.....3	.....4	.....5	.....6	.....7	.....8	.....9	.....10
1249	KK	R14.1									
1250	KM	ROUTE FLOW FROM RET14.1 TO CP14									
1251	KM	RET14.1									
1252	RS	1	FLOW								
1253	RC	.055	.045	.055	1900	.01					
1254	RX	0	16	26	30	50	54	64	80		
1255	RY	6	2	2	0	0	2	2	6		
	*										
1256	KK	SUB13N									
1257	KM	RUNOFF FROM SUBBASIN 13 NORTH 18 MODEL.									
1258	BA	.037									
1259	LS		77	24							
1260	UK	100	.015	.15	100						
1261	RK	2400	.007	.018		TRAP	50	20			
	*										
1262	KK	R14.1									
1263	KM	ROUTE FLOW FROM CP13 TO RET14 NORTH 18 MODEL.									
1264	RS	1	FLOW								
1265	RC	.055	.045	.055	950	.025					
1266	RX	0	8	13	17	22	26	31	39		
1267	RY	4	2	2	0	0	2	2	4		
	*										
1268	KK	SUB14N									
1269	KM	RUNOFF FROM SUBBASIN 14 NORTH 18 MODEL.									
1270	BA	.049									
1271	LS		81	0							
1272	UK	300	.025	.15	100						
1273	RK	2300	.01	.025		TRAP	10	4			
	*										
1274	KK	CP14									
1275	KM	ADD HYDROGRAPHS AT CP14									
1276	HC	3	0.5595								
	*										
1277	KK	RET14									
1278	KM	ROUTE FLOW THROUGH RETENTION BASIN NO. 14. 18" PIPE OUTFLOW WILL									
1279	KM	BLEED FLOWS TO DRAIN THE BASIN AFTER THE STORM HAS PASSED.									
1280	RS	1	STOR	0	0						
1281	SV	0	.08	.31	1.01	2.16	3.20	4.19	5.69	7.8	
1282	SQ	0	14	16	18	20	22	155	464	750	
1283	SE	1744	1746	1748	1750	1752	1753	1754	1755	1756	
	*										
1284	KK	R18.1									
1285	KM	ROUTE FLOW FROM RET14 TO CP18									
1286	RS	1	FLOW								
1287	RC	.055	.045	.055	500	.016					
1288	RX	0	16	26	34	54	68	78	96		
1289	RY	6	2	2	0	0	2	2	6		
	*										



LINE	ID	1	2	3	4	5	6	7	8	9	10
1326	KK	RPC1									
1327	KM	ROUTE FLOW FROM CP18N TO CPC1.									
1328	RS	1	FLOW								
1329	RC	.035	.035	.035	510	.013					
1330	RX	0	16	26	34	64	78	88	106		
1331	RY	6	2	2	0	0	2	2	6		
	*										
1332	KK	UB18NA									
1333	KM	RUNOFF FROM SUBBASIN 18NA.									
1334	BA	.022									
1335	LS		77	42							
1336	UK	100	.01	.15	100						
1337	RK	1450	.02	.018		TRAP	50	20			
	*										
1338	KK	1RPC1									
1339	KM	ROUTE FLOW FROM CP18NA TO CPC1.									
1340	RS	1	FLOW								
1341	RC	.035	.035	.035	2550	.01					
1342	RX	0	16	26	34	64	78	88	106		
1343	RY	8	4	2	0	0	2	4	8		
	*										
1344	KK	UB18NB									
1345	KM	RUNOFF FROM SUBBASIN 18NB.									
1346	BA	.0096									
1347	LS		77	42							
1348	UK	100	.01	.15	100						
1349	RK	800	.02	.018		TRAP	50	20			
	*										
1350	KK	2RPC1									
1351	KM	ROUTE FLOW FROM CP18NB TO CPC1.									
1352	RS	1	FLOW								
1353	RC	.035	.035	.035	2000	.01					
1354	RX	0	16	26	34	64	78	88	106		
1355	RY	8	4	2	0	0	2	4	8		
	*										
1356	KK	PC1									
1357	KM	RUNOFF FROM SUBBASIN PC1.									
1358	BA	.062									
1359	LS		77	10							
1360	UK	500	.015	.15	100						
1361	RK	2700	.01	.03		TRAP	30	4			
	*										
1362	KK	1CPC1									
1363	KM	ADD HYDROGRAPHS AT CPC1.									
1364	HC	3									
	*										











LINE	ID	1	2	3	4	5	6	7	8	9	10
1552	KK	CP11NB									
1553	KM	ADD HYDROGRAPHS AT CP11NB									
1554	HC	2									
	*										
1555	KK	SR11NB									
1556	KM	STOAGE ROUTE THROUGH FAIRWAY DETENTION AREA IN SUB11NB.									
1557	RS	1	STOR	0	0						
1558	SV	0	1.56	2.586							
1559	SQ	0	27	111							
1560	SE	1732	1737	1738							
	*										
1561	KK	R11NC									
1562	KM	ROUTE FLOW FROM CP11NB TO CP11NC.									
1563	RS	1	FLOW								
1564	RC	.025	.025	.025	300	.03					
1565	RX	0	12	24	36	56	68	80	92		
1566	RY	6	4	2	0	0	2	4	6		
	*										
1567	KK	UB11NC									
1568	KM	RUNOFF FROM SUBBASIN 11NC.									
1569	BA	.0069									
1570	LS		81	0							
1571	UK	100	.03	.15	100						
1572	RK	650	.028	.025			TRAP	20	5		
	*										
1573	KK	C11NC1									
1574	KM	ADD HYDROGRAPHS AT CP11NC.1									
1575	HC	2									
	*										
1576	KK	SUB10A									
1577	KM	RUNOFF FROM SUBBASIN 10A.									
1578	BA	.030									
1579	LS		77	42							
1580	UK	100	.015	.15	100						
1581	RK	350	.008	.018			TRAP	50	20		
1582	RK	800	.008	.025			TRAP	10	4		
	*										
1583	KK	R12NB									
1584	KM	ROUTE FLOW FROM CP10A TO CP12NB.									
1585	RS	1	FLOW								
1586	RC	.025	.025	.025	400	.03					
1587	RX	0	12	24	36	46	58	70	82		
1588	RY	6	4	2	0	0	2	4	6		
	*										



LINE	ID.....	1.....	2.....	3.....	4.....	5.....	6.....	7.....	8.....	9.....	10
1628	KK	CP11NC									
1629	KM	ADD HYDROGRAPHS	AT CP11NC								
1630	HC	2									
	*										
1631	KK	SR11NC									
1632	KM	ROUTE FLOW THROUGH RETENTION BASIN RT11NC.	18" PIPE OUTFLOW WILL								
1633	KM	BLEED FLOWS TO DRAIN THE BASIN AFTER THE STORM HAS PASSED.									
1634	RS	1	STOR	0	0						
1635	SV	0	1.665	2.303	3.062						
1636	SQ	0	27	111	344						
1637	SE	1730	1735	1736	1737						
	*										
1638	KK	R16NC									
1639	KM	ROUTE FLOW FROM CP11NC TO CP16NC.									
1640	RS	1	FLOW								
1641	RC	.035	.035	0.035	950	.025					
1642	RX	0	8	13	17	22	26	31	39		
1643	RY	4	2	2	0	0	2	2	4		
	*										
1644	KK	UB16NC									
1645	KM	RUNOFF FROM SUBBASIN 16NC.									
1646	BA	.0337									
1647	LS		77	42							
1648	UK	100	.015	.15	100						
1649	RK	1600	.015	.022		TRAP	50	20			
	*										
1650	KK	CP16NC									
1651	KM	ADD HYDROGRAPHS	AT CP16NC								
1652	HC	2									
	*										
1653	KK	R16NC1									
1654	KM	ROUTE FLOW FROM CP16NC TO CP16NC1.									
1655	RS	1	FLOW								
1656	RC	.03	.03	.03	550	.013					
1657	RX	0	16	26	34	44	58	68	86		
1658	RY	6	2	2	0	0	2	2	6		
	*										
1659	KK	C16NC1									
1660	KM	ADD HYDROGRAPHS	AT CP16NC1.								
1661	HC	2									
	*										
1662	KK	R15N1									
1663	KM	ROUTE FLOW FROM CP16NC1 TO CP15N1.									
1664	RS	1	FLOW								
1665	RC	.035	.035	.035	600	.013					
1666	RX	0	16	26	34	54	68	78	96		
1667	RY	6	2	2	0	0	2	2	6		

LINE	ID	1	2	3	4	5	6	7	8	9	10
1668	KK	PC2									
1669	KM	RUNOFF FROM SUBBASIN PC2.									
1670	BA	.054									
1671	LS		77	10							
1672	UK	100	.015	.15	100						
1673	RK	2700	.01	.03		TRAP	50	4			
	*										
1674	KK	CP15N1									
1675	KM	ADD HYDROGRAPHS AT CP15N1									
1676	HC	2									
	*										
1677	KK	SRPC2									
1678	KM	STORAGE ROUTE THRU DETENTION BASINS IN POWER CORRIDOR THIS IS THE TOTAL									
1679	KM	FLOW REACHING THE UPSTREAM SIDE OF THE THOMPSON PEAK PARKWAY BRIDGE									
1680	RS	1	STOR	0	0						
1681	SV	0	1.02	2.70	4.48	5.8	6.9				
1682	SQ	0	0	150	350	550	850				
1683	SE	1730	1731	1732	1733	1734	1735				
	*										
1684	KK	UB17NA									
1685	KM	RUNOFF FROM SUBBASIN SUB17NA.									
1686	BA	.00979									
1687	LS		81	0							
1688	UK	150	.025	.05	100						
1689	RK	960	.0292	.025		TRAP	30	50			
	*										
1690	KK	SR17NA									
1691	KM	STORAGE ROUTE THROUGH DETENTION BASIN SR17NA.									
1692	RS	1	STOR	0	0						
1693	SV	0	.0078	.241	.523	1.00	1.735				
1694	SQ	0	1	1	1	17.4	251				
1695	SE	1755.2	1756	1758	1759	1760	1761				
	*										
1696	KK	R17NB									
1697	KM	ROUTE FLOW FROM SR17NA TO CP17NB.									
1698	RS	1	FLOW								
1699	RC	0.03	0.03	0.03	280	0.0286					
1700	RX	0	10	20	35	70	85	90	100		
1701	RY	1757	1756.8	1756.6	1756	1756	1757	1758	1759		
	*										
1702	KK	UB17NB									
1703	KM	RUNOFF FROM SUBBASIN SUB17NB.									
1704	BA	.0111									
1705	LS		81	0							
1706	UK	150	.025	.05	100						
1707	RK	1200	.0217	.025		TRAP	30	50			
	*										

LINE	ID	1	2	3	4	5	6	7	8	9	10
1708	KK	CP17NB									
1709	KM	ADD HYDROGRAPHS AT SUB17NB.									
1710	HC	2									
	*										
1711	KK	SR17NB									
1712	KM	STORAGE ROUTE THROUGH DETENTION BASIN SR17NB.									
1713	RS	1	STOR	0	0						
1714	SV	0	.0113	.1469	.635	.9795	1.509	2.254	3.243		
1715	SQ	0	1	1	1	1	1	38.2	189		
1716	SE	1751.5	1752	1753	1755	1756	1757	1758	1759		
	*										
1717	KK	R17A									
1718	KM	ROUTE FLOW FROM SR17NB TO CP17A.									
1719	RS	1	FLOW								
1720	RC	0.03	0.03	0.03	280	0.033					
1721	RX	0	15	18	20	24	27	30	35		
1722	RY	1755	1754	1753	1752	1752	1753	1754	1755		
	*										
1723	KK	SUB17A									
1724	KM	RUNOFF FROM SUBBASIN SUB17A.									
1725	BA	.00792									
1726	LS		77	34							
1727	UK	75	.03	.05	100						
1728	RK	1500	.02	.025		TRAP	8	4			
	*										
1729	KK	CP17A1									
1730	KM	ADD HYDROGRAPHS AT CP17A1.									
1731	HC	2									
	*										
1732	KK	UB17NC									
1733	KM	RUNOFF FROM SUBBASIN SUB17NC.									
1734	BA	.00559									
1735	LS		77	12							
1736	UK	75	.03	.05	100						
1737	RK	910	.0187	.025		TRAP	8	4			
	*										
1738	KK	CP17A									
1739	KM	ADD ALL HYDROGRAPHS AT CP17A.									
1740	HC	2									
	*										
1741	KK	R15N									
1742	KM	ROUTE FLOW FROM CP17A TO CP15N.									
1743	RS	1	FLOW								
1744	RC	.035	.035	.035	1950	.025					
1745	RX	0	8	13	17	22	26	31	39		
1746	RY	4	2	2	0	0	2	2	4		
	*										

LINE	ID	1	2	3	4	5	6	7	8	9	10
1747	KK	SUB15N									
1748	KM	RUNOFF FROM SUBBASIN 15N.									
1749	BA	.0391									
1750	LS		77	68							
1751	UK	100	.01	.15	100						
1752	RK	400	.008	.018		TRAP	50	20			
1753	RK	1700	.015	.025		TRAP	10	4			
	*										
1754	KK	CP15N									
1755	KM	ADD HYDROGRAPHS AT CP15N									
1756	HC	2									
	*										
1757	KK	R15N2									
1758	KM	ROUTE FLOW FROM CP15N TO CP15N1.									
1759	RS	1	FLOW								
1760	RC	.02	.02	.02	700	.013					
1761	RX	0	8	13	17	22	26	31	39		
1762	RY	6	2	2	0	0	2	2	6		
	*										
1763	KK	CP15N2									
1764	KM	ADD HYDROGRAPHS AT CP15N1									
1765	KM	THIS IS THE INTERIM OUTFLOW DISCHARGE TO NATURAL WASH.									
1766	HC	2	1.1611								
	*										
1767	KK	R15N2									
1768	KM	ROUTE 15N2 IS ADDED BY GVSCE TO ROUTE THE HYDROGRAPH FROM CP15N2 TO THE									
1769	KM	POWER LINE CHANNEL CROSSING AT HAYDEN RD.									
1770	KM										
1771	KM	ROUTE FLOW FROM CP15N2 TO CPC3A.									
1772	RS	1	FLOW								
1773	RC	.035	.035	.035	2200	.013					
1774	RX	0	16	26	34	64	78	88	106		
1775	RY	6	2	2	0	0	2	2	6		
	*										
1776	KK	DPC3									
1777	KM	THIS OPERATION IS ADDED BY GVSCE IN ORDER TO ROUTE RUNOFF TO THE									
1778	KM	UNION HILLS DETENTION BASIN VIA THE POWER LINE CHANNEL.									
1779	KM										
1780	KM	RETRIEVE DIVERTED FLOW									
1781	DR	BPC3T									
	*										
1782	KK	CPC3A									
1783	KM	COMBINE CPC3A IS ADDED BY GVSCE TO ESTIMATE THE TOTAL DISCHARGE AT THE									
1784	KM	POWER LINE CHANNEL CROSSING AT HAYDEN RD.									
1785	KM										
1786	KM	COMBINE ROUTED HYDROGRAPH FROM CP15N2 WITH HYDROGRAPH FROM CPC3									
1787	HC	2	1.3446								
	*										

LINE	ID	1	2	3	4	5	6	7	8	9	10
1788	KK	RPC3A									
1789	KM	ROUTE PC3A IS ADDED BY GVSCE TO ROUTE THE HYDROGRAPH FROM CPC3A VIA									
1790	KM	THE POWER LINE CHANNEL.									
1791	KM										
1792	KM	ROUTE FLOW FROM CP15N2 TO CPC3A.									
1793	RS	1	FLOW								
1794	RC	.035	.035	.035	1100	.013					
1795	RX	0	16	26	34	64	78	88	106		
1796	RY	6	2	2	0	0	2	2	6		
	*										
1797	KK	DPC4									
1798	KM	THIS OPERATION IS ADDED BY GVSCE IN ORDER TO ROUTE RUNOFF TO THE									
1799	KM	UNION HILLS DETENTION BASIN VIA THE POWER LINE CHANNEL.									
1800	KM										
1801	KM	RETRIEVE DIVERTED FLOW									
1802	DR	BPC4T									
	*										
1803	KK	CPC4A									
1804	KM	COMBINE CPC4A IS ADDED BY GVSCE TO ESTIMATE THE TOTAL DISCHARGE IN THE									
1805	KM	POWER LINE CHANNEL									
1806	KM										
1807	KM	COMBINE ROUTED HYDROGRAPH FROM CPC3A WITH HYDROGRAPH FROM CPC4									
1808	HC	2	1.9946								
	*										
1809	KK	RPC4A									
1810	KM	ROUTE PC4A IS ADDED BY GVSCE TO ROUTE THE HYDROGRAPH FROM CPC4A TO THE									
1811	KM	POWER LINE CHANNEL CROSSING AT HUALAPAI RD.									
1812	KM										
1813	KM	ROUTE FLOW FROM CPC4A TO CPC5.									
1814	RS	1	FLOW								
1815	RC	.035	.035	.035	1900	.013					
1816	RX	0	16	26	34	64	78	88	106		
1817	RY	6	2	2	0	0	2	2	6		
	*										
1818	KK	DPC4AT									
1819	KM	DIVERT PC4A IS ADDED BY GVSCE IN ORDER TO ROUTE RUNOFF TO THE UNION									
1820	KM	HILLS DETENTION BASIN VIAL THE POWER LINE CHANNEL.									
1821	KM										
1822	KM	DIVERT 100% OF FLOW									
1823	DT	BPC4AT									
1824	DI	0	10000								
1825	DQ	0	10000								
	*										
1826	KK	SUB1-2									
1827	KM	RUNOFF FROM SUB 1 AND 2, SOUTH COURSE MODEL									
1828	BA	.0558									
1829	LS		77	68							
1830	UK	200	.010	.15	100						
1831	RK	1370	.027	.015		TRAP	50	20			



LINE	ID	1	2	3	4	5	6	7	8	9	10	
1872	KK	SUB7S										
1873	KM	RUNOFF FROM SUB BASIN 7, SOUTH COURSE										
1874	BA	.027										
1875	LS		77	42								
1876	UK	100	.010	.15	100							
1877	RK	2080	.023	.025		TRAP	50	20				
	*											
1878	KK	CPRET2										
1879	KM	COMBINE HYDROGRAPHS AT RETENTION BASIN 2, SOUTH COURSE										
1880	HC	5										
	*											
1881	KK	SRRET2										
1882	KM	STORAGE THRU RETENTION BASIN NO. 2, SOUTH COURSE										
1883	RS	1	STOR	0	0							
1884	SV	0	.617	3.474	9.858	20.063	35.353	52.685	57.749	62		
1885	SE	1670	1675	1680	1685	1690	1695	1699	1700	1701		
1886	SQ	0	0	0	0	0	0	32	386	594		
	*											
	*	NO FLOW RELEASED FROM RETENTION BASIN										
	*											
1887	KK	CLEAR										
1888	KM	THIS OPERATION IS ADDED BY GVSCE										
1889	KM											
1890	KM	CLEAR HYDROGRAPHS FROM THE STACK										
1891	HC	4										
	*											
1892	KK	SUB8S										
1893	KM	RUNOFF FROM SUB BASIN 8, SOUTH COURSE										
1894	BA	.0256										
1895	LS		77	42								
1896	UK	100	.010	.15	100							
1897	RK	1600	.015	.025		TRAP	50	20				
	*											
1898	KK	RGC36										
1899	KM	ROUTE SUB8S TO CPGC36										
1900	RS	1	FLOW									
1901	RC	.055	.045	.055	850	.02						
1902	RX	0	16	26	30	40	44	54	70			
1903	RY	6	2	2	0	0	2	2	6			
	*											
1904	KK	GC36										
1905	KM	RUNOFF FROM SOUTH COURSE HOLES 3, 6, AND NORTH HALF OF HOLE 4.										
1906	BA	.0406										
1907	LS		81	0								
1908	UK	200	.025	.15	100							
1909	RK	2350	.015	.035		TRAP	10	4				
	*											

LINE	ID	1	2	3	4	5	6	7	8	9	10
1910	KK	C1GC36									
1911	KM	COMBINE SUBS 8 AND GC36									
1912	HC	2									
	*										
1913	KK	SUB9S									
1914	KM	RUNOFF FROM SUB BASIN 9, SOUTH COURSE									
1915	BA	.021									
1916	LS		77	53							
1917	UK	100	.010	.15	100						
1918	RK	1100	.013	.025		TRAP	50	20			
	*										
1919	KK	R9S									
1920	KM	ROUTE SUB9S TO CPGC36									
1921	RS	1	FLOW								
1922	RC	.035	.035	.035	500	.02					
1923	RX	0	8	12	16	18	22	26	30		
1924	RY	6	4	3	2	2	3	4	6		
	*										
1925	KK	CPGC36									
1926	KM	COMBINE SUBS 8 AND 9 SOUTH AND GC36									
1927	HC	2									
	*										
1928	KK	SRGC36									
1929	KM	STORAGE THRU DETENTION BASIN ON GC36									
1930	RS	1	STOR	0	0						
1931	SV	0	0.85	1.0							
1932	SE	1664	1668	1669							
1933	SQ	0	20	150							
	*										
1934	KK	SUB7A									
1935	KM	RUNOFF FROM SUB7A, SOUTH COURSE EAST SIDE ADJACENT TO PIMA ROAD									
1936	BA	.0092									
1937	LS		77	42							
1938	UK	100	.025	.15	100						
1939	RK	950	.015	.025		TRAP	50	20			
	*										
1940	KK	SR7A									
1941	KM	STORAGE THRU DETENTION BASIN ON SUB7A									
1942	RS	1	STOR	0	0						
1943	SV	0	.68	.8							
1944	SE	1700	1703	1704							
1945	SQ	0	10	150							
	*										

LINE	ID	1	2	3	4	5	6	7	8	9	10
1946	KK	R10S									
1947	KM	ROUTE FLOW FROM CP7A TO CP10S									
1948	RS	1	FLOW								
1949	RC	.035	.035	.035	1400	.015					
1950	RX	0	8	12	16	18	22	26	30		
1951	RY	6	4	3	2	2	3	4	6		
	*										
1952	KK	SUB10S									
1953	KM	RUNOFF FROM SUB BASIN 10, SOUTH COURSE									
1954	BA	.0248									
1955	LS		77	53							
1956	UK	100	.010	.15	100						
1957	RK	1150	.020	.025		TRAP	50	20			
	*										
1958	KK	CP10S									
1959	KM	COMBINE HYDROGRAPHS AT CP10 SOUTH COURSE									
1960	HC	2									
	*										
1961	KK	SUB11S									
1962	KM	RUNOFF FROM SUB11, SOUTH COURSE									
1963	BA	.0234									
1964	LS		77	68							
1965	UK	100	.015	.018	100						
1966	RK	1050	.015	.025		TRAP	100	20			
	*										
1967	KK	R11S									
1968	KM	ROUTE 11S IS ADDED BY GVSCE TO ROUTE THE RUNOFF FROM SUB11S TO THE									
1969	KM	POWER LINE CHANNEL CROSSING AT HUALAPAI DR ALONG HUALAPAI DR.									
1970	KM										
1971	KM	ROUTE FLOW FROM SUB11S TO CPC5.									
1972	RS	1	FLOW								
1973	RC	.035	.035	.035	900	.015					
1974	RX	0	8	12	16	18	22	26	30		
1975	RY	6	4	3	2	2	3	4	6		
	*										
1976	KK	C10SA									
1977	KM	COMBINE 10SA IS ADDED BY GVSCE									
1978	KM										
1979	KM	COMBINE ROUTED HYDROGRAPH FROM 11S WITH HYDROGRAPH FROM CP10S									
1980	HC	2									
	*										
1981	KK	R10SA									
1982	KM	ROUTE 10SA IS ADDED BY GVSCE IN ORDER TO ROUTE RUNOFF TO THE UNION									
1983	KM	HILLS DETENTION BASIN VIA THE POWER LINE CHANNEL.									
1984	KM										
1985	KM	ROUTE FLOW FROM C10SAS TO CPC5.									
1986	RS	1	FLOW								
1987	RC	.035	.035	.035	900	.015					



LINE	ID	1	2	3	4	5	6	7	8	9	10
2027	KK	SCN5C									
2028	KM	RUNOFF FROM SUBBASIN CN5C									
2029	BA	0.2667									
2030	LS		74		20						
2031	UK	240	0.021	0.13	100						
2032	RK	1200	0.018	0.045	0.0067	TRAP	0	45			
2033	RK	5600	0.009	0.040		TRAP	15	3			
	*										
2034	KK	SCN6									
2035	KM	RUNOFF FROM SUBBASIN CN6A									
2036	BA	0.2597									
2037	LS		74		85						
2038	UK	180	0.019	0.13	100						
2039	RK	1075	0.019	0.045	0.0066	TRAP	5	7			
2040	RK	4430	0.013	0.040		TRAP	8	50			
	*										
2041	KK	D52									
2042	KM	BRING BACK DIVERTED HYDROGRAPH FROM R52									
2043	DR	B52T									
	*										
2044	KK	S53A									
2045	KM	RUNOFF FROM SUBBASIN 53A									
2046	BA	0.1692									
2047	LS		74		11						
2048	UK	300	0.022	0.13	100						
2049	RK	1475	0.026	0.045	0.0111	TRAP	3	5			
2050	RK	2700	0.021	0.04		TRAP	25	5			
	*										
2051	KK	C53									
2052	KM	COMBINE ROUTED HYDROGRAPH FROM									
2053	HC	2	8.0852								
	*										
2054	KK	R53									
2055	KM	NORMAL DEPTH CHANNEL ROUTE FROM C53 TO C53A THROUGH PIMA CHANNEL									
2056	RS	1	FLOW	-1							
2057	RC	0.035	0.025	0.035	2360	0.01					
2058	RX	1000	1020	1022	1034	1084	1096	1098	1118		
2059	RY	111.4	106.4	106.3	100	100	106.3	106.4	111.4		
	*										
2060	KK	S53A1									
2061	KM	RUNOFF FROM SUBBASIN 53A1									
2062	BA	0.3384									
2063	LS		74		12		74	30			
2064	UK	300	0.022	0.13	70						
2065	UK	150	0.027	0.13	30						
2066	RK	1250	0.023	0.045	0.0087	TRAP	4	5			
2067	RK	5650	0.017	0.04		TRAP	35	5			
	*										

LINE	ID	1	2	3	4	5	6	7	8	9	10	
2068	KK	C53A										
2069	KM	COMBINE ROUTED HYDROGRAPH FROM										
2070	HC	2	8.4236									
	*											
2071	KK	C1I										
2072	KM	COMBINE ROUTED HYDROGRAPH FROM										
2073	HC	4										
	*											
2074	KK	C10										
2075	KM	DETENTION BASIN AT UNION HILLS ROAD - NONREGULATORY STRUCTURE										
2076	KM	OUTLET RATING CURVE - USING HY8 FOR A 78" RCP WITH A SLOPE OF 0.9%										
2077	KM	7-ACRE-FEET OF STORAGE FOR SEDIMENTATION										
2078	RS	1	STOR									
2079	SV	0	0.36	0.82	1.42	2.23	3.01	37.59	123.30	222.97	337.88	
2080	SV	362.56	387.54									
2081	SE	1590	1591	1592	1593	1594	1595	1600	1605	1610	1615	
2082	SE	1616	1617									
2083	SQ	0	65	130	195	260	325	390	420	520	585	
2084	SQ	650	690	828	966	1104	1242	1382				
2085	SE	1590.0	1592.80	1594.36	1595.60	1596.80	1598.16	1599.79	1600.64	1604.03	1606.65	
2086	SE	1615.0	1615.28	1615.72	1616.04	1616.26	1616.40	1616.50				
	*											
2087	KK	RC1										
2088	KM	NORMAL DEPTH CHANNEL ROUTE FROM C1I TO CIA										
2089	RS	1	FLOW	-1								
2090	RC	0.025	0.025	0.025	2300	0.013						
2091	RX	1000	1008	1012	1016	1026	1030	1034	1042			
2092	RY	104	102	101	100	100	101	102	104			
	*											
2093	KK	S54										
2094	KM	RUNOFF FROM SUBBASIN 54										
2095	BA	0.0853										
2096	LS		74	22								
2097	UK	300	0.017	0.13	100							
2098	RK	3460	0.012	0.040		TRAP	5	2				
	*											
2099	KK	SCN6A										
2100	KM	RUNOFF FROM SUBBASIN CN6A										
2101	BA	0.1335										
2102	LS		74	20								
2103	UK	300	0.017	0.13	100							
2104	RK	1050	0.017	0.045	0.0057	TRAP	8	20				
2105	RK	2250	0.012	0.040		TRAP	10	4				
	*											

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

2106	KK	C1A
2107	KM	COMBINE ROUTED HYDROGRAPH FROM C10 WITH RUNOFF FROM SCN6A
2108	HC	3
	*	
2109	ZZ	

SCHEMATIC DIAGRAM OF STREAM NETWORK

INPUT  
 LINE (V) ROUTING (--->) DIVERSION OR PUMP FLOW  
 NO. (.) CONNECTOR (<---) RETURN OF DIVERTED OR PUMPED FLOW

26	✓ S30N	
	V	
	V	
35	R30N	
	.	
41	.	✓ S31.1
	.	
49	✓ C31.1.....	
	V	
	V	
52	✓ R31.1	
	.	
58	.	✓ S35N
	.	
68	.	✓ -----> D35NL
66	D35NR	
	V	
	V	
71	✓ R35NR	
	.	
78	.	✓ S36.2
	.	
86	✓ C36.2.....	
	.	
92	✓ -----> D36.2L	
90	D36.2R	
	V	
	V	
95	✓ R36.2R	
	.	
102	.	✓ S34.1
	.	
111	✓ C34.1I.....	
	V	
	V	
115	✓ C34.10	
	V	
	V	
128	✓ R34.1	
	.	
134	.	✓ S36.1
	.	

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141 ✓ C36.1.....
      V
      V
144 ✓ R36.1
      .
      .
152 ✓ .<----- D35NL
150 ✓ . B35NL
      ✓ V
      V
153 ✓ . R35NL
      .
      .
162 ✓ .<----- D36.2L
160 ✓ . B36.2L
      ✓ V
      V
163 ✓ . R36.2L
      .
      .
170 ✓ . S36R1
      .
      .
178 ✓ C36R1.....
      V
      V
183 ✓ R36R1
      .
      .
189 ✓ S36R2
      .
      .
196 ✓ C36R2.....
      .
      .
199 ✓ S51.1
      .
      .
207 ✓ C51.1I.....
      V
      V
210 C51.10
      V
      V
223 R51.1
      .
      .
231 ✓ -----> B51.1T
229 D51.1T
      .
      .
234 ✓ 52D4
      ✓ V
      V
240 ✓ 52D4R
      .
      .
243 ✓ 52D4B
      .
      .

```

*option 1*

249	.	.	.
	.	52D5C1.....	
	.	.	
252	.	.	52D5A
	.	.	V
	.	.	V
258	.	.	52D5AR
	.	.	.
261	.	52D5C2.....	
	.	V	
	.	V	
264	.	52D5R	
	.	.	
267	.	.	52C3
	.	.	V
	.	.	V
273	.	.	52C3R
	.	.	.
276	.	.	52C3B
	.	.	.
282	.	.	2C3BC1.....
	.	.	.
285	.	2C3BC2.....	
	.	V	
	.	V	
288	.	52C3BR	
	.	.	
291	.	.	51C
	.	.	.
299	.	.	-----> 51C1DV
297	.	.	51C1D
	.	.	V
	.	.	V
302	.	.	51C1R
	.	.	.
305	.	.	52C1
	.	.	.
311	.	.	52C1C.....
	.	.	V
	.	.	V
314	.	.	52C1R
	.	.	.
317	.	.	52C2A
	.	.	.
323	.	.	52C2AC.....
	.	.	.
326	.	.	52C2B

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332 . . . . . 52C2BC.....
. . . . . V
. . . . . V
335 . . . . . 52C2BR
. . . . .
. . . . .
338 . . . . . 52C2C
. . . . .
. . . . .
344 . . . . . 52C2CC.....
. . . . . V
. . . . . V
347 . . . . . 52C2R
. . . . .
. . . . .
350 . . . . . 52C4
. . . . .
. . . . .
356 . . . . . 52C4C1.....
. . . . .
. . . . .
359 . . . . . 52C4C2.....
. . . . . V
. . . . . V
362 . . . . . 52C4R
. . . . .
. . . . .
365 . . . . . 52C13
. . . . .
. . . . .
373 . . . . . -----> STORM
371 . . . . . 2C13DV
. . . . .
. . . . .
376 . . . . . 52C15
. . . . .
. . . . .
382 . . . . . 2C15C1.....
. . . . .
. . . . .
385 . . . . . 2C15C2.....
. . . . . V
. . . . . V
388 . . . . . 52C15R
. . . . .
. . . . .
391 . . . . . 52C14A
. . . . .
. . . . .
397 . . . . . 2C14AC.....
. . . . . V
. . . . . V
400 . . . . . 2C14AR
. . . . .
. . . . .
405 . . . . . <----- 51C1DV
403 . . . . . 51C1DV
.
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408 . . . . . -----> 51C2DV
406 . . . . . 51C2D
      . . . . . V
      . . . . . V
411 . . . . . 51C2R
      . . . . .
      . . . . .
414 . . . . . 52C5
      . . . . .
      . . . . .
420 . . . . . 52C5C.....
      . . . . . V
      . . . . . V
423 . . . . . 52C5R
      . . . . .
      . . . . .
426 . . . . . 52C6
      . . . . .
      . . . . .
432 . . . . . 52C6C.....
      . . . . . V
      . . . . . V
435 . . . . . 52C6R
      . . . . .
      . . . . .
440 . . . . . <----- 51C2DV
438 . . . . . 51C2DV
      . . . . . V
      . . . . . V
441 . . . . . 51C3R
      . . . . .
      . . . . .
444 . . . . . 51B
      . . . . .
      . . . . .
452 . . . . . -----> 51B1DV
450 . . . . . 51B1D
      . . . . . V
      . . . . . V
455 . . . . . 51B1R
      . . . . .
      . . . . .
458 . . . . . 52C7
      . . . . .
      . . . . .
464 . . . . . 52C7C.....
      . . . . . V
      . . . . . V
467 . . . . . 52C7R
      . . . . .
      . . . . .
472 . . . . . <----- 51B1DV
470 . . . . . 51B1DV
      . . . . .
      . . . . .
475 . . . . . -----> 51B2DV
473 . . . . . 51B2D
      . . . . . V
      . . . . . V

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478	.	.	.	.	51B2R	.
	.	.	.	.	.	.
481	.	.	.	.	.	52C8
	.	.	.	.	.	.
487	.	.	.	.	52C8C.....	.
	.	.	.	.	V	.
	.	.	.	.	V	.
490	.	.	.	.	52C8R	.
	.	.	.	.	.	.
493	.	.	.	.	52C9C1.....	.
	.	.	.	.	V	.
	.	.	.	.	V	.
496	.	.	.	.	52C9R1	.
	.	.	.	.	.	.
499	.	.	.	.	.	52C9
	.	.	.	.	.	.
505	.	.	.	.	52C9C2.....	.
	.	.	.	.	V	.
	.	.	.	.	V	.
508	.	.	.	.	52C9R2	.
	.	.	.	.	.	.
511	.	.	.	.	2C10C1.....	.
	.	.	.	.	V	.
	.	.	.	.	V	.
514	.	.	.	.	2C10R1	.
	.	.	.	.	.	.
517	.	.	.	.	.	52C10
	.	.	.	.	.	.
523	.	.	.	.	2C10C2.....	.
	.	.	.	.	.	.
526	.	.	.	.	.	52C11
	.	.	.	.	.	V
	.	.	.	.	.	V
532	.	.	.	.	2C11R1	.
	.	.	.	.	.	.
537	.	.	.	.	.	.
535	.	.	.	.	.	←----- STORM
	.	.	.	.	52C13D	.
	.	.	.	.	.	.
538	.	.	.	.	52C11C.....	.
	.	.	.	.	V	.
	.	.	.	.	V	.
541	.	.	.	.	2C11CR	.
	.	.	.	.	.	.
544	.	.	.	.	2C11C2.....	.
	.	.	.	.	V	.
	.	.	.	.	V	.
547	.	.	.	.	2C11R2	.
	.	.	.	.	.	.

550	.	.	.	52C12
	.	.	.	.
556	.	.	52C12C.....	.
	.	.	V	.
	.	.	V	.
559	.	.	52C12R	.
	.	.	.	.
562	.	.	.	52C14B
	.	.	.	.
568	.	.	C14BC1.....	.
	.	.	.	.
571	.	C14BC2.....	.	.
	.	V	.	.
	.	V	.	.
574	.	52C14R	.	.
	.	.	.	.
579	.	.	.<-----	51B2DV
577	.	51B2DV	.	.
	.	.	.	.
582	.	.	.----->	51B3DV
580	.	51B3D	.	.
	.	V	.	.
	.	V	.	.
585	.	51B3R	.	.
	.	.	.	.
588	.	.	.	52B1
	.	.	.	.
594	.	52B1C.....	.	.
	.	V	.	.
	.	V	.	.
597	.	52B1R	.	.
	.	.	.	.
602	.	.	.<-----	51B3DV
600	.	51B3DV	.	.
	.	.	.	.
605	.	.	.----->	51B4DV
603	.	51B4D	.	.
	.	V	.	.
	.	V	.	.
608	.	51B4R1	.	.
	.	.	.	.
611	.	52B2C1.....	.	.
	.	V	.	.
	.	V	.	.
614	.	52B2R1	.	.
	.	.	.	.
617	.	.	.	52B2

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623 . . . . . 52B2C2.....
. . . . . V
. . . . . V
626 . . . . . 52B2R2
. . . . . V
. . . . . V
629 . . . . . 52B3R1
. . . . .
. . . . .
632 . . . . . 52B3
. . . . .
. . . . .
638 . . . . . 52B3C2.....
. . . . . V
. . . . . V
641 . . . . . 52B3R2
. . . . .
. . . . .
644 . . . . . 52B4
. . . . .
. . . . .
650 . . . . . 52B4C.....
. . . . . V
. . . . . V
653 . . . . . 52B4R
. . . . .
. . . . .
656 . . . . . 52B5
. . . . .
. . . . .
662 . . . . . 52B5C1.....
. . . . .
. . . . .
665 . . . . . 52B5C2.....
. . . . . V
. . . . . V
668 . . . . . 52B5R
. . . . .
. . . . .
673 . . . . . .<----- 51B4DV
671 . . . . . 51B4DV
. . . . .
. . . . .
676 . . . . . .-----> 51B5DV
674 . . . . . 51B5D
. . . . . V
. . . . . V
679 . . . . . 51B5R
. . . . .
. . . . .
684 . . . . . .<----- 51B5DV
682 . . . . . 51B5DV
. . . . .
. . . . .
687 . . . . . .-----> 51B6DV
685 . . . . . 51B6D
. . . . . V
. . . . . V

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690	.	.	.	51B6R	
	.	.	.	.	
695	.	.	.	.	.<----- 51B6DV
693	.	.	.	51B6DV	
	.	.	.	.	
698	.	.	.	.	.-----> 51B7DV
696	.	.	.	51B7D	
	.	.	.	V	
	.	.	.	V	
701	.	.	.	51B7R1	
	.	.	.	.	
704	.	.	.	51B7C.....	
	.	.	.	V	
	.	.	.	V	
707	.	.	.	51B7R2	
	.	.	.	.	
710	.	.	.	52B6	
	.	.	.	.	
716	.	.	.	52B6C.....	
	.	.	.	V	
	.	.	.	V	
719	.	.	.	52B6R	
	.	.	.	.	
722	.	.	.	52B7	
	.	.	.	.	
728	.	.	.	52B7C1.....	
	.	.	.	.	
731	.	.	.	52B7C2.....	
	.	.	.	.	
734	.	.	.	52A2	
	.	.	.	.	
740	.	.	.	52A2C2.....	
	.	.	.	.	
745	.	.	.	.	.<----- 51B7DV
743	.	.	.	51B7DV	
	.	.	.	V	
	.	.	.	V	
746	.	.	.	51B8R	
	.	.	.	.	
749	.	.	.	52A1	
	.	.	.	.	
755	.	.	.	52A1C.....	
	.	.	.	.	
760	.	.	.	.	.<----- B51.1T
758	.	.	.	D51.1	
	.	.	.	.	

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761 . . . C52A.....
. . . V
. . . V
765 . . . R52A
. . .
. . .
771 . . . C52.....
. . . V
. . . V
775 . . . R52
. . .
. . .
783 . . . -----> B52T
781 . . . D52T
. . .
. . .
786 CLEAR.....
. . .
. . .
789 . . . 37A
. . .
. . .
806 . . . -----> 37AW
795 . . . 37AE
. . . V
. . . V
809 . . . 37AE1
. . .
. . .
816 . . . SUB5N
. . .
. . .
823 . . . CP5N.....
. . . V
. . . V
826 . . . RET5N
. . . V
. . . V
833 . . . R6N.1
. . .
. . .
841 . . . SUB6B
. . . V
. . . V
847 . . . SR6B
. . .
. . .
853 . . . CP6.1.....
. . .
. . .
856 . . . SUB1N
. . . V
. . . V
862 . . . R2NA
. . .
. . .
868 . . . SUB2NA
. . .
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874	.	.	CP2NA.....	
	.	.	V	
	.	.	V	
877	.	.	SR2NA	
	.	.	V	
	.	.	V	
883	.	.	R2NB	
	.	.	.	
	.	.	.	
889	.	.	.	SUB2NB
	.	.	.	.
	.	.	.	.
895	.	.	CP2NB.....	
	.	.	V	
	.	.	V	
898	.	.	SR2NB	
	.	.	V	
	.	.	V	
904	.	.	RCP4N	
	.	.	.	
	.	.	.	
910	.	.	.	SUB6N
	.	.	.	V
	.	.	.	V
916	.	.	.	RET6N
	.	.	.	V
	.	.	.	V
922	.	.	.	RCP4N1
	.	.	.	.
	.	.	.	.
928	.	.	CP4N.1.....	
	.	.	.	
	.	.	.	
931	.	.	.	SUB3N
	.	.	.	V
	.	.	.	V
937	.	.	.	RET3N
	.	.	.	V
	.	.	.	V
944	.	.	.	R4N
	.	.	.	.
	.	.	.	.
950	.	.	CP4N.2.....	
	.	.	.	
	.	.	.	
953	.	.	.	SUB4N
	.	.	.	.
	.	.	.	.
959	.	.	CP4N.....	
	.	.	V	
	.	.	V	
962	.	.	R6N	
	.	.	.	
	.	.	.	
968	.	.	.	SUB6A
	.	.	.	.
	.	.	.	.
974	.	.	CP6.2.....	
	.	.	.	
	.	.	.	

977	.	CP6N.....		
	.	V		
	.	V		
980	.	RCP6N		
	.	.		
986	.	.	SUB3C	
	.	.	.	
992	.	CP3C.....		
	.	V		
	.	V		
995	.	R3C		
	.	.		
1003	.	.	GC1018	
	.	.	.	
1009	.	.	.	GC1-9
	.	.	.	.
1015	.	.	.	SUB3S
	.	.	.	.
1021	.	CP3S.....		
	.	V		
	.	V		
1024	.	RT3S		
	.	.		
1030	.	.	SUB4S	
	.	.	V	
	.	.	V	
1036	.	.	RT4S	
	.	.	.	
1042	.	.	.	GC2-8
	.	.	.	.
1048	.	1PGC28.....		
	.	.		
1051	.	.	SUB3D3	
	.	.	.	
1057	.	CPGC28.....		
	.	V		
	.	V		
1060	.	SRGC28		
	.	V		
	.	V		
1066	.	RT7S		
	.	.		
1072	.	.	GC7	
	.	.	.	
1078	.	CP7S.....		
	.	.		

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1086 . . . . . -----> B7ST
1081 . . . . . D7ST
. . . . .
1089 CLEAR.....
. . . . .
1092 . . . . . SUB3D1
. . . . . V
. . . . . V
1097 . . . . . RD1B1
. . . . .
. . . . .
1103 . . . . . SUB3B1
. . . . .
. . . . .
1108 . . . . . CP3B1.....
. . . . . V
. . . . . V
1111 . . . . . RB13F
. . . . .
. . . . .
1117 . . . . . SUB3F
. . . . .
. . . . .
1123 . . . . . CP3F.....
. . . . .
. . . . .
1126 . . . . . SUB3B2
. . . . . V
. . . . . V
1131 . . . . . RB2E1
. . . . . V
. . . . . V
1137 . . . . . RB2E2
. . . . .
. . . . .
1143 . . . . . SUB3E1
. . . . .
. . . . .
1148 . . . . . 1CPE31.....
. . . . .
. . . . .
1151 . . . . . SUB3D2
. . . . . V
. . . . . V
1156 . . . . . RD2E2
. . . . .
. . . . .
1162 . . . . . SUB3E2
. . . . .
. . . . .
1167 . . . . . CP3E2.....
. . . . .
. . . . .
1170 . . . . . PC3
. . . . .
. . . . .
1179 . . . . . CPC3.....
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1302	.	.	.	SUB19N
	.	.	.	.
1308	.	.	CP19N.....	.
	.	.	V	.
	.	.	V	.
1311	.	.	R18NC	.
	.	.	.	.
1317	.	.	.	UB18NC
	.	.	.	.
1323	.	CP18NC.....	.	.
	.	V	.	.
	.	V	.	.
1326	.	RPC1	.	.
	.	.	.	.
1332	.	.	UB18NA	.
	.	.	V	.
	.	.	V	.
1338	.	.	1RPC1	.
	.	.	.	.
1344	.	.	.	UB18NB
	.	.	.	V
	.	.	.	V
1350	.	.	.	2RPC1
	.	.	.	.
1356	.	.	.	PC1
	.	.	.	.
1362	.	.	1CPC1.....	.
	.	.	V	.
	.	.	V	.
1365	.	.	SRPC1	.
	.	.	.	.
1371	.	CPC1.....	.	.
	.	V	.	.
	.	V	.	.
1374	.	R16NA1	.	.
	.	.	.	.
1380	.	.	UB16NA	.
	.	.	V	.
	.	.	V	.
1386	.	.	R16NA1	.
	.	.	.	.
1392	.	C16NA1.....	.	.
	.	V	.	.
	.	V	.	.
1395	.	R16NB1	.	.
	.	.	.	.
1401	.	.	UB16NB	.

	.	.	V	
	.	.	V	
1407	.	.	R16NB1	
	.	.	.	
	.	.	.	
1413	.	C16NB1.....		
	.	.	V	
	.	.	V	
1416	.	.	R16NC1	
	.	.	.	
	.	.	.	
1422	.	.	SUB7N	
	.	.	V	
	.	.	V	
1428	.	.	R8NC	
	.	.	.	
	.	.	.	
1434	.	.	SUB8NA	
	.	.	V	
	.	.	V	
1440	.	.	SR8NA	
	.	.	V	
	.	.	V	
1446	.	.	R8NB	
	.	.	.	
	.	.	.	
1452	.	.	.	SUB8NB
	.	.	.	.
	.	.	.	.
1458	.	.	CP8NB.....	
	.	.	V	
	.	.	V	
1461	.	.	SR8NB	
	.	.	V	
	.	.	V	
1467	.	.	R8NC	
	.	.	.	
	.	.	.	
1473	.	.	.	SUB8NC
	.	.	.	.
	.	.	.	.
1479	.	.	CP8NC.....	
	.	.	V	
	.	.	V	
1482	.	.	SR8NC	
	.	.	V	
	.	.	V	
1488	.	.	R9N	
	.	.	.	
	.	.	.	
1494	.	.	.	SUB9N
	.	.	.	.
	.	.	.	.
1500	.	.	CP9N.....	
	.	.	V	
	.	.	V	
1503	.	.	R10B	
	.	.	.	
	.	.	.	
1509	.	.	.	SUB10B

1516	.	.	CP10B.....	.	.
	.	.	V	.	.
	.	.	V	.	.
1519	.	.	R11NA	.	.
	.	.	.	.	.
1525	.	.	.	UB11NA	.
	.	.	.	.	.
1531	.	.	CP11NA.....	.	.
	.	.	V	.	.
	.	.	V	.	.
1534	.	.	SR11NA	.	.
	.	.	V	.	.
	.	.	V	.	.
1540	.	.	R11NB	.	.
	.	.	.	.	.
1546	.	.	.	UB11NB	.
	.	.	.	.	.
1552	.	.	CP11NB.....	.	.
	.	.	V	.	.
	.	.	V	.	.
1555	.	.	SR11NB	.	.
	.	.	V	.	.
	.	.	V	.	.
1561	.	.	R11NC	.	.
	.	.	.	.	.
1567	.	.	.	UB11NC	.
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1573	.	.	C11NC1.....	.	.
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1576	.	.	.	SUB10A	.
	.	.	.	V	.
	.	.	.	V	.
1583	.	.	.	R12NB	.
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1589	.	.	.	UB12NA	.
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1595	.	.	.	SR12NA	.
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	.	.	.	V	.
1601	.	.	.	R12NA	.
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1607	.	.	.	.	UB12NB
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1613	.	.	CP12NB.....	.	.
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	.	.	V	.	.
1616	.	.	SR12NB	.	.

	.	.	.	V
	.	.	.	V
1622	.	.	.	R11NC2
	.	.	.	.
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1628	.	.	CP11NC.....	
	.	.	V	
	.	.	V	
1631	.	.	SR11NC	
	.	.	V	
	.	.	V	
1638	.	.	R16NC	
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	.	.	.	
1644	.	.	.	UB16NC
	.	.	.	.
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1650	.	.	CP16NC.....	
	.	.	V	
	.	.	V	
1653	.	.	R16NC1	
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1659	.	.	C16NC1.....	
	.	.	V	
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1662	.	.	R15N1	
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1668	.	.	PC2	
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1674	.	.	CP15N1.....	
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1677	.	.	SRPC2	
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1684	.	.	UB17NA	
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1690	.	.	SR17NA	
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1696	.	.	R17NB	
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1702	.	.	.	UB17NB
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1708	.	.	CP17NB.....	
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1711	.	.	SR17NB	
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1717	.	.	R17A	
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1723	.	.	.	SUB17A

1729	.	.	.	.	CP17A1.....
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1732	.	.	.	.	UB17NC
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1738	.	.	.	.	CP17A.....
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1741	.	.	.	.	R15N
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1747	.	.	.	.	SUB15N
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1754	.	.	.	.	CP15N.....
	.	.	.	.	V
	.	.	.	.	V
1757	.	.	.	.	R15N2
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1763	.	.	.	.	CP15N2.....
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1767	.	.	.	.	R15N2
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1781	.	.	.	.	.<----- BPC3T
1776	.	.	.	.	DPC3
	.	.	.	.	
1782	.	.	.	.	CPC3A.....
	.	.	.	.	V
	.	.	.	.	V
1788	.	.	.	.	RPC3A
	.	.	.	.	
1802	.	.	.	.	.<----- BPC4T
1797	.	.	.	.	DPC4
	.	.	.	.	
1803	.	.	.	.	CPC4A.....
	.	.	.	.	V
	.	.	.	.	V
1809	.	.	.	.	RPC4A
	.	.	.	.	
1823	.	.	.	.	-----> BPC4AT
1818	.	.	.	.	DPC4AT
	.	.	.	.	
1826	.	.	.	.	SUB1-2
	.	.	.	.	
1832	.	.	.	.	GCRB18
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1839	.	.	.	.	CPRET1.....

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1842	.	.	SR18S		
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1848	.	.	.	SUB5S	
	.	.	.	.	
1854	.	.	.	GC1216	
	.	.	.	.	
1860	.	.	.	GC1415	
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1866	.	.	.	.	SUB6S
	.	.	.	.	.
1872	.	.	.	.	SUB7S
	.	.	.	.	.
1878	.	.	.	CPRET2	.....
	.	.	.	V	
	.	.	.	V	
1881	.	.	.	SRRET2	
	.	.	.	.	
1887	CLEAR	.....	.	.	
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1892	.	SUB8S	.	.	
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1898	.	RGC36	.	.	
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1904	.	.	GC36	.	
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1910	.	C1GC36	.....	.	
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1913	.	.	SUB9S	.	
	.	.	V	.	
	.	.	V	.	
1919	.	.	R9S	.	
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1925	.	CPGC36	.....	.	
	.	V	.	.	
	.	V	.	.	
1928	.	SRGC36	.	.	
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1934	.	.	SUB7A	.	
	.	.	V	.	
	.	.	V	.	
1940	.	.	SR7A	.	
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	.	.	V	.	
1946	.	.	R10S	.	



2071	.	.	.	.	.	C1I.....
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	.					V
2074	.					C1O
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	.					V
2087	.					RC1
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2093	.				S54	.
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2099	.					SCN6A
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2106	.					C1A.....

(\*\*\*) RUNOFF ALSO COMPUTED AT THIS LOCATION

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 \*  
 \* FLOOD HYDROGRAPH PACKAGE (HEC-1) \*  
 \* MAY 1991 \*  
 \* VERSION 4.0.1E \*  
 \* Lahey F77L-EM/32 version 5.01 \*  
 \* Dodson & Associates, Inc. \*  
 \* RUN DATE 12/30/96 TIME 16:29:28 \*  
 \*\*\*\*\*

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 \*  
 \* U.S. ARMY CORPS OF ENGINEERS \*  
 \* HYDROLOGIC ENGINEERING CENTER \*  
 \* 609 SECOND STREET \*  
 \* DAVIS, CALIFORNIA 95616 \*  
 \* (916) 551-1748 \*  
 \*  
 \*\*\*\*\*

PIMA ROAD CHANNEL  
 by GVSCE for the City of Scottsdale  
 Project: 95

File: OPT1-6.IH1  
 Original:09-13-96 mcg

100-YEAR 6-HR HYPOTHETICAL RAINFALL DISTRIBUTION  
 RAINFALL LOSSES: SCS CURVE NUMBERS  
 UNIT HYDROGRAPH: KINEMATIC WAVE  
 ROUTING: MODIFIED PULS - USING NORMAL DEPTH

COLLECTOR CHANNEL LENGTHS ARE AS FOLLOWS:  
 HAPPY VALLEY ROAD ..... 1.0 MILE  
 PINNACLE PEAK ROAD ..... 0.5 MILE  
 DEER VALLEY ROAD ..... 0.25 MILE  
 BEARDLSEY ROAD ..... 1.0 MILE

DETENTION BASINS AT HAPPY VALLEY, DEER VALLEY AND UNION HILLS ROADS.

19 IO OUTPUT CONTROL VARIABLES  
 IPRNT 5 PRINT CONTROL  
 IPLOT 0 PLOT CONTROL  
 QSCAL 0. HYDROGRAPH PLOT SCALE

IT HYDROGRAPH TIME DATA  
 NMIN 5 MINUTES IN COMPUTATION INTERVAL  
 IDATE 1 0 STARTING DATE  
 ITIME 0000 STARTING TIME  
 NQ 720 NUMBER OF HYDROGRAPH ORDINATES  
 NDDATE 3 0 ENDING DATE  
 NDTIME 1155 ENDING TIME  
 ICENT 19 CENTURY MARK

COMPUTATION INTERVAL 0.08 HOURS  
 TOTAL TIME BASE 59.92 HOURS

ENGLISH UNITS  
 DRAINAGE AREA SQUARE MILES  
 PRECIPITATION DEPTH INCHES  
 LENGTH, ELEVATION FEET  
 FLOW CUBIC FEET PER SECOND  
 STORAGE VOLUME ACRE-FEET  
 SURFACE AREA ACRES  
 TEMPERATURE DEGREES FAHRENHEIT

STRM 0.00 PRECIPITATION DEPTH  
TRDA 0.01 TRANSPOSITION DRAINAGE AREA

0 PI PRECIPITATION PATTERN

21 JD INDEX STORM NO. 2

STRM 0.00 PRECIPITATION DEPTH  
TRDA 0.10 TRANSPOSITION DRAINAGE AREA

0 PI PRECIPITATION PATTERN

22 JD INDEX STORM NO. 3

STRM 0.00 PRECIPITATION DEPTH  
TRDA 0.50 TRANSPOSITION DRAINAGE AREA

0 PI PRECIPITATION PATTERN

23 JD INDEX STORM NO. 4

STRM 0.00 PRECIPITATION DEPTH  
TRDA 1.00 TRANSPOSITION DRAINAGE AREA

0 PI PRECIPITATION PATTERN

24 JD INDEX STORM NO. 5

STRM 0.00 PRECIPITATION DEPTH  
TRDA 5.00 TRANSPOSITION DRAINAGE AREA

0 PI PRECIPITATION PATTERN

25 JD INDEX STORM NO. 6

STRM 0.00 PRECIPITATION DEPTH  
TRDA 25.00 TRANSPOSITION DRAINAGE AREA

0 PI PRECIPITATION PATTERN

\*\*\* FDKRUT - NEWTON RAPHSON FAILEDFIXED POINT ITERATION USED - ITERATION= 1

\*\*\* FDKRUT - NEWTON RAPHSON FAILEDFIXED POINT ITERATION USED - ITERATION= 1

\*\*\* FDKRUT - NEWTON RAPHSON FAILEDFIXED POINT ITERATION USED - ITERATION= 1

\*\*\* FDKRUT - NEWTON RAPHSON FAILEDFIXED POINT ITERATION USED - ITERATION= 1

RUNOFF SUMMARY  
 FLOW IN CUBIC FEET PER SECOND  
 TIME IN HOURS, AREA IN SQUARE MILES

OPERATION	STATION	PEAK FLOW	TIME OF PEAK	AVERAGE FLOW FOR MAXIMUM PERIOD			BASIN AREA	MAXIMUM STAGE	TIME O MAX STA
				6-HOUR	24-HOUR	72-HOUR			
HYDROGRAPH AT	S30N	1227.	3.33	128.	32.	13.	0.65		
ROUTED TO	R30N	1121.	3.42	128.	32.	13.	0.65		
HYDROGRAPH AT	S31.1	395.	3.33	43.	11.	4.	0.27		
2 COMBINED AT	C31.1	1465.	3.42	171.	43.	17.	0.92	1592	
ROUTED TO	R31.1	1476.	3.42	170.	43.	17.	0.92		
HYDROGRAPH AT	S35N	1298.	3.25	108.	27.	11.	0.55	2360	
DIVERSION TO	D35NL	519.	3.25	43.	11.	4.	0.55		
HYDROGRAPH AT	D35NR	779.	3.25	65.	16.	7.	0.55		
ROUTED TO	R35NR	630.	3.33	64.	16.	7.	0.55		
HYDROGRAPH AT	S36.2	400.	3.25	34.	9.	3.	0.21		
2 COMBINED AT	C36.2	947.	3.25	98.	25.	10.	0.54		
DIVERSION TO	D36.2L	284.	3.25	30.	7.	3.	0.54		
HYDROGRAPH AT	D36.2R	663.	3.25	69.	17.	7.	0.54		
ROUTED TO	R36.2R	430.	3.67	69.	17.	7.	0.54		
HYDROGRAPH AT	S34.1	2491.	3.33	262.	66.	27.	1.61		
3 COMBINED AT	C34.1I	3668.	3.33	497.	126.	50.	2.90	1265	
ROUTED TO	C34.1O	219.	5.50	211.	126.	50.	2.90		
ROUTED TO	R34.1	218.	5.58	211.	126.	50.	2.90		
HYDROGRAPH AT	S36.1	159.	3.42	19.	5.	2.	0.14		
2 COMBINED AT	C36.1	311.	3.42	226.	130.	52.	3.04		
ROUTED TO	R36.1	292.	3.58	225.	130.	52.	3.04		
HYDROGRAPH AT	B35NL	519.	3.25	43.	11.	4.	0.55		
ROUTED TO	R35NL	317.	3.58	43.	11.	4.	0.55		
HYDROGRAPH AT	B36.2L	284.	3.25	30.	7.	3.	0.54		
ROUTED TO	R36.2L	193.	3.58	29.	7.	3.	0.54		
HYDROGRAPH AT	S36R1	1107.	3.50	171.	43.	17.	1.22		

4 COMBINED AT	C36R1	1832.	3.58	459.	190.	76.	4.64
ROUTED TO	R36R1	1739.	3.67	456.	190.	76.	4.64
HYDROGRAPH AT	S36R2	489.	3.33	54.	14.	5.	0.37
2 COMBINED AT	C36R2	1922.	3.67	503.	204.	82.	5.01
HYDROGRAPH AT	S51.1	1058.	3.50	162.	41.	16.	1.13
2 COMBINED AT	C51.1I	2849.	3.58	657.	242.	97.	6.14
ROUTED TO	C51.1O	360.	6.67	354.	242.	97.	6.14
ROUTED TO	R51.1	360.	6.75	354.	242.	97.	6.14
DIVERSION TO	B51.1T	360.	6.75	354.	242.	97.	6.14
HYDROGRAPH AT	D51.1T	0.	0.08	0.	0.	0.	6.14
HYDROGRAPH AT	52D4	116.	3.25	11.	3.	1.	0.07
ROUTED TO	52D4R	106.	3.25	11.	3.	1.	0.07
HYDROGRAPH AT	52D4B	70.	3.17	6.	1.	1.	0.02
2 COMBINED AT	52D5C1	161.	3.25	17.	4.	2.	0.09
HYDROGRAPH AT	52D5A	79.	3.17	6.	2.	1.	0.02
ROUTED TO	52D5AR	75.	3.17	6.	2.	1.	0.02
2 COMBINED AT	52D5C2	217.	3.25	23.	6.	2.	0.12
ROUTED TO	52D5R	216.	3.25	23.	6.	2.	0.12
HYDROGRAPH AT	52C3	24.	3.08	2.	0.	0.	0.01
ROUTED TO	52C3R	23.	3.17	2.	0.	0.	0.01
HYDROGRAPH AT	52C3B	53.	3.08	4.	1.	0.	0.02
2 COMBINED AT	2C3BC1	74.	3.17	6.	1.	1.	0.02
2 COMBINED AT	2C3BC2	270.	3.17	29.	7.	3.	0.14
ROUTED TO	52C3BR	261.	3.25	29.	7.	3.	0.14
HYDROGRAPH AT	51C	166.	3.17	15.	4.	1.	0.10
DIVERSION TO	51C1DV	111.	3.17	10.	3.	1.	0.10
HYDROGRAPH AT	51C1D	55.	3.17	5.	1.	0.	0.10
ROUTED TO	51C1R	53.	3.25	5.	1.	0.	0.10
HYDROGRAPH AT	52C1	69.	3.17	5.	1.	0.	0.03
2 COMBINED AT	52C1C	106.	3.17	10.	2.	1.	0.06

ROUTED TO	52C1R	101.	3.25	10.	2.	1.	0.06
HYDROGRAPH AT	52C2A	35.	3.17	2.	1.	0.	0.02
2 COMBINED AT	52C2AC	125.	3.25	12.	3.	1.	0.08
HYDROGRAPH AT	52C2B	56.	3.17	4.	1.	0.	0.03
2 COMBINED AT	52C2BC	170.	3.17	16.	4.	2.	0.11
ROUTED TO	52C2BR	168.	3.25	16.	4.	2.	0.11
HYDROGRAPH AT	52C2C	46.	3.08	4.	1.	0.	0.01
2 COMBINED AT	52C2CC	194.	3.25	20.	5.	2.	0.12
ROUTED TO	52C2R	180.	3.25	20.	5.	2.	0.12
HYDROGRAPH AT	52C4	56.	3.17	4.	1.	0.	0.02
2 COMBINED AT	52C4C1	211.	3.25	24.	6.	2.	0.14
2 COMBINED AT	52C4C2	472.	3.25	53.	13.	5.	0.28
ROUTED TO	52C4R	462.	3.25	53.	14.	5.	0.28
HYDROGRAPH AT	52C13	69.	3.08	5.	1.	0.	0.02
DIVERSION TO	STORM	40.	3.08	4.	1.	0.	0.02
HYDROGRAPH AT	2C13DV	29.	3.08	1.	0.	0.	0.02
HYDROGRAPH AT	52C15	157.	3.08	13.	3.	1.	0.05
2 COMBINED AT	2C15C1	186.	3.08	13.	3.	1.	0.05
2 COMBINED AT	2C15C2	546.	3.17	66.	17.	7.	0.32
ROUTED TO	52C15R	544.	3.25	66.	17.	7.	0.32
HYDROGRAPH AT	52C14A	142.	3.17	11.	3.	1.	0.04
2 COMBINED AT	2C14AC	655.	3.17	78.	20.	8.	0.36
ROUTED TO	2C14AR	637.	3.17	78.	20.	8.	0.36
HYDROGRAPH AT	51C1DV	111.	3.17	10.	3.	1.	0.10
DIVERSION TO	51C2DV	30.	3.17	3.	1.	0.	0.10
HYDROGRAPH AT	51C2D	81.	3.17	7.	2.	1.	0.10
ROUTED TO	51C2R	78.	3.25	7.	2.	1.	0.10
HYDROGRAPH AT	52C5	40.	3.17	3.	1.	0.	0.02
2 COMBINED AT	52C5C	109.	3.17	10.	3.	1.	0.06
ROUTED TO	52C5R	104.	3.25	10.	3.	1.	0.06

HYDROGRAPH AT	52C6	82.	3.17	7.	2.	1.	0.04
2 COMBINED AT	52C6C	173.	3.25	17.	4.	2.	0.10
ROUTED TO	52C6R	165.	3.25	17.	4.	2.	0.10
HYDROGRAPH AT	51C2DV	30.	3.17	3.	1.	0.	0.10
ROUTED TO	51C3R	29.	3.25	3.	1.	0.	0.10
HYDROGRAPH AT	51B	596.	3.42	79.	20.	8.	0.57
DIVERSION TO	51B1DV	549.	3.42	72.	18.	7.	0.57
HYDROGRAPH AT	51B1D	48.	3.42	6.	2.	1.	0.57
ROUTED TO	51B1R	48.	3.42	6.	2.	1.	0.57
HYDROGRAPH AT	52C7	18.	3.08	1.	0.	0.	0.01
3 COMBINED AT	52C7C	76.	3.25	10.	3.	1.	0.07
ROUTED TO	52C7R	75.	3.33	10.	3.	1.	0.07
HYDROGRAPH AT	51B1DV	549.	3.42	72.	18.	7.	0.57
DIVERSION TO	51B2DV	461.	3.42	61.	15.	6.	0.57
HYDROGRAPH AT	51B2D	88.	3.42	12.	3.	1.	0.57
ROUTED TO	51B2R	88.	3.42	12.	3.	1.	0.57
HYDROGRAPH AT	52C8	21.	3.08	1.	0.	0.	0.01
2 COMBINED AT	52C8C	93.	3.42	13.	3.	1.	0.45
ROUTED TO	52C8R	92.	3.42	13.	3.	1.	0.45
2 COMBINED AT	52C9C1	163.	3.42	23.	6.	2.	0.52
ROUTED TO	52C9R1	162.	3.42	23.	6.	2.	0.52
HYDROGRAPH AT	52C9	174.	3.17	14.	3.	1.	0.07
2 COMBINED AT	52C9C2	255.	3.25	37.	9.	4.	0.59
ROUTED TO	52C9R2	254.	3.25	37.	9.	4.	0.59
2 COMBINED AT	2C10C1	418.	3.25	54.	14.	5.	0.69
ROUTED TO	2C10R1	412.	3.25	54.	14.	5.	0.69
HYDROGRAPH AT	52C10	28.	3.17	2.	1.	0.	0.01
2 COMBINED AT	2C10C2	428.	3.25	56.	14.	6.	0.70
HYDROGRAPH AT	52C11	96.	3.17	8.	2.	1.	0.04
ROUTED TO	2C11R1	88.	3.17	8.	2.	1.	0.04

HYDROGRAPH AT	52C13D	40.	3.08	4.	1.	0.	0.02
2 COMBINED AT	52C11C	128.	3.17	12.	3.	1.	0.07
ROUTED TO	2C11CR	120.	3.17	12.	3.	1.	0.07
2 COMBINED AT	2C11C2	541.	3.25	68.	17.	7.	0.77
ROUTED TO	2C11R2	530.	3.25	68.	17.	7.	0.77
HYDROGRAPH AT	52C12	119.	3.08	7.	2.	1.	0.02
2 COMBINED AT	52C12C	567.	3.25	75.	19.	8.	0.79
ROUTED TO	52C12R	549.	3.25	75.	19.	8.	0.79
HYDROGRAPH AT	52C14B	76.	3.08	6.	1.	1.	0.02
2 COMBINED AT	C14BC1	584.	3.25	81.	20.	8.	0.81
2 COMBINED AT	C14BC2	1200.	3.25	158.	40.	16.	1.17
ROUTED TO	52C14R	1194.	3.25	158.	40.	16.	1.17
HYDROGRAPH AT	51B2DV	461.	3.42	61.	15.	6.	0.57
DIVERSION TO	51B3DV	387.	3.42	51.	13.	5.	0.57
HYDROGRAPH AT	51B3D	74.	3.42	10.	2.	1.	0.57
ROUTED TO	51B3R	74.	3.42	10.	2.	1.	0.57
HYDROGRAPH AT	52B1	8.	3.08	1.	0.	0.	0.00
2 COMBINED AT	52B1C	76.	3.42	10.	3.	1.	0.07
ROUTED TO	52B1R	75.	3.42	10.	3.	1.	0.07
HYDROGRAPH AT	51B3DV	387.	3.42	51.	13.	5.	0.57
DIVERSION TO	51B4DV	317.	3.42	42.	11.	4.	0.57
HYDROGRAPH AT	51B4D	70.	3.42	9.	2.	1.	0.57
ROUTED TO	51B4R1	70.	3.42	9.	2.	1.	0.57
2 COMBINED AT	52B2C1	145.	3.42	20.	5.	2.	0.14
ROUTED TO	52B2R1	142.	3.42	20.	5.	2.	0.14
HYDROGRAPH AT	52B2	69.	3.17	5.	1.	1.	0.03
2 COMBINED AT	52B2C2	166.	3.42	25.	6.	3.	0.17
ROUTED TO	52B2R2	164.	3.42	25.	6.	3.	0.17
ROUTED TO	52B3R1	163.	3.42	25.	6.	3.	0.17
HYDROGRAPH AT	52B3	141.	3.17	12.	3.	1.	0.06

2 COMBINED AT	52B3C2	249.	3.25	37.	9.	4.	0.23
ROUTED TO	52B3R2	241.	3.33	37.	9.	4.	0.23
HYDROGRAPH AT	52B4	87.	3.17	7.	2.	1.	0.03
2 COMBINED AT	52B4C	284.	3.25	44.	11.	4.	0.26
ROUTED TO	52B4R	277.	3.25	44.	11.	4.	0.26
HYDROGRAPH AT	52B5	69.	3.08	5.	1.	1.	0.02
2 COMBINED AT	52B5C1	313.	3.25	49.	12.	5.	0.28
2 COMBINED AT	52B5C2	1496.	3.25	207.	52.	21.	1.45
ROUTED TO	52B5R	1474.	3.25	207.	53.	21.	1.45
HYDROGRAPH AT	51B4DV	317.	3.42	42.	11.	4.	0.57
DIVERSION TO	51B5DV	216.	3.42	28.	7.	3.	0.57
HYDROGRAPH AT	51B5D	102.	3.42	13.	3.	1.	0.57
ROUTED TO	51B5R	102.	3.42	13.	3.	1.	0.57
HYDROGRAPH AT	51B5DV	216.	3.42	28.	7.	3.	0.57
DIVERSION TO	51B6DV	114.	3.42	15.	4.	2.	0.57
HYDROGRAPH AT	51B6D	101.	3.42	13.	3.	1.	0.57
ROUTED TO	51B6R	101.	3.42	13.	3.	1.	0.57
HYDROGRAPH AT	51B6DV	114.	3.42	15.	4.	2.	0.57
DIVERSION TO	51B7DV	66.	3.42	9.	2.	1.	0.57
HYDROGRAPH AT	51B7D	48.	3.42	6.	2.	1.	0.57
ROUTED TO	51B7R1	48.	3.42	6.	2.	1.	0.57
3 COMBINED AT	51B7C	252.	3.42	33.	8.	3.	0.24
ROUTED TO	51B7R2	244.	3.42	33.	8.	3.	0.24
HYDROGRAPH AT	52B6	190.	3.17	15.	4.	2.	0.10
2 COMBINED AT	52B6C	313.	3.42	48.	12.	5.	0.34
ROUTED TO	52B6R	311.	3.42	48.	12.	5.	0.34
HYDROGRAPH AT	52B7	303.	3.17	24.	6.	2.	0.08
2 COMBINED AT	52B7C1	411.	3.25	72.	18.	7.	0.42
2 COMBINED AT	52B7C2	1871.	3.25	278.	71.	28.	1.87
HYDROGRAPH AT	52A2	263.	3.17	21.	5.	2.	0.06

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2 COMBINED AT	52A2C2	2033.	3.25	299.	76.	30.	1.62
HYDROGRAPH AT	51B7DV	66.	3.42	9.	2.	1.	0.57
ROUTED TO	51B8R	66.	3.50	9.	2.	1.	0.57
HYDROGRAPH AT	52A1	340.	3.17	26.	6.	3.	0.13
2 COMBINED AT	52A1C	344.	3.17	34.	9.	3.	0.13
HYDROGRAPH AT	D51.1	360.	6.75	354.	242.	97.	6.14
2 COMBINED AT	C52A	385.	3.17	362.	250.	100.	6.27
ROUTED TO	R52A	370.	6.00	362.	250.	100.	6.27
2 COMBINED AT	C52	2201.	3.25	622.	322.	129.	7.92
ROUTED TO	R52	2121.	3.33	621.	322.	129.	7.92
DIVERSION TO	B52T	2121.	3.33	621.	322.	129.	7.92
HYDROGRAPH AT	D52T	0.	0.08	0.	0.	0.	7.92
2 COMBINED AT	CLEAR	0.	0.08	0.	0.	0.	14.06
HYDROGRAPH AT	37A	1164.	3.25	119.	30.	12.	0.68
DIVERSION TO	37AW	815.	3.25	83.	21.	8.	0.68
HYDROGRAPH AT	37AE	349.	3.25	36.	9.	4.	0.68
ROUTED TO	37AE1	342.	3.25	36.	9.	4.	0.68
HYDROGRAPH AT	SUB5N	70.	3.17	5.	1.	1.	0.03
2 COMBINED AT	CP5N	394.	3.25	41.	10.	4.	0.23
ROUTED TO	RET5N	357.	3.33	40.	10.	4.	0.23
ROUTED TO	R6N.1	294.	3.42	40.	10.	4.	0.23
HYDROGRAPH AT	SUB6B	74.	3.17	5.	1.	1.	0.03
ROUTED TO	SR6B	43.	3.25	5.	1.	1.	0.03
2 COMBINED AT	CP6.1	326.	3.42	45.	12.	5.	0.26
HYDROGRAPH AT	SUB1N	47.	3.17	3.	1.	0.	0.02
ROUTED TO	R2NA	46.	3.17	3.	1.	0.	0.02
HYDROGRAPH AT	SUB2NA	34.	3.17	2.	1.	0.	0.01
2 COMBINED AT	CP2NA	80.	3.17	6.	1.	1.	0.03
ROUTED TO	SR2NA	70.	3.25	4.	1.	0.	0.03
ROUTED TO	R2NB	59.	3.33	4.	1.	0.	0.03

277.90

2667

HYDROGRAPH AT	SUB2NB	96.	3.17	8.	2.	1.	0.03
2 COMBINED AT	CP2NB	99.	3.33	12.	3.	1.	0.06
ROUTED TO	SR2NB	25.	3.75	11.	3.	1.	0.06
ROUTED TO	RCP4N	24.	3.75	11.	3.	1.	0.06
HYDROGRAPH AT	SUB6N	114.	3.17	8.	2.	1.	0.05
ROUTED TO	RET6N	0.	0.08	0.	0.	0.	0.05
ROUTED TO	RCP4N1	0.	0.08	0.	0.	0.	0.05
2 COMBINED AT	CP4N.1	24.	3.75	11.	3.	1.	0.11
HYDROGRAPH AT	SUB3N	67.	3.17	4.	1.	0.	0.03
ROUTED TO	RET3N	4.	4.17	3.	1.	0.	0.03
ROUTED TO	R4N	4.	4.25	3.	1.	0.	0.03
2 COMBINED AT	CP4N.2	27.	3.75	14.	4.	2.	0.14
HYDROGRAPH AT	SUB4N	80.	3.17	6.	1.	1.	0.03
2 COMBINED AT	CP4N	89.	3.17	19.	6.	2.	0.17
ROUTED TO	R6N	82.	3.17	19.	6.	2.	0.17
HYDROGRAPH AT	SUB6A	64.	3.08	4.	1.	0.	0.01
2 COMBINED AT	CP6.2	121.	3.17	23.	7.	3.	0.18
2 COMBINED AT	CP6N	376.	3.42	68.	18.	7.	0.45
ROUTED TO	RCP6N	373.	3.42	68.	18.	7.	0.45
HYDROGRAPH AT	SUB3C	55.	3.08	3.	1.	0.	0.01
2 COMBINED AT	CP3C	380.	3.42	70.	19.	8.	0.46
ROUTED TO	R3C	361.	3.50	70.	19.	8.	0.46
HYDROGRAPH AT	GC1018	101.	3.17	7.	2.	1.	0.04
HYDROGRAPH AT	GC1-9	58.	3.17	4.	1.	0.	0.03
HYDROGRAPH AT	SUB3S	33.	3.17	3.	1.	0.	0.01
4 COMBINED AT	CP3S	411.	3.50	84.	22.	9.	0.54
ROUTED TO	RT3S	409.	3.50	84.	22.	9.	0.54
HYDROGRAPH AT	SUB4S	87.	3.17	7.	2.	1.	0.03
ROUTED TO	RT4S	87.	3.17	7.	2.	1.	0.03
HYDROGRAPH AT	GC2-8	32.	3.17	2.	1.	0.	0.01

3 COMBINED AT	1PGC28	437.	3.50	93.	25.	10.	0.58
HYDROGRAPH AT	SUB3D3	35.	3.17	2.	1.	0.	0.01
2 COMBINED AT	CPGC28	444.	3.50	95.	25.	10.	0.59
ROUTED TO	SRGC28	443.	3.25	95.	25.	10.	0.59
ROUTED TO	RT7S	431.	3.58	95.	25.	10.	0.59
HYDROGRAPH AT	GC7	31.	3.17	2.	1.	0.	0.01
2 COMBINED AT	CP7S	437.	3.58	97.	26.	10.	0.61
DIVERSION TO	B7ST	437.	3.58	97.	26.	10.	0.61
HYDROGRAPH AT	D7ST	0.	0.08	0.	0.	0.	0.61
2 COMBINED AT	CLEAR	0.	0.08	0.	0.	0.	14.67
HYDROGRAPH AT	SUB3D1	27.	3.08	2.	0.	0.	0.01
ROUTED TO	RD1B1	22.	3.17	2.	0.	0.	0.01
HYDROGRAPH AT	SUB3B1	47.	3.08	3.	1.	0.	0.01
2 COMBINED AT	CP3B1	61.	3.08	5.	1.	1.	0.02
ROUTED TO	RB13F	48.	3.25	5.	1.	1.	0.02
HYDROGRAPH AT	SUB3F	141.	3.08	10.	2.	1.	0.03
2 COMBINED AT	CP3F	169.	3.08	15.	4.	2.	0.06
HYDROGRAPH AT	SUB3B2	67.	3.17	6.	1.	1.	0.02
ROUTED TO	RB2E1	64.	3.17	6.	1.	1.	0.02
ROUTED TO	RB2E2	61.	3.25	6.	1.	1.	0.02
HYDROGRAPH AT	SUB3E1	67.	3.17	6.	1.	1.	0.02
2 COMBINED AT	1CPE31	125.	3.17	11.	3.	1.	0.05
HYDROGRAPH AT	SUB3D2	58.	3.17	5.	1.	0.	0.02
ROUTED TO	RD2E2	56.	3.17	5.	1.	0.	0.02
HYDROGRAPH AT	SUB3E2	37.	3.08	3.	1.	0.	0.01
2 COMBINED AT	CP3E2	86.	3.17	7.	2.	1.	0.03
HYDROGRAPH AT	PC3	82.	3.17	7.	2.	1.	0.04
4 COMBINED AT	CPC3	449.	3.17	40.	10.	4.	0.18
DIVERSION TO	BPC3T	449.	3.17	40.	10.	4.	0.18
HYDROGRAPH AT	DPC3T	0.	0.08	0.	0.	0.	0.18

HYDROGRAPH AT	SUB3E3	60.	3.08	4.	1.	0.	0.02
HYDROGRAPH AT	PC4	43.	3.17	3.	1.	0.	0.02
HYDROGRAPH AT	D7S	437.	3.58	97.	26.	10.	0.61
3 COMBINED AT	CPC4	471.	3.33	104.	28.	11.	0.65
DIVERSION TO	BPC4T	471.	3.33	104.	28.	11.	0.65
HYDROGRAPH AT	DPC4T	0.	0.08	0.	0.	0.	0.65
3 COMBINED AT	CLEAR	0.	0.08	0.	0.	0.	15.50
HYDROGRAPH AT	37AW	815.	3.25	83.	21.	8.	0.68
ROUTED TO	R14R	659.	3.33	83.	21.	8.	0.68
ROUTED TO	RET141	631.	3.42	78.	21.	8.	0.68
ROUTED TO	R14.1	558.	3.50	78.	21.	8.	0.68
HYDROGRAPH AT	SUB13N	81.	3.17	7.	2.	1.	0.04
ROUTED TO	R14.1	78.	3.25	7.	2.	1.	0.04
HYDROGRAPH AT	SUB14N	88.	3.25	8.	2.	1.	0.05
3 COMBINED AT	CP14	625.	3.50	92.	25.	10.	0.56
ROUTED TO	RET14	574.	3.58	88.	25.	10.	0.56
ROUTED TO	R18.1	570.	3.58	88.	25.	10.	0.56
HYDROGRAPH AT	SUB20N	47.	3.17	4.	1.	0.	0.02
ROUTED TO	R19	48.	3.25	4.	1.	0.	0.02
HYDROGRAPH AT	SUB19N	94.	3.17	8.	2.	1.	0.04
2 COMBINED AT	CP19N	133.	3.17	12.	3.	1.	0.06
ROUTED TO	R18NC	132.	3.25	12.	3.	1.	0.06
HYDROGRAPH AT	UB18NC	62.	3.17	5.	1.	0.	0.02
3 COMBINED AT	CP18NC	619.	3.58	103.	29.	12.	0.64
ROUTED TO	RPC1	628.	3.58	103.	29.	12.	0.64
HYDROGRAPH AT	UB18NA	65.	3.17	5.	1.	1.	0.02
ROUTED TO	1RPC1	31.	3.33	5.	1.	1.	0.02
HYDROGRAPH AT	UB18NB	27.	3.17	2.	1.	0.	0.01
ROUTED TO	2RPC1	16.	3.25	2.	1.	0.	0.01
HYDROGRAPH AT	PC1	66.	3.42	10.	2.	1.	0.06

3 COMBINED AT	1CPC1	107.	3.42	17.	4.	2.	0.09
ROUTED TO	SRPC1	108.	3.42	16.	4.	2.	0.09
2 COMBINED AT	CPC1	712.	3.58	120.	33.	13.	0.74
ROUTED TO	R16NA1	720.	3.58	119.	33.	13.	0.74
HYDROGRAPH AT	UB16NA	42.	3.17	3.	1.	0.	0.01
ROUTED TO	R16NA1	37.	3.17	3.	1.	0.	0.01
2 COMBINED AT	C16NA1	728.	3.58	122.	34.	14.	0.75
ROUTED TO	R16NB1	717.	3.58	122.	34.	14.	0.75
HYDROGRAPH AT	UB16NB	48.	3.17	4.	1.	0.	0.02
ROUTED TO	R16NB1	43.	3.17	4.	1.	0.	0.02
2 COMBINED AT	C16NB1	725.	3.58	126.	35.	14.	0.77
ROUTED TO	R16NC1	727.	3.67	126.	35.	14.	0.77
HYDROGRAPH AT	SUB7N	74.	3.17	5.	1.	1.	0.03
ROUTED TO	R8NC	64.	3.25	5.	1.	1.	0.03
HYDROGRAPH AT	SUB8NA	13.	3.08	1.	0.	0.	0.00
ROUTED TO	SR8NA	1.	4.17	0.	0.	0.	0.00
ROUTED TO	R8NB	1.	4.17	0.	0.	0.	0.00
HYDROGRAPH AT	SUB8NB	34.	3.08	2.	1.	0.	0.01
2 COMBINED AT	CP8NB	34.	3.08	3.	1.	0.	0.02
ROUTED TO	SR8NB	2.	3.08	2.	1.	0.	0.02
ROUTED TO	R8NC	2.	3.08	2.	1.	0.	0.02
HYDROGRAPH AT	SUB8NC	51.	3.08	3.	1.	0.	0.02
3 COMBINED AT	CP8NC	103.	3.17	10.	3.	1.	0.07
ROUTED TO	SR8NC	18.	3.75	10.	3.	1.	0.07
ROUTED TO	R9N	17.	3.75	10.	3.	1.	0.07
HYDROGRAPH AT	SUB9N	143.	3.17	11.	3.	1.	0.05
2 COMBINED AT	CP9N	153.	3.17	21.	6.	2.	0.12
ROUTED TO	R10B	148.	3.17	21.	6.	2.	0.12
HYDROGRAPH AT	SUB10B	87.	3.08	6.	2.	1.	0.03
2 COMBINED AT	CP10B	226.	3.17	27.	7.	3.	0.15

ROUTED TO	R11NA	229.	3.17	27.	7.	3.	0.15
HYDROGRAPH AT	UB11NA	21.	3.08	1.	0.	0.	0.01
2 COMBINED AT	CP11NA	245.	3.17	28.	8.	3.	0.16
ROUTED TO	SR11NA	145.	3.33	28.	8.	3.	0.16
ROUTED TO	R11NB	140.	3.33	28.	8.	3.	0.16
HYDROGRAPH AT	UB11NB	22.	3.08	1.	0.	0.	0.01
2 COMBINED AT	CP11NB	146.	3.33	29.	8.	3.	0.17
ROUTED TO	SR11NB	84.	3.50	28.	8.	3.	0.17
ROUTED TO	R11NC	87.	3.50	28.	8.	3.	0.17
HYDROGRAPH AT	UB11NC	19.	3.08	1.	0.	0.	0.01
2 COMBINED AT	C11NC1	90.	3.50	30.	8.	3.	0.17
HYDROGRAPH AT	SUB10A	88.	3.08	7.	2.	1.	0.03
ROUTED TO	R12NB	95.	3.17	7.	2.	1.	0.03
HYDROGRAPH AT	UB12NA	36.	3.17	3.	1.	0.	0.02
ROUTED TO	SR12NA	1.	6.17	0.	0.	0.	0.02
ROUTED TO	R12NA	1.	6.17	0.	0.	0.	0.02
HYDROGRAPH AT	UB12NB	37.	3.17	3.	1.	0.	0.02
3 COMBINED AT	CP12NB	132.	3.17	10.	3.	1.	0.06
ROUTED TO	SR12NB	2.	3.17	2.	2.	1.	0.06
ROUTED TO	R11NC2	2.	3.50	2.	2.	1.	0.06
2 COMBINED AT	CP11NC	92.	3.50	32.	10.	4.	0.23
ROUTED TO	SR11NC	71.	3.75	30.	10.	4.	0.23
ROUTED TO	R16NC	71.	3.75	30.	10.	4.	0.23
HYDROGRAPH AT	UB16NC	102.	3.17	8.	2.	1.	0.03
2 COMBINED AT	CP16NC	107.	3.17	36.	12.	5.	0.27
ROUTED TO	R16NC1	106.	3.17	36.	12.	5.	0.27
2 COMBINED AT	C16NC1	788.	3.67	162.	47.	19.	1.03
ROUTED TO	R15N1	793.	3.67	162.	47.	19.	1.03
HYDROGRAPH AT	PC2	93.	3.25	8.	2.	1.	0.05
2 COMBINED AT	CP15N1	815.	3.67	170.	49.	20.	1.09

ROUTED TO	SRPC2	786.	3.75	169.	48.	20.	1.09
HYDROGRAPH AT	UB17NA	28.	3.08	2.	0.	0.	0.01
ROUTED TO	SR17NA	2.	3.75	1.	0.	0.	0.01
ROUTED TO	R17NB	2.	3.75	1.	0.	0.	0.01
HYDROGRAPH AT	UB17NB	27.	3.17	2.	0.	0.	0.01
2 COMBINED AT	CP17NB	28.	3.17	3.	1.	0.	0.02
ROUTED TO	SR17NB	1.	3.00	1.	1.	0.	0.02
ROUTED TO	R17A	1.	3.08	1.	1.	0.	0.02
HYDROGRAPH AT	SUB17A	30.	3.08	2.	0.	0.	0.01
2 COMBINED AT	CP17A1	31.	3.08	3.	1.	1.	0.03
HYDROGRAPH AT	UB17NC	19.	3.08	1.	0.	0.	0.01
2 COMBINED AT	CP17A	50.	3.08	3.	2.	1.	0.03
ROUTED TO	R15N	34.	3.17	3.	2.	1.	0.03
HYDROGRAPH AT	SUB15N	142.	3.17	11.	3.	1.	0.04
2 COMBINED AT	CP15N	175.	3.17	14.	4.	2.	0.07
ROUTED TO	R15N2	179.	3.17	14.	4.	2.	0.07
2 COMBINED AT	CP15N2	804.	3.75	182.	53.	22.	1.16
ROUTED TO	R15N2	768.	3.83	182.	53.	22.	1.16
HYDROGRAPH AT	DPC3	449.	3.17	40.	10.	4.	0.18
2 COMBINED AT	CPC3A	812.	3.75	217.	62.	25.	1.34
ROUTED TO	RPC3A	815.	3.83	217.	62.	25.	1.34
HYDROGRAPH AT	DPC4	471.	3.33	104.	28.	11.	0.65
2 COMBINED AT	CPC4A	1132.	3.75	319.	90.	36.	1.99
ROUTED TO	RPC4A	1123.	3.83	319.	90.	36.	1.99
DIVERSION TO	BPC4AT	1123.	3.83	319.	90.	36.	1.99
HYDROGRAPH AT	DPC4AT	0.	0.08	0.	0.	0.	1.99
HYDROGRAPH AT	SUB1-2	181.	3.17	16.	4.	2.	0.06
HYDROGRAPH AT	GCRB18	27.	3.17	2.	1.	0.	0.01
2 COMBINED AT	CPRET1	208.	3.17	18.	4.	2.	0.07
ROUTED TO	SR18S	0.	0.08	0.	0.	0.	0.07

606.0

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HYDROGRAPH AT	SUB5S	72.	3.17	5.	1.	1.	0.03
HYDROGRAPH AT	GC1216	83.	3.17	6.	2.	1.	0.04
HYDROGRAPH AT	GC1415	104.	3.17	7.	2.	1.	0.05
HYDROGRAPH AT	SUB6S	53.	3.17	5.	1.	0.	0.02
HYDROGRAPH AT	SUB7S	79.	3.17	6.	2.	1.	0.03
5 COMBINED AT	CPRET2	391.	3.17	30.	7.	3.	0.16
ROUTED TO	SRRET2	0.	0.08	0.	0.	0.	0.16
4 COMBINED AT	CLEAR	0.	0.08	0.	0.	0.	17.72
HYDROGRAPH AT	SUB8S	76.	3.17	6.	1.	1.	0.03
ROUTED TO	RGC36	64.	3.25	6.	1.	1.	0.03
HYDROGRAPH AT	GC36	77.	3.17	7.	2.	1.	0.04
2 COMBINED AT	C1GC36	141.	3.17	13.	3.	1.	0.07
HYDROGRAPH AT	SUB9S	68.	3.17	5.	1.	1.	0.02
ROUTED TO	R9S	69.	3.17	5.	1.	1.	0.02
2 COMBINED AT	CPGC36	210.	3.17	18.	4.	2.	0.09
ROUTED TO	SRGC36	208.	3.25	18.	4.	2.	0.09
HYDROGRAPH AT	SUB7A	27.	3.17	2.	1.	0.	0.01
ROUTED TO	SR7A	7.	3.42	2.	1.	0.	0.01
ROUTED TO	R10S	7.	3.58	2.	1.	0.	0.01
HYDROGRAPH AT	SUB10S	78.	3.17	6.	2.	1.	0.02
2 COMBINED AT	CP10S	81.	3.17	8.	2.	1.	0.03
HYDROGRAPH AT	SUB11S	118.	3.08	7.	2.	1.	0.02
ROUTED TO	R11S	88.	3.17	7.	2.	1.	0.02
2 COMBINED AT	C10SA	169.	3.17	15.	4.	2.	0.06
ROUTED TO	R10SA	173.	3.17	15.	4.	2.	0.06
HYDROGRAPH AT	GC45	45.	3.08	2.	1.	0.	0.01
HYDROGRAPH AT	PC5	60.	3.17	5.	1.	1.	0.04
HYDROGRAPH AT	DPC4A	1123.	3.83	319.	90.	36.	1.99
5 COMBINED AT	CPC5	1266.	3.33	356.	100.	40.	2.10
ROUTED TO	RPC5	1196.	3.42	356.	100.	40.	2.10

HYDROGRAPH AT	SCN5C	351.	3.42	44.	11.	4.	0.27	
HYDROGRAPH AT	SCN6	730.	3.25	82.	21.	8.	0.26	
HYDROGRAPH AT	D52	2121.	3.33	621.	322.	129.	7.92	
HYDROGRAPH AT	S53A	226.	3.33	24.	6.	2.	0.17	
2 COMBINED AT	C53	2321.	3.33	643.	328.	131.	8.09	
ROUTED TO	R53	2261.	3.33	642.	328.	131.	8.09	
HYDROGRAPH AT	S53A1	445.	3.33	53.	13.	5.	0.34	
2 COMBINED AT	C53A	2660.	3.33	691.	340.	136.	8.42	310
4 COMBINED AT	C1I	4455.	3.33	1136.	462.	186.	11.05	403
ROUTED TO	C10	636.	6.58	630.	462.	186.	11.05	
ROUTED TO	RC1	636.	6.58	630.	462.	186.	11.05	
HYDROGRAPH AT	S54	136.	3.25	14.	4.	1.	0.09	
HYDROGRAPH AT	SCN6A	198.	3.33	22.	6.	2.	0.13	
3 COMBINED AT	C1A	690.	3.42	646.	471.	189.	11.27	

\*\*\* NORMAL END OF HEC-1 \*\*\*

**APPENDIX B**

**HEC-1 Option 2 output file (100-year, 6-hour storm)**

```

*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
*      MAY 1991 *
*      VERSION 4.0.1E *
*      Lahey F77L-EM/32 version 5.01 *
*      Dodson & Associates, Inc. *
* RUN DATE 01/03/97 TIME 14:36:06 *
*****

```

```

*****
*
* U.S. ARMY CORPS OF ENGINE
* HYDROLOGIC ENGINEERING CE
* 609 SECOND STREET
* DAVIS, CALIFORNIA 9561
* (916) 551-1748
*
*****

```

```

X   X  XXXXXXX  XXXXX      X
X   X X      X   X      XX
X   X X      X           X
XXXXXXX XXXX  X          XXXXX X
X   X X      X           X
X   X X      X   X      X
X   X  XXXXXXX  XXXXX      XXX

```

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION. NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE, SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY, DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL, LOSS RATE:GREEN AND AMPT INFILTRATION, KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM.

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

1 ID PIMA ROAD CHANNEL File: OPT2-6.IH1

2 ID by GVSCE for the City of Scottsdale Original:09-13-96 mcg

3 ID Project: 95

4 ID

5 ID 100-YEAR 6-HR HYPOTHETICAL RAINFALL DISTRIBUTION

6 ID RAINFALL LOSSES: SCS CURVE NUMBERS

7 ID UNIT HYDROGRAPH: KINEMATIC WAVE

8 ID ROUTING: MODIFIED PULS - USING NORMAL DEPTH

9 ID

10 ID COLLECTOR CHANNEL LENGTHS ARE AS FOLLOWS:

11 ID HAPPY VALLEY ROAD ..... 1.0 MILE

12 ID PINNACLE PEAK ROAD ..... 0.5 MILE

13 ID DEER VALLEY ROAD ..... 0.25 MILE

14 ID BEARDLSEY ROAD ..... 1.0 MILE

15 ID

16 ID DETENTION BASINS AT HAPPY VALLEY, DEER VALLEY AND UNION HILLS ROADS.

17 ID

\*DIAGRAM

18 IT 5 720

19 IO 5

20 JD .01

21 JD .1

22 JD .5

23 JD 1

24 JD 5

25 JD 25

\*

26 KK S30N

27 KM RUNOFF FROM SUBBASIN 30N

28 BA 0.6518

29 PH .84 1.53 2.46 2.75 2.94 3.31

30 LS 82 13 82 13

31 UK 300 0.350 0.13 20

32 UK 300 0.050 0.13 80

33 RK 1550 0.069 0.045 0.0096 TRAP 0 12

34 RK 10520 0.038 0.040 TRAP 15 15

\*

35 KK R30N

36 KM NORMAL DEPTH CHANNEL ROUTE FROM C30N TO C31.1 THROUGH PIMA CHANNEL

37 RS 1 FLOW -1

38 RC 0.035 0.025 0.035 2685 0.01

39 RX 1000 1020 1022 1033 1068 1079 1081 1101

40 RY 110.6 105.6 105.5 100 100 105.5 105.6 110.6

\*

41 KK S31.1

42 KM RUNOFF FROM SUBBASIN 31.1

43 BA 0.2663

44 LS 76.6 13 76.6 13

45 UK 300 0.567 0.13 10

46 UK 300 0.050 0.13 90

47 RK 1950 0.056 0.045 0.0147 TRAP 0 10

48 RK 7600 0.035 0.040 TRAP 22 8

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

49 KK C31.1  
 50 KM COMBINE ROUTED HYDROGRAPH FROM S30N WITH RUNOFF FROM SUBBASIN 31.1  
 51 HC 2  
 \*

52 KK R31.1  
 53 KM NORMAL DEPTH CHANNEL ROUTE FROM C31.1 TO C34.1 THROUGH PIMA CHANNEL  
 54 RS 1 FLOW -1  
 55 RC 0.035 0.025 0.035 2200 0.01  
 56 RX 1000 1020 1022 1033 1068 1079 1081 1101  
 57 RY 110.6 105.6 105.5 100 100 105.5 105.6 110.6  
 \*

58 KK S35N  
 59 KM RUNOFF FROM SUBBASIN 35N  
 60 BA 0.5482  
 61 LS 82 13 82 13  
 62 UK 300 0.491 0.13 15  
 63 UK 300 0.113 0.13 85  
 64 RK 2700 0.079 0.045 0.0242 TRAP 3 6  
 65 RK 5050 0.028 0.040 TRAP 15 15  
 \*

66 KK D35NR  
 67 KM DIVERT 60% OF FLOW INTO S36.2 - THE REMAINDER ENTERS S36R1  
 68 DT D35NL  
 69 DI 0 2000  
 70 DQ 0 800  
 \*

71 KK R35NR  
 72 KM NORMAL DEPTH CHANNEL ROUTE FROM S35N TO C36.2  
 73 KM SOURCE: 1993 MAPPING (2' CI) PROVIDED BY COS  
 74 RS 1 FLOW -1  
 75 RC 0.06 0.04 0.06 3500 0.0343  
 76 RX 1000 1006 1026 1027 1057 1058 1078 1084  
 77 RY 105 103 101 100 100 101 103 105  
 \*

78 KK S36.2  
 79 KM RUNOFF FROM SUBBASIN 36.2  
 80 BA 0.2087  
 81 LS 76.6 13 76.6 13  
 82 UK 300 0.580 0.13 5  
 83 UK 300 0.100 0.13 95  
 84 RK 1800 0.036 0.045 0.0145 TRAP 10 10  
 85 RK 3520 0.028 0.040 TRAP 20 6  
 \*

LINE	ID	1	2	3	4	5	6	7	8	9	10
86	KK	C36.2									
87	KM	COMBINE ROUTED HYDROGRAPH FROM S35N WITH RUNOFF FROM SUBBASIN 36.2									
88	KM	AREA IS AREA OF S36.2 + 60% OF AREA FROM S35N									
89	HC	2	0.5411								
	*										
90	KK	D36.2R									
91	KM	DIVERT 70% OF FLOW INTO S34.1 - THE REMAINDER ENTERS S36R1									
92	DT	D36.2L									
93	DI	0	2000								
94	DQ	0	600								
	*										
95	KK	R36.2R									
96	KM	NORMAL DEPTH CHANNEL ROUTE FROM C36.2 TO C34.1									
97	KM	SOURCE: 1993 MAPPING (2' CI) PROVIDED BY COS									
98	RS	4	FLOW		-1						
99	RC	0.06	0.04	0.06	7800	0.0321					
100	RX	1000	1043	1053	1068	1093	1098	1133	1218		
101	RY	102.6	100.6	100.5	100	100	100.5	100.6	102.6		
	*										
102	KK	S34.1									
103	KM	RUNOFF FROM SUBBASIN 34.1									
104	KM	RAINFALL LOSSES FOR GREINER SUBBASINS 31.2 AND 34.1 ARE WEIGHTED BY AREA									
105	BA	1.6076									
106	LS		77.3	12		77.3	12				
107	UK	300	0.590	0.13	25						
108	UK	300	0.040	0.13	75						
109	RK	2570	0.085	0.045	0.0214	TRAP	0	10			
110	RK	9200	0.042	0.040		TRAP	50	9			
	*										
111	KK	C34.1I									
112	KM	COMBINE ROUTED HYDROGRAPH FROM C31.1 & C36.2 W/RUNOFF FROM SUBBASIN 34.1									
113	KM	AREA IS AREA FROM C31.1 + S34.1 + 70% OF AREA FROM C36.2									
114	HC	3	2.9029								
	*										
115	KK	C34.10									
116	KM	DETENTION BASIN AT HAPPY VALLEY ROAD - NONREGULATORY STRUCTURE									
117	KM	OUTLET RATING CURVE - USING HY8 FOR A 48" RCP WITH A SLOPE OF 0.5%									
118	KM	13 ACRE-FEET OF STORAGE FOR SEDIMENTAION									
119	RS	1	STOR								
120	SV	0	0.1	0.2	0.5	1.2	2.2	20.5	65.1	116.9	182.1
121	SV	195									
122	SE	2065	2066	2067	2068	2069	2070	2075	2080	2085	2090
123	SE	2091									
124	SQ	0	21	42	63	84	105	110	147	168	189
125	SQ	210	216	244	549	665	811	996	1300	1511	
126	SE	2065.0	2066.82	2067.83	2068.64	2069.47	2070.44	2070.70	2073.43	2078.36	2083.14
127	SE	2088.3	2090.00	2090.10	2090.50	2090.60	2090.70	2090.80	2090.90	2091.00	
	*										

LINE	ID	1	2	3	4	5	6	7	8	9	10
128	KK	R34.1									
129	KM	NORMAL DEPTH CHANNEL ROUTE FROM C34.1 TO C36.1 THROUGH PIMA CHANNEL									
130	RS	1	FLOW	-1							
131	RC	0.035	0.025	0.035	2300	0.01					
132	RX	1000	1020	1022	1034	1079	1091	1093	1113		
133	RY	111	106	105.9	100	100	105.9	106	111		
	*										
134	KK	S36.1									
135	KM	RUNOFF FROM SUBBASIN 36.1									
136	BA	0.1394									
137	LS		73.4	11							
138	UK	300	0.0420	0.130	100						
139	RK	2330	0.0320	0.045	0.0134	TRAP	10	30			
140	RK	3200	0.0270	0.040		TRAP	20	30			
	*										
141	KK	C36.1									
142	KM	COMBINE ROUTED HYDROGRAPH FROM C34.1 WITH RUNOFF FROM SUBBASIN 36.1									
143	HC	2									
	*										
144	KK	R36.1									
145	KM	NORMAL DEPTH CHANNEL ROUTE FROM C36.1 TO C36R1 THROUGH PIMA CHANNEL									
146	RS	1	FLOW	-1							
147	RC	0.035	0.025	0.035	2980	0.01					
148	RX	1000	1020	1022	1034	1079	1091	1093	1113		
149	RY	111	106	105.9	100	100	105.9	106	111		
	*										
150	KK	B35NL									
151	KM	BRING BACK DIVERTED HYDROGRAPH FROM C35N									
152	DR	D35NL									
	*										
153	KK	R35NL									
154	KM	NORMAL DEPTH CHANNEL ROUTE FROM S35N TO C36R1									
155	KM	SOURCE: 1993 MAPPING (2' CI) PROVIDED BY COS									
156	RS	5	FLOW	-1							
157	RC	0.06	0.04	0.06	14480	0.0318					
158	RX	1000	1040	1080	1086	1091	1097	1137	1174		
159	RY	105	104	103	100	100	103	104	105		
	*										
160	KK	B36.2L									
161	KM	BRING BACK DIVERTED HYDROGRAPH FROM C36.2									
162	DR	D36.2L									
	*										

LINE	ID	1	2	3	4	5	6	7	8	9	10
163	KK	R36.2L									
164	KM	NORMAL DEPTH CHANNEL ROUTE FROM C36.2 TO C36R1									
165	KM	SOURCE: 1993 MAPPING (2' CI) PROVIDED BY COS									
166	RS	3	FLOW	-1							
167	RC	0.06	0.04	0.06	10160	0.0342					
168	RX	1000	1030	1060	1066	1076	1082	1112	1142		
169	RY	103	102.5	102	100	100	102	102.5	103		
	*										
170	KK	S36R1									
171	KM	RUNOFF FROM SUBBASIN 36R1									
172	KM	RAINFALL LOSSES FOR GREINER SUBBASINS 36.3, 36R1 AND 35R ARE AREA WEIGHT									
173	BA	1.2173									
174	LS		74.3	10							
175	UK	300	0.020	0.200	100						
176	RK	1420	0.032	0.045	0.0061	TRAP	0	13			
177	RK	12600	0.033	0.040		TRAP	10	9			
	*										
178	KK	C36R1									
179	KM	COMBINE ROUTED HYDROGRAPH FROM C36.1, D35NL & D36.2L W/RUNOFF FROM S36R1									
180	KM	AREA IS AREA FROM C36.1 + S36R1 + 40% OF AREA FROM S35N + 30% OF AREA									
181	KM	FROM C36.2									
182	HC	4	4.6393								
	*										
183	KK	R36R1									
184	KM	NORMAL DEPTH CHANNEL ROUTE FROM C36R1 TO C36R2 THROUGH PIMA CHANNEL									
185	RS	1	FLOW	-1							
186	RC	0.035	0.025	0.035	4000	0.01					
187	RX	1000	1020	1022	1034	1084	1096	1098	1118		
188	RY	111.4	106.4	106.3	100	100	106.3	106.4	111.4		
	*										
189	KK	S36R2									
190	KM	RUNOFF FROM SUBBASIN 36R2									
191	BA	0.4258									
192	LS		72	16							
193	UK	280	0.045	0.100	100						
194	RK	1900	0.032	0.017	0.015	TRAP	15	7			
195	RK	8860	0.030	0.040		TRAP	30	10			
	*										
196	KK	C36R2									
197	KM	COMBINE ROUTED HYDROGRAPH FROM C36R1 W/RUNOFF FROM SUBBASIN 36R2									
198	HC	2	5.07								
	*										
199	KK	S51.1									
200	KM	RUNOFF FROM SUBBASIN 51.1									
201	KM	RAINFALL LOSSES FOR GREINER SUBBASINS 51.1 AND 49.1 ARE AREA WEIGHTED									
202	BA	1.0784									
203	LS		73.9	12							
204	UK	300	0.037	0.130	100						









LINE	ID	1	2	3	4	5	6	7	8	9	10
313	KK	51C1R									
314	KM	ROUTE 51C1D THROUGH SUBBASIN 52C1									
315	RK	1350	.0364	.045			TRAP	10		10	
	*										
316	KK	52C1									
317	KM	RUNOFF FROM SUBBASIN 52C1									
318	BA	.029									
319	LS		75	20.5							
320	UK	100	.02	.10	100						
321	RK	1350	.021	.045			TRAP	30		10	
	*										
322	KK	52C1C									
323	KM	COMBINE 51C1R AND 52C1									
324	HC	2	.0611								
	*										
325	KK	52C1R									
326	KM	ROUTE 52C1C THROUGH BASIN 52C2A TO CP 52C2BC									
327	RK	1500	.033	.045			TRAP	10		10	
	*										
328	KK	52C2A									
329	KM	RUNOFF FROM SUBBASIN 52C2A									
330	BA	.019									
331	LS		75	2							
332	UK	100	.02	.10	100						
333	RK	1500	.033	.045			TRAP	30		10	
	*										
334	KK	52C2AC									
335	KM	COMBINE 52C2A AND 52C1R									
336	HC	2									
	*										
337	KK	52C2B									
338	KM	RUNOFF FROM SUBBASIN 52C2B									
339	BA	.0275									
340	LS		75	11							
341	UK	100	.02	.10	100						
342	RK	2000	.030	.045			TRAP	30		10	
	*										
343	KK	52C2BC									
344	KM	COMBINE 52C2B AND 52C2AC									
345	HC	2									
	*										

LINE	ID	1	2	3	4	5	6	7	8	9	10
346	KK	52C2BR									
347	KM	ROUTE 52C2BC THROUGH 52C2C TO CP 52C2CC									
348	RK	1500	.040	.045			TRAP	10		10	
	*										
349	KK	52C2C									
350	KM	RUNOFF FROM SUBBASIN 52C2C									
351	BA	.014									
352	LS		75	62							
353	UK	100	.02	.10	100						
354	RK	1500	.04	.045			TRAP	30		10	
	*										
355	KK	52C2CC									
356	KM	COMBINE 52C2C AND 52C2BR									
357	HC	2									
	*										
358	KK	52C2R									
359	KM	ROUTE 52C2CC THROUGH SUBBASIN 52C4 TO CP 52C4C1									
360	RK	1550	.030	.045			TRAP	10		10	
	*										
361	KK	52C4									
362	KM	RUNOFF FROM SUBBASIN 52C4									
363	BA	.017									
364	LS		75	60							
365	UK	100	.02	.10	100						
366	RK	1550	.030	.045			TRAP	30		10	
	*										
367	KK	52C4C1									
368	KM	COMBINE 52C4 AND 52C2R									
369	HC	2									
	*										
370	KK	52C4C2									
371	KM	COMBINE 52C4C1 AND 52C3BR									
372	HC	2									
	*										
373	KK	52C4R									
374	KM	ROUTE 52C4C2 WEST IN BEARDSLEY CHANNEL TO CP 52C15C2									
375	RK	850	.0143	.035			TRAP	50		4	
	*										
376	KK	52C13									
377	KM	RUNOFF FROM SUBBASIN 52C13									
378	BA	.023									
379	LS		75	31							
380	UK	100	.02	.10	100						
381	RK	950	.040	.045			TRAP	30		10	
	*										

LINE	ID	1	2	3	4	5	6	7	8	9	10
382	KK	2C13DV									
383	KM	DIVERT FIRST 40 CFS INTO STORM DRAIN; REMAINDER FLOWS OVER ROAD									
384	DT	STORM									
385	DI	0	40	1000							
386	DQ	0	40	40							
	*										
	*	KK52C13R									
	*	KM ROUTE 52C13 THROUGH SUBBASIN 52C15 TO CP 52C15C1									
	RK	1800	.035	.045	TRAP		10	10			
	*										
387	KK	52C15									
388	KM	RUNOFF FROM SUBBASIN 52C15									
389	BA	.046									
390	LS	75		64.4							
391	UK	100	.02	.10	100						
392	RK	2050	.036	.045	TRAP		30	10			
	*										
393	KK	2C15C1									
394	KM	COMBINE 52C15 AND 52C13DV									
395	HC	2	.046								
	*										
396	KK	2C15C2									
397	KM	COMBINE 52C15C1 AND 52C4R									
398	HC	2									
	*										
399	KK	52C15R									
400	KM	ROUTE 52C15C2 IN BEARDSLEY CHANNEL TO CP 52C14C3									
401	RK	750	.0143	.035	TRAP		50	4			
	*										
402	KK	52C14A									
403	KM	RUNOFF FROM SUBBASIN 52C14A									
404	BA	.041									
405	LS	75		67.7							
406	UK	100	.02	.10	100						
407	RK	2050	.031	.045	TRAP		30	10			
	*										
408	KK	2C14AC									
409	KM	COMBINE 52C14A AND 52C15R									
410	HC	2									
	*										
411	KK	2C14AR									
412	KM	ROUTE 52C14AC IN BEARDSLEY CHANNEL TO CP 52C14BC2									
413	RK	380	.0143	.035	TRAP		50	4			
	*										
	*										

LINE	ID	1	2	3	4	5	6	7	8	9	10
414	KK	51C1DV									
415	KM	RETRIEVE DIVERTED FLOW									
416	DR	51C1DV									
	*										
417	KK	51C2D									
418	KM	DIVERT 27 PERCENT OF 51C1DV TO WEST (73 PERCENT TO SOUTH)									
419	DT	51C2DV									
420	DI	0	10000								
421	DQ	0	2700								
	*										
422	KK	51C2R									
423	KM	ROUTE 51C2D THROUGH SUBBASIN 52C5 TO CP 52C5C									
424	RK	700	.030	.045			TRAP	10	10		
	*										
425	KK	52C5									
426	KM	RUNOFF FROM SUBBASIN 52C5									
427	BA	.016									
428	LS		75	27							
429	UK	100	.02	.10	100						
430	RK	1200	.03	.045			TRAP	30	10		
	*										
431	KK	52C5C									
432	KM	COMBINE 51C2R AND 52C5									
433	HC	2	.0635								
	*										
434	KK	52C5R									
435	KM	ROUTE 52C5C THROUGH SUBBASIN 52C6 TO CP 52C6C									
436	RK	3100	.035	.045			TRAP	10	10		
	*										
437	KK	52C6									
438	KM	RUNOFF FROM SUBBASIN 52C6									
439	BA	.036									
440	LS		75	31.4							
441	UK	100	.02	.10	100						
442	RK	3100	.035	.045			TRAP	30	10		
	*										
443	KK	52C6C									
444	KM	COMBINE 52C5R AND 52C6									
445	HC	2									
	*										
446	KK	52C6R									
447	KM	ROUTE 52C6C THROUGH SUBBASIN 52C10 TO CP 52C10C2									
448	RK	450	.032	.045			TRAP	10	10		
	*										

LINE	ID	1	2	3	4	5	6	7	8	9	10
449	KK	51C2DV									
450	KM	RETRIEVE 52C2DV									
451	DR	51C2DV									
	*										
452	KK	51C3R									
453	KM	ROUTE 52C2DV THROUGH SUBBASIN 52C7 TO CP 52C7C									
454	RK	700	.040	.045			TRAP	10		10	
	*										
455	KK	51B	SUB								
456	KM	RUNOFF FROM SUB 51B									
457	BA	.5711									
458	LS	0	71.9	13.1							
459	UK	100	.0213	.10	100						
460	RK	8900	.0300	.045			TRAP	50		25	
	*										
461	KK	51B1D									
462	KM	DIVERT 92 PERCENT OF SUBBASIN 51B TO WEST (8 PERCENT TO SOUTH)									
463	DT	51B1DV									
464	DI	0	10000								
465	DQ	0	9200								
	*										
466	KK	51B1R									
467	KM	ROUTE 51B1D THROUGH SUBBASIN 52C7 TO CP 52C7C									
468	RK	450	.04	.045			TRAP	10		10	
	*										
469	KK	52C7									
470	KM	RUNOFF FROM SUBBASIN 52C7									
471	BA	.006									
472	LS		75	27							
473	UK	100	.02	.10	100						
474	RK	550	.04	.045			TRAP	30		10	
	*										
475	KK	52C7C									
476	KM	COMBINE 51B1R, 51C3R, AND 52C7									
477	HC	3	.0693								
	*										
478	KK	52C7R									
479	KM	ROUTE 52C7C THROUGH SUBBASIN 52C9 TO CP 52C9C1									
480	RK	1550	.036	.045			TRAP	10		10	
	*										
481	KK	51B1DV									
482	KM	RETRIEVE DIVERTED FLOW 51B1DV									
483	DR	51B1DV									
	*										



LINE	ID	1	2	3	4	5	6	7	8	9	10
519	KK	52C9R2									
520	KM	ROUTE 52C9C2 THROUGH SUBBASIN 52C10 TO CP 52C10C1									
521	RK	500	.032	.045			TRAP	10		10	
	*										
522	KK	2C10C1									
523	KM	COMBINE 52C9R2 AND 52C6R									
524	HC	2									
	*										
525	KK	2C10R1									
526	KM	ROUTE 52C10C1 THROUGH SUBBASIN 52C10 TO CP 52C10C2									
527	RK	300	.032	.045			TRAP	10		10	
	*										
528	KK	52C10									
529	KM	RUNOFF FROM SUBBASIN 52C10									
530	BA	.014									
531	LS		75	7.85							
532	UK	100	.02	.10	100						
533	RK	800	.032	.045			TRAP	30		10	
	*										
534	KK	2C10C2									
535	KM	COMBINE 52C10R1 AND 52C10									
536	HC	2									
	*										
537	KK	52C11									
538	KM	RUNOFF FROM SUBBASIN 52C11									
539	BA	.0425									
540	LS		75	27							
541	UK	100	.02	.10	100						
542	RK	2800	.031	.045			TRAP	30		10	
	*										
543	KK	2C11R1									
544	KM	PIPE ROUTE 52C11 TO CP 52C11C									
545	RK	650	.02	.045			CIRC		3		
	*										
546	KK	52C13D									
547	KM	RETRIEVE DIVERTED FLOW									
548	DR	STORM									
	*										
549	KK	52C11C									
550	KM	COMBINE 52C13D AND 52C11R1									
551	HC	2 .0655									
	*										

LINE	ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
552	KK 2C11CR
553	KM PIPE ROUTE 52C11C TO CP 52C11C2
554	RK 750 .02 .045 CIRC 3
	*
555	KK 2C11C2
556	KM COMBINE 52C11CR AND 52C10C2
557	HC 2
	*
558	KK 2C11R2
559	KM ROUTE 52C11C2 THROUGH SUBBASIN 52C12 TO CP 52C12C
560	RK 700 .03 .045 TRAP 10 10
	*
561	KK 52C12
562	KM RUNOFF FROM SUBBASIN 52C12
563	BA .023
564	LS 75 85
565	UK 100 .02 .10 100
566	RK 900 .03 .045 TRAP 30 10
	*
567	KK 52C12C
568	KM COMBINE 52C11R2 AND 52C12
569	HC 2
	*
570	KK 52C12R
571	KM ROUTE 52C12C THROUGH SUBBASIN 52C14 TO CP 52C14C1
572	RK 1150 .029 .045 TRAP 10 10
	*
573	KK 52C14B
574	KM RUNOFF FROM SUBBASIN 52C14B
575	BA .021
576	LS 75 60
577	UK 100 .02 .10 100
578	RK 1250 .029 .045 TRAP 30 10
	*
579	KK C14BC1
580	KM COMBINE 52C14B AND 52C12R
581	HC 2
	*
582	KK C14BC2
583	KM COMBINE 52C14BC1 AND 52C14AR
584	HC 2
	*



LINE	ID	1	2	3	4	5	6	7	8	9	10
619	KK	51B4R1									
620	KM	ROUTE 51B4D THROUGH SUBBASIN 52B2 TO CP 52B2C1									
621	RK	1350	.037	.045			TRAP	10		10	
	*										
622	KK	52B2C1									
623	KM	COMBINE 51B4R1 AND 52B1R									
624	HC	2	.1403								
	*										
625	KK	52B2R1									
626	KM	ROUTE 52B2R1 THROUGH SUBBASIN 52B2 TO CP 52B2C2									
627	RK	1000	.037	.045			TRAP	10		10	
	*										
628	KK	52B2									
629	KM	RUNOFF FROM SUBBASIN 52B2									
630	BA	.032									
631	LS		75	17							
632	UK	100	.02	.10	100						
633	RK	2350	.037	.045			TRAP	30		10	
	*										
634	KK	52B2C2									
635	KM	COMBINE 52B2 AND 52B2R1									
636	HC	2									
	*										
637	KK	52B2R2									
638	KM	ROUTE 52B2C2 THROUGH SUBBASIN 52B3 TO CP 52B3C2									
639	RK	850	.026	.045			TRAP	10		10	
	*										
640	KK	52B3R1									
641	KM	ROUTE 52B3C1 THROUGH SUBBASIN 52B3 TO CP 52B3C2									
642	RK	500	.024	.045			TRAP	10		10	
	*										
643	KK	52B3									
644	KM	RUNOFF FROM SUBBASIN 52B3									
645	BA	.062									
646	LS		75	31.8							
647	UK	100	.02	.10	100						
648	RK	3450	.030	.045			TRAP	30		10	
	*										
649	KK	52B3C2									
650	KM	COMBINE 52B3 AND 52B3R1									
651	HC	2									
	*										

LINE	ID	1	2	3	4	5	6	7	8	9	10
652	KK	52B3R2									
653	KM	ROUTE 52B3C2 THROUGH 52B4 TO CP 52B4C									
654	RK	1700	.024	.045			TRAP	10		10	
	*										
655	KK	52B4									
656	KM	RUNOFF FROM SUBBASIN 52B4									
657	BA	.026									
658	LS		75	62							
659	UK	100	.02	.10	100						
660	RK	1700	.024	.045			TRAP	30		10	
	*										
661	KK	52B4C									
662	KM	COMBINE 52B4 AND 52B3R2									
663	HC	2									
	*										
664	KK	52B4R									
665	KM	ROUTE 52B4C THROUGH SUBBASIN 52B5 TO CP 52B5C1									
666	RK	550	.027	.045			TRAP	10		10	
	*										
667	KK	52B5									
668	KM	RUNOFF FROM SUBBASIN 52B5									
669	BA	.021									
670	LS		75	56.9							
671	UK	100	.02	.10	100						
672	RK	1400	.03	.045			TRAP	30		10	
	*										
673	KK	52B5C1									
674	KM	COMBINE 52B5 AND 52B4R									
675	HC	2									
	*										
676	KK	52B5C2									
677	KM	COMBINE 52B5C1 AND 52C14R									
678	HC	2									
	*										
679	KK	52B5R									
680	KM	ROUTE 52B5C2 IN BEARDSLEY CHANNEL TO CP 52B7C2									
681	RK	1100	.0143	.035			TRAP	50		4	
	*										
682	KK	51B4DV									
683	KM	RETRIEVE DIVERTED FLOW 51B4DV									
684	DR	51B4DV									
	*										

LINE	ID	1	2	3	4	5	6	7	8	9	10
685	KK	51B5D									
686	KM	DIVERT 68 PERCENT OF 51B4DV TO WEST (32 PERCENT TO SOUTH)									
687	DT	51B5DV									
688	DI	0	10000								
689	DQ	0	6800								
	*										
690	KK	51B5R									
691	KM	ROUTE 51B5D THROUGH SUBBASIN 52B6 TO CP 51B7C									
692	RK	1250	.035	.045	TRAP	10	10				
	*										
693	KK	51B5DV									
694	KM	RETRIEVE DIVERTED FLOW									
695	DR	51B5DV									
	*										
696	KK	51B6D									
697	KM	DIVERT 53 PERCENT OF 51B5DV TO WEST (47 PERCENT TO SOUTH)									
698	DT	51B6DV									
699	DI	0	10000								
700	DQ	0	5300								
	*										
701	KK	51B6R									
702	KM	ROUTE 51B6D THROUGH SUBBASIN 52B6 TO CP 51B7C									
703	RK	925	.033	.045	TRAP	10	10				
	*										
704	KK	51B6DV									
705	KM	RETRIEVE DIVERTED FLOW 51B6DV									
706	DR	51B6DV									
	*										
707	KK	51B7D									
708	KM	DIVERT 58 PERCENT OF 51B6DV TO WEST (42 PERCENT TO SOUTH)									
709	DT	51B7DV									
710	DI	0	10000								
711	DQ	0	5800								
	*										
712	KK	51B7R1									
713	KM	ROUTE 51B7D THROUGH SUBBASIN 52B6 TO CP 51B7C									
714	RK	530	.033	.045	TRAP	10	10				
	*										
715	KK	51B7C									
716	KM	COMBINE 51B7R1, 51B5R, AND 51B6R									
717	HC	3	.2404								
	*										



LINE	ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
751	KK 52A2C2
752	KM COMBINE 52B7C2 AND 52A2
753	HC 2 1.62
	*
754	KK 51B7DV
755	KM RETRIEVE DIVERTED FLOW 51B7DV
756	DR 51B7DV
	*
757	KK 51B8R
758	KM ROUTE 51B7DV THROUGH SUBBASIN 52A1 TO CP 52A1C
759	RK 3400 .033 .045 TRAP 10 10
	*
760	KK 52A1
761	KM RUNOFF FROM SUBBASIN 52A1
762	BA .130
763	LS 75 32.25
764	UK 100 .02 .10 100
765	RK 3400 .033 .045 TRAP 30 10
	*
766	KK 52A1C
767	KM COMBINE 52A1 AND 51B8R
768	HC 2
	*
	*
	***** END DC RANCH WATERSHED *****
	*
	*
	***** BEGIN GVSCE MODIFICATIONS *****
	*
769	KK D51.1
770	KM RETRIEVE DIVERTED FLOW
771	DR B51.1T
	*
772	KK C52A
773	KM COMBINE ROUTED HYDROGRAPH FROM C51.1 WITH HYDROGRAPH FROM C52A1C AT
774	KM THOMPSON PEAK PARKWAY
775	HC 2 6.2735
	*
776	KK R52A
777	KM NORMAL DEPTH CHANNEL ROUTE FROM C52A TO C52 THROUGH PIMA CHANNEL
778	RS 1 FLOW -1
779	RC 0.035 0.025 0.035 2700 0.01
780	RX 1000 1020 1022 1034 1084 1096 1098 1118
781	RY 111.4 106.4 106.3 100 100 106.3 106.4 111.4
	*

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

782 KK C52  
 783 KM COMBINE ROUTED HYDROGRAPH FROM C52A WITH HYDROGRAPH FROM C52A2C AT  
 784 KM BEARDSLEY ROAD  
 785 HC 2 7.9160  
 \*

786 KK R52  
 787 KM NORMAL DEPTH CHANNEL ROUTE FROM C52 TO C53 THROUGH PIMA CHANNEL  
 788 RS 1 FLOW -1  
 789 RC 0.035 0.025 0.035 3600 0.01  
 790 RX 1000 1020 1022 1034 1084 1096 1098 1118  
 791 RY 111.4 106.4 106.3 100 100 106.3 106.4 111.4  
 \*

792 KK D52T  
 793 KM DIVERT 100% OF FLOW TO RETRIEVE JUST U/S OF UNION HILLS DETENTION BASIN  
 794 DT B52T  
 795 DI 0 10000  
 796 DQ 0 10000  
 \*

797 KK CLEAR  
 798 KM CLEAR HYDROGRAPHS FROM STACK  
 799 HC 2  
 \*

\*\*\*\*\* BEGIN GREYHAWK WATERSHED \*\*\*\*\*

THE GREYHAWK HEC-1 MODEL (VILLAGES II AND III) WAS DEVELOPED BY DEI  
 DEI FILE NAME: GH23FAB.H11  
 MODEL DATE: 21 MAY 96

800 KK 37A SUB  
 801 KM RUNOFF FROM SUB-BASIN 37A  
 802 BA .6765  
 803 LS 74 24.8  
 804 UK 61 .0213 .10 100  
 805 RK 4800 .0237 .045 TRAP 50 130  
 \*

806 KK 37AE DIV  
 807 KM SPLIT FLOWS AT SOUTH BOUNDARY OF SUB 37A FOR ROUTING TO DETENTION  
 808 KM BASIN 53R & 38R-1. THIS DIVERT OPERATION REFLECTS THE BREAK IN THE  
 809 KM DEER VALLEY ROAD CHANNEL BETWEEN HAYDEN & PIMA ROADS. THIS SPLIT IS  
 810 KM BASED ON NEW CORE NORTH PLAN DEVELOPED BY G.W. LARSON & ASSC., INC.  
 811 KM DATED 6/16/92. DIVERT RATIO IS BASED ON APPROXIMATE D.A. FROM SUB 37A  
 812 KM THAT IS INTERCEPTED BY EACH CHANNEL SEGMENT ALONG DEER VALLEY ROAD.  
 813 KM  
 814 KM (THIS SPLIT HAS BEEN UPDATED FROM THE OLP.6 MODEL TO REFLECT A 30% SPLIT  
 815 KM TO THE SOUTH AND A 70% SPLIT TO THE WEST FOR THIS STUDY AND IS BASED ON  
 816 KM UPSTREAM CONTRIBUTING WATERSHED AREA TO THIS CONCENTRATION POINT)  
 817 DT 37AW  
 818 DI 0 100 500 1000 1500  
 819 DQ 0 70 350 700 1050

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

820 KK 37AE1 CP  
 821 KM ROUTE NON-DIVERTED FLOW FROM DIV 37AE THROUGH SUB 5N. THIS IS A  
 822 KM PRELIMINARY CHANNEL CONFIGURATION FOR THE GOLF COURSE CHANNEL.  
 823 RS 1 FLOW  
 824 RC .055 .045 .055 800 .025  
 825 RX 0 16 26 30 40 44 54 70  
 826 RY 6 2 2 0 0 2 2 6  
 \*

827 KK SUB5N  
 828 KM RUNOFF FROM SUBBASIN 5 IN NORTH 18 MODEL.  
 829 BA 0.029  
 830 LS 77 18  
 831 UK 100 .013 .15 100  
 832 RK 1000 0.005 .018 .015 TRAP 50 20  
 833 RK 500 .015 .025 TRAP 10 4  
 \*

834 KK CP5N  
 835 KM ADD HYDROGRAPHS AT CP5N  
 836 HC 2 0.232  
 \*

837 KK RET5N  
 838 KM ROUTE FLOW THROUGH RETENTION BASIN NO. 5. 18" PIPE OUTFLOW WILL  
 839 KM BLEED FLOWS TO DRAIN THE BASIN AFTER THE STORM HAS PASSED.  
 840 RS 1 STOR 0 0  
 841 SV 0 .04 .33 .93 1.8 2.35 3.16 4.2 6.1  
 842 SQ 0 8 10 12 15 17 102 191 668  
 843 SE 1797 1798 1800 1802 1804 1805 1806 1807 1808  
 \*

844 KK R6N.1  
 845 KM ROUTE FLOW FROM CP5 TO CP6 IN NORTH 18 MODEL  
 846 KM ASSUME CHANNEL IS SAME CONFIGURATION AS ABOVE FOR PROPOSED GOLF COURSE  
 847 KM CHANNEL.  
 848 RS 1 FLOW  
 849 RC .055 .045 .055 2200 .025  
 850 RX 0 16 26 30 40 44 54 70  
 851 RY 6 2 2 0 0 2 2 6  
 \*

852 KK SUB6B  
 853 KM RUNOFF FROM WEST PORTION OF EXISTING SUB6N ADJACENT TO CHANNEL  
 854 BA .032  
 855 LS 81 0  
 856 UK 200 .025 .15 100  
 857 RK 1300 .015 .025 TRAP 10 4  
 \*



LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

894 KK R2NB  
 895 KM ROUTE FLOW FROM CP2NA TO CP2NB  
 896 RS 1 FLOW  
 897 RC .03 .03 .03 1050 .015  
 898 RX 0 8 13 17 22 26 31 39  
 899 RY 4 2 2 0 0 2 2 4  
 \*

900 KK SUB2NB  
 901 KM RUNOFF FROM SUBBASIN 2NB  
 902 BA .03  
 903 LS 77 53  
 904 UK 150 .013 .15 100  
 905 RK 1200 .015 .025 TRAP 20 50  
 \*

906 KK CP2NB  
 907 KM ADD HYDROGRAPHS AT CP2NB  
 908 HC 2  
 \*

909 KK SR2NB  
 910 KM STORAGE ROUTE FLOW THROUGH DETENTION BASIN IN SUB2NB  
 911 RS 1 STOR 0 0  
 912 SV 0 .19 .69 1.66 3.23 4.5  
 913 SQ 0 2 8 12 17 170  
 914 SE 1796 1798 1800 1802 1804 1805  
 \*

915 KK RCP4N  
 916 KM ROUTE FLOW FROM CP2NB TO CP4N  
 917 RS 1 FLOW  
 918 RC .03 .03 .03 740 .018  
 919 RX 0 8 13 17 22 26 31 39  
 920 RY 4 2 2 0 0 2 2 4  
 \*

921 KK SUB6N  
 922 KM RUNOFF FROM SUBBASIN 6 IN NORTH 18 MODEL. TO LAKE NORTH OF CLUBHOUSE.  
 923 BA .049  
 924 LS 81 0  
 925 UK 200 .025 .15 100  
 926 RK 1300 .015 .025 TRAP 10 4  
 \*

927 KK RET6N  
 928 KM RETENTION ROUTING THROUGH LAKE AT HOLE 18, NORTH COURSE.  
 929 RS 1 STOR  
 930 SV 0 3.01 6.64 10.75 13.09 15.90  
 931 SQ 0 0 0 10 26 100  
 932 SE 1782 1784 1786 1788 1789 1790  
 \*

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

933 KK RCP4N1  
 934 KM ROUTE FLOW FROM CP6N TO CP4N  
 935 RS 1 FLOW  
 936 RC .03 .03 .03 550 .018  
 937 RX 0 8 13 17 22 26 31 39  
 938 RY 4 2 2 0 0 2 2 4  
 \*

939 KK CP4N.1  
 940 KM ADD HYDROGRAPHS AT CP4N.1  
 941 HC 2  
 \*

942 KK SUB3N  
 943 KM RUNOFF FROM SUBBASIN 3N, NORTH 18 MODEL  
 944 BA .027  
 945 LS 81 0  
 946 UK 100 .02 .15 100  
 947 RK 2800 0.0207 .025 TRAP 10 4  
 \*

948 KK RET3N  
 949 KM ROUTE FLOW THROUGH RETENTION BASIN NO. 3. 18" PIPE OUTFLOW WILL  
 950 KM BLEED FLOWS TO DRAIN THE BASIN AFTER THE STORM HAS PASSED.  
 951 RS 1 STOR 0 0  
 952 SV 0 1.73 8.97 13.32 15.74  
 953 SQ 0 4 7 9 11  
 954 SE 1793 1795 1800 1803 1804  
 \*

955 KK R4N  
 956 KM ROUTE FLOW FROM CP3N TO CP4N IN NORTH MODEL  
 957 RS 1 FLOW  
 958 RC .035 .035 .035 950 .018  
 959 RX 0 8 13 17 22 26 31 39  
 960 RY 4 2 2 0 0 2 2 4  
 \*

961 KK CP4N.2  
 962 KM ADD HYDROGRAPHS AT CPN.2  
 963 HC 2  
 \*

964 KK SUB4N  
 965 KM RUNOFF FROM SUBBASIN 4N.  
 966 BA .032  
 967 LS 77 18  
 968 UK 100 .015 .15 100  
 969 RK 1200 0.007 .018 TRAP 50 20  
 \*





LINE	ID	1	2	3	4	5	6	7	8	9	10	
1041	KK	SUB4S										
1042	KM	RUNOFF FROM SUB BASIN 4 SOUTH COURSE										
1043	BA	.0273										
1044	LS		77	53								
1045	UK	100	.010	.15	100							
1046	RK	1780	.018	.015		TRAP	50	20				
	*											
1047	KK	RT4S										
1048	KM	ROUTE FLOW FROM CP4S TO CPGC28										
1049	RS	1	FLOW	0	0							
1050	RC	.035	.035	.035	650	.015						
1051	RX	0	20	30	40	45	55	65	75			
1052	RY	1750	1746	1744	1742	1742	1744	1746	1750			
	*											
1053	KK	GC2-8										
1054	KM	RUNOFF FROM SOUTH GOLF COURSE HOLES NO. 2 AND 8										
1055	BA	.014										
1056	LS		81	0								
1057	UK	200	.025	.15	100							
1058	RK	980	.016	.025		TRAP	10	4				
	*											
1059	KK	1PGC28										
1060	KM	ADD HYDROGRAPHS AT CPGC28 AT PROPOSED LOOP ROAD, SOUTH COURSE										
1061	HC	3										
	*											
1062	KK	SUB3D3										
1063	KM	RUNOFF FROM GRAYHAWK ROAD SOUTH OF THOMPOSON PEAK										
1064	BA	.014										
1065	LS		81	0								
1066	UK	50	.015	.1	100							
1067	RK	2450	.016	.025		TRAP	5	4				
	*											
1068	KK	CPGC28										
1069	KM	ADD HYDROGRAPHS AT CPGC28 AT PROPOSED LOOP ROAD, SOUTH COURSE										
1070	HC	2										
	*											
1071	KK	SRGC28										
1072	KM	STORAGE THRU DETENTION BASIN ON HOLES 2 AND 8.										
1073	RS	1	STOR	0	0							
1074	SV	0	.018	.085	.22	.5	1.0	1.7	2.68	3.9		
1075	SE	1706	1707	1708	1709	1710	1711	1712	1713	1714		
1076	SQ	0	10	18	20	30	108	324	651	1070		
	*											

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

1077 KK RT7S  
 1078 KM ROUTE FLOW FROM SRGC28 TO CP7S  
 1079 RS 1 STOR 0 0  
 1080 RC .055 .045 .055 1700 .0187  
 1081 RK 0 20 30 40 60 70 80 100  
 1082 RY 1750 1746 1744 1742 1742 1744 1746 1750  
 \*

1083 KK GC7  
 1084 KM RUNOFF FROM SOUTH GOLF COURSE HOLE NO. 7  
 1085 BA .0134  
 1086 LS 81 0  
 1087 UK 200 .025 .15 100  
 1088 RK 1380 .020 .025 TRAP 10 4  
 \*

1089 KK CP7S  
 1090 KM ADD HYDROGRAPHS AT CP7S ON SOUTH COURSE  
 1091 HC 2 0.6083  
 \*

1092 KK D7ST  
 1093 KM D7ST IS A DIVERSION ADDED BY GVSCE IN ORDER TO ROUTE RUNOFF TO THE  
 1094 KM UNION HILLS DETENTION BASIN VIA THE POWER LINE CHANNEL.  
 1095 KM  
 1096 KM DIVERT 100% OF FLOW  
 1097 DT B7ST  
 1098 DI 0 10000  
 1099 DQ 0 10000  
 \*

1100 KK CLEAR  
 1101 KM CLEAR HYDROGRAPHS FROM THE STACK.  
 1102 HC 2  
 \*  
 \*  
 \* THIS PORTION OF MODEL TAKEN FROM, "DRAINAGE REPORT FOR VILLAGE 3 - PHASE 1",  
 \* APPROVED BY THE CITY OF SCOTTSDALE 7-19-95. MODIFIED TO ACCOUNT FOR ASBUILT  
 \* CONDITION  
 \*  
 \*  
 \*  
 \*

1103 KK SUB3D1  
 1104 KM RUNOFF FROM SUBBASIN 3D1, PARCEL 3D.  
 1105 BA .0088  
 1106 LS 77 34  
 1107 UD .06  
 \*

LINE	ID	1	2	3	4	5	6	7	8	9	10
1108	KK	RD1B1									
1109	KM	FOUTE FLOW FROM 3D1 TO 3B1									
1110	RS	1	FLOW	-1							
1111	RC	0.03	0.03	0.03	1250	.015					
1112	RX	0	0.5	1	7	12	19	19.5	20		
1113	RY	3.2	3.1	3.0	1.0	1.0	3.0	3.1	3.2		
	*										
1114	KK	SUB3B1									
1115	KM	RUNOFF FROM SUBBASIN 3B1, PARCEL 3B.									
1116	BA	.0137									
1117	LS		77	47							
1118	UD	.06									
	*										
1119	KK	CP3B1									
1120	KM	ADD HYDROGRAGHS AT CP3B1									
1121	HC	2									
	*										
1122	KK	RB13F									
1123	KM	ROUTE FLOW FROM 3B1 TO SUB3F									
1124	RS	1	FLOW	-1							
1125	RC	0.03	0.03	0.03	2150	.015					
1126	RX	0	0.5	1	7	17	24	24.5	25		
1127	RY	3.2	3.1	3.0	1.0	1.0	3.0	3.1	3.2		
	*										
1128	KK	SUB3F									
1129	KM	RUNOFF FROM SUBBASIN 3F, PARCEL 3F, SOUTH COURSE MODEL.									
1130	BA	.0344									
1131	LS		77	68							
1132	UK	100	.025	.15	100						
1133	RK	1000	.015	.025		TRAP	100	20			
	*										
1134	KK	CP3F									
1135	KM	ESTIMATED PEAK DISCHARGE RATE AT POINT CP3F ALONG THE POWER CORRIDOR									
1136	HC	2									
	*										
1137	KK	SUB3B2									
1138	KM	RUNOFF FROM SUBBASIN 3B2, PARCEL 3B.									
1139	BA	.0246									
1140	LS		77	40							
1141	UD	.10									
	*										
1142	KK	RB2E1									
1143	KM	1/2 OF ENTIRE ROUTING REACH FROM 3B2 TO CP3E1									
1144	RS	1	FLOW	-1							
1145	RC	0.03	0.03	0.03	800	0.02					
1146	RX	0	0.5	1	7	17	24	24.5	25		
1147	RY	3.2	3.1	3.0	1.0	1.0	3.0	3.1	3.2		

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

1148	KK	RB2E2								
1149	KM	SECOND 1/2 OF ENTIRE ROUTING REACH FROM 3B2 TO CP3E1								
1150	RS	1	FLOW	-1						
1151	RC	0.03	0.03	0.03	600	.015				
1152	RX	0	0.5	1	7	17	24	24.5	25	
1153	RY	3.2	3.1	3.0	1.0	1.0	3.0	3.1	3.2	
		*								
1154	KK	SUB3E1								
1155	KM	RUNOFF FROM SUBBASIN 3E1, PARCEL 3E.								
1156	BA	.0246								
1157	LS		77	40						
1158	UD	.10								
		*								
1159	KK	1CPE31								
1160	KM	ESTIMATED PEAK DISCHARGE RATE AT POINT CP3E1 ALONG THE POWER CORRIDOR								
1161	HC	2								
		*								
1162	KK	SUB3D2								
1163	KM	RUNOFF FROM SUBBASIN 3D2, PARCEL 3D.								
1164	BA	.022								
1165	LS		77	35						
1166	UD	.08								
		*								
1167	KK	RD2E2								
1168	KM	ROUTE EXCESS FROM 3D2 TO CP3E2								
1169	RS	1	FLOW	-1						
1170	RC	0.03	0.03	0.03	1200	.0216				
1171	RX	0	0.5	1	7	17	24	24.5	25	
1172	RY	3.2	3.1	3.0	1.0	1.0	3.0	3.1	3.2	
		*								
1173	KK	SUB3E2								
1174	KM	RUNOFF FROM SUBBASIN 3E2, PARCEL 3E.								
1175	BA	.012								
1176	LS		77	35						
1177	UD	.06								
		*								
1178	KK	CP3E2								
1179	KM	ESTIMATED PEAK DISCHARGE RATE AT POINT CP3E2 ALONG THE POWER CORRIDOR								
1180	HC	2								
		*								
1181	KK	PC3								
1182	KM	PC3 IS A SUBBASIN ADDED BY GVSCE TO ESTIMATE THE SURFACE RUNOFF FROM								
1183	KM	THE POWER LINE CORRIDOR WHICH ENTERS THE POWER LINE CHANNEL								
1184	KM									
1185	KM	RUNOFF FROM SUBBASIN PC3.								
1186	BA	0.0434								
1187	LS		77	10						



LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

1231 KK DPC4T  
 1232 KM DPC3T IS A DIVERSION ADDED BY GVSCE IN ORDER TO ROUTE RUNOFF TO THE  
 1233 KM UNION HILLS DETENTION BASIN VIA THE POWER LINE CHANNEL.  
 1234 KM  
 1235 KM DIVERT 100% OF FLOW  
 1236 DT BPC4T  
 1237 DI 0 10000  
 1238 DQ 0 10000  
 \*

1239 KK CLEAR  
 1240 KM CLEAR HYDROGRAPHS FROM THE STACK.  
 1241 HC 3  
 \*

\* THIS ENDS THE PORTION OF THE MODEL TAKEN FROM DRAINAGE REPORT  
 \* FOR VILLAGE 3 - PHASE I HEC-1 MODEL BY GILBERTSON ASSOC. INC.  
 \* DATED 7-19-95  
 \*

\* RETURN TO NORTH 18\VILLAGE 2\TPP3 MODEL.  
 \* THE REMAINDER OF THE SUBBASINS IN THIS MODEL WILL CONTRIBUTE TO THE  
 \* PROPOSED CHANNNEL IN THE POWER EASEMENT AS IDENTIFIED IN THE  
 \* "COMMUNITY DRAINAGE STUDY - CORE NORTH AND WILL DISCHARGE TO REGIONAL  
 \* RETENTION BASIN 38R1.  
 \*

1242 KK 37AW RET  
 1243 KM RETRIEVE DIVERTED FLOW FROM SOUTH BOUNDARY OF SUB 37A TO REFLECT  
 1244 KM BREAK IN DEER VALLEY ROAD CHANNEL BETWEEN HAYDEN & PIMA ROADS  
 1245 DR 37AW  
 \*

1246 KK R14R  
 1247 KM ROUTE FLOW FROM DIVERT AT DEER VALLEY ROAD (UPSTREAM OF SUBBAIN 5) TO  
 1248 KM RET14.1  
 1249 RS 1 FLOW  
 1250 RC .055 .045 .055 2900 .01  
 1251 RX 0 16 26 30 50 54 64 80  
 1252 RY 6 2 2 0 0 2 2 6

\* RET 141 HAS BEEN REVISED FOLLOWING REFINEMENT OF GRADING PLANS 11-16-94  
 \*

1253 KK RET141  
 1254 KM ROUTE FLOW THROUGH RETENTION BASIN NO. 14.1. 18" PIPE OUTFLOW WILL  
 1255 KM BLEED FLOWS TO DRAIN THE BASIN AFTER THE STORM HAS PASSED.  
 1256 RS 1 STOR 0 0  
 1257 SV 0 .46 2.79 4.56 5.71 6.92 8.24  
 1258 SQ 0 11 15 22 147 463 968  
 1259 SE 1778 1785 1790 1792 1793 1794 1795  
 \*

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

1260	KK	R14.1									
1261	KM	ROUTE FLOW FROM RET14.1 TO CP14									
1262	KM	RET14.1									
1263	RS	1	FLOW								
1264	RC	.055	.045	.055	1900	.01					
1265	RX	0	16	26	30	50	54	64	80		
1266	RY	6	2	2	0	0	2	2	6		
	*										
1267	KK	SUB13N									
1268	KM	RUNOFF FROM SUBBASIN 13 NORTH 18 MODEL.									
1269	BA	.037									
1270	LS		77	24							
1271	UK	100	.015	.15	100						
1272	RK	2400	.007	.018		TRAP	50	20			
	*										
1273	KK	R14.1									
1274	KM	ROUTE FLOW FROM CP13 TO RET14 NORTH 18 MODEL.									
1275	RS	1	FLOW								
1276	RC	.055	.045	.055	950	.025					
1277	RX	0	8	13	17	22	26	31	39		
1278	RY	4	2	2	0	0	2	2	4		
	*										
1279	KK	SUB14N									
1280	KM	RUNOFF FROM SUBBASIN 14 NORTH 18 MODEL.									
1281	BA	.049									
1282	LS		81	0							
1283	UK	300	.025	.15	100						
1284	RK	2300	.01	.025		TRAP	10	4			
	*										
1285	KK	CP14									
1286	KM	ADD HYDROGRAPHS AT CP14									
1287	HC	3	0.5595								
	*										
1288	KK	RET14									
1289	KM	ROUTE FLOW THROUGH RETENTION BASIN NO. 14. 18" PIPE OUTFLOW WILL									
1290	KM	BLEED FLOWS TO DRAIN THE BASIN AFTER THE STORM HAS PASSED.									
1291	RS	1	STOR	0	0						
1292	SV	0	.08	.31	1.01	2.16	3.20	4.19	5.69	7.8	
1293	SQ	0	14	16	18	20	22	155	464	750	
1294	SE	1744	1746	1748	1750	1752	1753	1754	1755	1756	
	*										
1295	KK	R18.1									
1296	KM	ROUTE FLOW FROM RET14 TO CP18									
1297	RS	1	FLOW								
1298	RC	.055	.045	.055	500	.016					
1299	RX	0	16	26	34	54	68	78	96		
1300	RY	6	2	2	0	0	2	2	6		
	*										



LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

1337 KK RPC1  
 1338 KM ROUTE FLOW FROM CP18N TO CPC1.  
 1339 RS 1 FLOW  
 1340 RC .035 .035 .035 510 .013  
 1341 RX 0 16 26 34 64 78 88 106  
 1342 RY 6 2 2 0 0 2 2 6  
 \*

1343 KK UB18NA  
 1344 KM RUNOFF FROM SUBBASIN 18NA.  
 1345 BA .022  
 1346 LS 77 42  
 1347 UK 100 .01 .15 100  
 1348 RK 1450 .02 .018 TRAP 50 20  
 \*

1349 KK 1RPC1  
 1350 KM ROUTE FLOW FROM CP18NA TO CPC1.  
 1351 RS 1 FLOW  
 1352 RC .035 .035 .035 2550 .01  
 1353 RX 0 16 26 34 64 78 88 106  
 1354 RY 8 4 2 0 0 2 4 8  
 \*

1355 KK UB18NB  
 1356 KM RUNOFF FROM SUBBASIN 18NB.  
 1357 BA .0096  
 1358 LS 77 42  
 1359 UK 100 .01 .15 100  
 1360 RK 800 .02 .018 TRAP 50 20  
 \*

1361 KK 2RPC1  
 1362 KM ROUTE FLOW FROM CP18NB TO CPC1.  
 1363 RS 1 FLOW  
 1364 RC .035 .035 .035 2000 .01  
 1365 RX 0 16 26 34 64 78 88 106  
 1366 RY 8 4 2 0 0 2 4 8  
 \*

1367 KK PC1  
 1368 KM RUNOFF FROM SUBBASIN PC1.  
 1369 BA .062  
 1370 LS 77 10  
 1371 UK 500 .015 .15 100  
 1372 RK 2700 .01 .03 TRAP 30 4  
 \*

1373 KK 1CPC1  
 1374 KM ADD HYDROGRAPHS AT CPC1.  
 1375 HC 3  
 \*









LINE	ID	1	2	3	4	5	6	7	8	9	10
1527	KK	CP10B									
1528	KM	ADD HYDROGRAPHS AT CP10B									
1529	HC	2									
	*										
1530	KK	R11NA									
1531	KM	ROUTE FLOW FROM CP10B TO CP11NA.									
1532	RS	1 FLOW									
1533	RC	.03	.03	.03	200	.04					
1534	RX	0	8	16	24	29	37	45	53		
1535	RY	6	4	2	0	0	2	4	6		
	*										
1536	KK	UB11NA									
1537	KM	RUNOFF FROM SUBBASIN 11NA.									
1538	BA	.0076									
1539	LS		81	0							
1540	UK	100	.025	.15	100						
1541	RK	500	.03	.025			TRAP	30	6		
	*										
1542	KK	CP11NA									
1543	KM	ADD HYDROGRAPHS AT CP11NA									
1544	HC	2									
	*										
1545	KK	SR11NA									
1546	KM	STOAGE ROUTE THROUGH FAIRWAY DETENTION AREA IN SUB11NA.									
1547	RS	1	STOR	0	0						
1548	SV	0	.0462	1.425	2.480	3.109	3.856				
1549	SQ	0	10	27	27	27	237				
1550	SE	1734	1735	1740	1742	1743	1744				
	*										
1551	KK	R11NB									
1552	KM	ROUTE FLOW FROM CP11NA TO CP11NB.									
1553	RS	1 FLOW									
1554	RC	.025	.025	.025	250	.03					
1555	RX	0	12	24	36	56	68	80	92		
1556	RY	6	4	2	0	0	2	4	6		
	*										
1557	KK	UB11NB									
1558	KM	RUNOFF FROM SUBBASIN 11NB.									
1559	BA	.0078									
1560	LS		81	0							
1561	UK	100	.04	.15	100						
1562	RK	700	.025	.025			TRAP	30	6		
	*										





LINE	ID	1	2	3	4	5	6	7	8	9	10
1639	KK	CP11NC									
1640	KM	ADD HYDROGRAPHS AT CP11NC									
1641	HC	2									
	*										
1642	KK	SR11NC									
1643	KM	ROUTE FLOW THROUGH RETENTION BASIN RT11NC. 18" PIPE OUTFLOW WILL									
1644	KM	BLEED FLOWS TO DRAIN THE BASIN AFTER THE STORM HAS PASSED.									
1645	RS	1	STOR	0	0						
1646	SV	0	1.665	2.303	3.062						
1647	SQ	0	27	111	344						
1648	SE	1730	1735	1736	1737						
	*										
1649	KK	R16NC									
1650	KM	ROUTE FLOW FROM CP11NC TO CP16NC.									
1651	RS	1	FLOW								
1652	RC	.035	.035	0.035	950	.025					
1653	RX	0	8	13	17	22	26	31	39		
1654	RY	4	2	2	0	0	2	2	4		
	*										
1655	KK	UB16NC									
1656	KM	RUNOFF FROM SUBBASIN 16NC.									
1657	BA	.0337									
1658	LS		77	42							
1659	UK	100	.015	.15	100						
1660	RK	1600	.015	.022		TRAP	50	20			
	*										
1661	KK	CP16NC									
1662	KM	ADD HYDROGRAPHS AT CP16NC									
1663	HC	2									
	*										
1664	KK	R16NC1									
1665	KM	ROUTE FLOW FROM CP16NC TO CP16NC1.									
1666	RS	1	FLOW								
1667	RC	.03	.03	.03	550	.013					
1668	RX	0	16	26	34	44	58	68	86		
1669	RY	6	2	2	0	0	2	2	6		
	*										
1670	KK	C16NC1									
1671	KM	ADD HYDROGRAPHS AT CP16NC1.									
1672	HC	2									
	*										
1673	KK	R15N1									
1674	KM	ROUTE FLOW FROM CP16NC1 TO CP15N1.									
1675	RS	1	FLOW								
1676	RC	.035	.035	.035	600	.013					
1677	RX	0	16	26	34	54	68	78	96		
1678	RY	6	2	2	0	0	2	2	6		





LINE	ID	1	2	3	4	5	6	7	8	9	10
1758	KK	SUB15N									
1759	KM	RUNOFF FROM SUBBASIN 15N.									
1760	BA	.0391									
1761	LS		77	68							
1762	UK	100	.01	.15	100						
1763	RK	400	.008	.018		TRAP	50	20			
1764	RK	1700	.015	.025		TRAP	10	4			
	*										
1765	KK	CP15N									
1766	KM	ADD HYDROGRAPHS AT CP15N									
1767	HC	2									
	*										
1768	KK	R15N2									
1769	KM	ROUTE FLOW FROM CP15N TO CP15N1.									
1770	RS	1	FLOW								
1771	RC	.02	.02	.02	700	.013					
1772	RX	0	8	13	17	22	26	31	39		
1773	RY	6	2	2	0	0	2	2	6		
	*										
1774	KK	CP15N2									
1775	KM	ADD HYDROGRAPHS AT CP15N1									
1776	KM	THIS IS THE INTERIM OUTFLOW DISCHARGE TO NATURAL WASH.									
1777	HC	2 1.1611									
	*										
1778	KK	R15N2									
1779	KM	ROUTE 15N2 IS ADDED BY GVSCE TO ROUTE THE HYDROGRAPH FROM CP15N2 TO THE									
1780	KM	POWER LINE CHANNEL CROSSING AT HAYDEN RD.									
1781	KM										
1782	KM	ROUTE FLOW FROM CP15N2 TO CPC3A.									
1783	RS	1	FLOW								
1784	RC	.035	.035	.035	2200	.013					
1785	RX	0	16	26	34	64	78	88	106		
1786	RY	6	2	2	0	0	2	2	6		
	*										
1787	KK	DPC3									
1788	KM	THIS OPERATION IS ADDED BY GVSCE IN ORDER TO ROUTE RUNOFF TO THE									
1789	KM	UNION HILLS DETENTION BASIN VIA THE POWER LINE CHANNEL.									
1790	KM										
1791	KM	RETRIEVE DIVERTED FLOW									
1792	DR	BPC3T									
	*										
1793	KK	CPC3A									
1794	KM	COMBINE CPC3A IS ADDED BY GVSCE TO ESTIMATE THE TOTAL DISCHARGE AT THE									
1795	KM	POWER LINE CHANNEL CROSSING AT HAYDEN RD.									
1796	KM										
1797	KM	COMBINE ROUTED HYDROGRAPH FROM CP15N2 WITH HYDROGRAPH FROM CPC3									
1798	HC	2 1.3446									
	*										

LINE	ID	1	2	3	4	5	6	7	8	9	10
1799	KK	RPC3A									
1800	KM	ROUTE PC3A IS ADDED BY GVSCE TO ROUTE THE HYDROGRAPH FROM CPC3A VIA									
1801	KM	THE POWER LINE CHANNEL.									
1802	KM										
1803	KM	ROUTE FLOW FROM CP15N2 TO CPC3A.									
1804	RS	1	FLOW								
1805	RC	.035	.035	.035	1100	.013					
1806	RX	0	16	26	34	64	78	88	106		
1807	RY	6	2	2	0	0	2	2	6		
	*										
1808	KK	DPC4									
1809	KM	THIS OPERATION IS ADDED BY GVSCE IN ORDER TO ROUTE RUNOFF TO THE									
1810	KM	UNION HILLS DETENTION BASIN VIA THE POWER LINE CHANNEL.									
1811	KM										
1812	KM	RETRIEVE DIVERTED FLOW									
1813	DR	BPC4T									
	*										
1814	KK	CPC4A									
1815	KM	COMBINE CPC4A IS ADDED BY GVSCE TO ESTIMATE THE TOTAL DISCHARGE IN THE									
1816	KM	POWER LINE CHANNEL									
1817	KM										
1818	KM	COMBINE ROUTED HYDROGRAPH FROM CPC3A WITH HYDROGRAPH FROM CPC4									
1819	HC	2	1.9946								
	*										
1820	KK	RPC4A									
1821	KM	ROUTE PC4A IS ADDED BY GVSCE TO ROUTE THE HYDROGRAPH FROM CPC4A TO THE									
1822	KM	POWER LINE CHANNEL CROSSING AT HUALAPAI RD.									
1823	KM										
1824	KM	ROUTE FLOW FROM CPC4A TO CPC5.									
1825	RS	1	FLOW								
1826	RC	.035	.035	.035	1900	.013					
1827	RX	0	16	26	34	64	78	88	106		
1828	RY	6	2	2	0	0	2	2	6		
	*										
1829	KK	DPC4AT									
1830	KM	DIVERT PC4A IS ADDED BY GVSCE IN ORDER TO ROUTE RUNOFF TO THE UNION									
1831	KM	HILLS DETENTION BASIN VIA THE POWER LINE CHANNEL.									
1832	KM										
1833	KM	DIVERT 100% OF FLOW									
1834	DT	BPC4AT									
1835	DI	0	10000								
1836	DQ	0	10000								
	*										
1837	KK	SUB1-2									
1838	KM	RUNOFF FROM SUB 1 AND 2, SOUTH COURSE MODEL									
1839	BA	.0558									
1840	LS		77	68							
1841	UK	200	.010	.15	100						
1842	RK	1370	.027	.015		TRAP	50	20			



LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

1883	KK	SUB7S								
1884	KM	RUNOFF FROM SUB BASIN 7, SOUTH COURSE								
1885	BA	.027								
1886	LS		77	42						
1887	UK	100	.010	.15	100					
1888	RK	2080	.023	.025		TRAP	50	20		
	*									
1889	KK	CPRET2								
1890	KM	COMBINE HYDROGRAPHS AT RETENTION BASIN 2, SOUTH COURSE								
1891	HC	5								
	*									
1892	KK	SRRET2								
1893	KM	STORAGE THRU RETENTION BASIN NO. 2, SOUTH COURSE								
1894	RS	1	STOR	0	0					
1895	SV	0	.617	3.474	9.858	20.063	35.353	52.685	57.749	62
1896	SE	1670	1675	1680	1685	1690	1695	1699	1700	1701
1897	SQ	0	0	0	0	0	0	32	386	594
	*									
	*	NO FLOW RELEASED FROM RETENTION BASIN								
	*									
1898	KK	CLEAR								
1899	KM	THIS OPERATION IS ADDED BY GVSCE								
1900	KM									
1901	KM	CLEAR HYDROGRAPHS FROM THE STACK								
1902	HC	4								
	*									
1903	KK	SUB8S								
1904	KM	RUNOFF FROM SUB BASIN 8, SOUTH COURSE								
1905	BA	.0256								
1906	LS		77	42						
1907	UK	100	.010	.15	100					
1908	RK	1600	.015	.025		TRAP	50	20		
	*									
1909	KK	RGC36								
1910	KM	ROUTE SUB8S TO CPGC36								
1911	RS	1	FLOW							
1912	RC	.055	.045	.055	850	.02				
1913	RX	0	16	26	30	40	44	54	70	
1914	RY	6	2	2	0	0	2	2	6	
	*									
1915	KK	GC36								
1916	KM	RUNOFF FROM SOUTH COURSE HOLES 3, 6, AND NORTH HALF OF HOLE 4.								
1917	BA	.0406								
1918	LS		81	0						
1919	UK	200	.025	.15	100					
1920	RK	2350	.015	.035		TRAP	10	4		
	*									



LINE	ID.....	1.....	2.....	3.....	4.....	5.....	6.....	7.....	8.....	9.....	10
1957	KK	R10S									
1958	KM	ROUTE FLOW FROM CP7A TO CP10S									
1959	RS	1	FLOW								
1960	RC	.035	.035	.035	1400	.015					
1961	RX	0	8	12	16	18	22	26	30		
1962	RY	6	4	3	2	2	3	4	6		
	*										
1963	KK	SUB10S									
1964	KM	RUNOFF FROM SUB BASIN 10, SOUTH COURSE									
1965	BA	.0248									
1966	LS		77	53							
1967	UK	100	.010	.15	100						
1968	RK	1150	.020	.025			TRAP	50	20		
	*										
1969	KK	CP10S									
1970	KM	COMBINE HYDROGRAPHS AT CP10 SOUTH COURSE									
1971	HC	2									
	*										
1972	KK	SUB11S									
1973	KM	RUNOFF FROM SUB11, SOUTH COURSE									
1974	BA	.0234									
1975	LS		77	68							
1976	UK	100	.015	.018	100						
1977	RK	1050	.015	.025			TRAP	100	20		
	*										
1978	KK	R11S									
1979	KM	ROUTE 11S IS ADDED BY GVSCE TO ROUTE THE RUNOFF FROM SUB11S TO THE									
1980	KM	POWER LINE CHANNEL CROSSING AT HUALAPAI DR ALONG HUALAPAI DR.									
1981	KM										
1982	KM	ROUTE FLOW FROM SUB11S TO CPC5.									
1983	RS	1	FLOW								
1984	RC	.035	.035	.035	900	.015					
1985	RX	0	8	12	16	18	22	26	30		
1986	RY	6	4	3	2	2	3	4	6		
	*										
1987	KK	C10SA									
1988	KM	COMBINE 10SA IS ADDED BY GVSCE									
1989	KM										
1990	KM	COMBINE ROUTED HYDROGRAPH FROM 11S WITH HYDROGRAPH FROM CP10S									
1991	HC	2									
	*										
1992	KK	R10SA									
1993	KM	ROUTE 10SA IS ADDED BY GVSCE IN ORDER TO ROUTE RUNOFF TO THE UNION									
1994	KM	HILLS DETENTION BASIN VIA THE POWER LINE CHANNEL.									
1995	KM										
1996	KM	ROUTE FLOW FROM C10SAS TO CPC5.									
1997	RS	1	FLOW								
1998	RC	.035	.035	.035	900	.015					



LINE	ID	1	2	3	4	5	6	7	8	9	10
2038	KK	SCN5C									
2039	KM	RUNOFF FROM SUBBASIN CN5C									
2040	BA	0.2667									
2041	LS		74	20							
2042	UK	240	0.021	0.13	100						
2043	RK	1200	0.018	0.045	0.0067	TRAP	0	45			
2044	RK	5600	0.009	0.040		TRAP	15	3			
	*										
2045	KK	SCN6									
2046	KM	RUNOFF FROM SUBBASIN CN6A									
2047	BA	0.2597									
2048	LS		74	85							
2049	UK	180	0.019	0.13	100						
2050	RK	1075	0.019	0.045	0.0066	TRAP	5	7			
2051	RK	4430	0.013	0.040		TRAP	8	50			
	*										
2052	KK	D52									
2053	KM	BRING BACK DIVERTED HYDROGRAPH FROM R52									
2054	DR	B52T									
	*										
2055	KK	S53A									
2056	KM	RUNOFF FROM SUBBASIN 53A									
2057	BA	0.1692									
2058	LS		74	11							
2059	UK	300	0.022	0.13	100						
2060	RK	1475	0.026	0.045	0.0111	TRAP	3	5			
2061	RK	2700	0.021	0.04		TRAP	25	5			
	*										
2062	KK	C53									
2063	KM	COMBINE ROUTED HYDROGRAPH FROM									
2064	HC	2	8.0852								
	*										
2065	KK	R53									
2066	KM	NORMAL DEPTH CHANNEL ROUTE FROM C53 TO C53A THROUGH PIMA CHANNEL									
2067	RS	1	FLOW	-1							
2068	RC	0.035	0.025	0.035	2360	0.01					
2069	RX	1000	1020	1022	1034	1084	1096	1098	1118		
2070	RY	111.4	106.4	106.3	100	100	106.3	106.4	111.4		
	*										
2071	KK	S53A1									
2072	KM	RUNOFF FROM SUBBASIN 53A1									
2073	BA	0.3384									
2074	LS		74	12		74	30				
2075	UK	300	0.022	0.13	70						
2076	UK	150	0.027	0.13	30						
2077	RK	1250	0.023	0.045	0.0087	TRAP	4	5			
2078	RK	5650	0.017	0.04		TRAP	35	5			
	*										

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

2079	KK	C53A										
2080	KM	COMBINE ROUTED HYDROGRAPH FROM										
2081	HC	2	8.4236									
	*											
2082	KK	C1I										
2083	KM	COMBINE ROUTED HYDROGRAPH FROM										
2084	HC	4										
	*											
2085	KK	C10										
2086	KM	DETENTION BASIN AT UNION HILLS ROAD - NONREGULATORY STRUCTURE										
2087	KM	OUTLET RATING CURVE - USING HY8 FOR A 78" RCP WITH A SLOPE OF 0.9%										
2088	KM	7-ACRE-FEET OF STORAGE FOR SEDIMENTATION										
2089	RS	1	STOR									
2090	SV	0	0.36	0.82	1.42	2.23	3.01	37.59	123.30	222.97	337.88	
2091	SV	362.56	387.54									
2092	SE	1590	1591	1592	1593	1594	1595	1600	1605	1610	1615	
2093	SE	1616	1617									
2094	SQ	0	65	130	195	260	325	390	420	520	585	
2095	SQ	650	690	828	966	1104	1242	1382				
2096	SE	1590.0	1592.80	1594.36	1595.60	1596.80	1598.16	1599.79	1600.64	1604.03	1606.65	
2097	SE	1615.0	1615.28	1615.72	1616.04	1616.26	1616.40	1616.50				
	*											
	*											
2098	KK	RC1										
2099	KM	NORMAL DEPTH CHANNEL ROUTE FROM C1I TO CIA										
2100	RS	1	FLOW	-1								
2101	RC	0.025	0.025	0.025	2300	0.013						
2102	RX	1000	1008	1012	1016	1026	1030	1034	1042			
2103	RY	104	102	101	100	100	101	102	104			
	*											
2104	KK	S54										
2105	KM	RUNOFF FROM SUBBASIN 54										
2106	BA	0.0853										
2107	LS		74	22								
2108	UK	300	0.017	0.13	100							
2109	RK	3460	0.012	0.040		TRAP	5	2				
	*											
2110	KK	SCN6A										
2111	KM	RUNOFF FROM SUBBASIN CN6A										
2112	BA	0.1335										
2113	LS		74	20								
2114	UK	300	0.017	0.13	100							
2115	RK	1050	0.017	0.045	0.0057	TRAP	8	20				
2116	RK	2250	0.012	0.040		TRAP	10	4				



SCHEMATIC DIAGRAM OF STREAM NETWORK

INPUT LINE	(V) ROUTING	(--->) DIVERSION OR PUMP FLOW
NO.	(.) CONNECTOR	(<---) RETURN OF DIVERTED OR PUMPED FLOW
26	S30N V V	
35	R30N .	
41	. S31.1 .	
49	C31.1..... V V	
52	R31.1 .	
58	. S35N .	
68	. .	-----> D35NL
66	D35NR V V	
71	R35NR .	
78	. .	S36.2
86	C36.2..... .	
92	. .	-----> D36.2L
90	D36.2R V V	
95	R36.2R .	
102	. .	S34.1
111	C34.1I..... V V	
115	C34.1O V V	
128	R34.1 .	
134	. S36.1 .	

```

141 C36.1.....
      V
      V
144 R36.1
      .
      .
152 . <----- D35NL
150 . B35NL
      . V
      . V
153 . R35NL
      .
      .
162 . <----- D36.2L
160 . B36.2L
      . V
      . V
163 . R36.2L
      .
      .
170 . S36R1
      .
      .
178 C36R1.....
      V
      V
183 R36R1
      .
      .
189 . S36R2
      .
      .
196 C36R2.....
      .
      .
199 . S51.1
      .
      .
209 . -----> D51.1L
207 . D51.1
      .
      .
212 C51.1I.....
      V
      V
215 C51.1O
      .
      .
230 . <----- D51.1L
228 . B51.1L
      .
      .
231 C51.1A.....
      V
      V
234 R51.1
      .
      .
242 . -----> B51.1T

```

240	D51.1T	.	
245	.	52D4	
	.	V	
	.	V	
251	.	52D4R	
	.	.	
254	.	52D4B	
	.	.	
260	.	52D5C1.....	
	.	.	
263	.	52D5A	
	.	V	
	.	V	
269	.	52D5AR	
	.	.	
272	.	52D5C2.....	
	.	V	
	.	V	
275	.	52D5R	
	.	.	
278	.	52C3	
	.	V	
	.	V	
284	.	52C3R	
	.	.	
287	.	52C3B	
	.	.	
293	.	2C3BC1.....	
	.	.	
296	.	2C3BC2.....	
	.	V	
	.	V	
299	.	52C3BR	
	.	.	
302	.	51C	
	.	.	
310	.	-----> 51C1DV	
308	.	51C1D	
	.	V	
	.	V	
313	.	51C1R	
	.	.	
316	.	52C1	
	.	.	
322	.	52C1C.....	
	.	V	

		V	
325	.	52C1R	
	.	.	
328	.	.	52C2A
	.	.	
334	.	52C2AC.....	
	.	.	
337	.	.	52C2B
	.	.	
343	.	52C2BC.....	
	.	V	
	.	V	
346	.	52C2BR	
	.	.	
349	.	.	52C2C
	.	.	
355	.	52C2CC.....	
	.	V	
	.	V	
358	.	52C2R	
	.	.	
361	.	.	52C4
	.	.	
367	.	52C4C1.....	
	.	.	
370	.	52C4C2.....	
	.	V	
	.	V	
373	.	52C4R	
	.	.	
376	.	52C13	
	.	.	
384	.	.	-----> STORM
382	.	2C13DV	
	.	.	
387	.	.	52C15
	.	.	
393	.	2C15C1.....	
	.	.	
396	.	2C15C2.....	
	.	V	
	.	V	
399	.	52C15R	
	.	.	
402	.	52C14A	

408	2C14AC.....		
	V		
	V		
411	2C14AR		
416		<-----	51C1DV
414	51C1DV		
419		----->	51C2DV
417	51C2D		
	V		
	V		
422	51C2R		
425			52C5
431	52C5C.....		
	V		
	V		
434	52C5R		
437			52C6
443	52C6C.....		
	V		
	V		
446	52C6R		
451		<-----	51C2DV
449	51C2DV		
	V		
	V		
452	51C3R		
455			51B
463		----->	51B1DV
461	51B1D		
	V		
	V		
466	51B1R		
469			52C7
475	52C7C.....		
	V		
	V		

478	.	.	.	52C7R	
483	.	.	.		←----- 51B1DV
481	.	.	.	51B1DV	
486	.	.	.		-----> 51B2DV
484	.	.	.	51B2D	
	.	.	.	V	
	.	.	.	V	
489	.	.	.	51B2R	
492	.	.	.		52C8
498	.	.	.	52C8C.....	
	.	.	.	V	
	.	.	.	V	
501	.	.	.	52C8R	
504	.	.	.	52C9C1.....	
	.	.	.	V	
	.	.	.	V	
507	.	.	.	52C9R1	
510	.	.	.		52C9
516	.	.	.	52C9C2.....	
	.	.	.	V	
	.	.	.	V	
519	.	.	.	52C9R2	
522	.	.	.	2C10C1.....	
	.	.	.	V	
	.	.	.	V	
525	.	.	.	2C10R1	
528	.	.	.		52C10
534	.	.	.	2C10C2.....	
537	.	.	.		52C11
	.	.	.	V	
	.	.	.	V	
543	.	.	.	2C11R1	
548	.	.	.		←----- STORM
546	.	.	.	52C13D	

549	.	.	.	52C11C.....
	.	.	.	V
	.	.	.	V
552	.	.	.	2C11CR
	.	.	.	.
555	.	.	.	2C11C2.....
	.	.	.	V
	.	.	.	V
558	.	.	.	2C11R2
	.	.	.	.
561	.	.	.	52C12
	.	.	.	.
567	.	.	.	52C12C.....
	.	.	.	V
	.	.	.	V
570	.	.	.	52C12R
	.	.	.	.
573	.	.	.	52C14B
	.	.	.	.
579	.	.	.	C14BC1.....
	.	.	.	.
582	.	.	.	C14BC2.....
	.	.	.	V
	.	.	.	V
585	.	.	.	52C14R
	.	.	.	.
590	.	.	.	.<----- 51B2DV
588	.	.	.	51B2DV
	.	.	.	.
593	.	.	.	.-----> 51B3DV
591	.	.	.	51B3D
	.	.	.	V
	.	.	.	V
596	.	.	.	51B3R
	.	.	.	.
599	.	.	.	52B1
	.	.	.	.
605	.	.	.	52B1C.....
	.	.	.	V
	.	.	.	V
608	.	.	.	52B1R
	.	.	.	.
613	.	.	.	.<----- 51B3DV
611	.	.	.	51B3DV
	.	.	.	.
616	.	.	.	.-----> 51B4DV
614	.	.	.	51B4D
	.	.	.	V

			V
619			51B4R1
622		52B2C1.....	
		V	
		V	
625		52B2R1	
628			52B2
634		52B2C2.....	
		V	
		V	
637		52B2R2	
		V	
		V	
640		52B3R1	
643			52B3
649		52B3C2.....	
		V	
		V	
652		52B3R2	
655			52B4
661		52B4C.....	
		V	
		V	
664		52B4R	
667			52B5
673		52B5C1.....	
676	52B5C2.....		
	V		
	V		
679	52B5R		
684			<----- 51B4DV
682		51B4DV	
687			-----> 51B5DV
685		51B5D	
		V	
		V	

690	.	.	51B5R	.	.
695	.	.	.	.	.<----- 51B5DV
693	.	.	51B5DV	.	.
698	.	.	.	.	.-----> 51B6DV
696	.	.	51B6D	.	.
	.	.	V	.	.
	.	.	V	.	.
701	.	.	51B6R	.	.
706	.	.	.	.	.<----- 51B6DV
704	.	.	51B6DV	.	.
709	.	.	.	.	.-----> 51B7DV
707	.	.	51B7D	.	.
	.	.	V	.	.
	.	.	V	.	.
712	.	.	51B7R1	.	.
715	.	.	51B7C.....	.	.
	.	.	V	.	.
	.	.	V	.	.
718	.	.	51B7R2	.	.
721	.	.	.	.	52B6
727	.	.	52B6C.....	.	.
	.	.	V	.	.
	.	.	V	.	.
730	.	.	52B6R	.	.
733	.	.	.	.	52B7
739	.	.	52B7C1.....	.	.
742	.	.	52B7C2.....	.	.
745	.	.	52A2	.	.
751	.	.	52A2C2.....	.	.
756	.	.	.	.	.<----- 51B7DV
754	.	.	51B7DV	.	.
	.	.	V	.	.
	.	.	V	.	.
757	.	.	51B8R	.	.

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760 . . . . . 52A1
. . . . .
766 . . . . . 52A1C.....
. . . . .
771 . . . . . <----- B51.1T
769 . . . . . D51.1
. . . . .
772 . . . . . C52A.....
. . . . . V
. . . . . V
776 . . . . . R52A
. . . . .
782 . . . . . C52.....
. . . . . V
. . . . . V
786 . . . . . R52
. . . . .
794 . . . . . -----> B52T
792 . . . . . D52T
. . . . .
797 CLEAR.....
. . . . .
800 . . . . . 37A
. . . . .
817 . . . . . -----> 37AW
806 . . . . . 37AE
. . . . . V
. . . . . V
820 . . . . . 37AE1
. . . . .
827 . . . . . SUB5N
. . . . .
834 . . . . . CP5N.....
. . . . . V
. . . . . V
837 . . . . . RET5N
. . . . . V
. . . . . V
844 . . . . . R6N.1
. . . . .
852 . . . . . SUB6B
. . . . . V
. . . . . V
858 . . . . . SR6B
. . . . .
864 . . . . . CP6.1.....

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867		SUB1N	
		V	
		V	
873		R2NA	
879			SUB2NA
885		CP2NA.....	
		V	
		V	
888		SR2NA	
		V	
		V	
894		R2NB	
900			SUB2NB
906		CP2NB.....	
		V	
		V	
909		SR2NB	
		V	
		V	
915		RCP4N	
921			SUB6N
			V
			V
927			RET6N
			V
			V
933			RCP4N1
939		CP4N.1.....	
942			SUB3N
			V
			V
948			RET3N
			V
			V
955			R4N
961		CP4N.2.....	
964			SUB4N
970		CP4N.....	

	.	.	V	
	.	.	V	
973	.	.	R6N	
	.	.	.	
979	.	.	.	SUB6A
	.	.	.	
985	.	.	CP6.2.....	
	.	.	.	
988	.	.	CP6N.....	
	.	.	V	
	.	.	V	
991	.	.	RCP6N	
	.	.	.	
997	.	.	.	SUB3C
	.	.	.	
1003	.	.	CP3C.....	
	.	.	V	
	.	.	V	
1006	.	.	R3C	
	.	.	.	
1014	.	.	.	GC1018
	.	.	.	
1020	.	.	.	GC1-9
	.	.	.	
1026	.	.	.	SUB3S
	.	.	.	
1032	.	.	CP3S.....	
	.	.	V	
	.	.	V	
1035	.	.	RT3S	
	.	.	.	
1041	.	.	.	SUB4S
	.	.	V	
	.	.	V	
1047	.	.	RT4S	
	.	.	.	
1053	.	.	.	GC2-8
	.	.	.	
1059	.	.	1PGC28.....	
	.	.	.	
1062	.	.	.	SUB3D3
	.	.	.	
1068	.	.	CPGC28.....	
	.	.	V	
	.	.	V	
1071	.	.	SRGC28	

	.	V	
	.	V	
1077	.	RT7S	
	.	.	
1083	.		GC7
	.	.	
1089	.	CP7S.....	
	.	.	
1097	.	----->	B7ST
1092	.	D7ST	
	.	.	
1100	.	CLEAR.....	
	.	.	
1103	.	SUB3D1	
	.	V	
	.	V	
1108	.	RD1B1	
	.	.	
1114	.		SUB3B1
	.	.	
1119	.	CP3B1.....	
	.	V	
	.	V	
1122	.	RB13F	
	.	.	
1128	.		SUB3F
	.	.	
1134	.	CP3F.....	
	.	.	
1137	.		SUB3B2
	.	V	
	.	V	
1142	.		RB2E1
	.	V	
	.	V	
1148	.		RB2E2
	.	.	
1154	.		SUB3E1
	.	.	
1159	.		1CPE31.....
	.	.	
1162	.		SUB3D2
	.	V	
	.	V	
1167	.		RD2E2
	.	.	
	.	.	

```

1173 . . . . . SUB3E2
. . . . .
1178 . . . . . CP3E2.....
. . . . .
1181 . . . . . PC3
. . . . .
1190 . . . . . CPC3.....
. . . . .
1202 . . . . . -----> BPC3T
1197 . . . . . DPC3T
. . . . .
1205 . . . . . SUB3E3
. . . . .
1210 . . . . . PC4
. . . . .
1224 . . . . . <----- B7ST
1219 . . . . . D7S
. . . . .
1225 . . . . . CPC4.....
. . . . .
1236 . . . . . -----> BPC4T
1231 . . . . . DPC4T
. . . . .
1239 . . . . . CLEAR.....
. . . . .
1245 . . . . . <----- 37AW
1242 . . . . . 37AW
. . . . . V
. . . . . V
1246 . . . . . R14R
. . . . . V
. . . . . V
1253 . . . . . RET141
. . . . . V
. . . . . V
1260 . . . . . R14.1
. . . . .
. . . . .
1267 . . . . . SUB13N
. . . . . V
. . . . . V
1273 . . . . . R14.1
. . . . .
. . . . .
1279 . . . . . SUB14N
. . . . .
1285 . . . . . CP14.....
. . . . . V

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1288	V	RET14		
	V			
	V			
1295		R18.1		
1301		SUB20N		
		V		
		V		
1307		R19		
1313			SUB19N	
1319		CP19N.....		
		V		
		V		
1322		R18NC		
1328			UB18NC	
1334		CP18NC.....		
		V		
		V		
1337		RPC1		
1343		UB18NA		
		V		
		V		
1349		1RPC1		
1355			UB18NB	
			V	
			V	
1361			2RPC1	
1367				PC1
1373		1CFC1.....		
		V		
		V		
1376		SRFC1		
1382		CPC1.....		
		V		
		V		
1385		R16NA1		
1391			UB16NA	
			V	

			V	
1397			R16NA1	
1403		C16NA1.....		
			V	
			V	
1406			R16NB1	
1412			UB16NB	
			V	
			V	
1418			R16NB1	
1424		C16NB1.....		
			V	
			V	
1427			R16NC1	
1433			SUB7N	
			V	
			V	
1439			R8NC	
1445			SUB8NA	
			V	
			V	
1451			SR8NA	
			V	
			V	
1457			R8NB	
1463				SUB8NB
1469			CP8NB.....	
			V	
			V	
1472			SR8NB	
			V	
			V	
1478			R8NC	
1484				SUB8NC
1490			CP8NC.....	
			V	
			V	
1493			SR8NC	
			V	
			V	
1499			R9N	

1505	.	.	.	SUB9N
	.	.	.	.
1511	.	.	CP9N.....	.
	.	.	V	.
	.	.	V	.
1514	.	.	R10B	.
	.	.	.	.
1520	.	.	.	SUB10B
	.	.	.	.
1527	.	.	CP10B.....	.
	.	.	V	.
	.	.	V	.
1530	.	.	R11NA	.
	.	.	.	.
1536	.	.	.	UB11NA
	.	.	.	.
1542	.	.	CP11NA.....	.
	.	.	V	.
	.	.	V	.
1545	.	.	SR11NA	.
	.	.	V	.
	.	.	V	.
1551	.	.	R11NB	.
	.	.	.	.
1557	.	.	.	UB11NB
	.	.	.	.
1563	.	.	CP11NB.....	.
	.	.	V	.
	.	.	V	.
1566	.	.	SR11NB	.
	.	.	V	.
	.	.	V	.
1572	.	.	R11NC	.
	.	.	.	.
1578	.	.	.	UB11NC
	.	.	.	.
1584	.	.	C11NC1.....	.
	.	.	.	.
1587	.	.	.	SUB10A
	.	.	.	V
	.	.	.	V
1594	.	.	.	R12NB
	.	.	.	.
1600	.	.	.	UB12NA
	.	.	.	V
	.	.	.	V
1606	.	.	.	SR12NA
	.	.	.	V

				V
1612				R12NA
1618				UB12NB
1624			CP12NB.....	
			V	
			V	
1627			SR12NB	
			V	
			V	
1633			R11NC2	
1639			CP11NC.....	
			V	
			V	
1642			SR11NC	
			V	
			V	
1649			R16NC	
1655				UB16NC
1661			CP16NC.....	
			V	
			V	
1664			R16NC1	
1670			C16NC1.....	
			V	
			V	
1673			R15N1	
1679			PC2	
1685			CP15N1.....	
			V	
			V	
1688			SRPC2	
1695			UB17NA	
			V	
			V	
1701			SR17NA	
			V	
			V	
1707			R17NB	
1713				UB17NB

1719	.	.	CP17NB.....	
	.	.	V	
	.	.	V	
1722	.	.	SR17NB	
	.	.	V	
	.	.	V	
1728	.	.	R17A	
	.	.		
	.	.		
1734	.	.		SUB17A
	.	.		
	.	.		
1740	.	.	CP17A1.....	
	.	.		
	.	.		
1743	.	.		UB17NC
	.	.		
	.	.		
1749	.	.	CP17A.....	
	.	.	V	
	.	.	V	
1752	.	.	R15N	
	.	.		
	.	.		
1758	.	.		SUB15N
	.	.		
	.	.		
1765	.	.	CP15N.....	
	.	.	V	
	.	.	V	
1768	.	.	R15N2	
	.	.		
	.	.		
1774	.	.	CP15N2.....	
	.	.	V	
	.	.	V	
1778	.	.	R15N2	
	.	.		
	.	.		
1792	.	.		<----- BPC3T
1787	.	.	DPC3	
	.	.		
	.	.		
1793	.	.	CPC3A.....	
	.	.	V	
	.	.	V	
1799	.	.	RPC3A	
	.	.		
	.	.		
1813	.	.		<----- BPC4T
1808	.	.	DPC4	
	.	.		
	.	.		
1814	.	.	CPC4A.....	
	.	.	V	
	.	.	V	
1820	.	.	RPC4A	
	.	.		
	.	.		

1834	.	----->	BPC4AT		
1829	.	DPC4AT			
1837	.		SUB1-2		
1843	.			GCRB18	
1850	.		CPRET1.....		
	.		V		
	.		V		
1853	.		SR18S		
1859	.			SUB5S	
1865	.				GC1216
1871	.				GC1415
1877	.				SUB6S
1883	.				SUB7S
1889	.			CPRET2.....	
	.			V	
	.			V	
1892	.			SRRET2	
1898	.	CLEAR.....			
1903	.		SUB8S		
	.		V		
	.		V		
1909	.		RGC36		
1915	.			GC36	
1921	.		C1GC36.....		
1924	.			SUB9S	
	.			V	
	.			V	
1930	.			R9S	
1936	.		CPGC36.....		
	.		V		

		V		
1939	SRGC36			
1945		SUB7A		
		V		
		V		
1951		SR7A		
		V		
		V		
1957		R10S		
1963			SUB10S	
1969		CF10S.....		
1972			SUB11S	
			V	
			V	
1978			R11S	
1987		C10SA.....		
		V		
		V		
1992		R10SA		
2001			GC45	
2007				PC5
2021				.<----- BPC4AT
2016				DPC4A
2022	CPC5.....			
		V		
		V		
2029	RPC5			
2038		SCN5C		
2045			SCN6	
2054				.<----- B52T
2052			D52	
2055				S53A

2062	.	.	.	.	C53.....
	.	.	.	.	V
	.	.	.	.	V
2065	.	.	.	.	R53
	.	.	.	.	.
2071	.	.	.	.	S53A1
	.	.	.	.	.
2079	.	.	.	.	C53A.....
	.	.	.	.	.
2082	.	C1I.....	.	.	.
	.	V	.	.	.
	.	V	.	.	.
2085	.	C1O	.	.	.
	.	V	.	.	.
	.	V	.	.	.
2098	.	RC1	.	.	.
	.	.	.	.	.
2104	.	.	S54	.	.
	.	.	.	.	.
2110	.	.	.	SCN6A	.
	.	.	.	.	.
2117	.	C1A.....	.	.	.

(\*\*\*) RUNOFF ALSO COMPUTED AT THIS LOCATION

\*\*\*\*\*  
 \* FLOOD HYDROGRAPH PACKAGE (HEC-1) \*  
 \* MAY 1991 \*  
 \* VERSION 4.0.1E \*  
 \* Lahey F77L-EM/32 version 5.01 \*  
 \* Dodson & Associates, Inc. \*  
 \* RUN DATE 01/03/97 TIME 14:36:06 \*  
 \*\*\*\*\*

\*\*\*\*\*  
 \* U.S. ARMY CORPS OF ENGINE  
 \* HYDROLOGIC ENGINEERING CE  
 \* 609 SECOND STREET  
 \* DAVIS, CALIFORNIA 9561  
 \* (916) 551-1748  
 \*  
 \*\*\*\*\*

PIMA ROAD CHANNEL  
 by GVSCE for the City of Scottsdale  
 Project: 95

File: OPT2-6.IH1  
 Original:09-13-96 mcg

100-YEAR 6-HR HYPOTHETICAL RAINFALL DISTRIBUTION  
 RAINFALL LOSSES: SCS CURVE NUMBERS  
 UNIT HYDROGRAPH: KINEMATIC WAVE  
 ROUTING: MODIFIED PULS - USING NORMAL DEPTH

COLLECTOR CHANNEL LENGTHS ARE AS FOLLOWS:

HAPPY VALLEY ROAD ..... 1.0 MILE  
 PINNACLE PEAK ROAD ..... 0.5 MILE  
 DEER VALLEY ROAD ..... 0.25 MILE  
 BEARDLSEY ROAD ..... 1.0 MILE

DETENTION BASINS AT HAPPY VALLEY, DEER VALLEY AND UNION HILLS ROADS.

19 IO OUTPUT CONTROL VARIABLES  
 IPRNT 5 PRINT CONTROL  
 IPLOT 0 PLOT CONTROL  
 QSCAL 0. HYDROGRAPH PLOT SCALE

IT HYDROGRAPH TIME DATA  
 NMIN 5 MINUTES IN COMPUTATION INTERVAL  
 IDATE 1 0 STARTING DATE  
 ITIME 0000 STARTING TIME  
 NQ 720 NUMBER OF HYDROGRAPH ORDINATES  
 NDDATE 3 0 ENDING DATE  
 NDTIME 1155 ENDING TIME  
 ICENT 19 CENTURY MARK

COMPUTATION INTERVAL 0.08 HOURS  
 TOTAL TIME BASE 59.92 HOURS

ENGLISH UNITS  
 DRAINAGE AREA SQUARE MILES  
 PRECIPITATION DEPTH INCHES  
 LENGTH, ELEVATION FEET  
 FLOW CUBIC FEET PER SECOND  
 STORAGE VOLUME ACRE-FEET  
 SURFACE AREA ACRES  
 TEMPERATURE DEGREES FAHRENHEIT

20 JD INDEX STORM NO. 1

STRM 0.00 PRECIPITATION DEPTH  
TRDA 0.01 TRANSPOSITION DRAINAGE AREA

0 PI PRECIPITATION PATTERN

21 JD INDEX STORM NO. 2

STRM 0.00 PRECIPITATION DEPTH  
TRDA 0.10 TRANSPOSITION DRAINAGE AREA

0 PI PRECIPITATION PATTERN

22 JD INDEX STORM NO. 3

STRM 0.00 PRECIPITATION DEPTH  
TRDA 0.50 TRANSPOSITION DRAINAGE AREA

0 PI PRECIPITATION PATTERN

23 JD INDEX STORM NO. 4

STRM 0.00 PRECIPITATION DEPTH  
TRDA 1.00 TRANSPOSITION DRAINAGE AREA

0 PI PRECIPITATION PATTERN

24 JD INDEX STORM NO. 5

STRM 0.00 PRECIPITATION DEPTH  
TRDA 5.00 TRANSPOSITION DRAINAGE AREA

0 PI PRECIPITATION PATTERN

25 JD INDEX STORM NO. 6

STRM 0.00 PRECIPITATION DEPTH  
TRDA 25.00 TRANSPOSITION DRAINAGE AREA

0 PI PRECIPITATION PATTERN

RUNOFF SUMMARY  
 FLOW IN CUBIC FEET PER SECOND  
 TIME IN HOURS, AREA IN SQUARE MILES

OPERATION	STATION	PEAK FLOW	TIME OF PEAK	AVERAGE FLOW FOR MAXIMUM PERIOD			BASIN AREA	MAXIMUM STAGE	TIME OF MAX STA
				6-HOUR	24-HOUR	72-HOUR			
HYDROGRAPH AT	S30N	1227.	3.33	128.	32.	13.	0.65		
ROUTED TO	R30N	1121.	3.42	128.	32.	13.	0.65		
HYDROGRAPH AT	S31.1	395.	3.33	43.	11.	4.	0.27		
2 COMBINED AT	C31.1	1465.	3.42	171.	43.	17.	0.92		
ROUTED TO	R31.1	1476.	3.42	170.	43.	17.	0.92		
HYDROGRAPH AT	S35N	1298.	3.25	108.	27.	11.	0.55		
DIVERSION TO	D35NL	519.	3.25	43.	11.	4.	0.55		
HYDROGRAPH AT	D35NR	779.	3.25	65.	16.	7.	0.55		
ROUTED TO	R35NR	630.	3.33	64.	16.	7.	0.55		
HYDROGRAPH AT	S36.2	400.	3.25	34.	9.	3.	0.21		
2 COMBINED AT	C36.2	947.	3.25	98.	25.	10.	0.54		
DIVERSION TO	D36.2L	284.	3.25	30.	7.	3.	0.54		
HYDROGRAPH AT	D36.2R	663.	3.25	69.	17.	7.	0.54		
ROUTED TO	R36.2R	430.	3.67	69.	17.	7.	0.54		
HYDROGRAPH AT	S34.1	2491.	3.33	262.	66.	27.	1.61		
3 COMBINED AT	C34.1I	3668.	3.33	497.	126.	50.	2.90		
ROUTED TO	C34.1O	219.	5.50	211.	126.	50.	2.90		
ROUTED TO	R34.1	218.	5.58	211.	126.	50.	2.90		
HYDROGRAPH AT	S36.1	159.	3.42	19.	5.	2.	0.14		
2 COMBINED AT	C36.1	311.	3.42	226.	130.	52.	3.04		
ROUTED TO	R36.1	292.	3.58	225.	130.	52.	3.04		
HYDROGRAPH AT	B35NL	519.	3.25	43.	11.	4.	0.55		
ROUTED TO	R35NL	317.	3.58	43.	11.	4.	0.55		
HYDROGRAPH AT	B36.2L	284.	3.25	30.	7.	3.	0.54		
ROUTED TO	R36.2L	193.	3.58	29.	7.	3.	0.54		
HYDROGRAPH AT	S36R1	1107.	3.50	171.	43.	17.	1.22		

4 COMBINED AT	C36R1	1832.	3.58	459.	190.	76.	4.64
ROUTED TO	R36R1	1739.	3.67	456.	190.	76.	4.64
HYDROGRAPH AT	S36R2	509.	3.33	62.	16.	6.	0.43
2 COMBINED AT	C36R2	1964.	3.67	510.	206.	82.	5.07
HYDROGRAPH AT	S51.1	998.	3.58	155.	39.	16.	1.08
DIVERSION TO	D51.1L	998.	3.58	155.	39.	16.	1.08
HYDROGRAPH AT	D51.1	0.	0.08	0.	0.	0.	1.08
2 COMBINED AT	C51.1I	1964.	3.67	510.	206.	82.	6.14
ROUTED TO	C51.1O	282.	7.17	278.	204.	82.	6.14
HYDROGRAPH AT	B51.1L	998.	3.58	155.	39.	16.	1.08
2 COMBINED AT	C51.1A	1156.	3.58	414.	242.	97.	6.14
ROUTED TO	R51.1	1129.	3.58	412.	242.	97.	6.14
DIVERSION TO	B51.1T	1129.	3.58	412.	242.	97.	6.14
HYDROGRAPH AT	D51.1T	0.	0.08	0.	0.	0.	6.14
HYDROGRAPH AT	52D4	116.	3.25	11.	3.	1.	0.07
ROUTED TO	52D4R	106.	3.25	11.	3.	1.	0.07
HYDROGRAPH AT	52D4B	70.	3.17	6.	1.	1.	0.02
2 COMBINED AT	52D5C1	161.	3.25	17.	4.	2.	0.09
HYDROGRAPH AT	52D5A	79.	3.17	6.	2.	1.	0.02
ROUTED TO	52D5AR	75.	3.17	6.	2.	1.	0.02
2 COMBINED AT	52D5C2	217.	3.25	23.	6.	2.	0.12
ROUTED TO	52D5R	216.	3.25	23.	6.	2.	0.12
HYDROGRAPH AT	52C3	24.	3.08	2.	0.	0.	0.01
ROUTED TO	52C3R	23.	3.17	2.	0.	0.	0.01
HYDROGRAPH AT	52C3B	53.	3.08	4.	1.	0.	0.02
2 COMBINED AT	2C3BC1	74.	3.17	6.	1.	1.	0.02
2 COMBINED AT	2C3BC2	270.	3.17	29.	7.	3.	0.14
ROUTED TO	52C3BR	261.	3.25	29.	7.	3.	0.14
HYDROGRAPH AT	51C	166.	3.17	15.	4.	1.	0.10
DIVERSION TO	51C1DV	111.	3.17	10.	3.	1.	0.10

HYDROGRAPH AT	51C1D	55.	3.17	5.	1.	0.	0.10
ROUTED TO	51C1R	53.	3.25	5.	1.	0.	0.10
HYDROGRAPH AT	52C1	69.	3.17	5.	1.	0.	0.03
2 COMBINED AT	52C1C	106.	3.17	10.	2.	1.	0.06
ROUTED TO	52C1R	101.	3.25	10.	2.	1.	0.06
HYDROGRAPH AT	52C2A	35.	3.17	2.	1.	0.	0.02
2 COMBINED AT	52C2AC	125.	3.25	12.	3.	1.	0.08
HYDROGRAPH AT	52C2B	56.	3.17	4.	1.	0.	0.03
2 COMBINED AT	52C2BC	170.	3.17	16.	4.	2.	0.11
ROUTED TO	52C2BR	168.	3.25	16.	4.	2.	0.11
HYDROGRAPH AT	52C2C	46.	3.08	4.	1.	0.	0.01
2 COMBINED AT	52C2CC	194.	3.25	20.	5.	2.	0.12
ROUTED TO	52C2R	180.	3.25	20.	5.	2.	0.12
HYDROGRAPH AT	52C4	56.	3.17	4.	1.	0.	0.02
2 COMBINED AT	52C4C1	211.	3.25	24.	6.	2.	0.14
2 COMBINED AT	52C4C2	472.	3.25	53.	13.	5.	0.28
ROUTED TO	52C4R	462.	3.25	53.	14.	5.	0.28
HYDROGRAPH AT	52C13	69.	3.08	5.	1.	0.	0.02
DIVERSION TO	STORM	40.	3.08	4.	1.	0.	0.02
HYDROGRAPH AT	2C13DV	29.	3.08	1.	0.	0.	0.02
HYDROGRAPH AT	52C15	157.	3.08	13.	3.	1.	0.05
2 COMBINED AT	2C15C1	186.	3.08	13.	3.	1.	0.05
2 COMBINED AT	2C15C2	546.	3.17	66.	17.	7.	0.32
ROUTED TO	52C15R	544.	3.25	66.	17.	7.	0.32
HYDROGRAPH AT	52C14A	142.	3.17	11.	3.	1.	0.04
2 COMBINED AT	2C14AC	655.	3.17	78.	20.	8.	0.36
ROUTED TO	2C14AR	637.	3.17	78.	20.	8.	0.36
HYDROGRAPH AT	51C1DV	111.	3.17	10.	3.	1.	0.10
DIVERSION TO	51C2DV	30.	3.17	3.	1.	0.	0.10
HYDROGRAPH AT	51C2D	81.	3.17	7.	2.	1.	0.10

ROUTED TO	51C2R	78.	3.25	7.	2.	1.	0.10
HYDROGRAPH AT	52C5	40.	3.17	3.	1.	0.	0.02
2 COMBINED AT	52C5C	109.	3.17	10.	3.	1.	0.06
ROUTED TO	52C5R	104.	3.25	10.	3.	1.	0.06
HYDROGRAPH AT	52C6	82.	3.17	7.	2.	1.	0.04
2 COMBINED AT	52C6C	173.	3.25	17.	4.	2.	0.10
ROUTED TO	52C6R	165.	3.25	17.	4.	2.	0.10
HYDROGRAPH AT	51C2DV	30.	3.17	3.	1.	0.	0.10
ROUTED TO	51C3R	29.	3.25	3.	1.	0.	0.10
HYDROGRAPH AT	51B	596.	3.42	79.	20.	8.	0.57
DIVERSION TO	51B1DV	549.	3.42	72.	18.	7.	0.57
HYDROGRAPH AT	51B1D	48.	3.42	6.	2.	1.	0.57
ROUTED TO	51B1R	48.	3.42	6.	2.	1.	0.57
HYDROGRAPH AT	52C7	18.	3.08	1.	0.	0.	0.01
3 COMBINED AT	52C7C	76.	3.25	10.	3.	1.	0.07
ROUTED TO	52C7R	75.	3.33	10.	3.	1.	0.07
HYDROGRAPH AT	51B1DV	549.	3.42	72.	18.	7.	0.57
DIVERSION TO	51B2DV	461.	3.42	61.	15.	6.	0.57
HYDROGRAPH AT	51B2D	88.	3.42	12.	3.	1.	0.57
ROUTED TO	51B2R	88.	3.42	12.	3.	1.	0.57
HYDROGRAPH AT	52C8	21.	3.08	1.	0.	0.	0.01
2 COMBINED AT	52C8C	93.	3.42	13.	3.	1.	0.45
ROUTED TO	52C8R	92.	3.42	13.	3.	1.	0.45
2 COMBINED AT	52C9C1	163.	3.42	23.	6.	2.	0.52
ROUTED TO	52C9R1	162.	3.42	23.	6.	2.	0.52
HYDROGRAPH AT	52C9	174.	3.17	14.	3.	1.	0.07
2 COMBINED AT	52C9C2	255.	3.25	37.	9.	4.	0.59
ROUTED TO	52C9R2	254.	3.25	37.	9.	4.	0.59
2 COMBINED AT	2C10C1	418.	3.25	54.	14.	5.	0.69
ROUTED TO	2C10R1	412.	3.25	54.	14.	5.	0.69

HYDROGRAPH AT	52C10	28.	3.17	2.	1.	0.	0.01
2 COMBINED AT	2C10C2	428.	3.25	56.	14.	6.	0.70
HYDROGRAPH AT	52C11	96.	3.17	8.	2.	1.	0.04
ROUTED TO	2C11R1	88.	3.17	8.	2.	1.	0.04
HYDROGRAPH AT	52C13D	40.	3.08	4.	1.	0.	0.02
2 COMBINED AT	52C11C	128.	3.17	12.	3.	1.	0.07
ROUTED TO	2C11CR	120.	3.17	12.	3.	1.	0.07
2 COMBINED AT	2C11C2	541.	3.25	68.	17.	7.	0.77
ROUTED TO	2C11R2	530.	3.25	68.	17.	7.	0.77
HYDROGRAPH AT	52C12	119.	3.08	7.	2.	1.	0.02
2 COMBINED AT	52C12C	567.	3.25	75.	19.	8.	0.79
ROUTED TO	52C12R	549.	3.25	75.	19.	8.	0.79
HYDROGRAPH AT	52C14B	76.	3.08	6.	1.	1.	0.02
2 COMBINED AT	C14BC1	584.	3.25	81.	20.	8.	0.81
2 COMBINED AT	C14BC2	1200.	3.25	158.	40.	16.	1.17
ROUTED TO	52C14R	1194.	3.25	158.	40.	16.	1.17
HYDROGRAPH AT	51B2DV	461.	3.42	61.	15.	6.	0.57
DIVERSION TO	51B3DV	387.	3.42	51.	13.	5.	0.57
HYDROGRAPH AT	51B3D	74.	3.42	10.	2.	1.	0.57
ROUTED TO	51B3R	74.	3.42	10.	2.	1.	0.57
HYDROGRAPH AT	52B1	8.	3.08	1.	0.	0.	0.00
2 COMBINED AT	52B1C	76.	3.42	10.	3.	1.	0.07
ROUTED TO	52B1R	75.	3.42	10.	3.	1.	0.07
HYDROGRAPH AT	51B3DV	387.	3.42	51.	13.	5.	0.57
DIVERSION TO	51B4DV	317.	3.42	42.	11.	4.	0.57
HYDROGRAPH AT	51B4D	70.	3.42	9.	2.	1.	0.57
ROUTED TO	51B4R1	70.	3.42	9.	2.	1.	0.57
2 COMBINED AT	52B2C1	145.	3.42	20.	5.	2.	0.14
ROUTED TO	52B2R1	142.	3.42	20.	5.	2.	0.14
HYDROGRAPH AT	52B2	69.	3.17	5.	1.	1.	0.03

2 COMBINED AT	52B2C2	166.	3.42	25.	6.	3.	0.17
ROUTED TO	52B2R2	164.	3.42	25.	6.	3.	0.17
ROUTED TO	52B3R1	163.	3.42	25.	6.	3.	0.17
HYDROGRAPH AT	52B3	141.	3.17	12.	3.	1.	0.06
2 COMBINED AT	52B3C2	249.	3.25	37.	9.	4.	0.23
ROUTED TO	52B3R2	241.	3.33	37.	9.	4.	0.23
HYDROGRAPH AT	52B4	87.	3.17	7.	2.	1.	0.03
2 COMBINED AT	52B4C	284.	3.25	44.	11.	4.	0.26
ROUTED TO	52B4R	277.	3.25	44.	11.	4.	0.26
HYDROGRAPH AT	52B5	69.	3.08	5.	1.	1.	0.02
2 COMBINED AT	52B5C1	313.	3.25	49.	12.	5.	0.28
2 COMBINED AT	52B5C2	1496.	3.25	207.	52.	21.	1.45
ROUTED TO	52B5R	1474.	3.25	207.	53.	21.	1.45
HYDROGRAPH AT	51B4DV	317.	3.42	42.	11.	4.	0.57
DIVERSION TO	51B5DV	216.	3.42	28.	7.	3.	0.57
HYDROGRAPH AT	51B5D	102.	3.42	13.	3.	1.	0.57
ROUTED TO	51B5R	102.	3.42	13.	3.	1.	0.57
HYDROGRAPH AT	51B5DV	216.	3.42	28.	7.	3.	0.57
DIVERSION TO	51B6DV	114.	3.42	15.	4.	2.	0.57
HYDROGRAPH AT	51B6D	101.	3.42	13.	3.	1.	0.57
ROUTED TO	51B6R	101.	3.42	13.	3.	1.	0.57
HYDROGRAPH AT	51B6DV	114.	3.42	15.	4.	2.	0.57
DIVERSION TO	51B7DV	66.	3.42	9.	2.	1.	0.57
HYDROGRAPH AT	51B7D	48.	3.42	6.	2.	1.	0.57
ROUTED TO	51B7R1	48.	3.42	6.	2.	1.	0.57
3 COMBINED AT	51B7C	252.	3.42	33.	8.	3.	0.24
ROUTED TO	51B7R2	244.	3.42	33.	8.	3.	0.24
HYDROGRAPH AT	52B6	190.	3.17	15.	4.	2.	0.10
2 COMBINED AT	52B6C	313.	3.42	48.	12.	5.	0.34
ROUTED TO	52B6R	311.	3.42	48.	12.	5.	0.34

HYDROGRAPH AT	52B7	303.	3.17	24.	6.	2.	0.08
2 COMBINED AT	52B7C1	411.	3.25	72.	18.	7.	0.42
2 COMBINED AT	52B7C2	1871.	3.25	278.	71.	28.	1.87
HYDROGRAPH AT	52A2	263.	3.17	21.	5.	2.	0.06
2 COMBINED AT	52A2C2	2033.	3.25	299.	76.	30.	1.62
HYDROGRAPH AT	51B7DV	66.	3.42	9.	2.	1.	0.57
ROUTED TO	51B8R	66.	3.50	9.	2.	1.	0.57
HYDROGRAPH AT	52A1	340.	3.17	26.	6.	3.	0.13
2 COMBINED AT	52A1C	344.	3.17	34.	9.	3.	0.13
HYDROGRAPH AT	D51.1	1129.	3.58	412.	242.	97.	6.14
2 COMBINED AT	C52A	1242.	3.58	437.	250.	100.	6.27
ROUTED TO	R52A	1211.	3.67	435.	250.	100.	6.27
2 COMBINED AT	C52	2365.	3.50	700.	322.	129.	7.92
ROUTED TO	R52	2346.	3.58	699.	322.	129.	7.92
DIVERSION TO	B52T	2346.	3.58	699.	322.	129.	7.92
HYDROGRAPH AT	D52T	0.	0.08	0.	0.	0.	7.92
2 COMBINED AT	CLEAR	0.	0.08	0.	0.	0.	14.06
HYDROGRAPH AT	37A	1164.	3.25	119.	30.	12.	0.68
DIVERSION TO	37AW	815.	3.25	83.	21.	8.	0.68
HYDROGRAPH AT	37AE	349.	3.25	36.	9.	4.	0.68
ROUTED TO	37AE1	342.	3.25	36.	9.	4.	0.68
HYDROGRAPH AT	SUB5N	70.	3.17	5.	1.	1.	0.03
2 COMBINED AT	CP5N	394.	3.25	41.	10.	4.	0.23
ROUTED TO	RET5N	357.	3.33	40.	10.	4.	0.23
ROUTED TO	R6N.1	294.	3.42	40.	10.	4.	0.23
HYDROGRAPH AT	SUB6B	74.	3.17	5.	1.	1.	0.03
ROUTED TO	SR6B	43.	3.25	5.	1.	1.	0.03
2 COMBINED AT	CP6.1	326.	3.42	45.	12.	5.	0.26
HYDROGRAPH AT	SUB1N	47.	3.17	3.	1.	0.	0.02
ROUTED TO	R2NA	46.	3.17	3.	1.	0.	0.02

HYDROGRAPH AT	SUB2NA	34.	3.17	2.	1.	0.	0.01
2 COMBINED AT	CP2NA	80.	3.17	6.	1.	1.	0.03
ROUTED TO	SR2NA	70.	3.25	4.	1.	0.	0.03
ROUTED TO	R2NB	59.	3.33	4.	1.	0.	0.03
HYDROGRAPH AT	SUB2NB	96.	3.17	8.	2.	1.	0.03
2 COMBINED AT	CP2NB	99.	3.33	12.	3.	1.	0.06
ROUTED TO	SR2NB	25.	3.75	11.	3.	1.	0.06
ROUTED TO	RCP4N	24.	3.75	11.	3.	1.	0.06
HYDROGRAPH AT	SUB6N	114.	3.17	8.	2.	1.	0.05
ROUTED TO	RET6N	0.	0.08	0.	0.	0.	0.05
ROUTED TO	RCP4N1	0.	0.08	0.	0.	0.	0.05
2 COMBINED AT	CP4N.1	24.	3.75	11.	3.	1.	0.11
HYDROGRAPH AT	SUB3N	67.	3.17	4.	1.	0.	0.03
ROUTED TO	RET3N	4.	4.17	3.	1.	0.	0.03
ROUTED TO	R4N	4.	4.25	3.	1.	0.	0.03
2 COMBINED AT	CP4N.2	27.	3.75	14.	4.	2.	0.14
HYDROGRAPH AT	SUB4N	80.	3.17	6.	1.	1.	0.03
2 COMBINED AT	CP4N	89.	3.17	19.	6.	2.	0.17
ROUTED TO	R6N	82.	3.17	19.	6.	2.	0.17
HYDROGRAPH AT	SUB6A	64.	3.08	4.	1.	0.	0.01
2 COMBINED AT	CP6.2	121.	3.17	23.	7.	3.	0.18
2 COMBINED AT	CP6N	376.	3.42	68.	18.	7.	0.45
ROUTED TO	RCP6N	373.	3.42	68.	18.	7.	0.45
HYDROGRAPH AT	SUB3C	55.	3.08	3.	1.	0.	0.01
2 COMBINED AT	CP3C	380.	3.42	70.	19.	8.	0.46
ROUTED TO	R3C	361.	3.50	70.	19.	8.	0.46
HYDROGRAPH AT	GC1018	101.	3.17	7.	2.	1.	0.04
HYDROGRAPH AT	GC1-9	58.	3.17	4.	1.	0.	0.03
HYDROGRAPH AT	SUB3S	33.	3.17	3.	1.	0.	0.01
4 COMBINED AT	CP3S	411.	3.50	84.	22.	9.	0.54

ROUTED TO	RT3S	409.	3.50	84.	22.	9.	0.54
HYDROGRAPH AT	SUB4S	87.	3.17	7.	2.	1.	0.03
ROUTED TO	RT4S	87.	3.17	7.	2.	1.	0.03
HYDROGRAPH AT	GC2-8	32.	3.17	2.	1.	0.	0.01
3 COMBINED AT	1PGC28	437.	3.50	93.	25.	10.	0.58
HYDROGRAPH AT	SUB3D3	35.	3.17	2.	1.	0.	0.01
2 COMBINED AT	CPGC28	444.	3.50	95.	25.	10.	0.59
ROUTED TO	SRGC28	443.	3.25	95.	25.	10.	0.59
ROUTED TO	RT7S	431.	3.58	95.	25.	10.	0.59
HYDROGRAPH AT	GC7	31.	3.17	2.	1.	0.	0.01
2 COMBINED AT	CP7S	437.	3.58	97.	26.	10.	0.61
DIVERSION TO	B7ST	437.	3.58	97.	26.	10.	0.61
HYDROGRAPH AT	D7ST	0.	0.08	0.	0.	0.	0.61
2 COMBINED AT	CLEAR	0.	0.08	0.	0.	0.	14.66
HYDROGRAPH AT	SUB3D1	27.	3.08	2.	0.	0.	0.01
ROUTED TO	RD1B1	22.	3.17	2.	0.	0.	0.01
HYDROGRAPH AT	SUB3B1	47.	3.08	3.	1.	0.	0.01
2 COMBINED AT	CP3B1	61.	3.08	5.	1.	1.	0.02
ROUTED TO	RB13F	48.	3.25	5.	1.	1.	0.02
HYDROGRAPH AT	SUB3F	141.	3.08	10.	2.	1.	0.03
2 COMBINED AT	CP3F	169.	3.08	15.	4.	2.	0.06
HYDROGRAPH AT	SUB3B2	67.	3.17	6.	1.	1.	0.02
ROUTED TO	RB2E1	64.	3.17	6.	1.	1.	0.02
ROUTED TO	RB2E2	61.	3.25	6.	1.	1.	0.02
HYDROGRAPH AT	SUB3E1	67.	3.17	6.	1.	1.	0.02
2 COMBINED AT	1CPE31	125.	3.17	11.	3.	1.	0.05
HYDROGRAPH AT	SUB3D2	58.	3.17	5.	1.	0.	0.02
ROUTED TO	RD2E2	56.	3.17	5.	1.	0.	0.02
HYDROGRAPH AT	SUB3E2	37.	3.08	3.	1.	0.	0.01
2 COMBINED AT	CP3E2	86.	3.17	7.	2.	1.	0.03

HYDROGRAPH AT	PC3	82.	3.17	7.	2.	1.	0.04
4 COMBINED AT	CPC3	449.	3.17	40.	10.	4.	0.18
DIVERSION TO	BPC3T	449.	3.17	40.	10.	4.	0.18
HYDROGRAPH AT	DPC3T	0.	0.08	0.	0.	0.	0.18
HYDROGRAPH AT	SUB3E3	60.	3.08	4.	1.	0.	0.02
HYDROGRAPH AT	PC4	43.	3.17	3.	1.	0.	0.02
HYDROGRAPH AT	D7S	437.	3.58	97.	26.	10.	0.61
3 COMBINED AT	CPC4	471.	3.33	104.	28.	11.	0.65
DIVERSION TO	BPC4T	471.	3.33	104.	28.	11.	0.65
HYDROGRAPH AT	DPC4T	0.	0.08	0.	0.	0.	0.65
3 COMBINED AT	CLEAR	0.	0.08	0.	0.	0.	15.50
HYDROGRAPH AT	37AW	815.	3.25	83.	21.	8.	0.68
ROUTED TO	R14R	659.	3.33	83.	21.	8.	0.68
ROUTED TO	RET141	631.	3.42	78.	21.	8.	0.68
ROUTED TO	R14.1	558.	3.50	78.	21.	8.	0.68
HYDROGRAPH AT	SUB13N	81.	3.17	7.	2.	1.	0.04
ROUTED TO	R14.1	78.	3.25	7.	2.	1.	0.04
HYDROGRAPH AT	SUB14N	88.	3.25	8.	2.	1.	0.05
3 COMBINED AT	CP14	625.	3.50	92.	25.	10.	0.56
ROUTED TO	RET14	574.	3.58	88.	25.	10.	0.56
ROUTED TO	R18.1	570.	3.58	88.	25.	10.	0.56
HYDROGRAPH AT	SUB20N	47.	3.17	4.	1.	0.	0.02
ROUTED TO	R19	48.	3.25	4.	1.	0.	0.02
HYDROGRAPH AT	SUB19N	94.	3.17	8.	2.	1.	0.04
2 COMBINED AT	CP19N	133.	3.17	12.	3.	1.	0.06
ROUTED TO	R18NC	132.	3.25	12.	3.	1.	0.06
HYDROGRAPH AT	UB18NC	62.	3.17	5.	1.	0.	0.02
3 COMBINED AT	CP18NC	619.	3.58	103.	29.	12.	0.64
ROUTED TO	RPC1	628.	3.58	103.	29.	12.	0.64
HYDROGRAPH AT	UB18NA	65.	3.17	5.	1.	1.	0.02

ROUTED TO	1RPC1	31.	3.33	5.	1.	1.	0.02
HYDROGRAPH AT	UB18NB	27.	3.17	2.	1.	0.	0.01
ROUTED TO	2RPC1	16.	3.25	2.	1.	0.	0.01
HYDROGRAPH AT	PC1	66.	3.42	10.	2.	1.	0.06
3 COMBINED AT	1CPC1	107.	3.42	17.	4.	2.	0.09
ROUTED TO	SRPC1	108.	3.42	16.	4.	2.	0.09
2 COMBINED AT	CPC1	712.	3.58	120.	33.	13.	0.74
ROUTED TO	R16NA1	720.	3.58	119.	33.	13.	0.74
HYDROGRAPH AT	UB16NA	42.	3.17	3.	1.	0.	0.01
ROUTED TO	R16NA1	37.	3.17	3.	1.	0.	0.01
2 COMBINED AT	C16NA1	728.	3.58	122.	34.	14.	0.75
ROUTED TO	R16NB1	717.	3.58	122.	34.	14.	0.75
HYDROGRAPH AT	UB16NB	48.	3.17	4.	1.	0.	0.02
ROUTED TO	R16NB1	43.	3.17	4.	1.	0.	0.02
2 COMBINED AT	C16NB1	725.	3.58	126.	35.	14.	0.77
ROUTED TO	R16NC1	727.	3.67	126.	35.	14.	0.77
HYDROGRAPH AT	SUB7N	74.	3.17	5.	1.	1.	0.03
ROUTED TO	R8NC	64.	3.25	5.	1.	1.	0.03
HYDROGRAPH AT	SUB8NA	13.	3.08	1.	0.	0.	0.00
ROUTED TO	SR8NA	1.	4.17	0.	0.	0.	0.00
ROUTED TO	R8NB	1.	4.17	0.	0.	0.	0.00
HYDROGRAPH AT	SUB8NB	34.	3.08	2.	1.	0.	0.01
2 COMBINED AT	CP8NB	34.	3.08	3.	1.	0.	0.02
ROUTED TO	SR8NB	2.	3.08	2.	1.	0.	0.02
ROUTED TO	R8NC	2.	3.08	2.	1.	0.	0.02
HYDROGRAPH AT	SUB8NC	51.	3.08	3.	1.	0.	0.02
3 COMBINED AT	CP8NC	103.	3.17	10.	3.	1.	0.07
ROUTED TO	SR8NC	18.	3.75	10.	3.	1.	0.07
ROUTED TO	R9N	17.	3.75	10.	3.	1.	0.07
HYDROGRAPH AT	SUB9N	143.	3.17	11.	3.	1.	0.05

2 COMBINED AT	CP9N	153.	3.17	21.	6.	2.	0.12
ROUTED TO	R10B	148.	3.17	21.	6.	2.	0.12
HYDROGRAPH AT	SUB10B	87.	3.08	6.	2.	1.	0.03
2 COMBINED AT	CP10B	226.	3.17	27.	7.	3.	0.15
ROUTED TO	R11NA	229.	3.17	27.	7.	3.	0.15
HYDROGRAPH AT	UB11NA	21.	3.08	1.	0.	0.	0.01
2 COMBINED AT	CP11NA	245.	3.17	28.	8.	3.	0.16
ROUTED TO	SR11NA	145.	3.33	28.	8.	3.	0.16
ROUTED TO	R11NB	140.	3.33	28.	8.	3.	0.16
HYDROGRAPH AT	UB11NB	22.	3.08	1.	0.	0.	0.01
2 COMBINED AT	CP11NB	146.	3.33	29.	8.	3.	0.17
ROUTED TO	SR11NB	84.	3.50	28.	8.	3.	0.17
ROUTED TO	R11NC	87.	3.50	28.	8.	3.	0.17
HYDROGRAPH AT	UB11NC	19.	3.08	1.	0.	0.	0.01
2 COMBINED AT	C11NC1	90.	3.50	30.	8.	3.	0.17
HYDROGRAPH AT	SUB10A	88.	3.08	7.	2.	1.	0.03
ROUTED TO	R12NB	95.	3.17	7.	2.	1.	0.03
HYDROGRAPH AT	UB12NA	36.	3.17	3.	1.	0.	0.02
ROUTED TO	SR12NA	1.	6.17	0.	0.	0.	0.02
ROUTED TO	R12NA	1.	6.17	0.	0.	0.	0.02
HYDROGRAPH AT	UB12NB	37.	3.17	3.	1.	0.	0.02
3 COMBINED AT	CP12NB	132.	3.17	10.	3.	1.	0.06
ROUTED TO	SR12NB	2.	3.17	2.	2.	1.	0.06
ROUTED TO	R11NC2	2.	3.50	2.	2.	1.	0.06
2 COMBINED AT	CP11NC	92.	3.50	32.	10.	4.	0.23
ROUTED TO	SR11NC	71.	3.75	30.	10.	4.	0.23
ROUTED TO	R16NC	71.	3.75	30.	10.	4.	0.23
HYDROGRAPH AT	UB16NC	102.	3.17	8.	2.	1.	0.03
2 COMBINED AT	CP16NC	107.	3.17	36.	12.	5.	0.27
ROUTED TO	R16NC1	106.	3.17	36.	12.	5.	0.27

2 COMBINED AT	C16NC1	788.	3.67	162.	47.	19.	1.03
ROUTED TO	R15N1	793.	3.67	162.	47.	19.	1.03
HYDROGRAPH AT	PC2	93.	3.25	8.	2.	1.	0.05
2 COMBINED AT	CP15N1	815.	3.67	170.	49.	20.	1.09
ROUTED TO	SRPC2	786.	3.75	169.	48.	20.	1.09
HYDROGRAPH AT	UB17NA	28.	3.08	2.	0.	0.	0.01
ROUTED TO	SR17NA	2.	3.75	1.	0.	0.	0.01
ROUTED TO	R17NB	2.	3.75	1.	0.	0.	0.01
HYDROGRAPH AT	UB17NB	27.	3.17	2.	0.	0.	0.01
2 COMBINED AT	CP17NB	28.	3.17	3.	1.	0.	0.02
ROUTED TO	SR17NB	1.	3.00	1.	1.	0.	0.02
ROUTED TO	R17A	1.	3.08	1.	1.	0.	0.02
HYDROGRAPH AT	SUB17A	30.	3.08	2.	0.	0.	0.01
2 COMBINED AT	CP17A1	31.	3.08	3.	1.	1.	0.03
HYDROGRAPH AT	UB17NC	19.	3.08	1.	0.	0.	0.01
2 COMBINED AT	CP17A	50.	3.08	3.	2.	1.	0.03
ROUTED TO	R15N	34.	3.17	3.	2.	1.	0.03
HYDROGRAPH AT	SUB15N	142.	3.17	11.	3.	1.	0.04
2 COMBINED AT	CP15N	175.	3.17	14.	4.	2.	0.07
ROUTED TO	R15N2	179.	3.17	14.	4.	2.	0.07
2 COMBINED AT	CP15N2	804.	3.75	182.	53.	22.	1.16
ROUTED TO	R15N2	768.	3.83	182.	53.	22.	1.16
HYDROGRAPH AT	DPC3	449.	3.17	40.	10.	4.	0.18
2 COMBINED AT	CPC3A	812.	3.75	217.	62.	25.	1.34
ROUTED TO	RPC3A	815.	3.83	217.	62.	25.	1.34
HYDROGRAPH AT	DPC4	471.	3.33	104.	28.	11.	0.65
2 COMBINED AT	CPC4A	1132.	3.75	319.	90.	36.	1.99
ROUTED TO	RPC4A	1123.	3.83	319.	90.	36.	1.99
DIVERSION TO	BPC4AT	1123.	3.83	319.	90.	36.	1.99
HYDROGRAPH AT	DPC4AT	0.	0.08	0.	0.	0.	1.99

HYDROGRAPH AT	SUB1-2	181.	3.17	16.	4.	2.	0.06
HYDROGRAPH AT	GCRB18	27.	3.17	2.	1.	0.	0.01
2 COMBINED AT	CPRET1	208.	3.17	18.	4.	2.	0.07
ROUTED TO	SR18S	0.	0.08	0.	0.	0.	0.07
HYDROGRAPH AT	SUB5S	72.	3.17	5.	1.	1.	0.03
HYDROGRAPH AT	GC1216	83.	3.17	6.	2.	1.	0.04
HYDROGRAPH AT	GC1415	104.	3.17	7.	2.	1.	0.05
HYDROGRAPH AT	SUB6S	53.	3.17	5.	1.	0.	0.02
HYDROGRAPH AT	SUB7S	79.	3.17	6.	2.	1.	0.03
5 COMBINED AT	CPRET2	391.	3.17	30.	7.	3.	0.16
ROUTED TO	SRRET2	0.	0.08	0.	0.	0.	0.16
4 COMBINED AT	CLEAR	0.	0.08	0.	0.	0.	17.72
HYDROGRAPH AT	SUB8S	76.	3.17	6.	1.	1.	0.03
ROUTED TO	RGC36	64.	3.25	6.	1.	1.	0.03
HYDROGRAPH AT	GC36	77.	3.17	7.	2.	1.	0.04
2 COMBINED AT	C1GC36	141.	3.17	13.	3.	1.	0.07
HYDROGRAPH AT	SUB9S	68.	3.17	5.	1.	1.	0.02
ROUTED TO	R9S	69.	3.17	5.	1.	1.	0.02
2 COMBINED AT	CPGC36	210.	3.17	18.	4.	2.	0.09
ROUTED TO	SRGC36	202.	3.25	18.	4.	2.	0.09
HYDROGRAPH AT	SUB7A	27.	3.17	2.	1.	0.	0.01
ROUTED TO	SR7A	7.	3.42	2.	1.	0.	0.01
ROUTED TO	R10S	7.	3.58	2.	1.	0.	0.01
HYDROGRAPH AT	SUB10S	78.	3.17	6.	2.	1.	0.02
2 COMBINED AT	CP10S	81.	3.17	8.	2.	1.	0.03
HYDROGRAPH AT	SUB11S	118.	3.08	7.	2.	1.	0.02
ROUTED TO	R11S	88.	3.17	7.	2.	1.	0.02
2 COMBINED AT	C10SA	169.	3.17	15.	4.	2.	0.06
ROUTED TO	R10SA	173.	3.17	15.	4.	2.	0.06
HYDROGRAPH AT	GC45	45.	3.08	2.	1.	0.	0.01

HYDROGRAPH AT	PC5	60.	3.17	5.	1.	1.	0.04
HYDROGRAPH AT	DPC4A	1123.	3.83	319.	90.	36.	1.99
5 COMBINED AT	CPC5	1263.	3.33	356.	100.	40.	2.10
ROUTED TO	RPC5	1195.	3.42	356.	100.	40.	2.10
HYDROGRAPH AT	SCN5C	351.	3.42	44.	11.	4.	0.27
HYDROGRAPH AT	SCN6	730.	3.25	82.	21.	8.	0.26
HYDROGRAPH AT	D52	2346.	3.58	699.	322.	129.	7.92
HYDROGRAPH AT	S53A	226.	3.33	24.	6.	2.	0.17
2 COMBINED AT	C53	2464.	3.50	721.	327.	131.	8.09
ROUTED TO	R53	2463.	3.50	720.	327.	131.	8.09
HYDROGRAPH AT	S53A1	445.	3.33	53.	13.	5.	0.34
2 COMBINED AT	C53A	2824.	3.42	769.	340.	136.	8.42
4 COMBINED AT	C1I	4637.	3.42	1214.	462.	186.	11.05
ROUTED TO	C10	704.	5.75	655.	462.	186.	11.05
ROUTED TO	RC1	704.	5.83	655.	462.	186.	11.05
HYDROGRAPH AT	S54	136.	3.25	14.	4.	1.	0.09
HYDROGRAPH AT	SCN6A	198.	3.33	22.	6.	2.	0.13
3 COMBINED AT	C1A	717.	5.75	670.	471.	189.	11.27

\*\*\* NORMAL END OF HEC-1 \*\*\*

## APPENDIX C

### Detention basin area-capacity curves, outlet rating curves, stage hydrographs, and hydrographs for 100-year, 24-hour storms

#### FIGURES

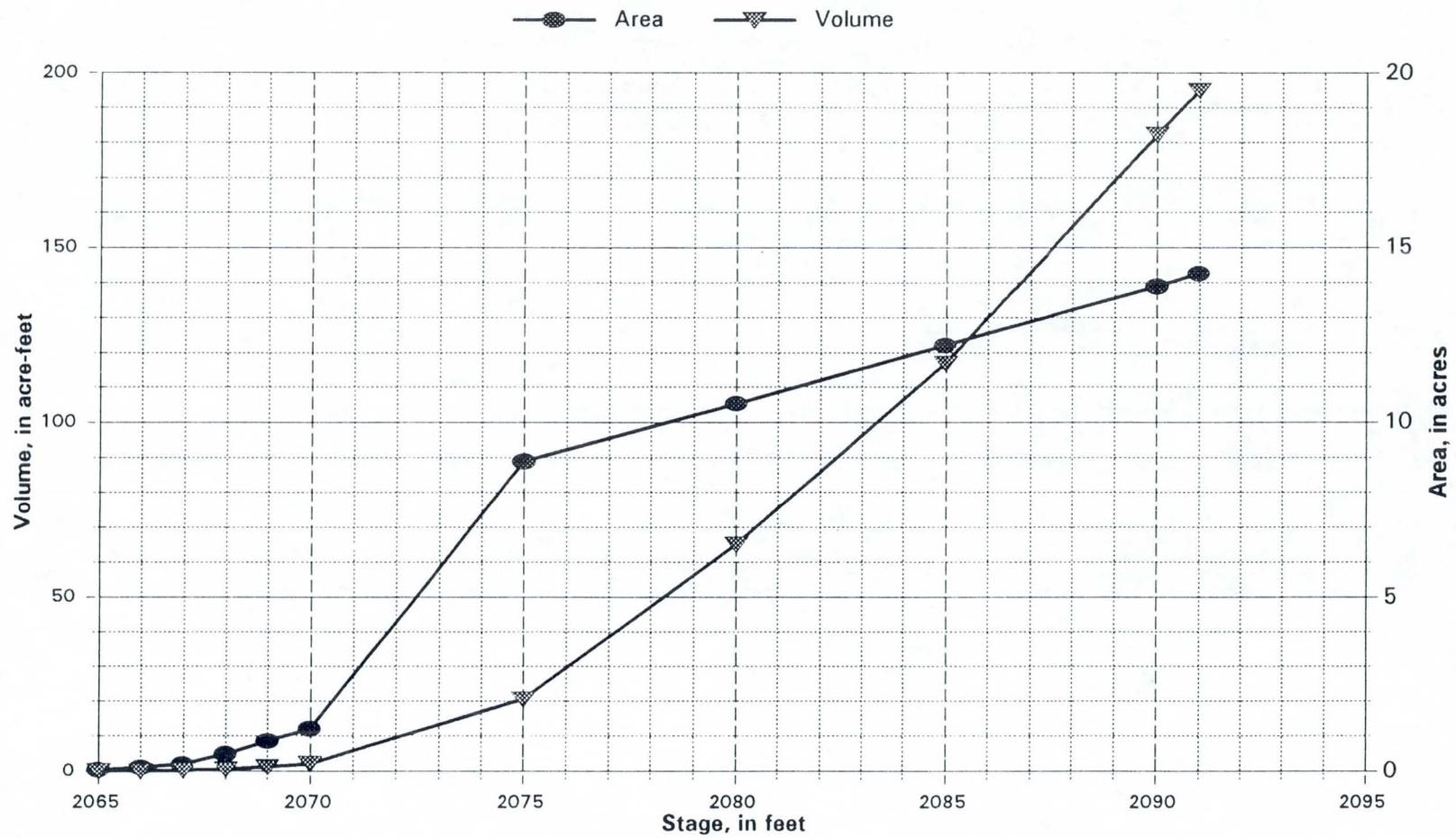
- C-1 Happy Valley Detention Basin area - capacity curves
- C-2 Happy Valley Detention Basin outlet rating curve
- C-3 Happy Valley Detention Basin hydrographs with 100% of runoff entering the basin for the 100-year, 24-hour storm
- C-4 Happy Valley Detention Basin stage hydrographs
- C-5 Deer Valley Detention Basin - Option 1, area-capacity curves
- C-6 Deer Valley Detention Basin - Option 1, outlet rating curve
- C-7 Deer Valley Detention Basin - Option 1, Case 1, hydrographs for the 100-year, 24-hour storm
- C-8 Deer Valley Detention Basin - Option 1, Case 1, stage hydrographs
- C-9 Deer Valley Detention Basin - Option 1, Case 2, hydrographs for the 100-year, 24-hour storm
- C10 Deer Valley Detention Basin - Option 1, Case 2, stage hydrographs
- C-11 Deer Valley Detention Basin - Option 2, area-capacity curves
- C-12 Deer Valley Detention Basin - Option 2, outlet rating curve
- C-13 Deer Valley Detention Basin - Option 2, Case 1, hydrographs for the 100-year, 24-hour storm
- C-14 Deer Valley Detention Basin - Option 2, Case 1, stage hydrographs
- C-15 Deer Valley Detention Basin - Option 2, Case 2, hydrographs for the 100-year, 24-hour storm
- C-16 Deer Valley Detention Basin - Option 2, Case 2, stage hydrographs
- C-17 Union Hills Detention Basin - Option 1, area-capacity curves
- C-18 Union Hills Detention Basin outlet rating curve

## APPENDIX C

### Detention basin area-capacity curves, outlet rating curves, stage hydrographs, and hydrographs for 100-year, 24-hour storms

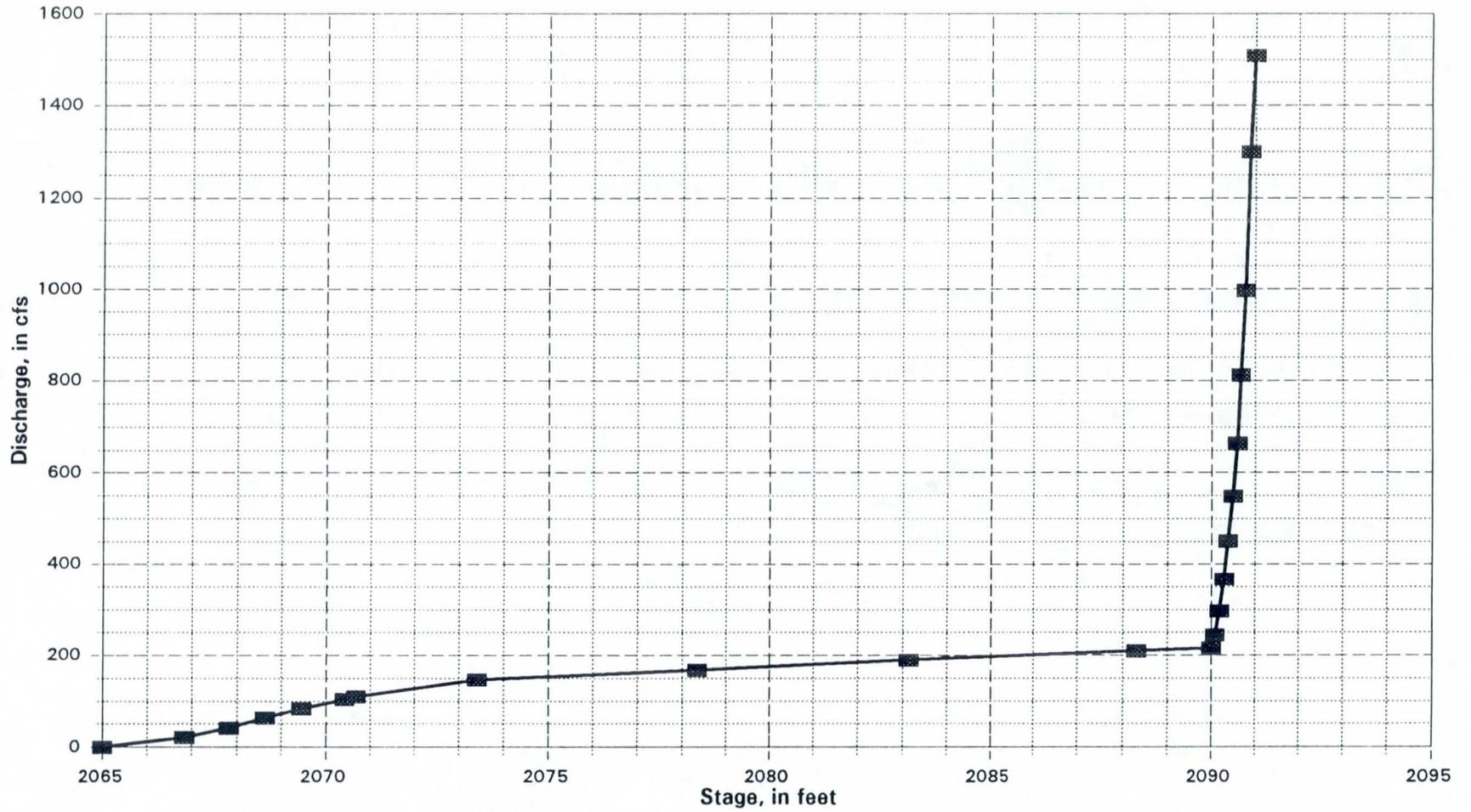
#### FIGURES

- C-19 Union Hills Detention Basin - Option 1, Case 1, hydrographs for the 100-year, 24-hour storm
- C-20 Union Hills Detention Basin - Option 1, Case 1, stage hydrographs
- C-21 Union Hills Detention Basin - Option 1, Case 2, hydrographs for the 100-year, 24-hour storm
- C-22 Union Hills Detention Basin - Option 1, Case 2, stage hydrographs
- C-23 Union Hills Detention Basin - Option 2, area-capacity curves
- C-24 Union Hills Detention Basin - Option 2, outlet rating curve
- C-25 Union Hills Detention Basin - Option 2, Case 1, hydrographs for the 100-year, 24-hour storm
- C-26 Union Hills Detention Basin - Option 2, Case 1, stage hydrographs
- C-27 Union Hills Detention Basin - Option 2, Case 2 - hydrographs for the 100-year, 24-hour storm
- C-28 Union Hills Detention Basin - Option 2, Case 2, stage hydrographs

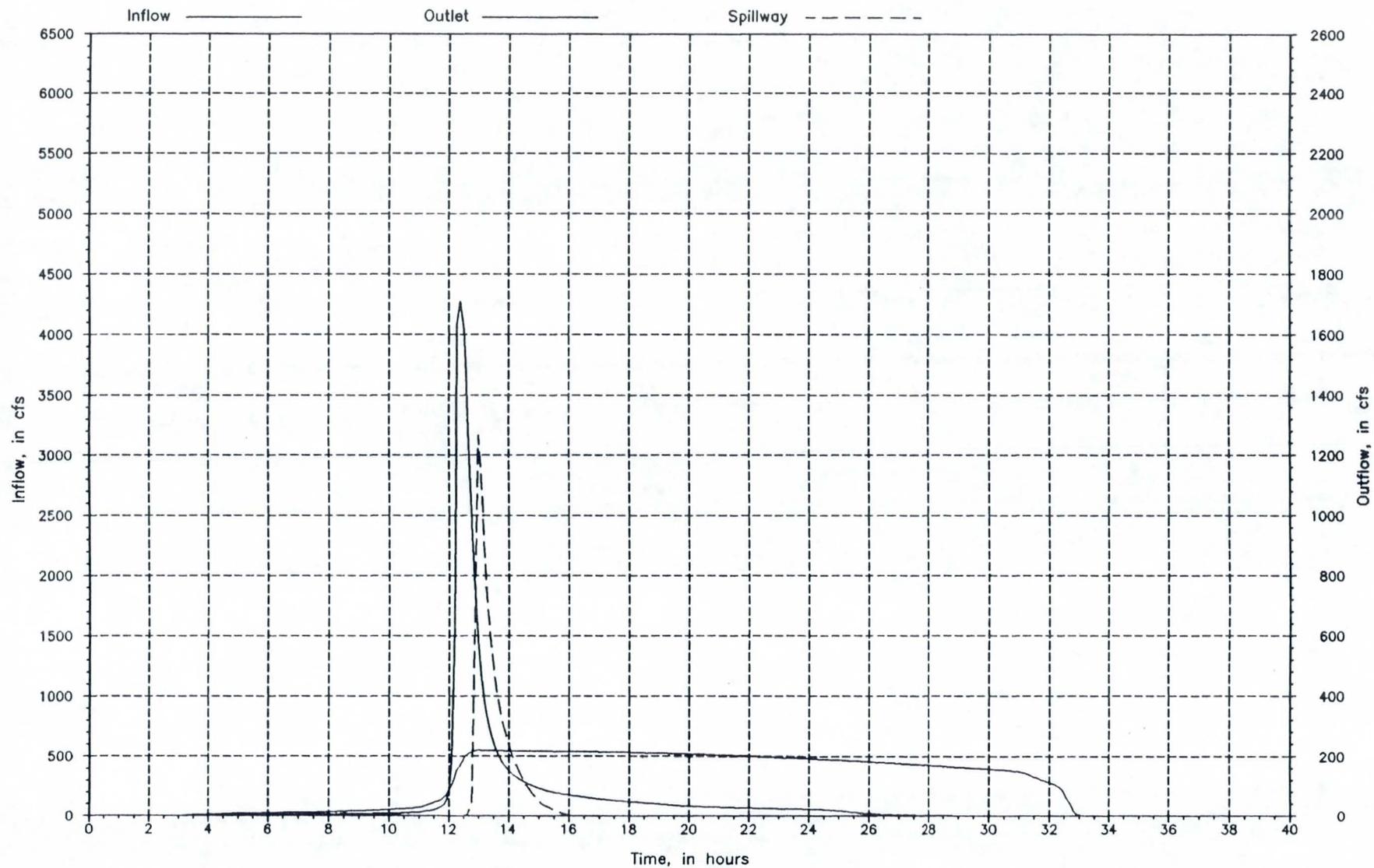


**FIGURE C-1**  
**Happy Valley Detention Basin**  
**area - capacity curves**

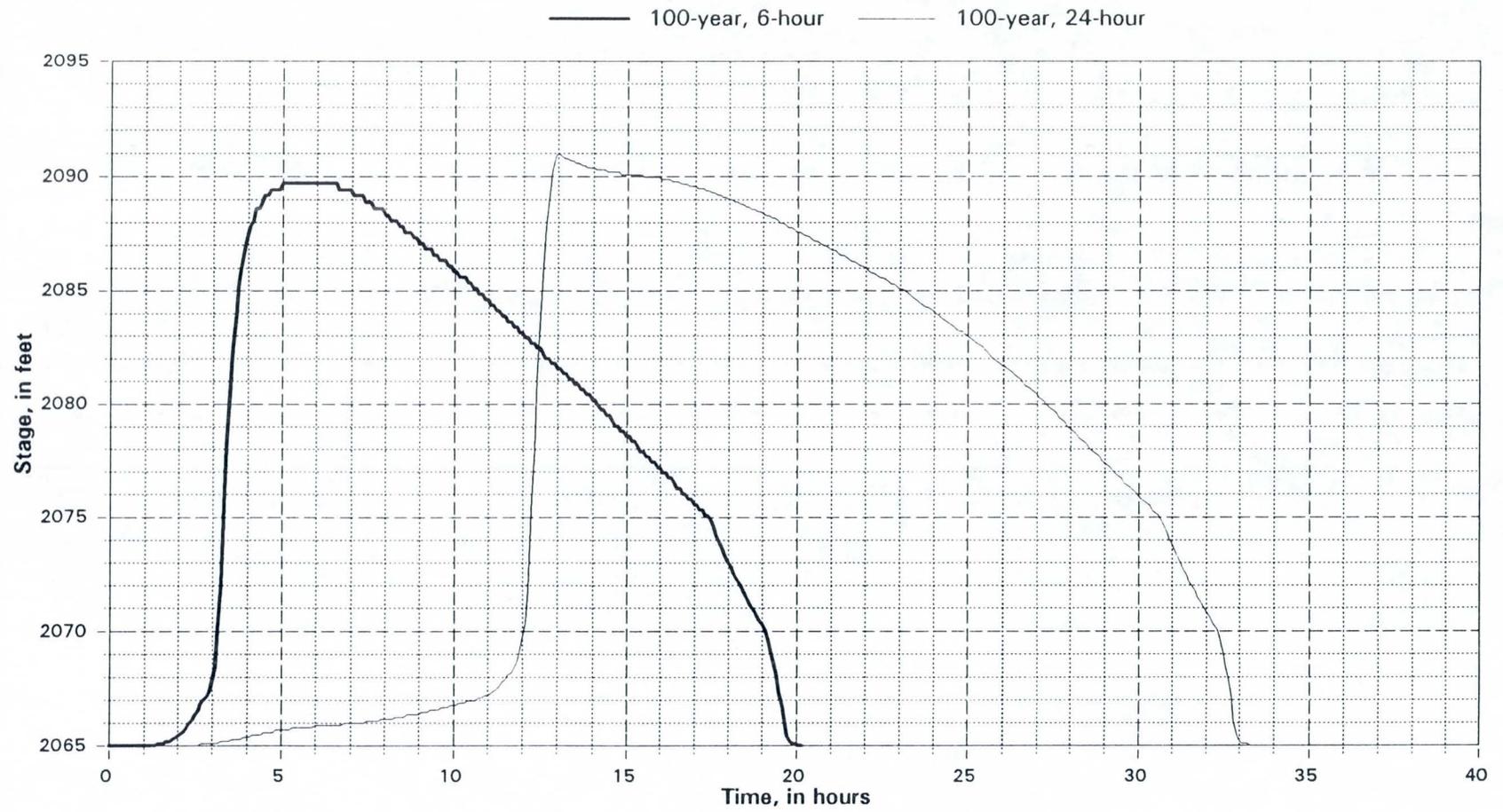
48 inch outlet conduit



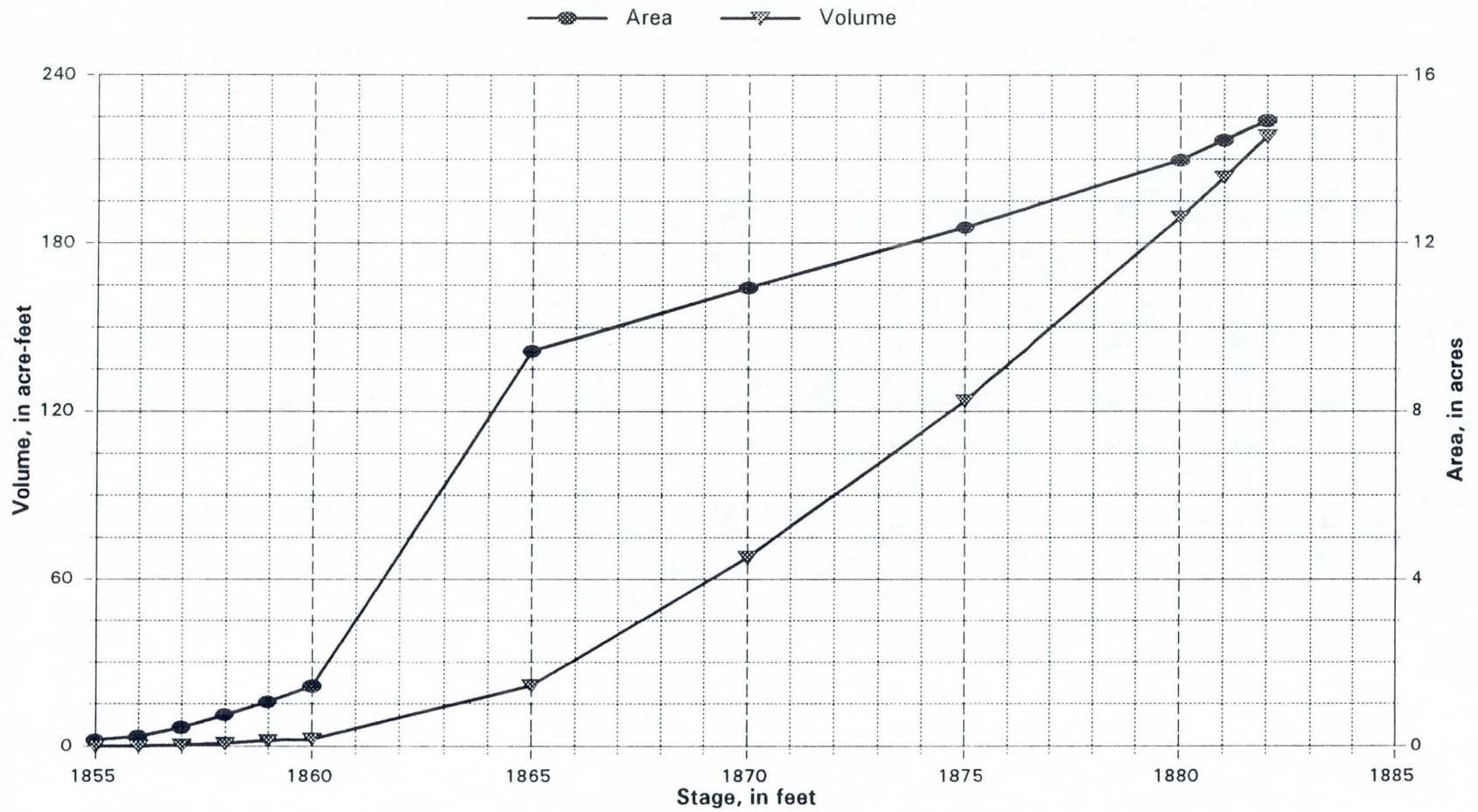
**FIGURE C-2**  
**Happy Valley Detention Basin**  
**outlet rating curve**



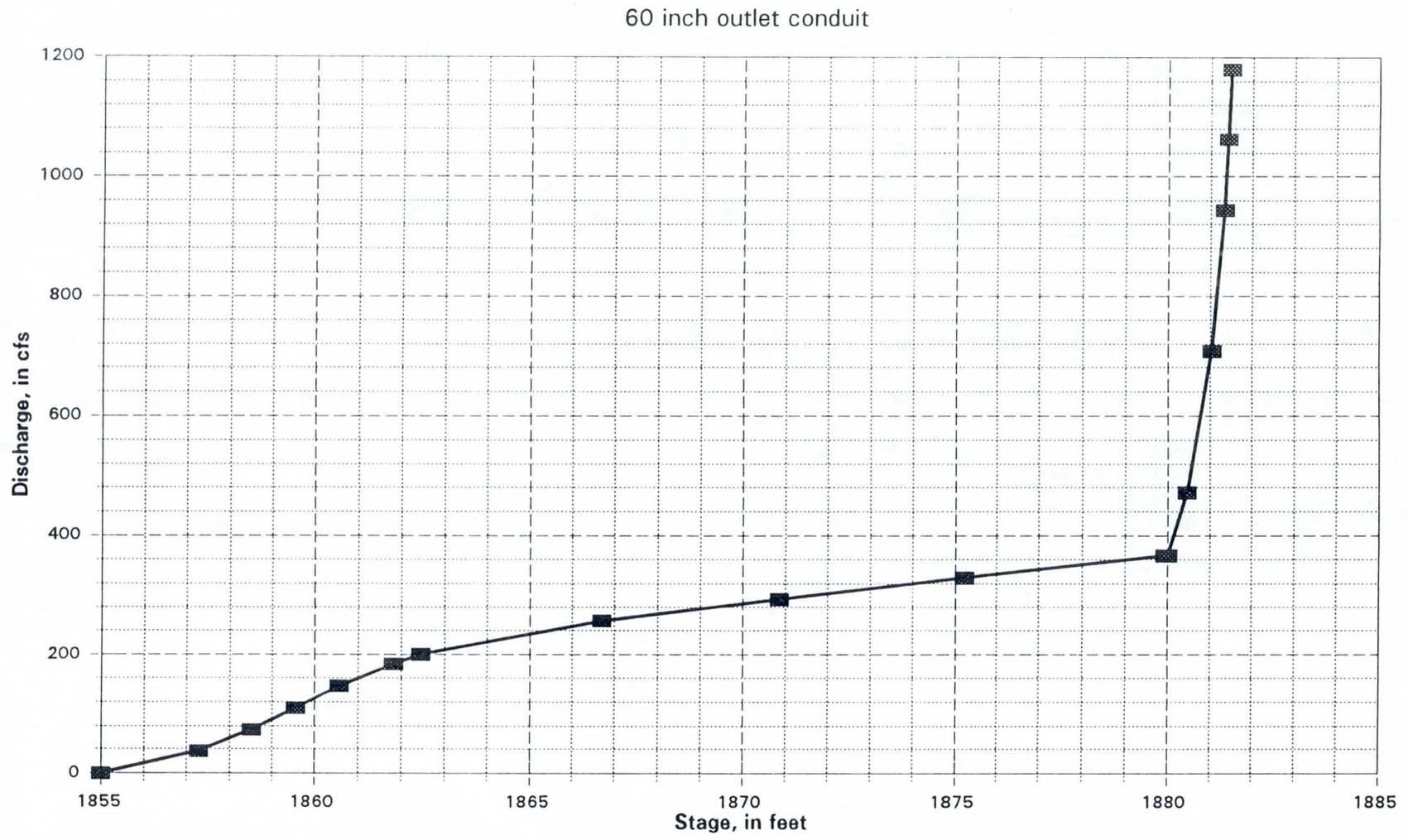
**FIGURE C-3**  
 Happy Valley Detention Basin hydrographs  
 with 100% of runoff entering the basin  
 for the 100-year, 24-hour storm



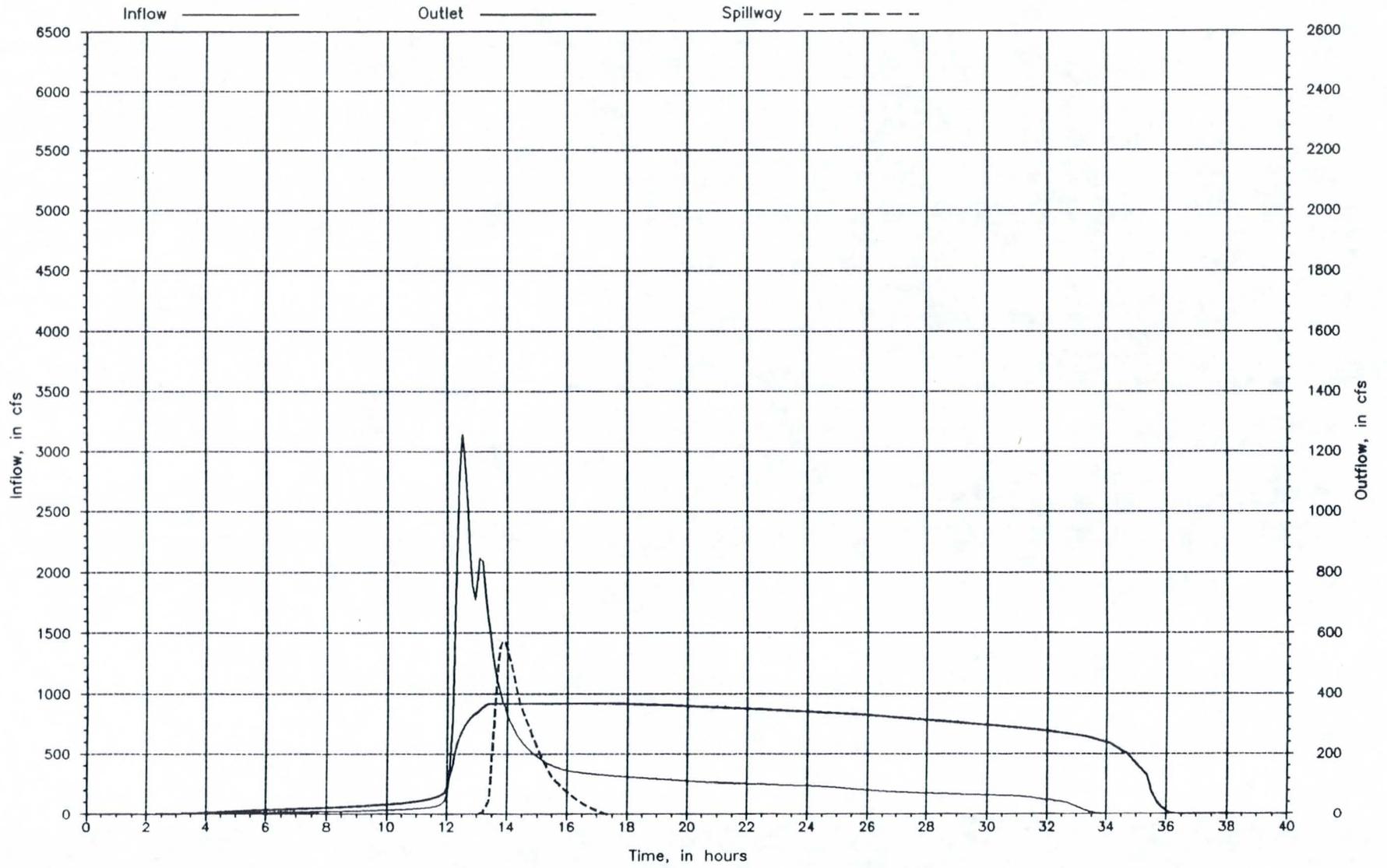
**FIGURE C-4**  
**Happy Valley Detention Basin**  
**stage hydrographs**



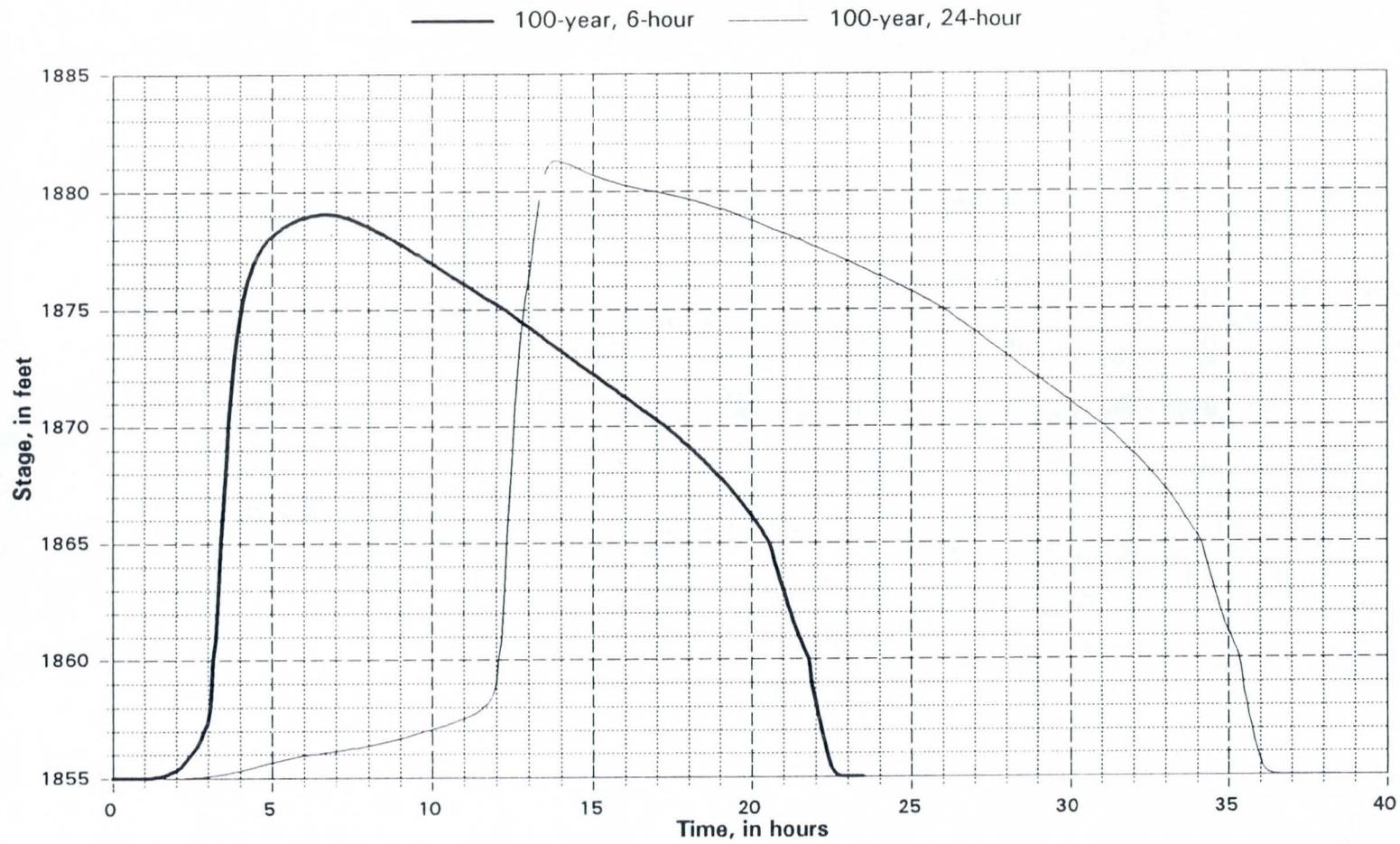
**FIGURE C-5**  
**Deer Valley Detention Basin - Option 1**  
**area-capacity curves**



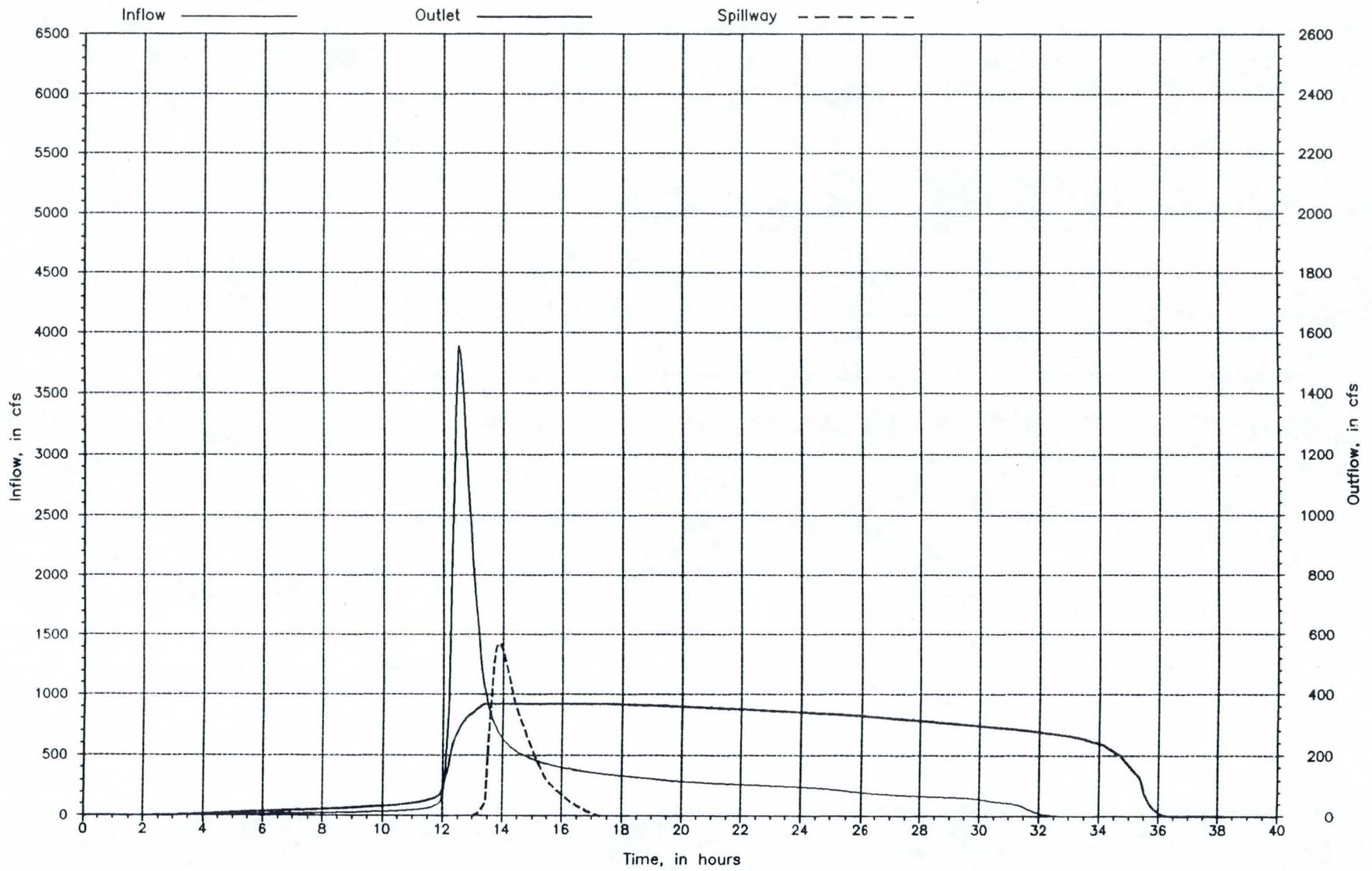
**FIGURE C-6**  
**Deer Valley Detention Basin - Option 1**  
**outlet rating curve**



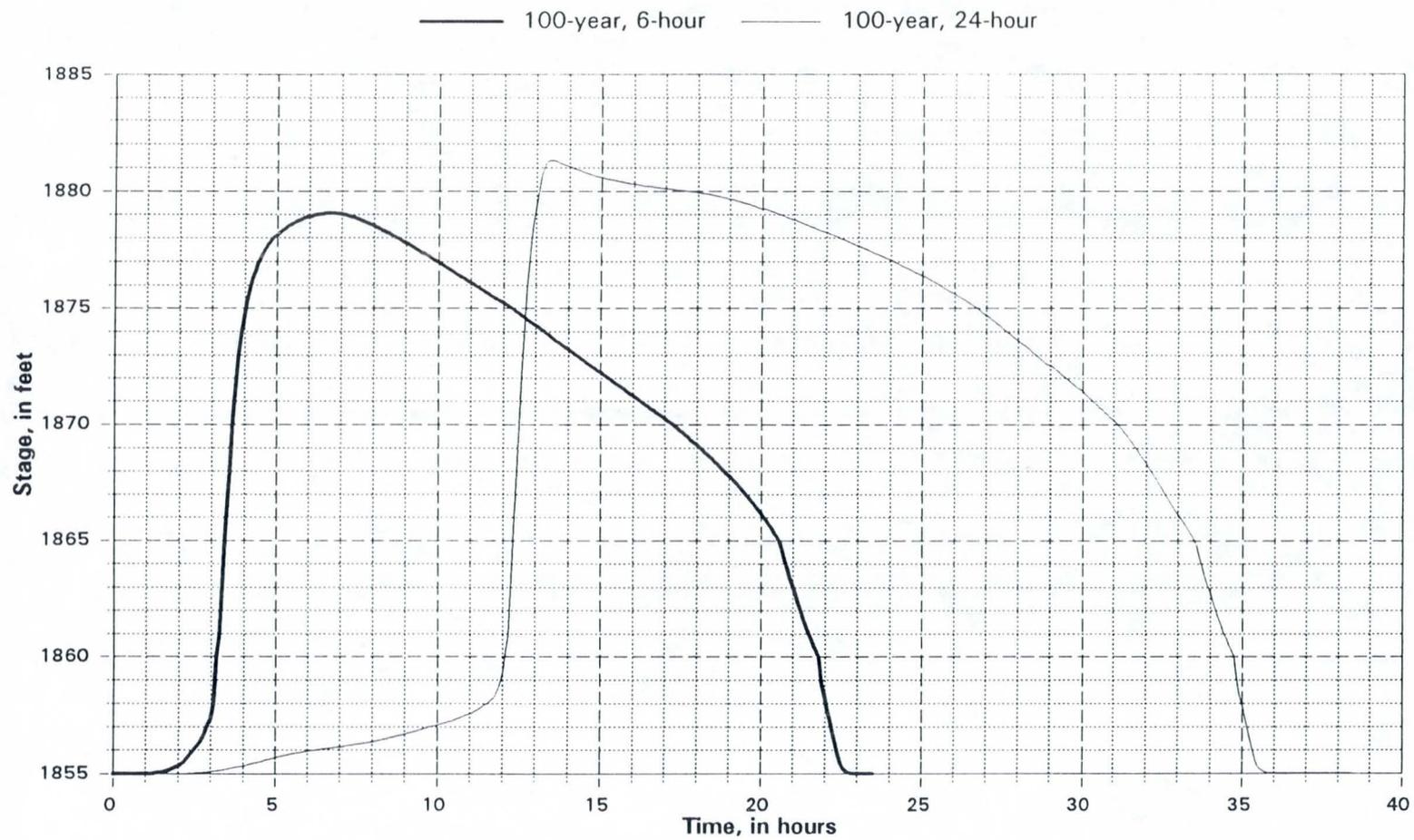
**FIGURE C-7**  
 Deer Valley Detention Basin - Option 1, Case 1  
 hydrographs for the 100-year, 24-hour storm



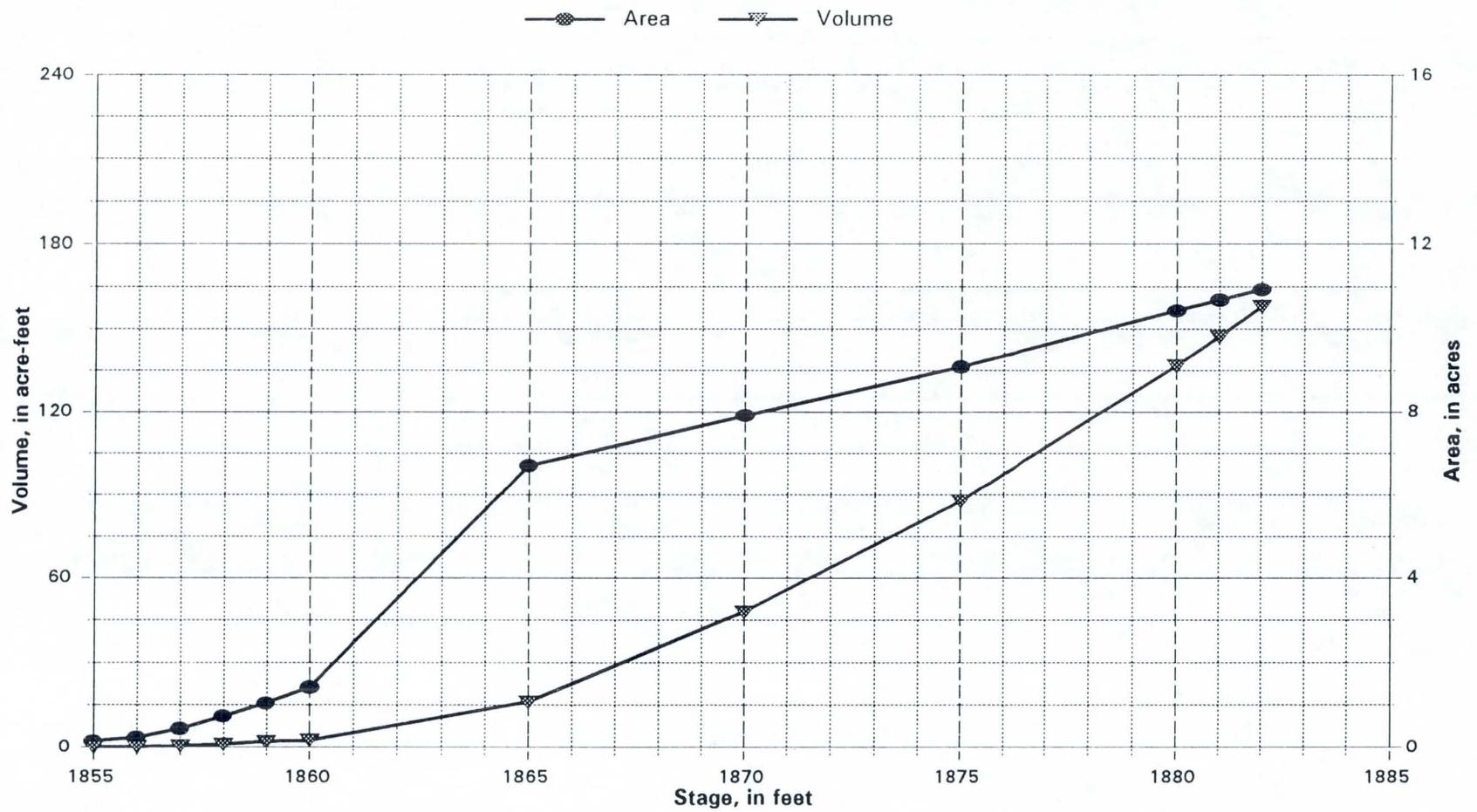
**FIGURE C-8**  
**Deer Valley Detention Basin - Option 1, Case 1**  
**stage hydrographs**



**FIGURE C-9**  
 Deer Valley Detention Basin - Option 1, Case 2  
 hydrographs for the 100-year, 24-hour storm

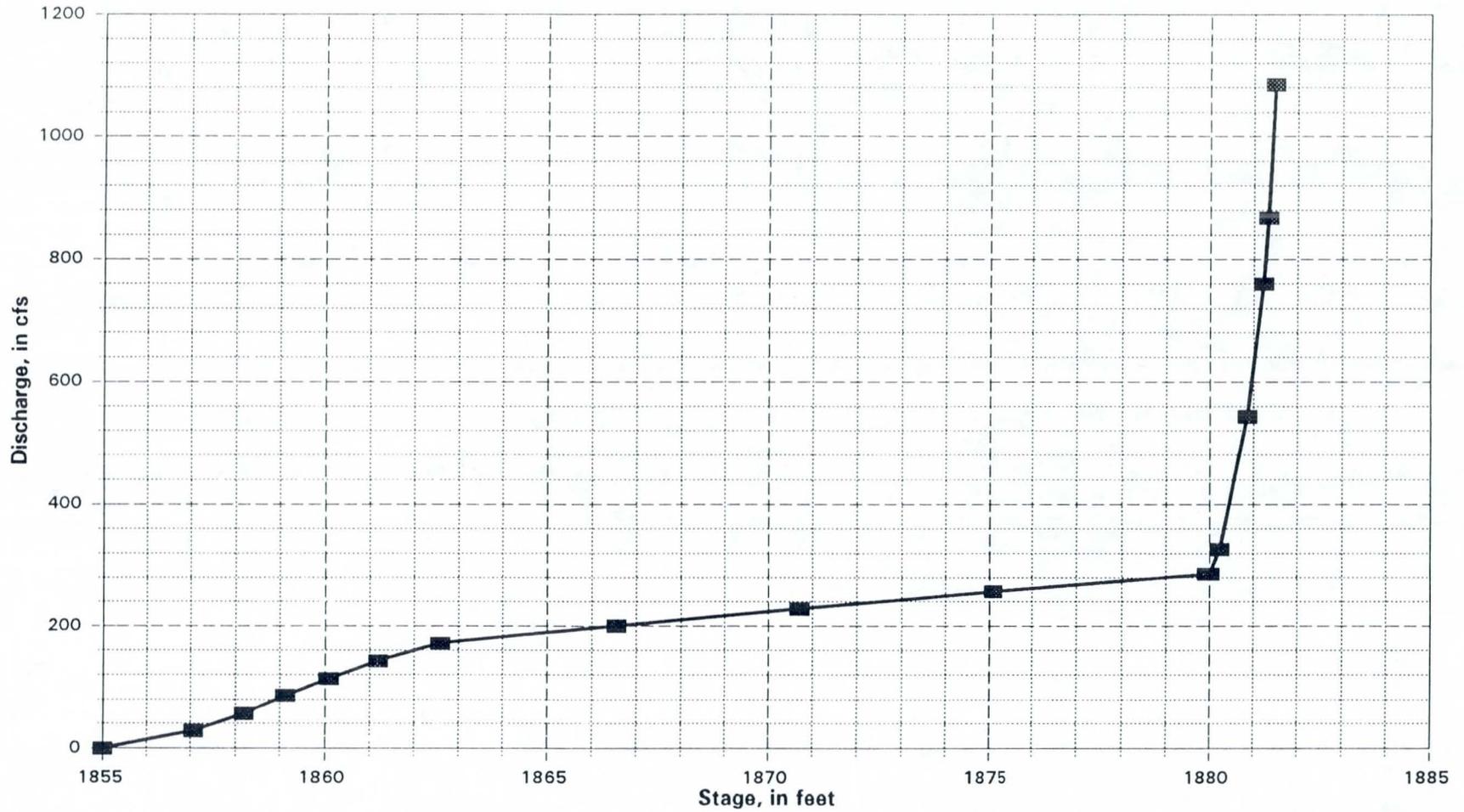


**FIGURE C-10**  
**Deer Valley Detention Basin - Option 1, Case 2**  
**stage hydrographs**

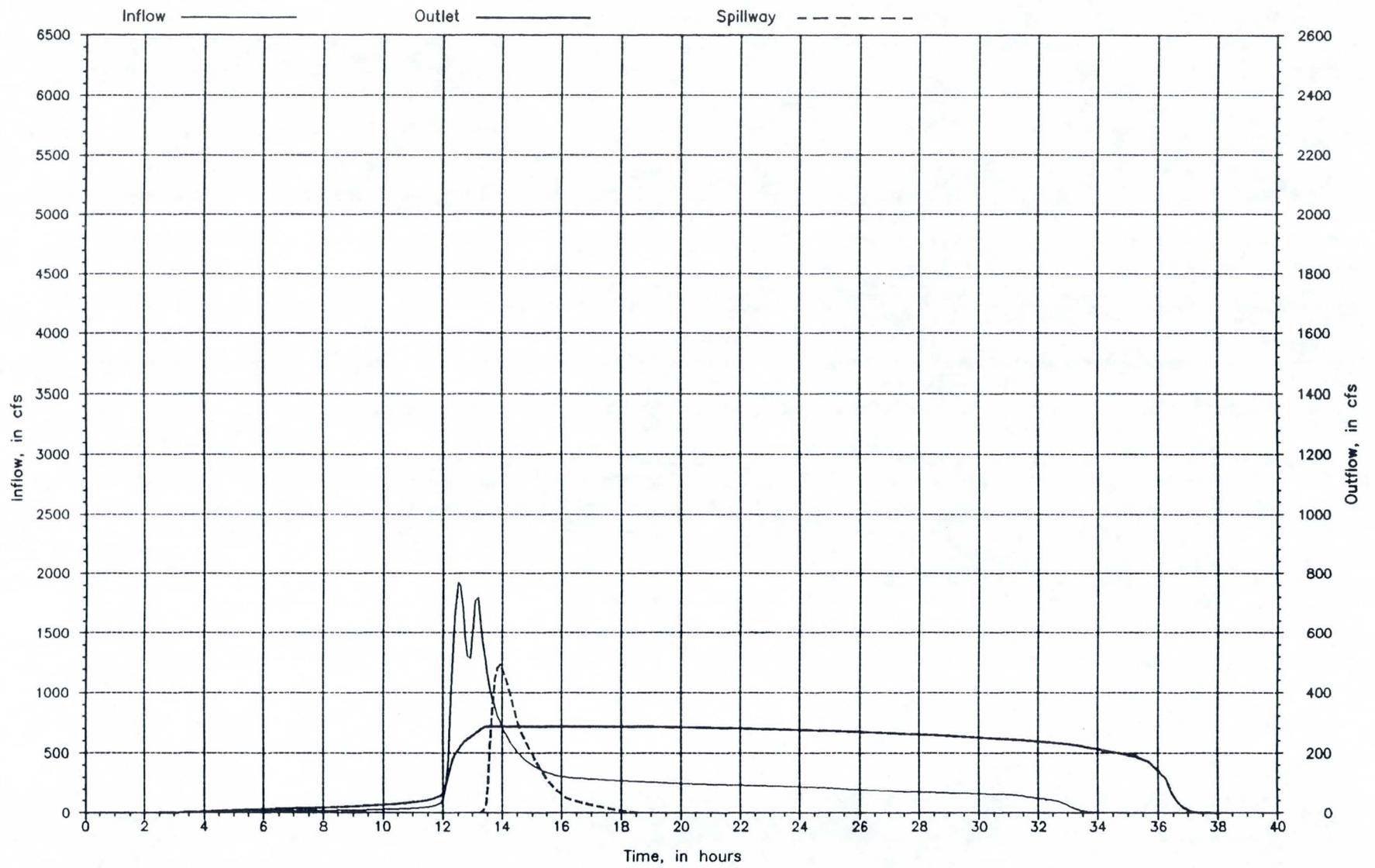


**FIGURE C-11**  
**Deer Valley Detention Basin - Option 2**  
**area-capacity curves**

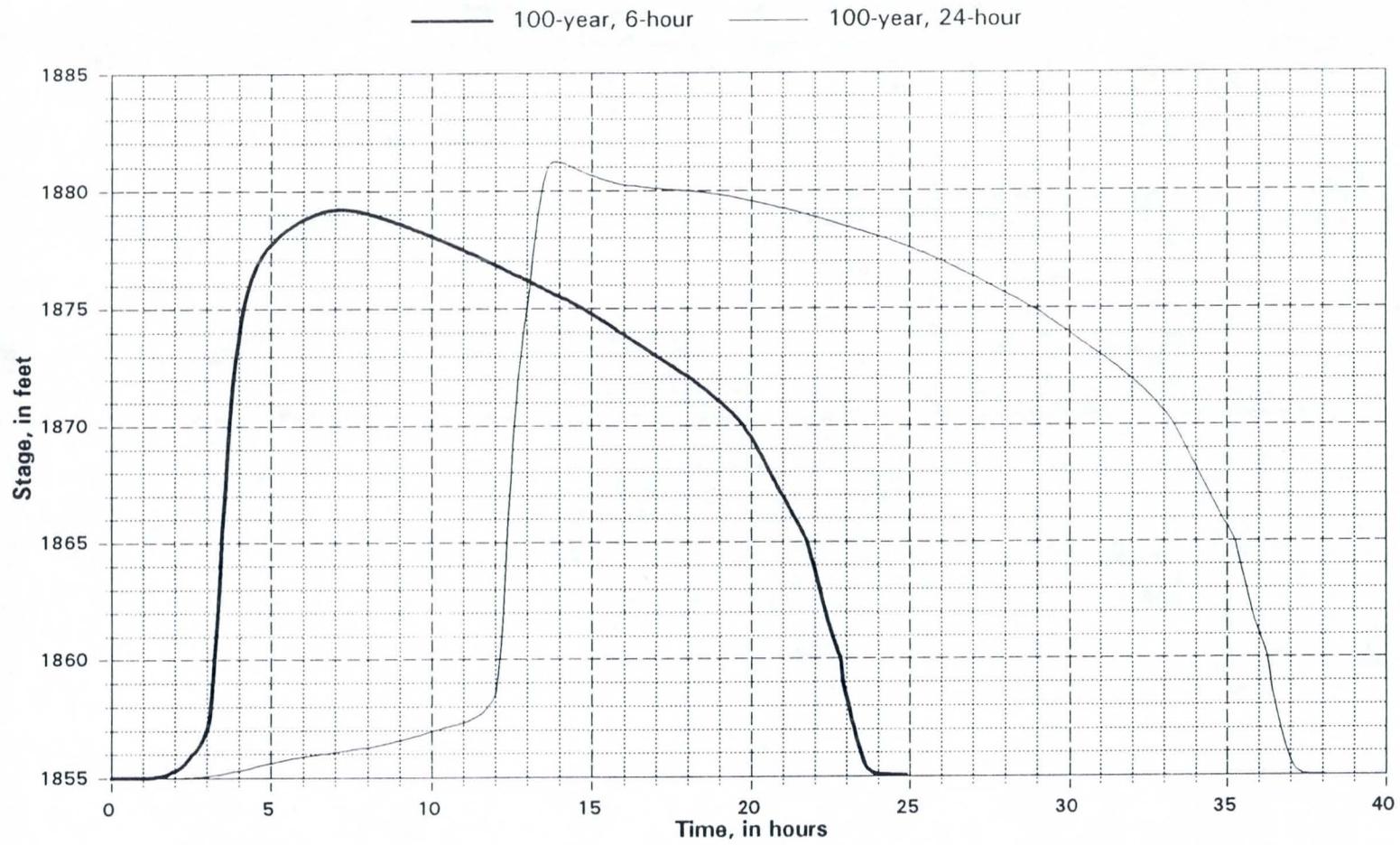
54 inch outlet conduit



**FIGURE C-12**  
**Deer Valley Detention Basin - Option 2**  
**outlet rating curve**



**FIGURE C-13**  
 Deer Valley Detention Basin - Option 2, Case 1  
 hydrographs for the 100-year, 24-hour storm



**FIGURE C-14**  
**Deer Valley Detention Basin - Option 2, Case 1**  
**stage hydrographs**

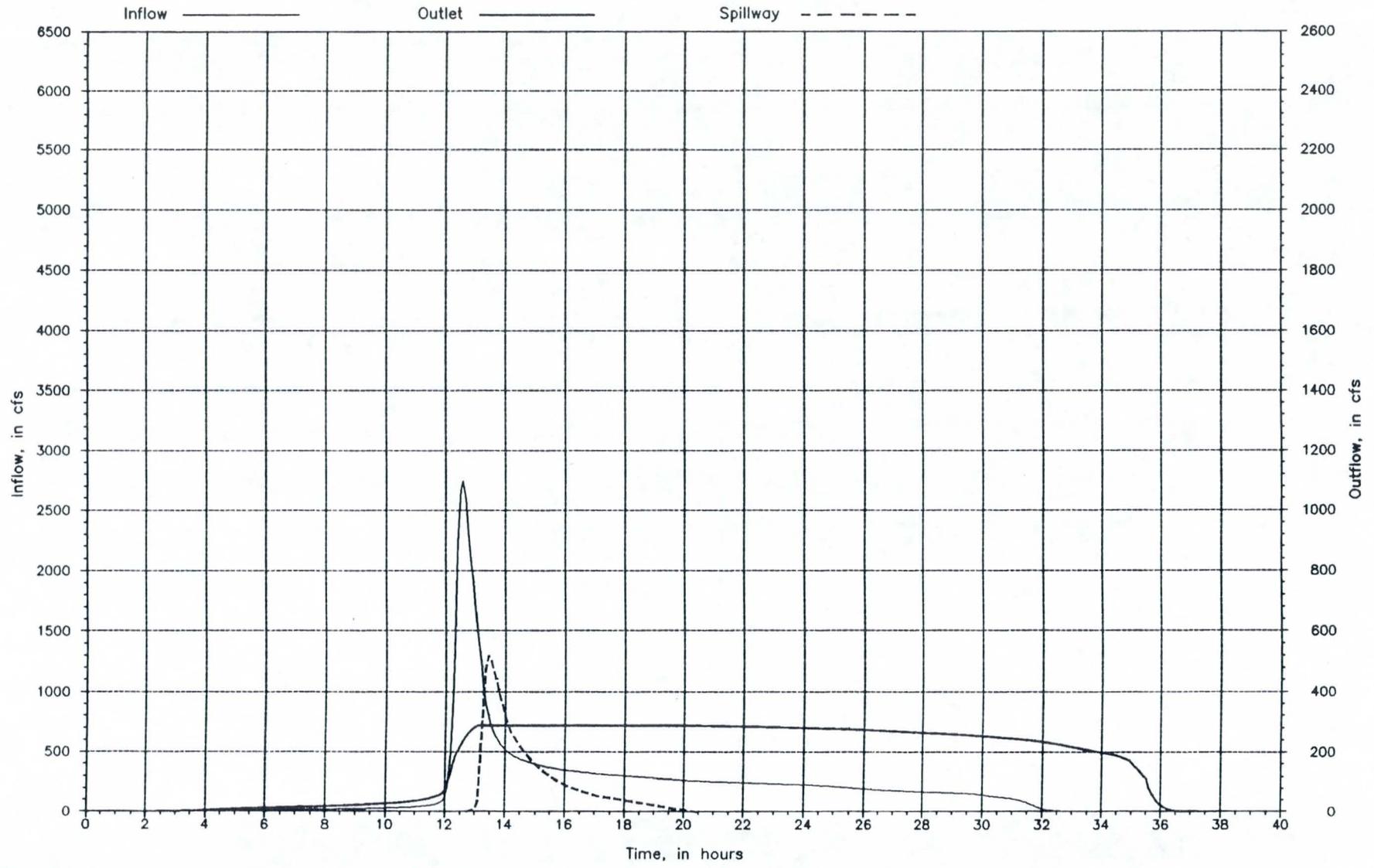
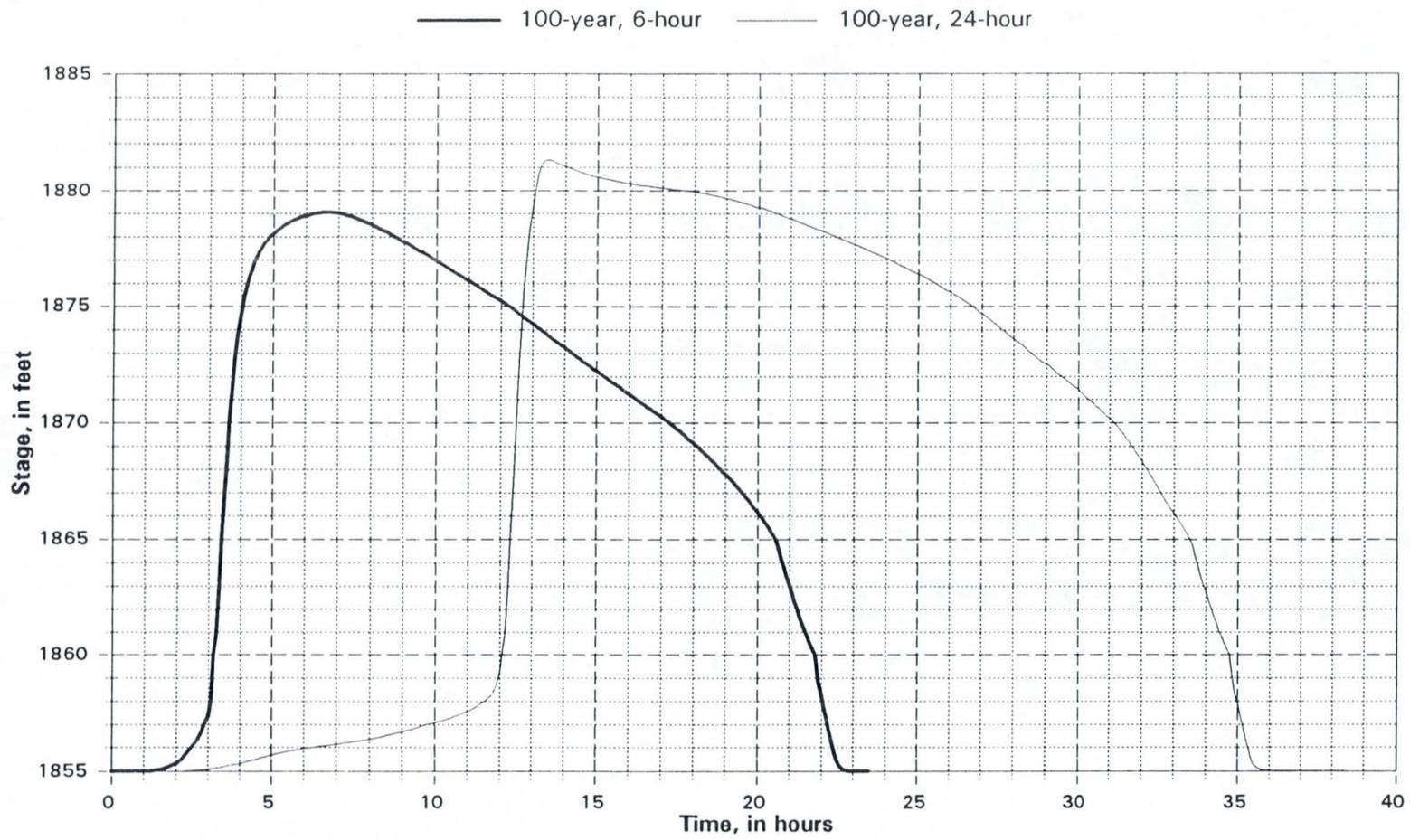
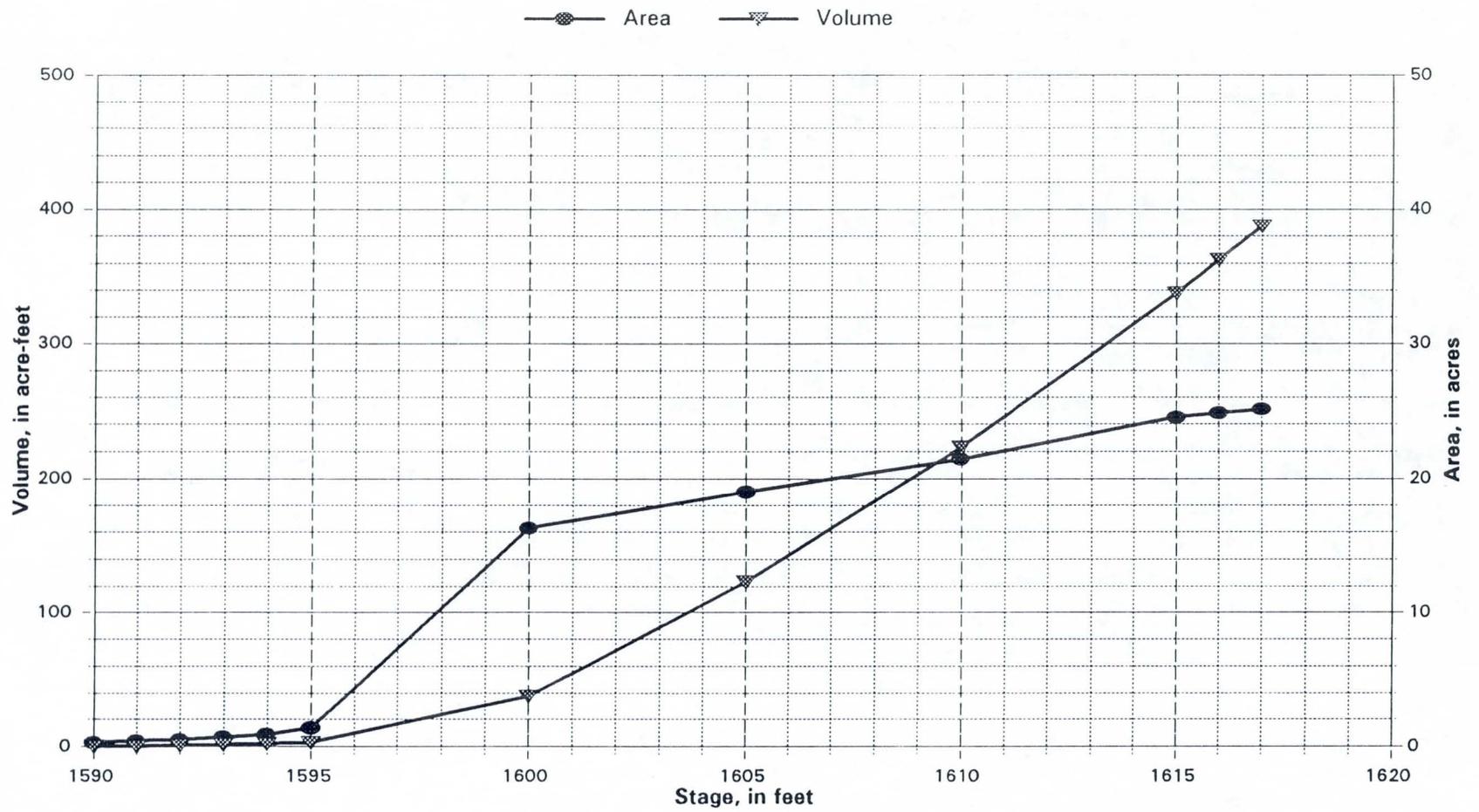


FIGURE C-15  
 Deer Valley Detention Basin - Option 2, Case 2  
 hydrographs for the 100-year, 24-hour storm

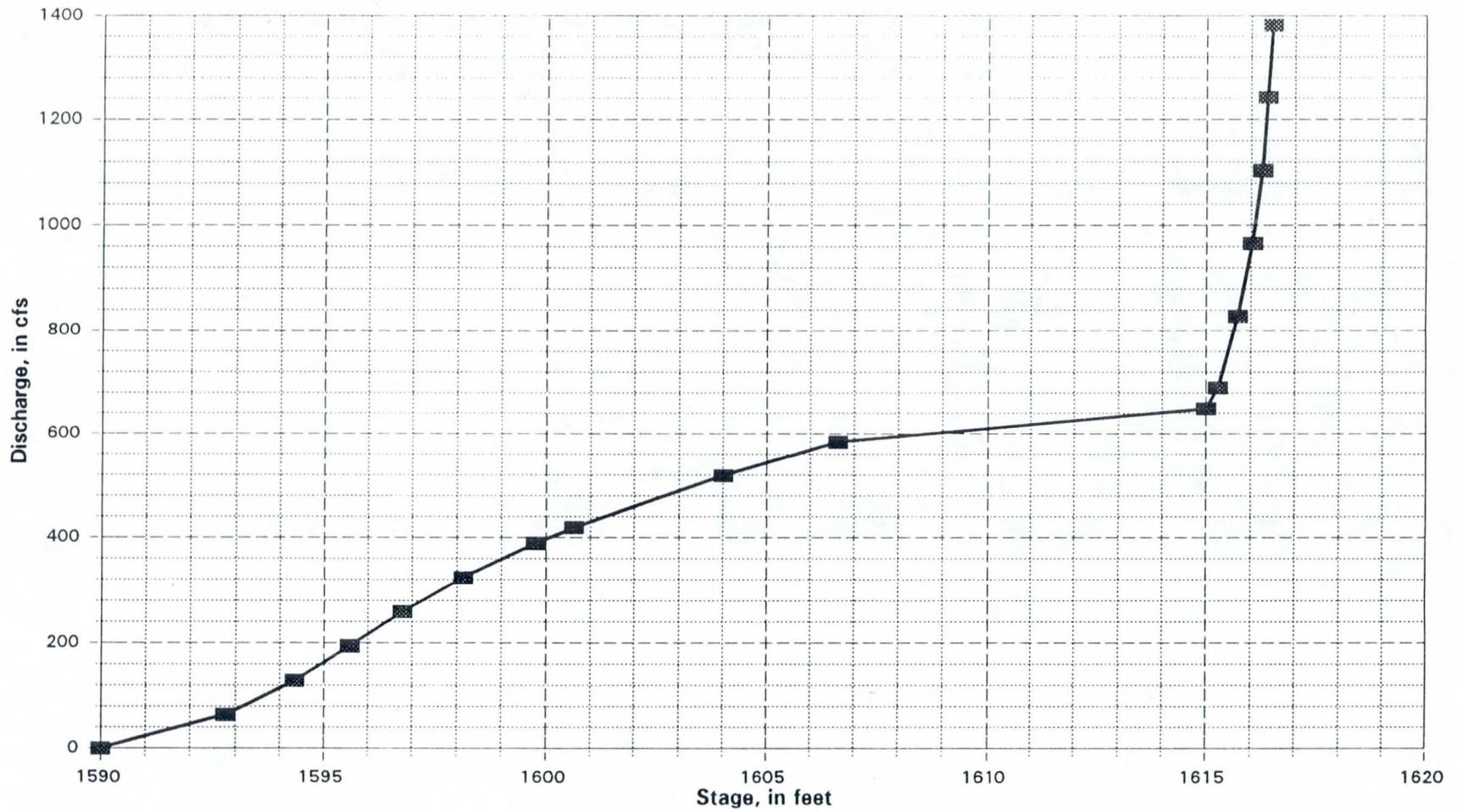


**FIGURE C-16**  
**Deer Valley Detention Basin - Option 2, Case 2**  
**stage hydrographs**



**FIGURE C-17**  
**Union Hills Detention Basin - Option 1**  
**area-capacity curves**

78 inch outlet conduit



**FIGURE C-18**  
**Union Hills Detention Basin**  
**outlet rating curve**

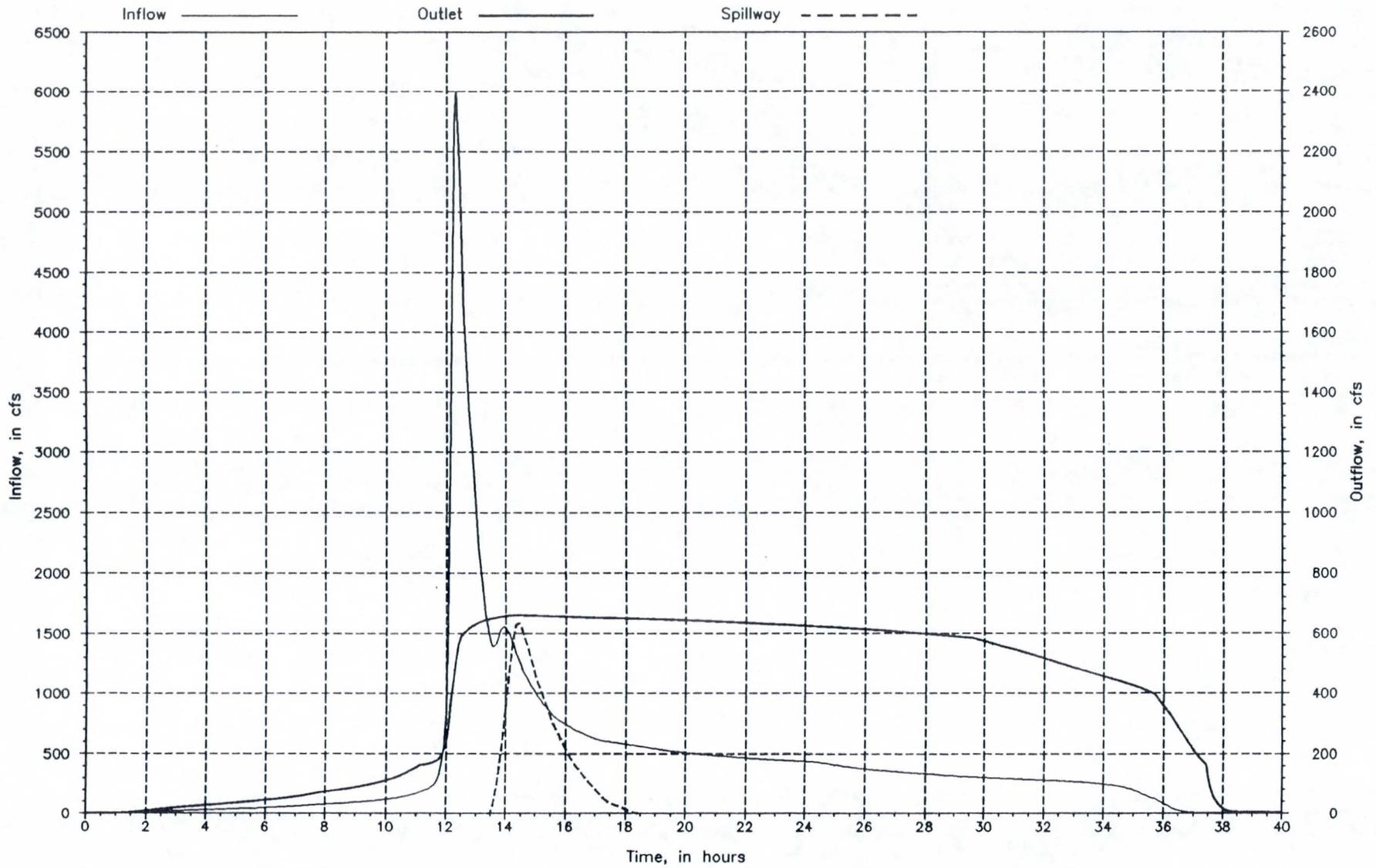
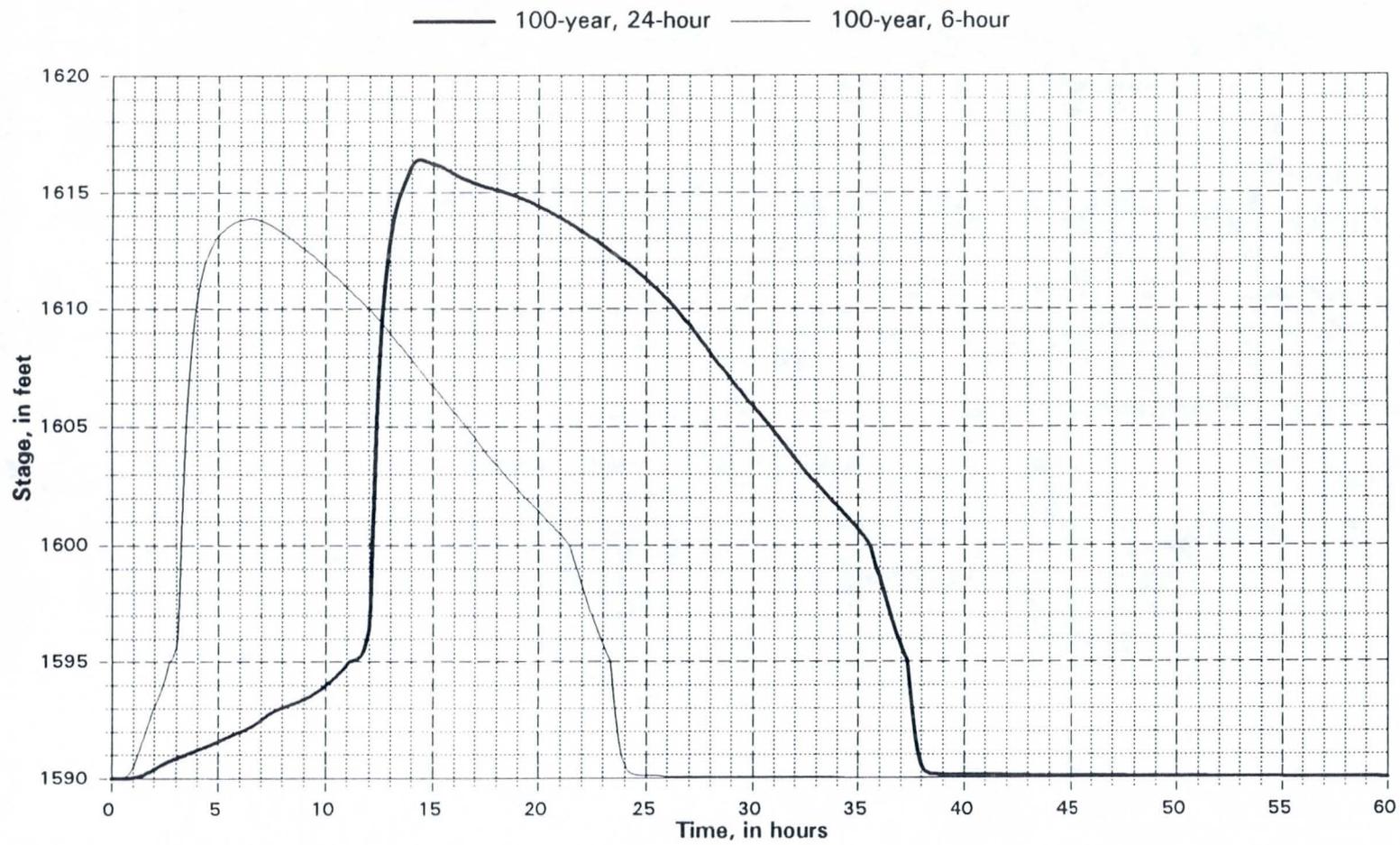
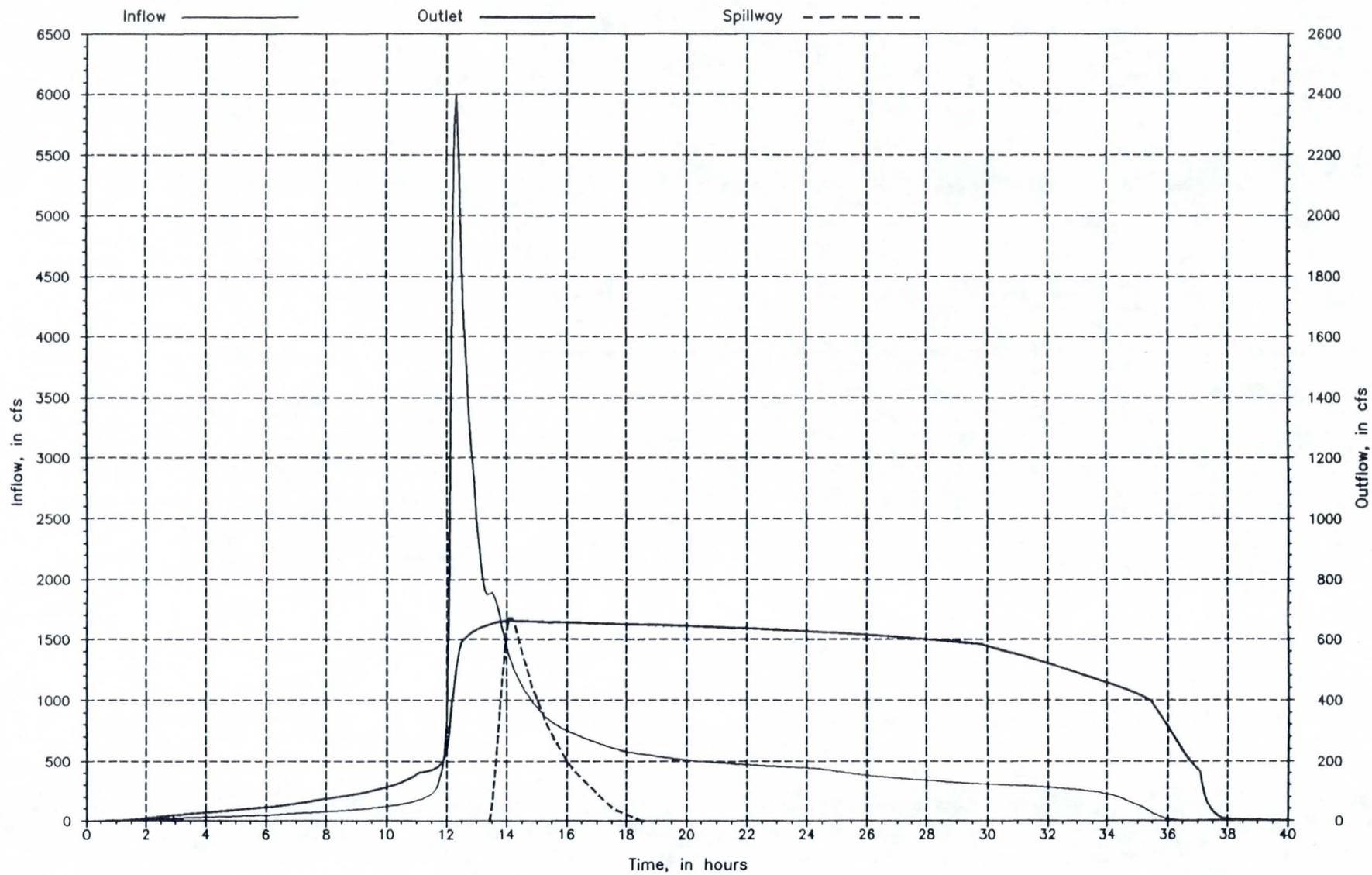


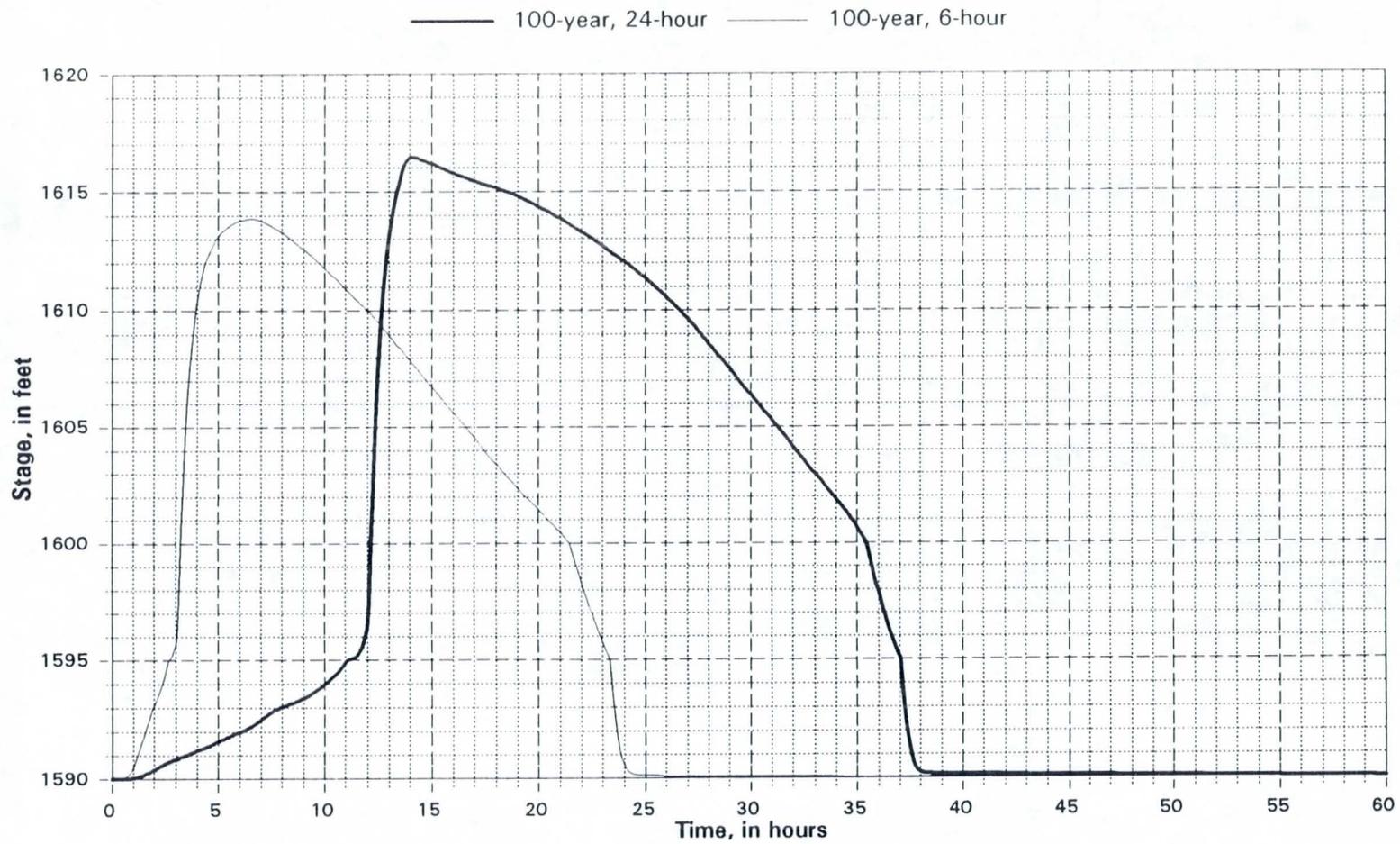
FIGURE C-19  
 Union Hills Detention Basin - Option 1, Case 1  
 hydrographs for the 100-year, 24-hour storm



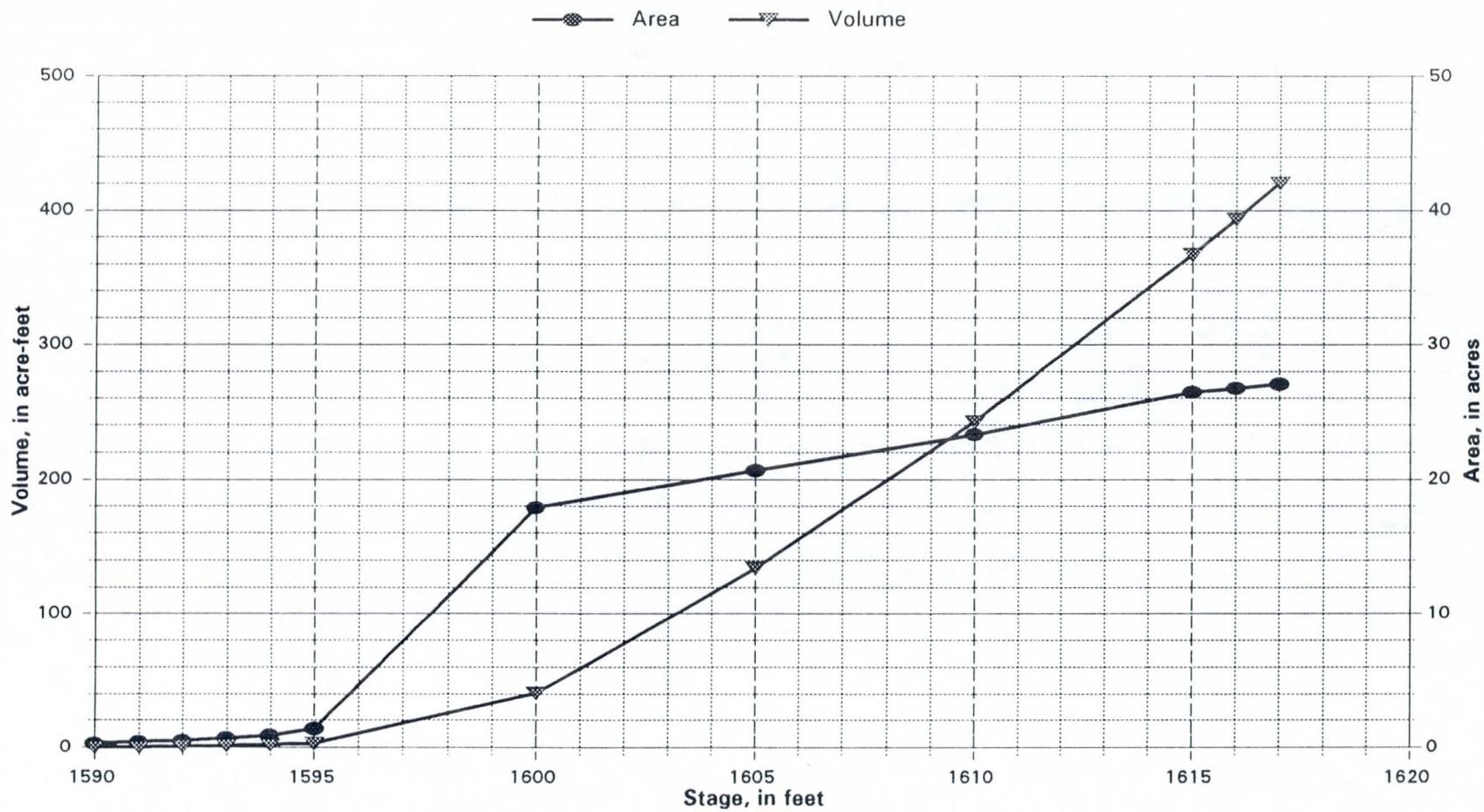
**FIGURE C-20**  
**Union Hills Detention Basin - Option 1, Case 1**  
**stage hydrographs**



**FIGURE C-21**  
 Union Hills Detention Basin - Option 1, Case 2  
 hydrographs for the 100-year, 24-hour storm

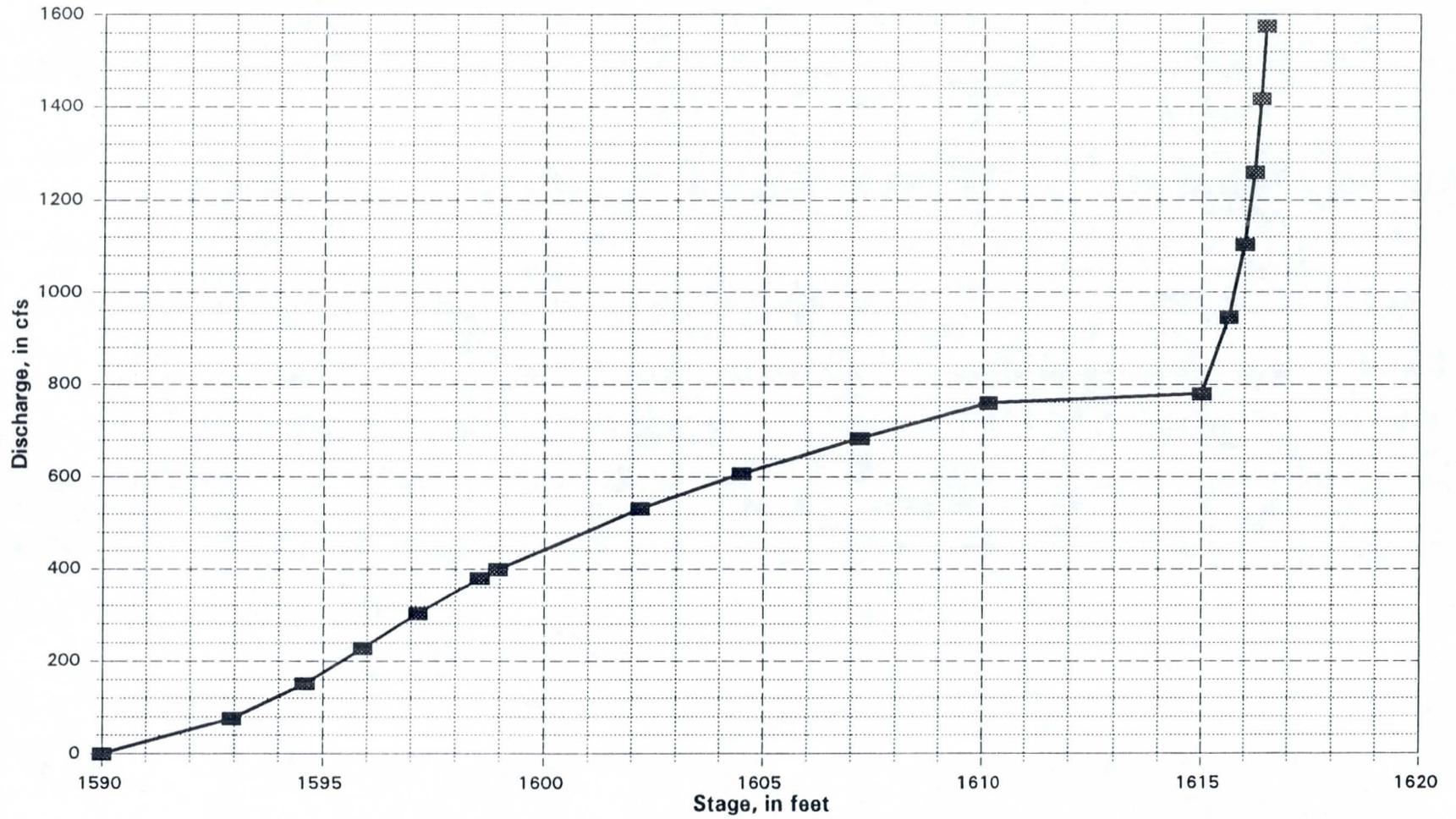


**FIGURE C-22**  
**Union Hills Detention Basin - Option 1, Case 2**  
**stage hydrographs**

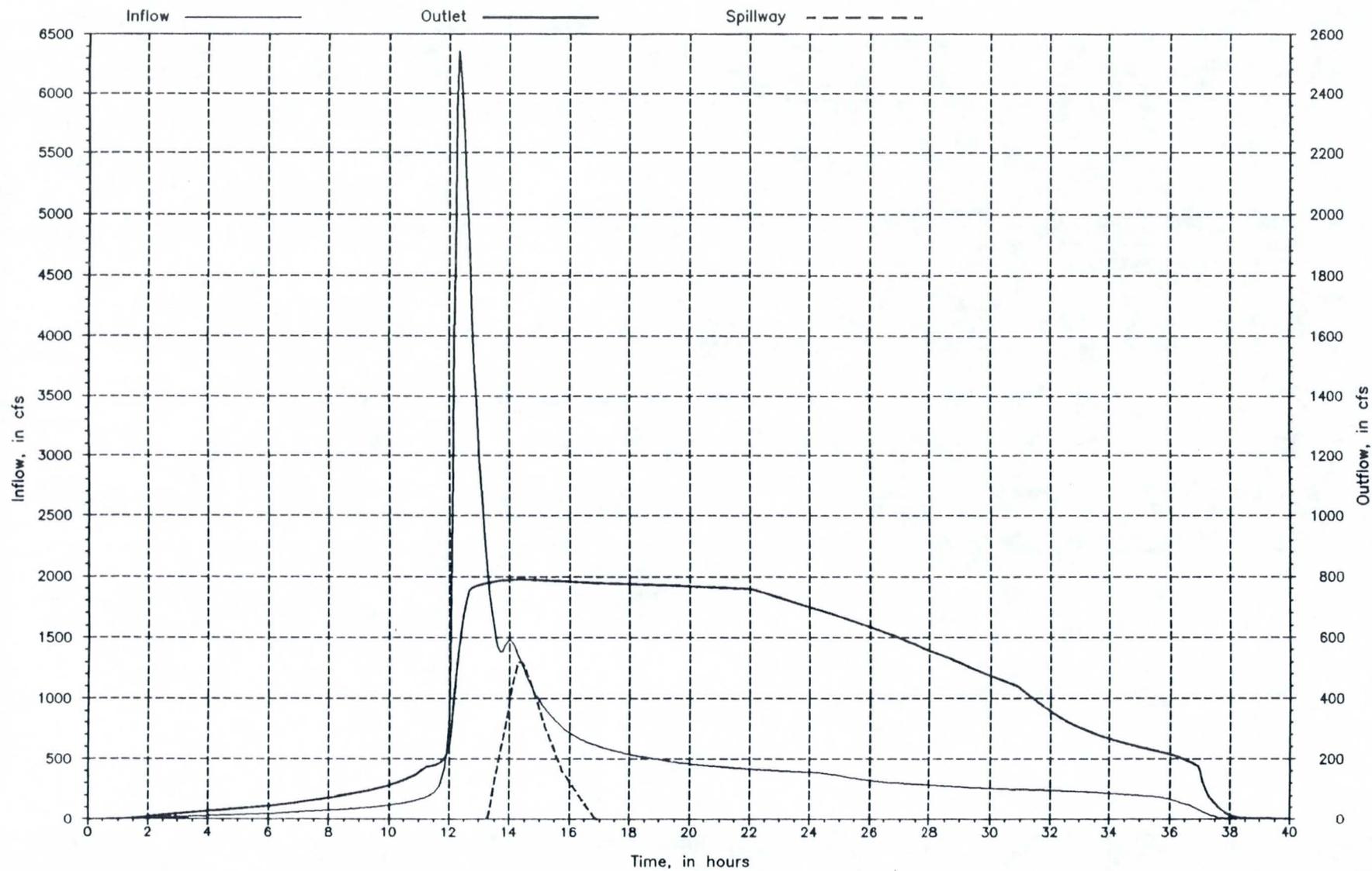


**FIGURE C-23**  
**Union Hills Detention Basin - Option 2**  
**area-capacity curves**

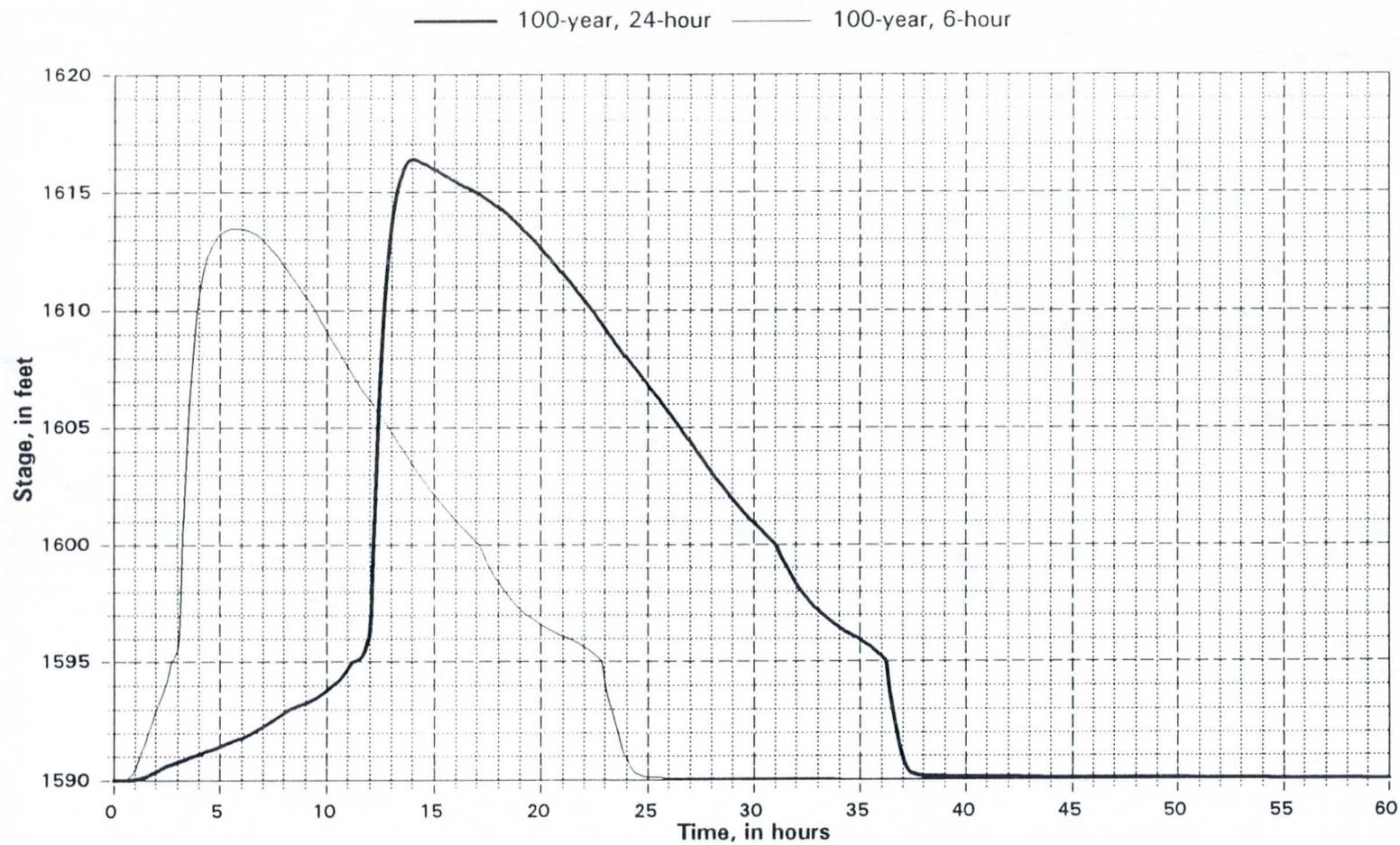
84 inch outlet conduit



**FIGURE C-24**  
**Union Hills Detention Basin - Option 2**  
**outlet rating curve**



**FIGURE C-25**  
 Union Hills Detention Basin - Option 2, Case 1  
 hydrographs for the 100-year, 24-hour storm



**FIGURE C-26**  
**Union Hills Detention Basin - Option 2, Case 1**  
**stage hydrographs**

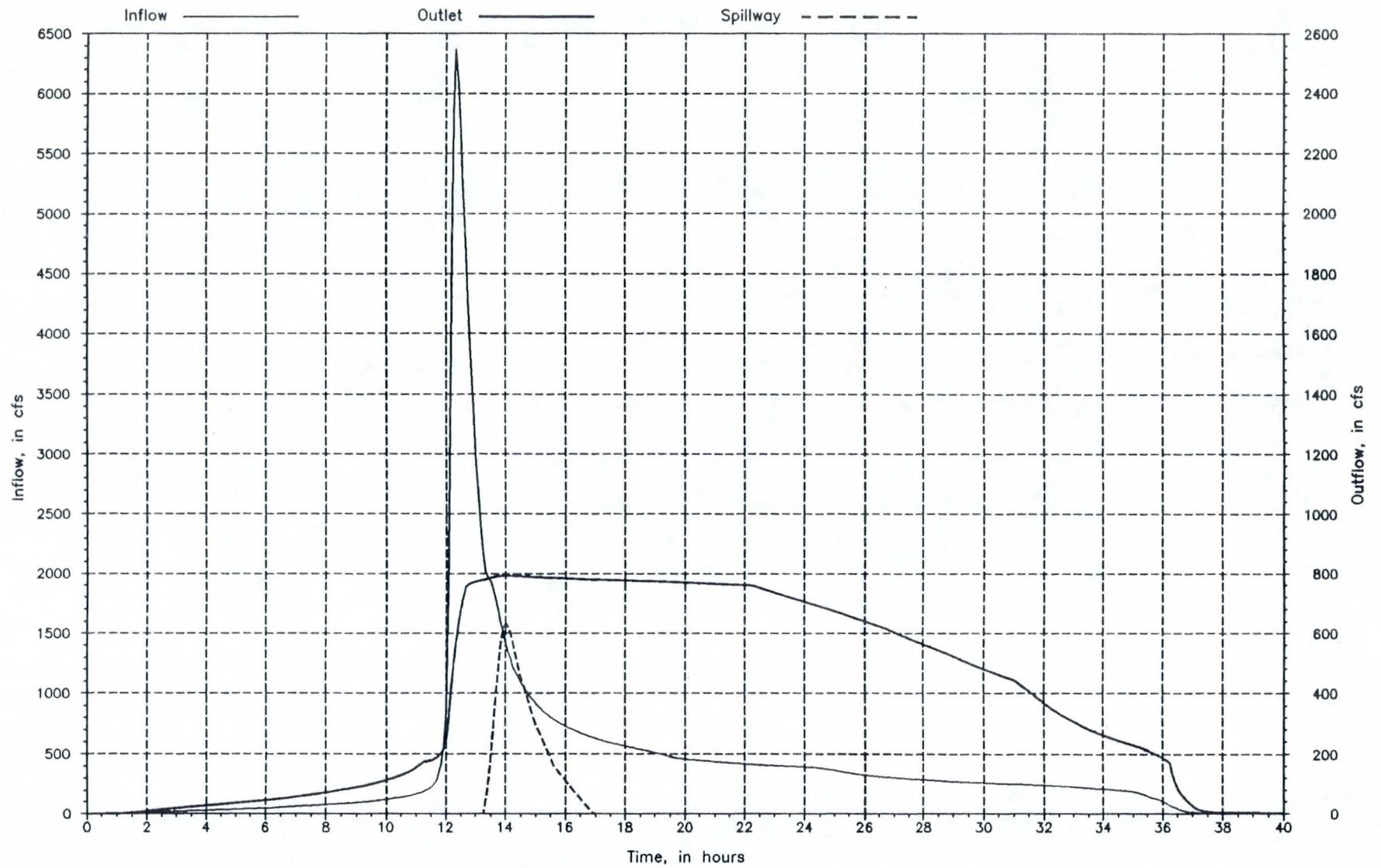
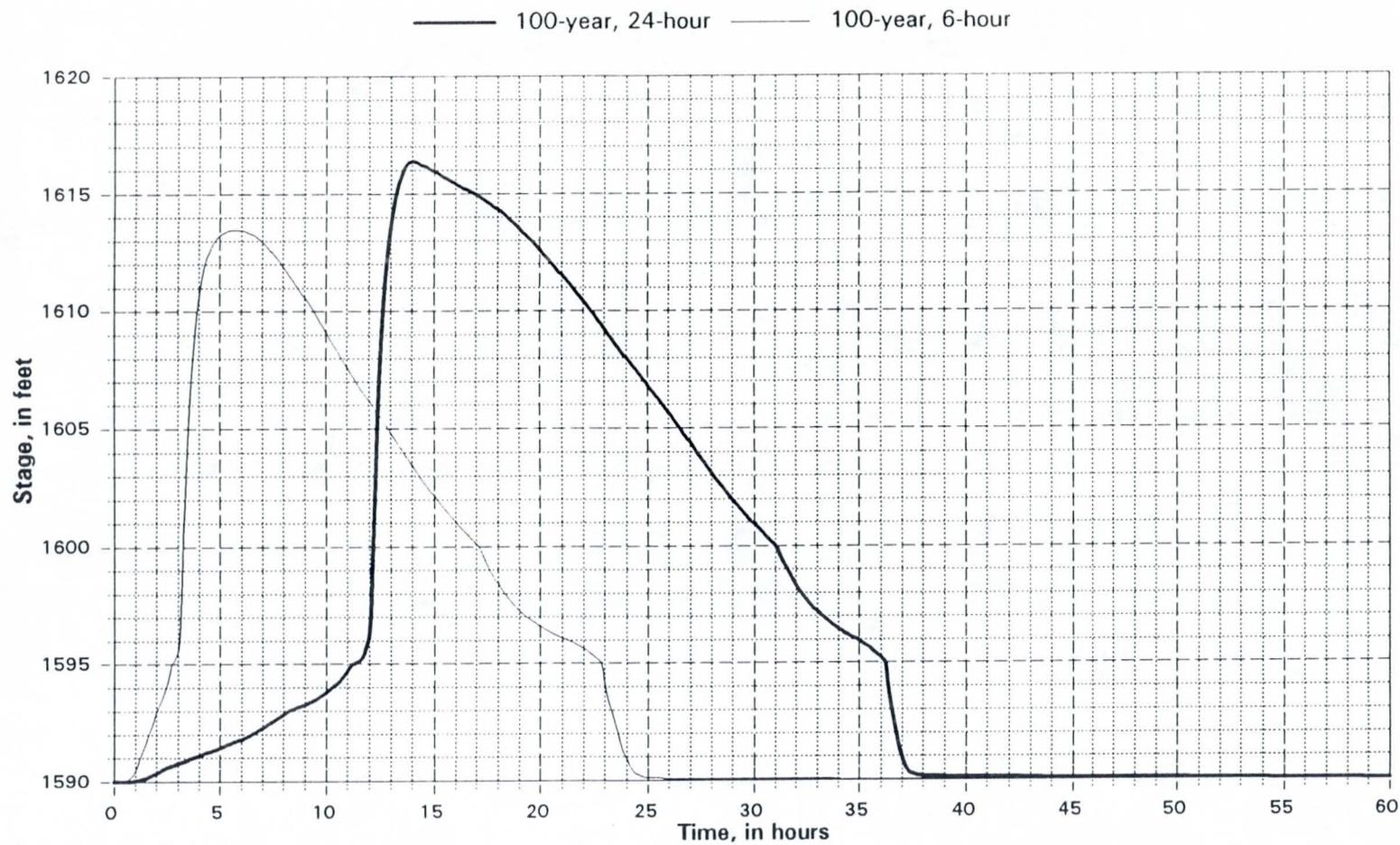


FIGURE C-27  
 Union Hill Detention Basin - Option 2, Case 2  
 hydrographs for the 100-year, 24-hour storm



**FIGURE C-28**  
**Union Hills Detention Basin - Option 2, Case 2**  
**stage hydrographs**