



9<sup>TH</sup> AVE. STORM DRAIN  
SYSTEM - PEORIA TO ACDC  
FINAL DRAINAGE REPORT

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SYSTEM - PEORIA TO ACDC  
FINAL DRAINAGE REPORT**



City of Phoenix No. ST83130249

Entellus Project No. 115.076F

**December 2005**

*Prepared by:*

*Intelligent Engineering*

*Environmental Solutions*



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TO: Laura Fritschi  
FROM: Jacob Sweeting  
JOB NO: 115.076F (ST83130249)  
DATE: 12/21/2005  
CC: File

PROJECT NAME: 9<sup>th</sup> Avenue Storm Drain: ACDC - Peoria

## *Final Drainage Report*

### *RE: Drainage Analysis*

#### *1. Project Description*

This technical memorandum summarizes the hydrologic analysis and hydraulic design performed for the design of the 9<sup>th</sup> Avenue Storm Drain System, from Peoria Avenue to the ACDC. This project is a cooperative effort between the Flood Control District of Maricopa County (*District*) and the City of Phoenix (*City*).

The *Sunnyslope Candidate Assessment Report* (hereinafter referred to as the *CAR*) (**Ref 1**), was prepared by the *District* and includes conceptual solutions for drainage problems identified throughout the study area. The 9<sup>th</sup> Avenue storm drain system was one of the conceptual solutions proposed in the *CAR*. **Attachment A** is an exhibit showing the project vicinity.

#### *2. Existing Conditions*

The total contributing drainage area to the proposed storm drain system is approximately one square mile. The watershed includes a significant amount of mountain runoff, as well as the outflows from two upstream flood control dams.

A detailed summary of the existing drainage conditions in the vicinity of this project was included in the *CAR*. The *CAR* also summarized several existing drainage problems or undesirable conditions as shown below:

1. Runoff ponds along the inside edge of the curve in 7<sup>th</sup> Avenue at the southwest corner of Mountain View Park (7<sup>th</sup> Avenue about ½ mile south of Peoria Avenue), causing long standing nuisance and maintenance problems. The watershed contributing to this runoff extends up into the North Mountain Preserve, and includes the discharge from the upstream East Park Flood Control Dam.

2. The discharge from the northwest flood control dam at Peoria and 7<sup>th</sup> Avenues is conveyed through private property in a series of culverts and short channel drains into 11<sup>th</sup> Avenue and is collected in the existing 11<sup>th</sup> Avenue storm drain. This channel also creates undesirable dip sections in the street crossings at North Lane and at Cochise Drive.
3. Overflow from the detention basin at the middle school at 9<sup>th</sup> Avenue and Cheryl Avenue discharges across private property, through a 60-inch culvert, then into a channel that eventually discharges downstream into Cinnabar Avenue.
4. The 7<sup>th</sup> Avenue storm drain, upstream of Cheryl Avenue, discharges across private property through a series of culverts and short channel sections, eventually spilling out into 9<sup>th</sup> Avenue.
5. The discharge from the southeast flood control dam (combined with substantial downstream local runoff) discharges through Mountain View Park, across private property and down 9<sup>th</sup> Avenue to the ACDC, creating a significant flooding potential.

**Attachment B** includes a map from the *CAR* that has been reproduced and labeled with the various conditions listed above.

### **3. *Proposed Conditions***

A Memorandum of Understanding (MOU) between the District and the City summarized the proposed storm drain system as follows:

The 9<sup>th</sup> Avenue storm drain would collect and convey the 10-year flood from Peoria Avenue downstream to the ACDC.

The new 9<sup>th</sup> Avenue storm drain will include four laterals. The first is a short run in North Lane, west of 9<sup>th</sup> Avenue, which will collect the flow that currently flows through private property in an undersized culvert. The North Lane lateral will allow the downstream privately owned culvert to be abandoned. The second is in Cheryl Drive from 9<sup>th</sup> Avenue to 7<sup>th</sup> Avenue; collecting flow from the existing channel outfall at 7<sup>th</sup> Avenue and Cheryl Avenue. The Cheryl Avenue lateral would also collect flows from the intersection at 8<sup>th</sup> Avenue, allowing the downstream private culvert to be abandoned. The third lateral is in Cinnabar Avenue from 9<sup>th</sup> Avenue to 7<sup>th</sup> Avenue. This lateral will collect a significant concentration of runoff at the southwest corner of Mountain View Park, which includes the discharge from the upstream flood control dam. This lateral will also collect the discharge from the middle school detention basin at 9<sup>th</sup> Avenue, allowing the downstream, privately owned 60-inch culvert to be abandoned. The fourth lateral, in Cochise Street, will connect to the existing 11<sup>th</sup> Avenue storm drain. It will drain the low spot in Cochise Street and allow the downstream, privately owned culvert to be abandoned.

**Attachment B** includes an exhibit showing the proposed layout of the storm drain and laterals.

#### **4. Off Site Flows - Hydrology Modeling**

The CAR presented peak flows for the proposed storm drain system estimated using a flow versus area relationship based on the *1994 ACDC ADMS Hydrology Report (Ref 2)*. These approximate flows were adequate for developing a conceptual layout of the storm drain system. However, a more detailed estimate of the peak flows was needed to design the system of inlets and pipes.

The U.S. Army Corp of Engineers' computer program HEC-1 (**Ref 3**), was used to develop the rainfall-runoff hydrology models for this project. The procedures and modeling parameters were based on the *Draft Drainage Design Manual for Maricopa County – Volume 1 – Hydrology* (hereinafter referred to as the *Hydrology Manual*) (**Ref 4**).

The hydrology models were created in order to model offsite flows entering the storm drain system. However, local drainage areas were also included in the hydrology models in order to develop design flows used for preliminary sizing of the pipe. The local drainage areas will be revisited later using the rational method when designing the inlets.

Two models were created to estimate off-site flows for this project: 10-year 6-hour and 100-year 6-hour. The storm drain system was sized in order to convey the peak flows estimated using the 10-year model. The 100-year model was used to verify that the City's dry lane requirements were met. The 6-hour duration storm controls in this watershed and was used for both models. Areal reduction was not used in the models because the watershed area is relatively small (less than 1 square mile). Maps showing delineated watershed are included in **Attachment C**.

##### **4.1. Precipitation**

Precipitation data was obtained from the *NOAA Atlas 2, Volume VIII Arizona (Ref 5)*, and selected isopluvial maps for Maricopa County, which are located in *The Hydrology Manual*. This information was used in the Precipitation Frequency (PreFre) module of the *DDMS* program (**Ref 6**). Copies of the isopluvial maps, as well as the PreFre output are included in **Attachment D**.

##### **4.2. Subbasin Delineation**

In order to determine peak flows at key locations, the 0.91 square mile watershed was delineated into twenty-two subbasins. The subbasin boundaries and lengths were delineated in *ArcMap (Ref 7)* using *2004 Color Aerial Photography (Ref 8)*, and *2 foot Contours (Ref 9)*, provided by the District. The subbasin boundaries and lengths were imported into *WMS 7.1 (Ref 10)* and the subbasin parameters were

extracted. A map showing the delineated subbasins is included in **Attachment C**.

#### **4.3. *Rainfall Losses***

The Green-Ampt method was used to determine rainfall losses throughout the project watershed. The digital GIS formats of the *MAG General Plan (Ref 11)*, and the *Soil Conservation Service Soil Survey for Maricopa County (Ref 12)*, were obtained from the District and imported into WMS. Because the area is completely developed, there were no significant differences between the landuse information included in the *General Plan* and the existing landuse in the area. The Green-Ampt parameters for each subbasin were generated in WMS using District parameter tables along with the land use and soil information. Maps showing the landuse and soils data are included in the **Attachment E**.

#### **4.4. *Unit Hydrograph***

The excess runoff in each subbasin was routed to the subbasin concentration point using the Clark Unit Hydrograph. WMS was used to estimate the Clark Unit Hydrograph time of concentration and storage coefficient for each subbasin. In order to estimate these parameters, WMS required the adjusted slope, length and resistance coefficient for each subbasin. The length and slope of each subbasin were estimated using ArcMap. The slopes were adjusted using Table 5.2 from *The Hydrology Manual*. The resistance coefficient (Kb) for each subbasin was estimated using the criteria shown in Table 5.3 of *The Hydrology Manual*. The parameters used to estimate the Clark Unit Hydrograph have been summarized on a table included in **Attachment F**.

#### **4.5. *Routing Parameters***

Normal depth routing was used to route the discharges from the dam outlets, through downstream subbasins via natural washes. The geometries of these washes were modeled using eight point cross sections developed from the project topography. The route slopes were estimated using the project topography as well. The Manning's roughness coefficients and route lengths were estimated using the aerial photography provided by the District.

Kinematic wave routing was used to route flows through the proposed storm drain system. The slopes used for each route were estimated using the project topography and represent an estimate of the existing ground slope. It is likely that the proposed slope will be different than the routing slopes used in the hydrologic model which is acceptable because the peak flows are virtually unaffected by the pipe slopes. Furthermore, the pipe sizes used in the routing parameters were initial estimates based on the *CAR*, and will be different than those used in

the final design. Data used for the routing has been included in **Attachment G**.

#### **4.6. Storage**

Discharges from the two flood control dams upstream from the storm drain system were estimated using relevant portions of the *East and West Park Dam Safety Analysis Models (Ref 13)*. The upstream subbasin boundaries and storage routing routines for each dam were extracted from the models and inserted into the model developed for this project.

#### **4.7. Results**

The design flows obtained from the 10-year hydrology models were used to estimate the required pipe sizes throughout the system. The HEC-1 input and output have been included as **Attachment H**. *StormCAD Version 5.5 (Ref 14)* was used to determine the required pipe sizes based on the City's design criteria. Output from the software showing calculations for the size selection is included in **Attachment I**.

### **5. On-Site Hydrology / Drainage**

The peak 10-year flows from the local drainage areas were determined by delineating subbasins within the project area along 9<sup>th</sup> Ave. The Rational Method was used determine the 10-year peak flows from each of the local subbasins. Off-site sub-basin flows that contributed to the 9<sup>th</sup> Ave. storm drain were determined using HEC-1. The Local Hydrology and Catch Basins exhibit in **Attachment C** shows the location of each catch basin and the local and off-site subbasins that contribute flow to them. **Attachment J** includes a spreadsheet that shows hydrologic and hydraulic results for the local peak flows and catch basins. The table includes estimates of catch basin interception and flow by.

### **6. Hydraulics**

#### **6.1. Main Storm Drain Sizing**

The main storm drain pipe was sized using results from the off-site and local hydrology estimates and hydraulic modeling software (**see section 4.7**). The hydraulic grade line for the 10-year event is shown on the plans and is summarized in **Attachment I**. It should be noted that all pipes were sized using the 10-year peak flows, except the lateral on Cochise Drive. This lateral connects to the existing 11<sup>th</sup> Avenue storm drain system. The capacity of the existing storm drain limited the size of the proposed lateral on Cochise Drive to 18", whereas a 24" pipe would more effectively convey the 10-year peak flow.

Design constraints for sizing the pipes were:

- 10-year peak flows
- Existing storm drains
- Hydraulic grade line at 1ft. or more below proposed grade
- Maximum 10-year velocity of 20 fps.

The StormCAD output included in **Attachment I** shows the average velocity in all pipes to be less than 20 fps. Some of this flow is in the supercritical flow range and has the potential to create a hydraulic jump within the storm drain. Effects of possible hydraulic jumps occurring on the pipe were considered when placing manholes and catch basins.

## **6.2. Catch Basin / Inlet Design**

The amount of flow that was intercepted by each catch basin was determined using *Flow Master 2005 (Ref 15)* and the results are summarized in **Attachment J**. The catch basins were designed using guidelines from the City of Phoenix's *Storm Water Policies*. Catch basins were generally placed as follows:

- At existing sumps or low points
- Where the 2-year or 100-year flows were expected to exceed the City's dry lane / flow depth requirements
- Curb returns (where applicable)

The typical catch basin used was the type "M" (curb openings) from the City of Phoenix supplement. Catch basins type "N" (City of Phoenix), or the type "G" (MAG) were used where grated inlets were more applicable than curb openings.

The table below lists design flows at key locations throughout the storm drain system. The “Map ID” column refers to the “Proposed Storm Drain System Layout” map which is included with **Attachment A**.

### *Design Peak Flows and Pipe Sizes*

<b>Map ID</b>	<b>Location</b>	<b>Design Description</b>	<b>ID</b>	<b>Design Flow (cfs)</b>	<b>Pipe Size (in)</b>
1	Cochise Dr., Dip at 10 <sup>th</sup> Ave. Align. to 11 <sup>th</sup> Ave.	Headwall-Inlet	S7	10	18
2	Peoria Ave. and 9 <sup>th</sup> Ave.	Join to Existing Culvert	C2	70	N/A
3	9 <sup>th</sup> Ave., Peoria Ave. - North Ln.	Main Pipe	CSD1	90	36
4	Wash Crossing at North Ln., Just West of 9 <sup>th</sup> Ave.	Headwall-Inlet/Lateral	S4	5	24
5	9 <sup>th</sup> Ave. and North Ln. at School Entrance	Catch Basin	S6	<b>See Attachment J</b>	
6	9 <sup>th</sup> Ave., North Ln. - Cheryl Dr.	Main Pipe	CSD2	90	42
7	7 <sup>th</sup> Ave. and Cheryl Dr.	Join to Existing Culvert	S3	100	24 x 36
8	Cheryl Dr., 7 <sup>th</sup> Ave. - Dip at 8 <sup>th</sup> Ave. Align.	Lateral Pipe	C10	130	48
9	9 <sup>th</sup> Ave. and Cheryl Dr. from School Basin	Join to Existing Culvert	S9	30	60 (Existing)
10	Cheryl Dr., Dip at 8 <sup>th</sup> Ave. Align. - 9 <sup>th</sup> Ave.	Lateral Pipe	C9*	130	48
11	9 <sup>th</sup> Ave., Cheryl Dr. - Cinnabar Ave.	Main Pipe	CSD3	220	54
12	Bend in 7 <sup>th</sup> Ave. at SW Corner of Mtn. View Park	Catch Basin	S17	<b>See Attachment J</b>	
13	7 <sup>th</sup> Ave., Bend to Cinnabar	Lateral Pipe	S17	120	48
14	7 <sup>th</sup> Ave. and Cinnabar Ave.	Headwall/Inlet	C14b	<b>See Attachment J</b>	
15	Cinnabar Ave., 7 <sup>th</sup> Ave. - Dip 8 <sup>th</sup> Ave. Align.	Lateral Pipe	C13	120	54
16	Cinnabar Ave., Dip at 8 <sup>th</sup> Ave. Align. - 9 <sup>th</sup> Ave.	Lateral Pipe	C12*	120	54
17	9 <sup>th</sup> Ave., Cinnabar Ave. - Mountain View Rd.	Main Pipe	CSD4	340	66
18	9 <sup>th</sup> Ave., Mtn. View Rd. - Purdue Ave. Align.	Main Pipe	CSD5	380	66
19	9 <sup>th</sup> Ave. and Vogel Ave.	Catch Basin	S19	<b>See Attachment J</b>	
20	9 <sup>th</sup> Ave., Purdue Ave. Align. - Vogel Ave.	Main Pipe	CSD6	380	66
21	9 <sup>th</sup> Ave., Vogel Ave. - Hatcher Rd.	Main Pipe	S20	380	66
22	9 <sup>th</sup> Ave., Vogel Ave. - Hatcher Rd.	Main Pipe	CSD7	380	66
23	9 <sup>th</sup> Ave., Hatcher Rd. - ACDC	Main Pipe	CSD8	380	72

Note: All flows were rounded to the nearest 5 cfs. Local flows were included in hydrology models but are not shown on this table.

## *List of References*

- 1 Flood Control District of Maricopa County and Engineering and Environmental Consultants Inc., *Sunnyslope Candidate Assessment Report FCD 2003C052*, October 2004.
- 2 Flood Control District of Maricopa County and Kaminski Hubbard Engineering, Inc, *Arizona Canal Diversion Channel, Area Drainage Master Study - 10<sup>th</sup> Street to Cave Creek Watershed, Volume 1.6*, November 1994
- 3 United States Department of Army, Corps of Engineers, Hydrologic Engineering Center, Generalized Computer Program 723-X6-L2010, *HEC-1 Flood Hydrograph Package*, California, February 1981, Revised May 1991.
- 4 Flood Control District of Maricopa County, *Draft Drainage Design Manual for Maricopa County, Volume-1 Hydrology*, November 2003.
- 5 National Oceanic and Atmospheric Administration, *NOAA Atlas 2, Precipitation-Frequency Atlas of the Western United States, Volume VIII-Arizona*, 1973.
- 6 Flood Control District of Maricopa County and KVL Consultants, Inc., *Drainage Design Management System (DDMS), Version 1.8 Software*, October 2002.
- 7 ESRI, *ArcMap 9.0*, 2004.
- 8 Flood Control District of Maricopa County, *2004 Color Aerial Photography*, 2004.
- 9 Flood Control District of Maricopa County, *2004 2' Contour Mapping*, 2004.
- 10 Brigham Young University, *Watershed Modeling System Version 7.1*, 2004.
- 11 Maricopa Association of Governments, *MAG General Plan*, (Electronic Format from the Flood Control District of Maricopa County)
- 12 U.S. Department of Agriculture, *Soil Survey of Maricopa County, Arizona-Central Part*, April 1986. (Electronic Format from the Flood Control District of Maricopa County)
- 13 City of Phoenix and PrimaTech LLC, *Engineers and Consultants, East and West Park Dam Safety Analysis Models*, 2004
- 14 Haestad Methods, *StormCAD for Windows Version 5.5*, 2004
- 15 Haestad Methods, *Flow Master for Windows*, 2005
- 16 City of Phoenix, *Storm Water Policies and Standards*, March 2004.

## ATTACHMENTS

- A. Vicinity Map
- B. Proposed Storm Drain Layout/ Map from CAR
- C. Hydrology Maps
- D. Precipitation Data
- E. Soil and Landuse Data
- F. Clark Unit Hydrograph Data
- G. Hydraulic Routing Data
- H. HEC-1 Input/Output
- I. StormCAD Output
- J. Hydrology / Hydraulics Supporting Data
- K. Electronic Files



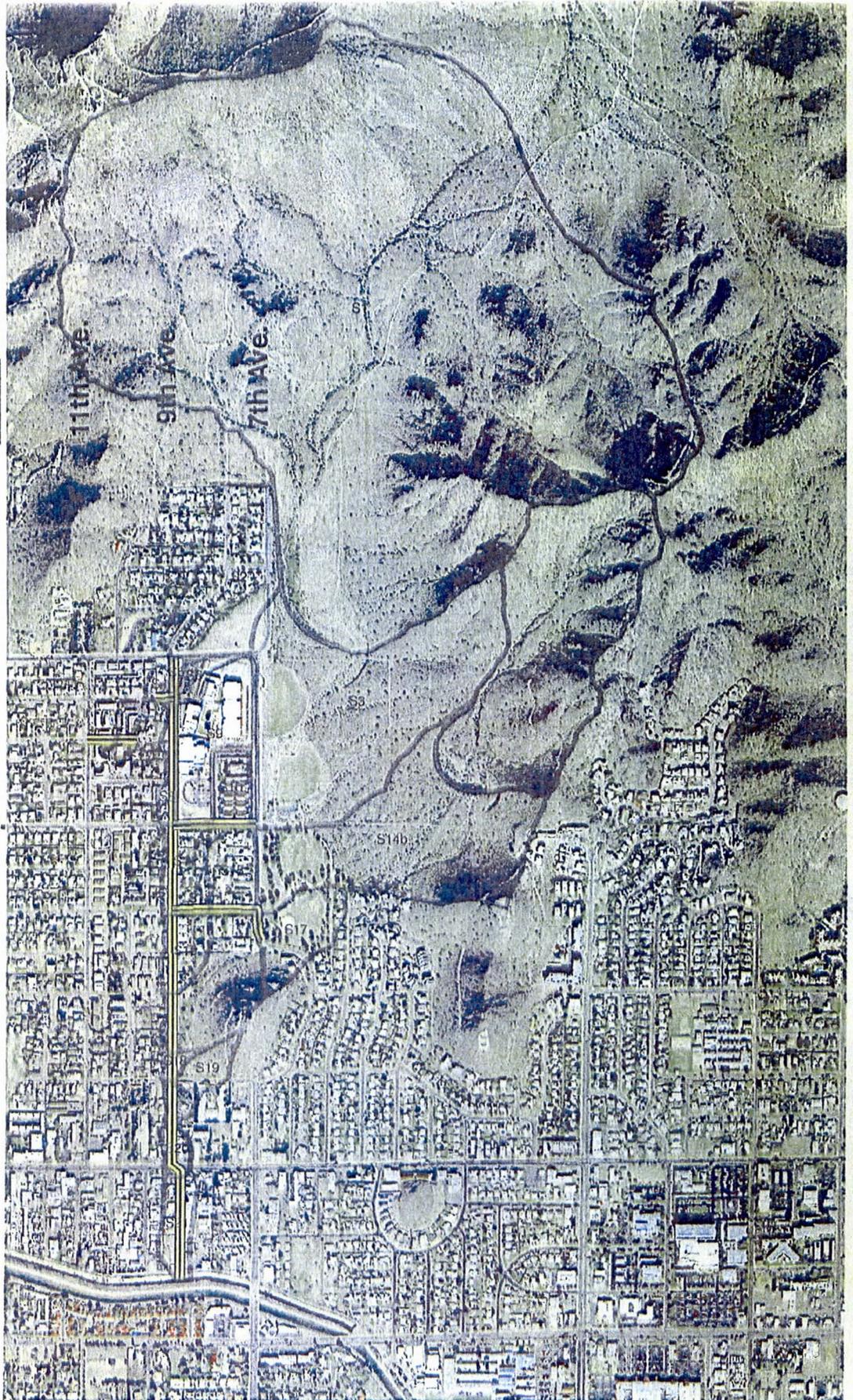
# 9th Avenue Storm Drain - Peoria to ACDC Drainage Technical Memorandum Vicinity Map



Not To Scale

### Legend

 Proposed Storm Drain



Peoria Ave.  
North Ln.  
Cochise Dr.

Cheryl Ave.

Cinnabar Ave.

Mountain View Rd.

Purdue Ave.

Vogel Ave.

Hatcher Dr.

ACDC

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9th Avenue Storm Drain - Peoria to ACDC  
 Drainage Technical Memorandum  
 Proposed Storm Drain System Layout



Not To Scale

**Legend**  
 Proposed Storm Drain

*Map 10 (See Flow Summary Table)*

Peoria Ave.  
 North Ln.  
 Cochise Dr.

Cheryl Ave.

Cinnabar Ave.

Mountain View Rd.

Purdue Ave.

Vogel Ave.

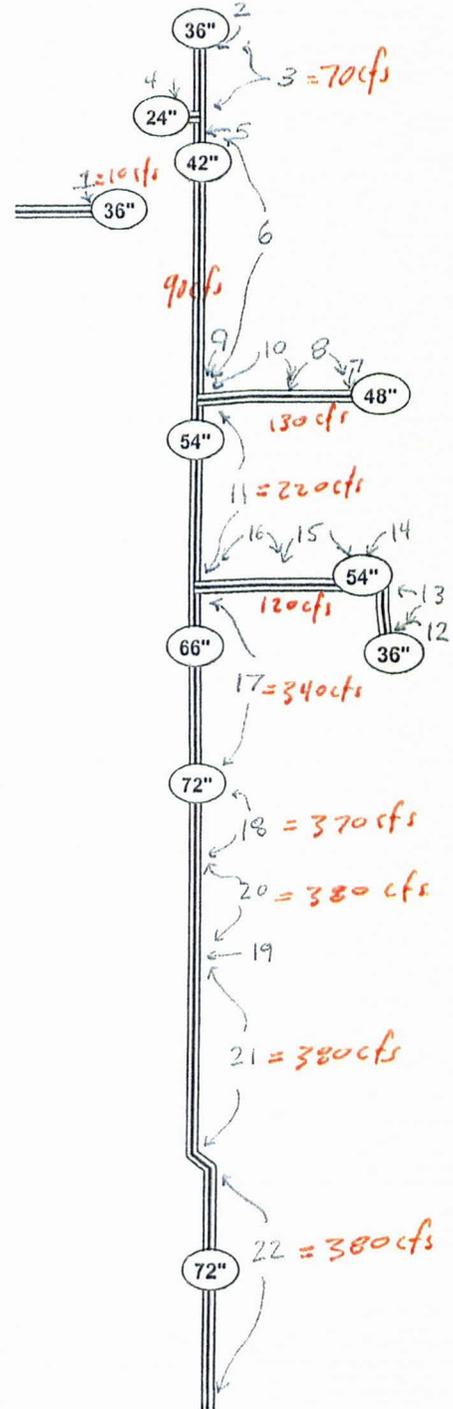
Hatcher Dr.

ACDC

11th Ave.

9th Ave.

7th Ave.





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# 9th Avenue Storm Drain - Peoria to ACDC

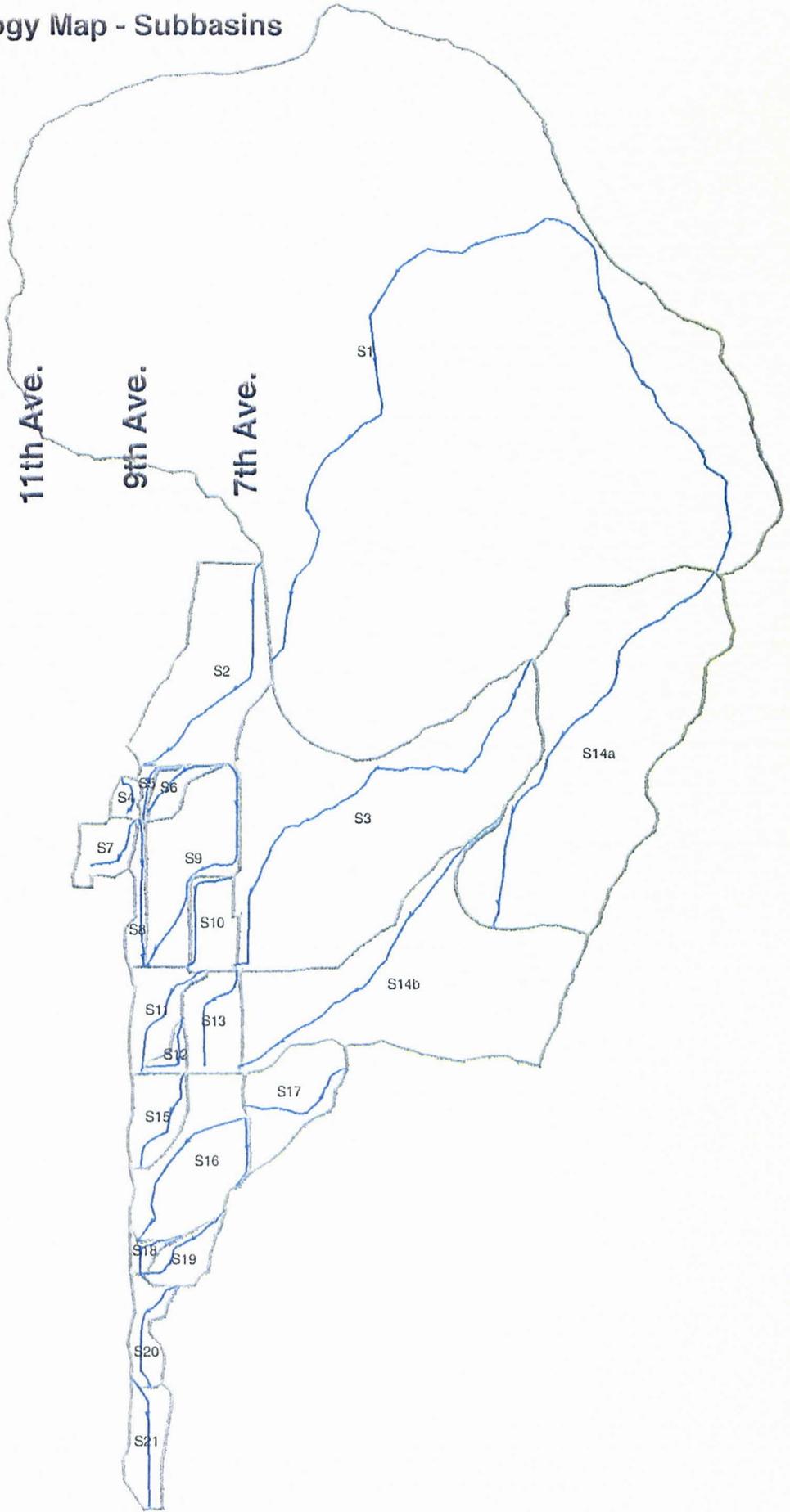
## Hydrology Map - Subbasins



1 inch equals 1,000 feet

### Legend

-  Subbasin Boundaries
-  Hydrologic Routing



Peoria Ave.  
North Ln.  
Cochise Dr.  
  
Cheryl Ave.  
  
Cinnabar Ave.  
  
Mountain View Rd.  
Purdue Ave.  
Vogel Ave.  
  
Hatcher Dr.  
  
ACDC



# 9th Avenue Storm Drain - Peoria to ACDC

## Hydrology Map - Routes and CP's



1 inch equals 1,000 feet

**Legend**

- Subbasin Boundaries
- Hydraulic Routing
- Concentration Points

11th Ave.

9th Ave.

7th Ave.

Peoria Ave.  
North Ln.  
Cochise Dr.

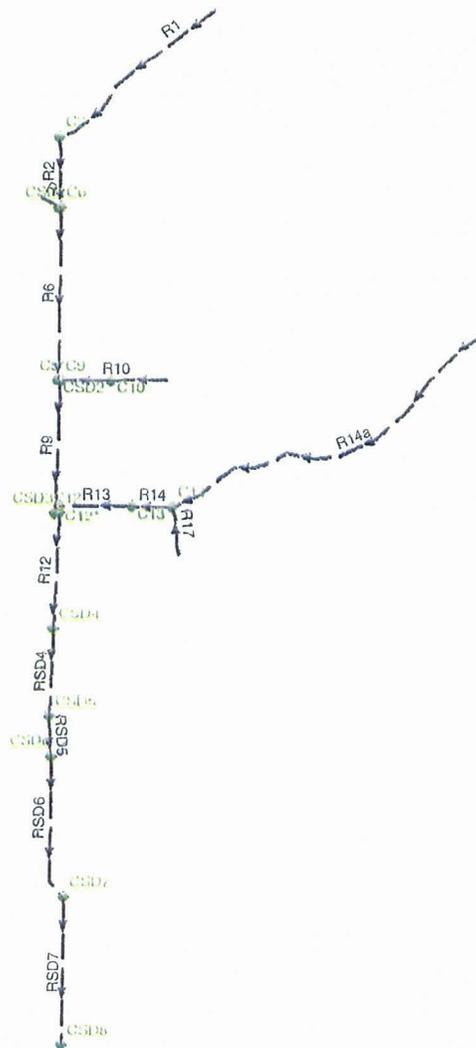
Cheryl Ave.

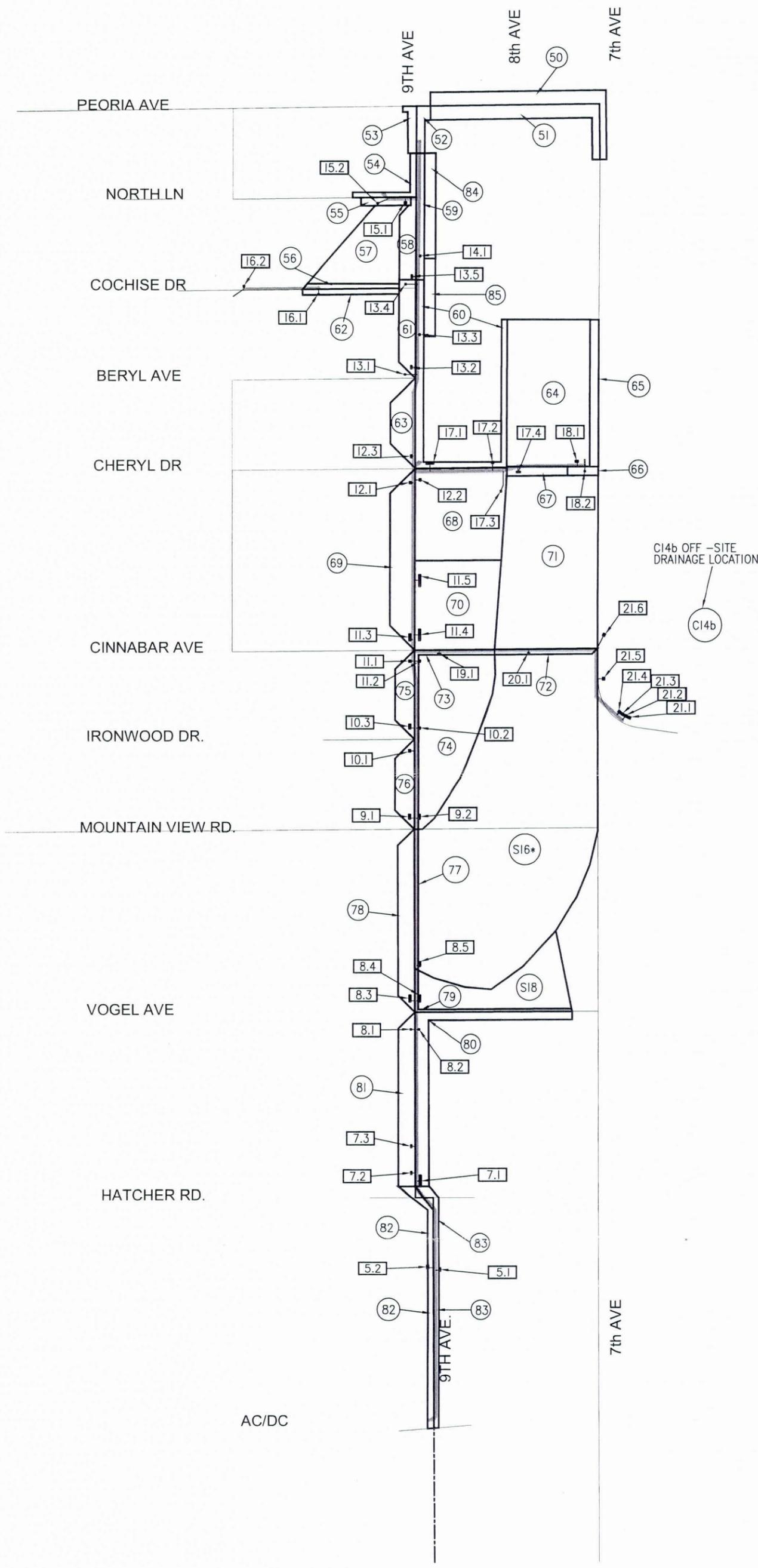
Cinnabar Ave.

Mountain View Rd.  
Purdue Ave.  
Vogel Ave.

Hatcher Dr.

ACDC





AC/DC

1" = 400 FEET

HYDROLOGY MAP LEGEND

- SUBBASIN BOUNDARY
- CATCH BASIN ID
- SUBBASIN ID
- MONUMENT LINE
- STREETS
- PROPOSED STORM DRAIN

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9th Ave. Storm Drain System - Peoria to ACDC  
 City Of Phoenix  
 CONTRACT #STR3130249

LOCAL HYDROLOGY  
 AND CATCH BASINS  
 DATE: 12/13/05

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- K. Electronic Files

- Output from Pre-Pre module in DDM500 -

15 515.5

Flood Control District of Maricopa County  
SUNNYSO - 9th Avenue Storm Drain from Peoria Avenue to ACDC  
Rainfall Data

Pre-Pre input data  
derived using  
atmospheric regional  
model.

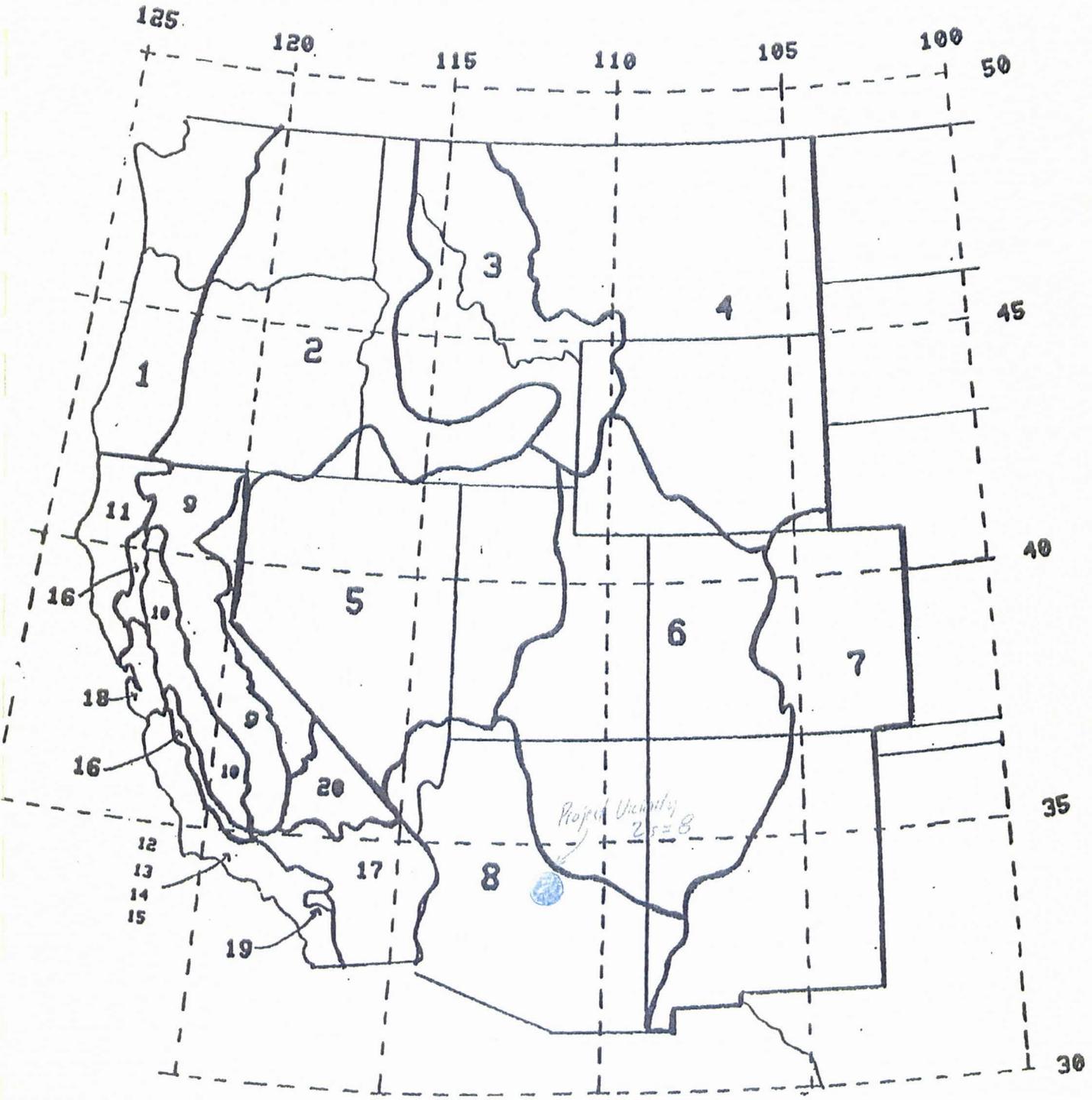
4/26/2005

Page 1

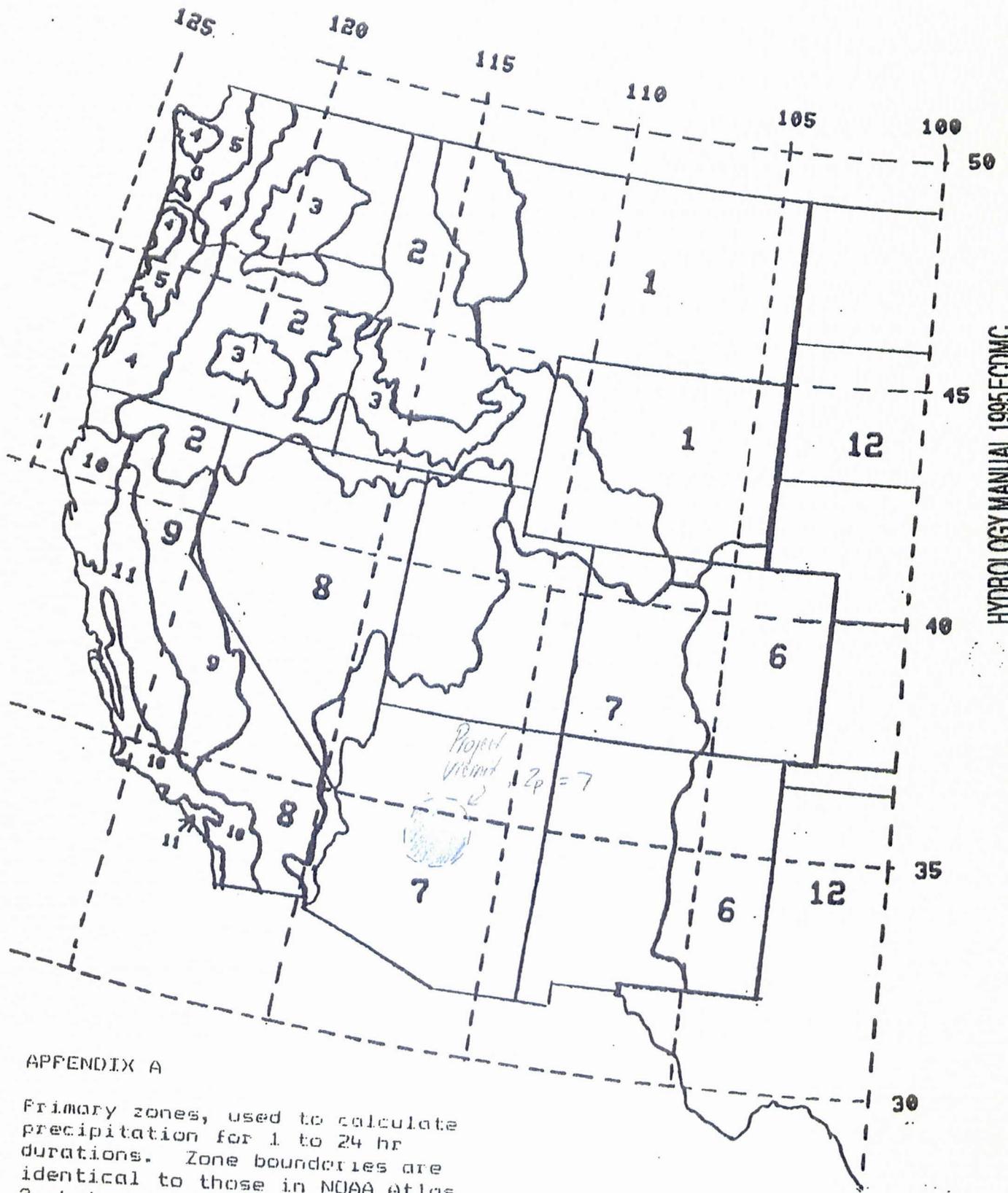
Primary Zone Number: 7      Latitude: 0.0      Elevation: 0  
Short Duration Zone Number: 8      Longitude: 0.0

2-year 100-year  
6-hour 1.2 3.1  
24-hour 1.4 3.8

Duration	Point Values (in)						
	2-Yr	5-Yr	10-Yr	25-Yr	50-Yr	100-Yr	
5 MIN	0.33	0.42	0.49	0.58	0.65	0.72	
10 MIN	0.49	0.64	0.74	0.88	0.99	1.11	
15 MIN	0.59	0.80	0.93	1.12	1.27	1.42	
30 MIN	0.79	1.06	1.25	1.52	1.72	1.92	
1 HOUR	0.96	1.31	1.56	1.89	2.15	2.40	
2 HOUR	1.04	1.44	1.70	2.07	2.36	2.64	
3 HOUR	1.10	1.52	1.80	2.19	2.50	2.80	
6 HOUR	1.20	1.67	1.99	2.43	2.76	3.10	
12 HOUR	1.30	1.84	2.20	2.69	3.07	3.45	
24 HOUR	1.40	2.00	2.40	2.95	3.38	3.80	

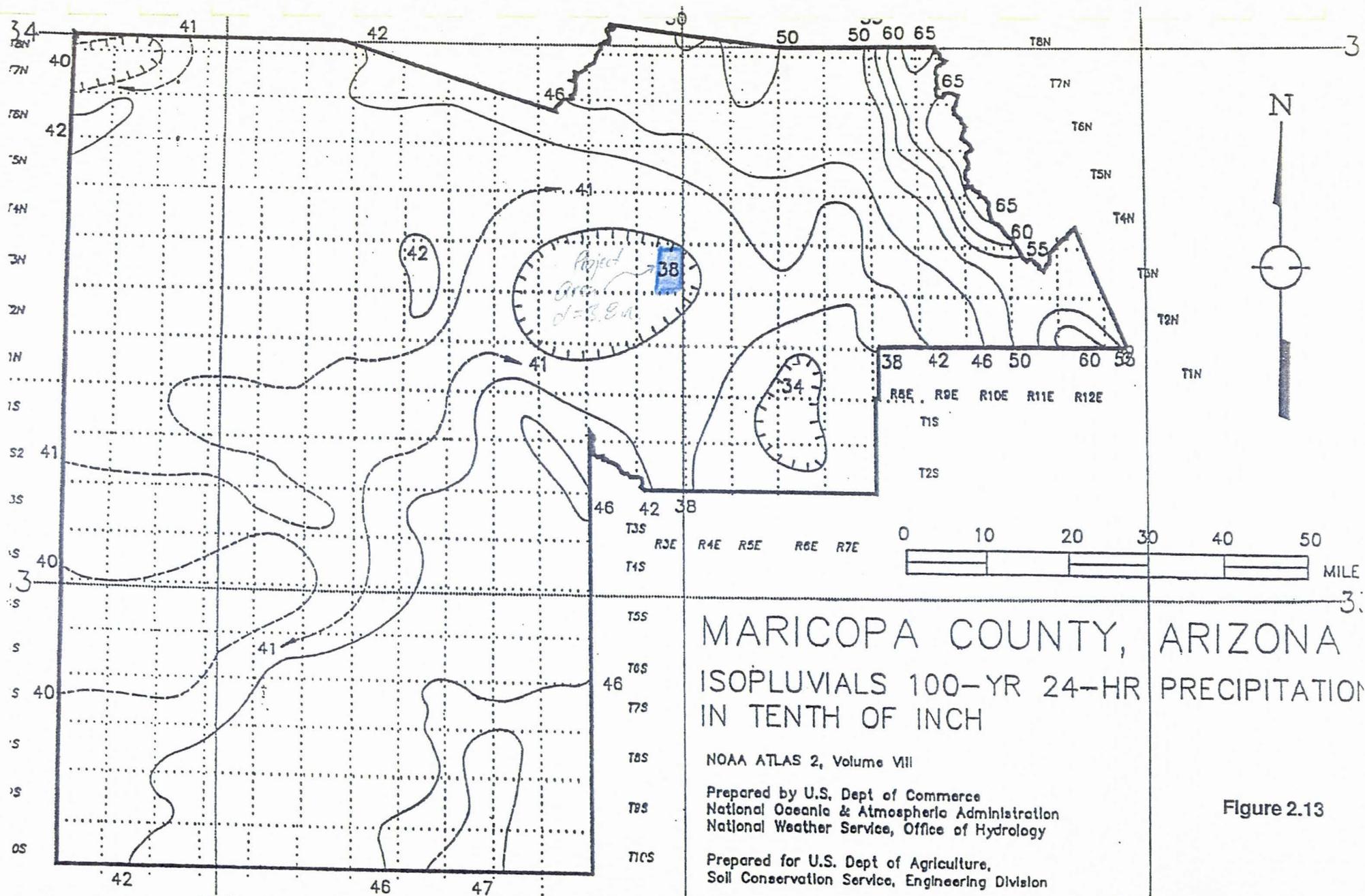


APPENDIX B  
Short-duration zones, used to  
calculate 5 to 30 min durations.



APPENDIX A

Primary zones, used to calculate precipitation for 1 to 24 hr durations. Zone boundaries are identical to those in NOAA Atlas 2, but zone numbers may differ.



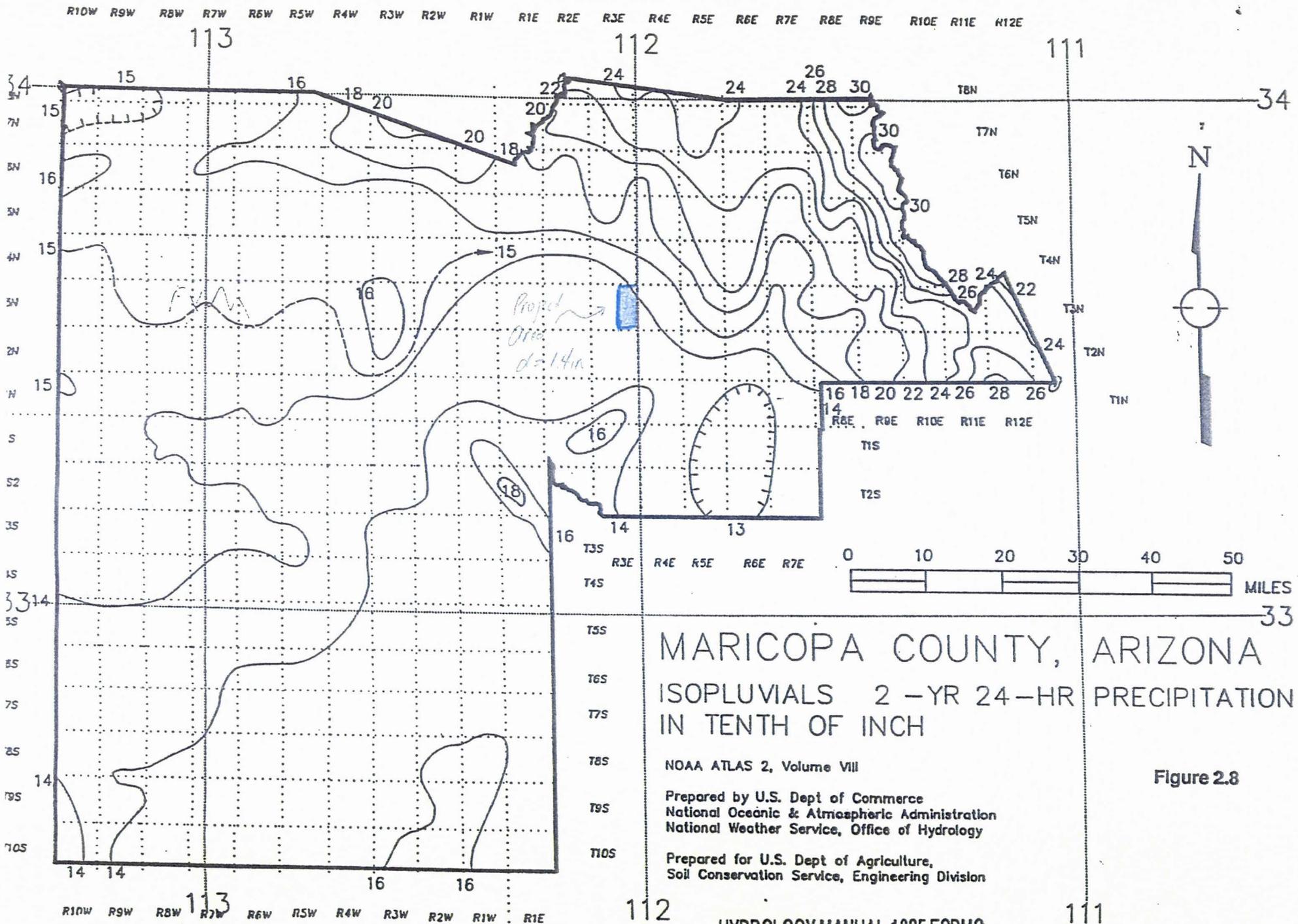
MARICOPA COUNTY, ARIZONA  
 ISOPLUVIALS 100-YR 24-HR PRECIPITATION  
 IN TENTH OF INCH

NOAA ATLAS 2, Volume VIII  
 Prepared by U.S. Dept of Commerce  
 National Oceanic & Atmospheric Administration  
 National Weather Service, Office of Hydrology  
 Prepared for U.S. Dept of Agriculture,  
 Soil Conservation Service, Engineering Division

Figure 2.13

113  
 R10W R9W R8W R7W R6W R5W R4W R3W R2W R1W R1E

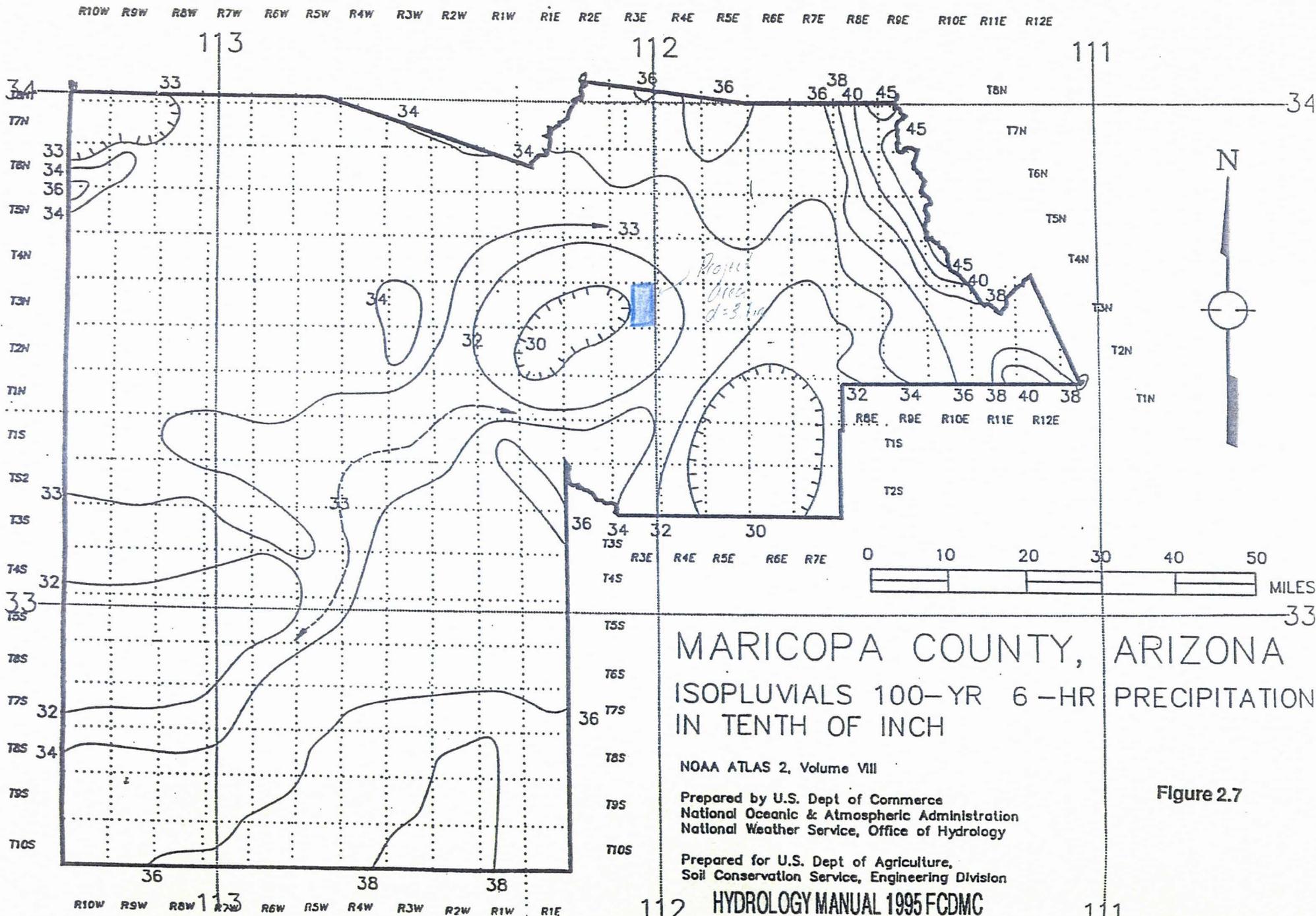
112  
 111



MARICOPA COUNTY, ARIZONA  
 ISOPLUVIALS 2-YR 24-HR PRECIPITATION  
 IN TENTH OF INCH

NOAA ATLAS 2, Volume VIII  
 Prepared by U.S. Dept of Commerce  
 National Oceanic & Atmospheric Administration  
 National Weather Service, Office of Hydrology  
 Prepared for U.S. Dept of Agriculture,  
 Soil Conservation Service, Engineering Division

Figure 2.8



MARICOPA COUNTY, ARIZONA  
 ISOPLUVIALS 100-YR 6-HR PRECIPITATION  
 IN TENTH OF INCH

NOAA ATLAS 2, Volume VIII  
 Prepared by U.S. Dept of Commerce  
 National Oceanic & Atmospheric Administration  
 National Weather Service, Office of Hydrology

Prepared for U.S. Dept of Agriculture,  
 Soil Conservation Service, Engineering Division

Figure 2.7

R10W R9W R8W R7W R6W R5W R4W R3W R2W R1W R1E R2E R3E R4E R5E R6E R7E R8E R9E R10E R11E R12E

113

112

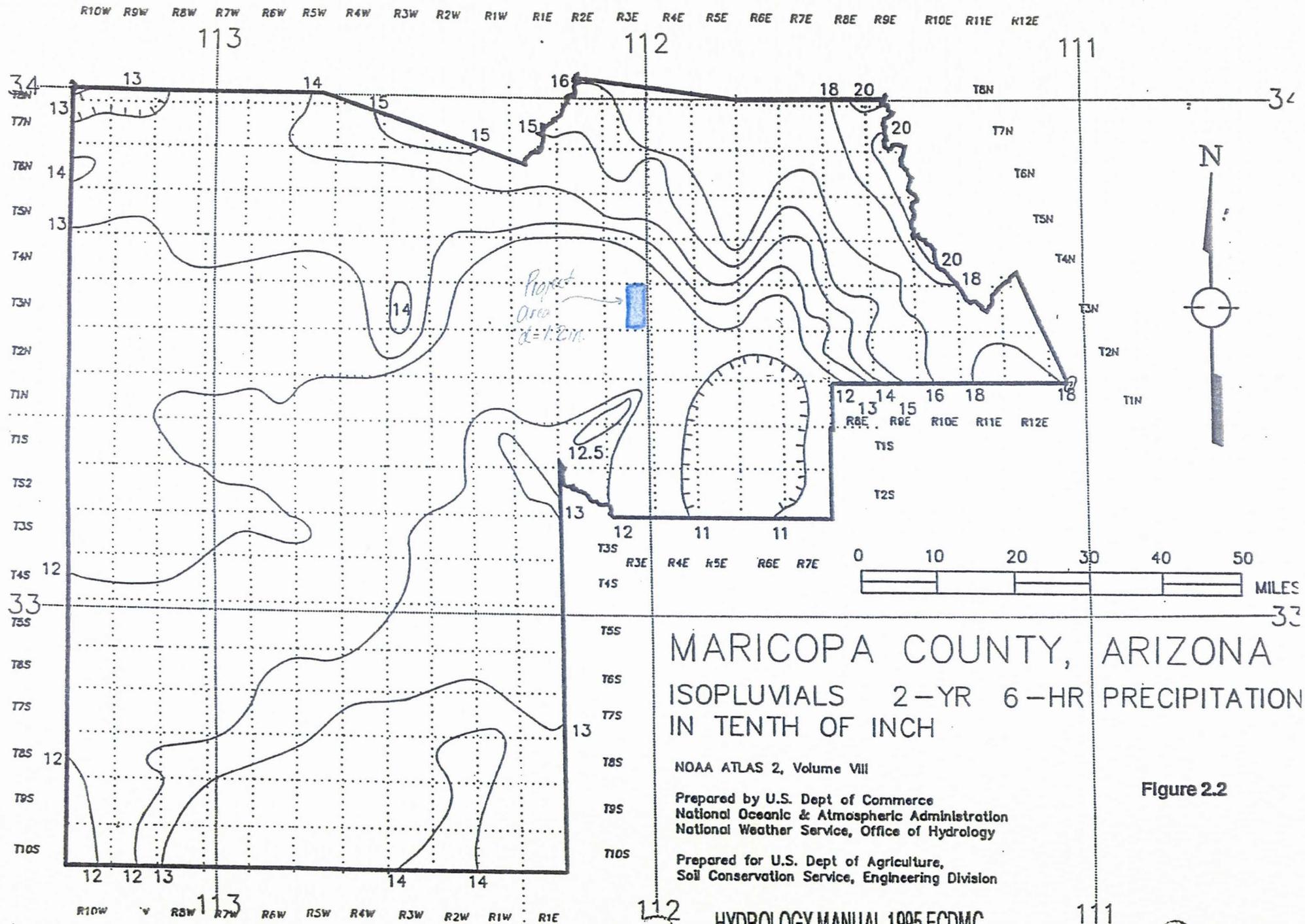
111

T8N  
T7N  
T6N  
T5N  
T4N  
T3N  
T2N  
T1N  
T1S  
T2S  
T3S  
T4S  
T5S  
T6S  
T7S  
T8S  
T10S

R10W R9W R8W R7W R6W R5W R4W R3W R2W R1W R1E

112

111



MARICOPA COUNTY, ARIZONA  
 ISOPLUVIALS 2-YR 6-HR PRECIPITATION  
 IN TENTH OF INCH

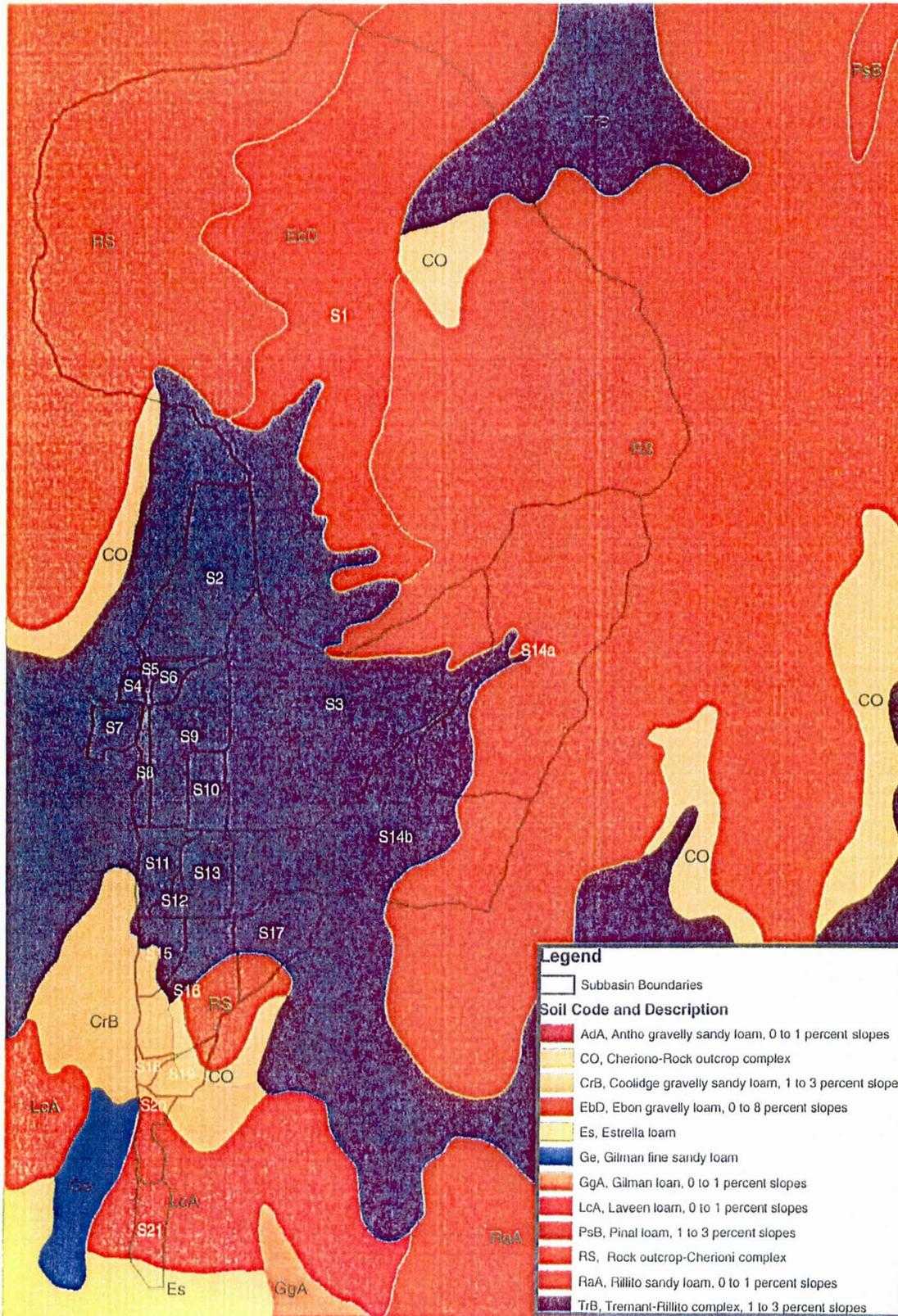
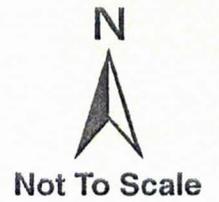
NOAA ATLAS 2, Volume VIII  
 Prepared by U.S. Dept of Commerce  
 National Oceanic & Atmospheric Administration  
 National Weather Service, Office of Hydrology  
 Prepared for U.S. Dept of Agriculture,  
 Soil Conservation Service, Engineering Division

Figure 2.2

## ATTACHMENTS

- A. Vicinity Map
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- J. Hydrology / Hydraulics Supporting Data
- K. Electronic Files

Drainage Technical Memorandum  
 Soil Data (SCS Soil Survey)  
 9th Avenue Storm Drain - Peoria to ACDC



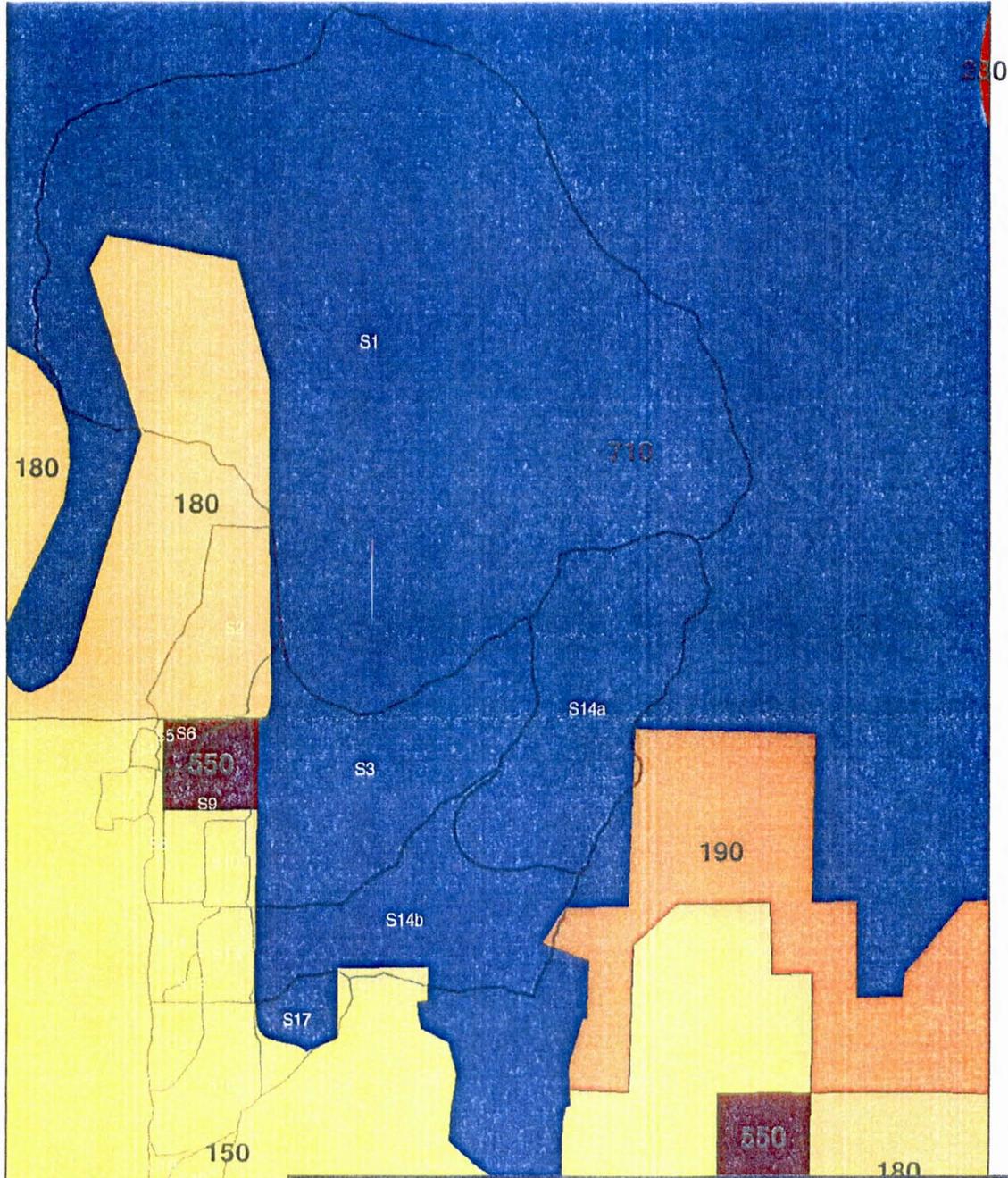
**Legend**

Subbasin Boundaries

**Soil Code and Description**

AdA	Antho gravelly sandy loam, 0 to 1 percent slopes
CO	Cheriono-Rock outcrop complex
CrB	Coolidge gravelly sandy loam, 1 to 3 percent slopes
EbD	Ebon gravelly loam, 0 to 8 percent slopes
Es	Estrella loam
Ge	Gilman fine sandy loam
GgA	Gilman loam, 0 to 1 percent slopes
LcA	Laveen loam, 0 to 1 percent slopes
PsB	Pinal loam, 1 to 3 percent slopes
RS	Rock outcrop-Cherioni complex
RaA	Rillito sandy loam, 0 to 1 percent slopes
TrB	Tremant-Rillito complex, 1 to 3 percent slopes

Drainage Technical Memorandum  
 Landuse Data (MAG General Plan)  
 9th Avenue Storm Drain - Peoria to ACDC



Legend	
	Subbasin Boundaries
Landuse Code and Description	
	150, Small Lot Residential - Single Family (4-6 du per acre)
	180, High Density Residential - Multi Family (10-15 du per acre)
	190, Very High Density Residential - Multi Family (> 15 du per acre)
	220, Neighborhood Commercial (50,000 to 100,000 sq. ft.)
	230, Community Commercial (100,000 to 500,000 sq. ft.)
	320, Industrial
	520, Educational (Public schools, private schools and universities)
	550, Public Facilities (Includes community centers, power sub-stations, libraries, city halls, police / fire stations and other government facilities)
	710, Active Open Space (Includes parks)

**Entellus Inc.**

CLIENT COP and FCD  
 JOB 9th Avenue Storm Drain

BY JCS

DATE 6/30/2004

JOB No. 115076F

**Landuse and Soil Parameters**

*This information was obtained from the District and imported into WMS in order to generate the Green and Ampt Parameters.  
 The District Tables were clipped to only show the landuse and soil types present in the study area.*

Soil Code	Description	Soil Name	XKSAT	RTIMP	% Effective
651202720	Antho gravelly sandy loam, 0 to 1 percent slopes	AdA	0.4	0	100
6512448	Cheriono-Rock outcrop complex	CO	0.29	20	100
651245522	Coolidge gravelly sandy loam, 1 to 3 percent slopes	CrB	0.4	0	100
651282326	Ebon gravelly loam, 0 to 8 percent slopes	EbD	0.1	0	100
6512857	Estrella loam	Es	0.25	0	100
6513229	Gilman fine sandy loam	Ge	0.26	0	100
651323320	Gilman loam, 0 to 1 percent slopes	GgA	0.25	0	100
651422520	Laveen loam, 0 to 1 percent slopes	LcA	0.25	0	100
651505722	Pinal loam, 1 to 3 percent slopes	PsB	0.26	0	100
651542120	Rillito sandy loam, 0 to 1 percent slopes	RaA	0.39	0	100
6515456	Rock outcrop-Cherioni complex	RS	0.4	65	100
651585522	Tremant-Rillito complex, 1 to 3 percent slopes	TrB	0.13	0	100

Landuse Code	Description	IA	RTIMP	Percent Veg	Saturation
150	Small Lot Residential - Single Family (4-6 du per acre)	0.25	35	50	normal
180	High Density Residential - Multi Family (10-15 du per acre)	0.25	65	50	normal
190	Very High Density Residential - Multi Family (> 15 du per acre)	0.25	85	50	normal
220	Neighborhood Commercial (50,000 to 100,000 sq. ft.)	0.1	80	65	normal
230	Community Commercial (100,000 to 500,000 sq. ft.)	0.1	80	75	normal
320	Industrial	0.15	55	60	normal
520	Educational (Public schools, private schools and universities)	0.29	45	80	normal
550	Public Facilities (Includes community centers, power sub-stations, libraries)	0.1	80	75	normal
710	Active Open Space (Includes parks)	0.1	5	50	normal

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**Entellus Inc.**

CLIENT COP and FCD

JOB 9th Avenue Storm Drain

BY JCS

DATE 6/30/2004

JOB No. 115076F

**Clark Unit Hydrograph Parameters**

The information shown on the table below was inputted into WMS in order to generate the Clark Unit Hydrograph Parameters.

Subbasin ID	Length (Miles)	Upstream Elevation (Feet)	Downstream Elevation (Feet)	Slope (Feet/Mile)	Adjusted Slope <sup>1</sup> (Feet/Mile)	Roughness "Kb"	Subbasin Area (Sq.Miles)	100-Year Precipitation		10-Year Precipitation	
								Tc Hours	Rs	Tc Hours	Rs
S1	1.3	2100	1316	603	313	D	0.5385			0.542	0.329
S2	0.32	1342	1303	122	122	A	0.0283			0.15	0.138
S3	0.624	1760	1286	718	313	C	0.0861			0.3	0.27
S4	0.056	1302	1296	107	107	A	0.0017			0.083	0.088
S5	0.104	1306	1296	96	96	A	0.0012			0.104	0.224
S6	0.123	1310	1296	114	114	A	0.003			0.104	0.153
S7	0.094	1295	1284	117	117	A	0.0049			0.088	0.077
S8	0.18	1310	1281	161	161	A	0.0032			0.113	0.216
S9	0.31	1310	1280	97	97	A	0.0183			0.163	0.188
S10	0.152	1297	1284	86	86	A	0.0065			0.121	0.137
S11	0.165	1283	1268	91	91	A	0.0073			0.125	0.143
S12	0.101	1280	1268	119	119	A	0.0018			0.096	0.16
S13	0.141	1284	1272	85	85	A	0.0085			0.117	0.107
S14a	0.538	2100	1348	1398	313	D	0.082			0.329	0.242
S14b	0.464	1420	1274	315	268	C	0.0624			0.271	0.228
S15	0.138	1272	1258	101	101	A	0.0068			0.108	0.11
S16	0.313	1418	1254	524	305	C	0.0197			0.221	0.256
S17	0.16	1288	1270	113	113	B	0.0126			0.158	0.113
S18	0.083	1270	1250	241	233	A	0.0015			0.083	0.128
S19	0.141	1418	1250	1191	313	D	0.0046			0.183	0.252
S20	1.51	1248	1242	40	40	A	0.005			0.154	0.209
S21	0.168	1242	1234	48	48	A	0.0067			0.154	0.192

<sup>1</sup> The Slope were adjusted using Table 5.2 from the District Hydrology Manual

<sup>2</sup> Kb values were estimated using the criteria in Table 5.3 from the District Hydrology Manual

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SHEET \_\_\_\_\_ OF \_\_\_\_\_

BY 11 DATE 5/5/15

CHECK \_\_\_\_\_ DATE \_\_\_\_\_

CLIENT COP-FCD

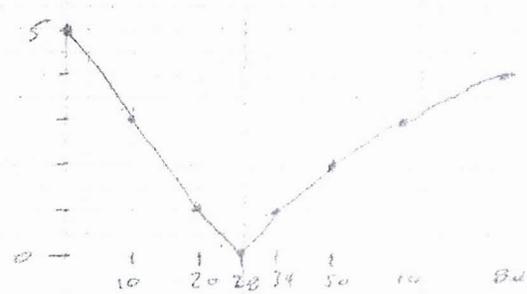
JOB NAME 9th Ave SD - Review to 9000

JOB NO. 115076F

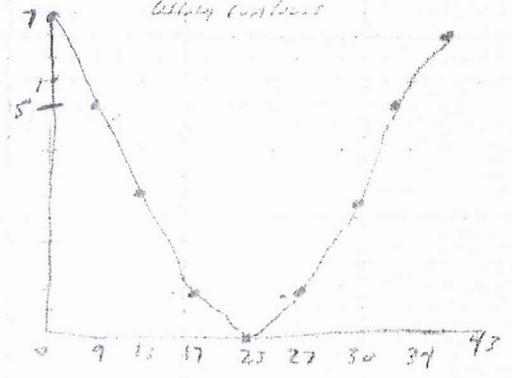
*Road Notes*

ID	Length (ft)	Upstream Elevation	Downstream Elevation	Slope	Other
R1	1086	1316	1303	.0120	Manhole (.04, .055, .04)
R2	375	1303	1296	.0187	Pipe $\phi = 60"$ , manhole = .013
R4	128	1296.5'	1296	.0039	Pipe $\phi = 36"$ , manhole = .013
R6	935	1296	1280	.0171	Pipe $\phi = 60"$ , manhole = .013
R3	310	1286	1284	.0065	Pipe $\phi = 48"$ , manhole = .013
R10	262	1284	1280	.0153	Pipe $\phi = 48"$ , manhole = .013
R9	695	1280	1268	.0177	Pipe $\phi = 72"$ , manhole = .013
R17	257	1270	1269.5	.0019	Pipe $\phi = 36"$ , manhole = .013
R14a	2034	1350	1272	.0383	Manhole (.04, .055, .04)
R14	219	1274	1272	.0091	Pipe $\phi = 36"$ , manhole = .013
R13	340	1272	1268	.0103	
R12	613	1268	1258	.0163	Pipe $\phi = 48"$ Manhole = .013 Pipe $\phi = 84"$ Manhole = .013
RSD4	478	1258	1254	.0084	Pipe $\phi = 84"$ , manhole = .013
RSD5	213	1254	1250	.0188	" "
RSD6	764	1250	1242	.0105	" "
RSD7	788	1242	1234	.0102	" "

R14a - Geometry approximated using contours



R1 - Geometry approximated using contours



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*****
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
* JUN 1998 *
* VERSION 4.1 *
* RUN DATE 18MAY05 TIME 09:44:09 *
*****

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*****
* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 756-1104 *
*****

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THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HECIGS, HECIDB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE.

THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION

NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE, SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY, DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL, LOSS RATE:GREEN AND AMPT INFILTRATION

KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1 HEC-1 INPUT PAGE 1

```

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
1 ID City of Phoenix and the Flood Control District of Maricopa County
2 ID COP# ST83130249, FCD#580.02.20
3 ID 9th Avenue Storm Drain from Peoria Avenue to ACDC (Sunnyslope Storm Drai
4 ID
5 ID EVENT: 10 Year - 6 hour
6 ID RAINFALL DISTRIBUTION: Per Flood Control District of Maricopa County H
7 ID TIME OF CONCENTRATION: Per Arizona Department of Transportation Hydrol
8 ID INPUT FILE NAME: 10ySunnysSD.hcl
9 ID DATE: May 2005
10 ID
11 ID PREPARED BY: Entellus Inc.
12 ID ADDRESS: 2255 N. 44th Street
13 ID Phoenix, ARIZONA 85008
14 ID TEL: (602)244-2566
15 ID FAX: (602)244-8947
16 ID
17 ID
18 ID NOTES BY ENTELLUS:
19 ID Regarding runoff routing through the proposed storm drain system, all pi
20 ID based on a preliminary estimate of the required pipe size. The pipe size
21 ID not necessarily the pipe size proposed for the system. The pipe slope wa
22 ID using the existing grade determined using the District provided 2' conto
23 ID shown in the model are not necessarily the proposed slopes.
24 ID
25 ID Green and Ampt parameters were estimated using WMS 7.1, with the SCS Soi
26 ID the MAG General Plan.
27 ID
28 ID Clark Unit Hydrograph parameters were estimated using WMS 7.1.
29 ID
*
*
*DIAGRAM
*
*
30 IT 1 600
31 IO 5
*
*
* The peak flow in S7 is the design flow for the inlets and pipe along
* Cochise Drive.
32 KK S7
33 KO 0 0 0.0 0 22
34 BA 0.0049
35 PH .49 .93 1.56 1.70 1.80 1.99
36 LG 0.25 0.21 6.4 0.188 35.0
* 10 Year Clark Unit Hydrograph Parameters
37 UC .088 .077
*
*

```

1 HEC-1 INPUT PAGE 2

```

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

```

38 KK S1  
 39 KO 0 0 0.0 0 22  
 40 BA 0.5385  
 41 LG 0.115 0.25 4.915 0.282 46.991  
 \* 10 Year Clark Unit Hydrograph Parameters  
 42 UC .542 .329  
 \*  
 \*  
 \* The stage, storage, discharge operation below was obtained from the West Park  
 \* Dam Safety Analysis Model created by PrimaTech. The rating curve represents  
 \* the outflow from the principal outlet pipe.

43 KK WPD  
 44 KM Runoff is stored behind West Park Dam.  
 45 RS 1 STOR 0 -1  
 46 SV 0.0 1.50 6.20 28.05 53.80 109.10 109.10 131.90 157.65 186.85  
 47 SE 1313.4 1317.00 1320.00 1326.00 1330.00 1336.00 1336.10 1338.00 1340.00 1342.00  
 48 SQ 0.0 14.31 19.36 26.73 30.67 35.78 45.42 892.79 2458.42 4485.34  
 \*  
 \*  
 \* R1 routes runoff from the West Park Dam principal outlet through a wash  
 \* to the intersection of Peoria and 9th Avenues.  
 \* The route parameters were extracted using the 2' contours supplied by the  
 \* District. The normal depth routing methodology was used.

49 KK R1  
 50 RS 1 FLOW -1  
 51 RC .04 .035 .04 1086 .0120  
 52 RX 0 13 17 23 27 30 34 43  
 53 RY 7 3 1 0 1 3 5 7  
 \*  
 \*

54 KK S2  
 55 KO 0 0 0.0 0 22  
 56 BA 0.0283  
 57 LG 0.25 0.21 6.4 0.188 65.0  
 \* 10 Year Clark Unit Hydrograph Parameters  
 58 UC .150 .138  
 \*  
 \*  
 \* C2 combines runoff from subbasin S2 and route R1  
 \* The peak flow from this concentration point is the design flow for the inlet  
 \* into the storm drain system at the intersection of Peoria Avenue and 9th Avenue

59 KK C2  
 60 HC 2  
 \*  
 \*  
 \* Route R2  
 \* The route is through the proposed 9th Avenue storm drain between  
 \* Peoria Avenue and North Lane.

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

61 KK R2  
 62 RS 1 FLOW -1  
 63 RK 375 .0187 .013 CIRC 5  
 \*  
 \*  
 \* The peak flow from S5 is the design flow for inlets into  
 \* the 9th Avenue storm drain between Peoria Avenue and North Lane.

64 KK S5  
 65 KO 0 0 0.0 0 22  
 66 BA 0.0012  
 67 LG 0.2 0.21 6.4 0.2 50.0  
 \* 10 Year Clark Unit Hydrograph Parameters  
 68 UC .104 .224  
 \*  
 \*  
 \* CSD1 (Storm Drain Reach 1) combines runoff from S5 and R1  
 \* The peak flow at CSD1 is the design flow for the 9th Avenue  
 \* storm drain pipe between Peoria Avenue and the North Lane, and is the

69 KK CSD1  
 70 HC 2  
 \*  
 \*  
 \* The peak flow from S4 is the design flow for inlets into the  
 \* lateral pipe along North Lane, and the design flow for the  
 \* lateral pipe along North Lane.

71 KK S4  
 72 KO 0 0 0.0 0 22  
 73 BA 0.0017  
 74 LG 0.25 0.21 6.4 0.188 35.0  
 \* 10 Year Clark Unit Hydrograph Parameters  
 75 UC 0.083 0.088  
 \*  
 \*  
 \* Route R4

\* The route is through the proposed lateral along North Lane

76 KK R4  
77 RS 1 FLOW -1  
78 RK 128 .0039 .013 CIRC 3

\*  
\* The peak flow from subbasin S6 is the design flow for the inlets at the  
\* intersection of 9th Avenue and North Lane. The inlet will catch runoff  
\* leaving the school parking lot.

79 KK S6  
80 KO 0 0 0.0 0 22  
81 BA 0.0030  
82 LG 0.1 0.21 6.4 0.224 80.0  
83 UC 0.104 0.153

\* 10 Year Clark Unit Hydrograph Parameters

\* C6 combines runoff from subbasin S6, Route R4 and C5  
HEC-1 INPUT

PAGE 4

1  
LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

84 KK C6  
85 HC 3

\*  
\* Route R6 routes runoff concentrating near the intersection of North Lane  
\* and 9th Avenue to the intersection of Cheryl Drive and 9th Avenue,  
\* along 9th Avenue. The route is through the proposed 9th Avenue storm drain.

86 KK R6  
87 RS 1 FLOW -1  
88 RK 935 .0171 .013 CIRC 5

\* The peak flow from S8 is the design flow for inlets into  
\* the 9th Avenue storm drain between North Lane and Cheryl Drive.

89 KK S8  
90 KO 0 0 0.0 0 22  
91 BA 0.0032  
92 LG 0.25 0.21 6.4 0.188 35.0  
93 UC .113 .216

\* 10 Year Clark Unit Hydrograph Parameters  
\* CSD2 (Storm Drain Reach 2) combines runoff from subbasin S8 and Route R6.  
\* The peak flow will be the design flow for the 9th Avenue storm drain  
\* between North Lane and Cheryl Drive.

94 KK CSD2  
95 HC 2

\* The peak flow from S3 is the design flow for inlets into  
\* the lateral along Cheryl Drive at 7th Avenue.

96 KK S3  
97 KO 0 0 0.0 0 22  
98 BA 0.0861  
99 LG 0.106 0.25 5.879 0.215 18.356  
100 UC .300 .270

\* 10 Year Clark Unit Hydrograph Parameters  
\* Route R3 routes runoff concentrating near the intersection of 7th  
\* Avenue and Cheryl Drive to the dip section on Cheryl Drive  
\* at approximately the 8th Avenue Alignment.  
\* The route is through the proposed lateral along Cheryl Drive.

101 KK R3  
102 RS 1 FLOW -1  
103 RK 310 .0065 .013 CIRC 4

\* The peak flow at S10 will be the design flow at the inlets at the dip  
\* section on Cheryl Drive at approximately the 8th Avenue alignment.  
HEC-1 INPUT

PAGE 5

1  
LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

104 KK S10  
105 KO 0 0 0.0 0 22  
106 BA 0.0065  
107 LG 0.25 0.21 6.4 0.188 35.0  
108 UC .121 .137

\* 10 Year Clark Unit Hydrograph Parameters  
\* C10 combines runoff from subbasin S10 and Route R3.  
\* The peak flow at C10 will be the design flow for the lateral along Cheryl

\* drive between 7th Avenue and the dip section on Cheryl drive

109  
110

KK C10  
HC 2

\*  
\* Route R10 routes runoff concentrating at the dip section on Cheryl Drive  
\* to 9th Avenue.  
\* The route is through the proposed lateral along Cheryl Drive.

111  
112  
113

KK R10  
RS 1 FLOW -1  
RK 262 .0153 .013 CIRC 4

\*  
\* The peak flow from subbasin S9 is the design flow for the inlets at the  
\* intersection of 9th Avenue and Cheryl Drive. The inlet will catch runoff  
\* leaving the school site.

114  
115  
116  
117

KK S9  
KO 0 0 0.0 0 22  
BA 0.0183  
LG 0.158 0.21 6.4 0.21 62.572

\* 10 Year Clark Unit Hydrograph Parameters  
UC .163 .188

\* C9\* combines runoff from subbasin S9, Route R10 and C8.

119  
120

KK C9\*  
HC 2

\* C9 combines runoff from subbasin CSD2 and C9\*

121  
122

KK C9  
HC 2

\* Route R9 routes runoff concentrating near the intersection of Cheryl Drive  
\* and 9th Avenue to the intersection of Cinnabar Avenue and 9th Avenue,  
\* along 9th Avenue. The route is through the proposed 9th Avenue storm drain.  
HEC-1 INPUT

1

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

123  
124  
125

KK R9  
RS 1 FLOW -1  
RK 695 .0173 .013 CIRC 6

\* The peak flow from S11 will be the design flow for inlets along 9th Avenue  
\* between Cheryl Drive and Cinnabar Avenue.

126  
127  
128  
129

KK S11  
KO 0 0 0.0 0 22  
BA 0.0073  
LG 0.25 0.21 6.4 0.188 35.0

\* 10 Year Clark Unit Hydrograph Parameters  
UC .125 .143

\* CSD3 (Storm Drain Reach 3) combines runoff from subbasin S11 and Route R9.  
\* The flow will be the design flow for the 9th Avenue Storm drain  
\* pipe between Cheryl Drive and Cinnabar Avenue.

131  
132

KK CSD3  
HC 2

\* The peak flow from S17 will be the design flow for inlets at the bend  
\* along 7th Avenue near the southwest corner of Mountain View Park

133  
134  
135  
136

KK S17  
KO 0 0 0.0 0 22  
BA 0.0126  
LG 0.147 0.25 5.671 0.23 30.962

\* 10 Year Clark Unit Hydrograph Parameters  
UC .158 .133

\* Route R17 routes runoff from the bend at 7th Avenue, north to the lateral  
\* along Cinnabar Avenue through a proposed lateral pipe section.

138  
139  
140

KK R17  
RS 1 FLOW -1  
RK 257 .0019 .013 CIRC 3

141  
142  
143  
144

KK S14a  
KO 3  
BA 0.082  
LG 0.101 0.25 4.293 0.363 60.989

\* 10 Year Clark Unit Hydrograph Parameters by Entellus

145 UC 0.329 0.242

\*  
\* The stage, storage, discharge operation below was obtained from the East Park  
\* Dam Safety Analysis Model created by PrimaTech. The rating curve represents  
\* the outflow from the principal outlet pipe.  
HEC-1 INPUT

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

146 KK EPD  
147 KM Runoff is stored behind West Park Dam.  
148 RS 1 STOR 0 -1  
149 SV 0.00 0.10 0.45 1.30 2.40 6.75 14.50 21.00 26.25 34.00  
150 SE 1345. 1348.20 1350.00 1352.50 1355.00 1360.00 1365.00 1368.00 1370.00 1372.70  
151 SQ 0.00 0.00 5.00 9.12 11.64 15.00 17.05 18.18 390.81 1359.72

\*  
\* R14a routes runoff from the East Park Dam principal outlet through a wash  
\* to the intersection of 7th Avenue and Cinnabar Avenue.  
\* The route parameters were extracted using the 2' contours supplied by the  
\* District. The normal depth routing methodology was used.

152 KK R14a  
153 RS 1 FLOW -1  
154 RC .04 .035 .04 2034 .0383  
155 RX 0 10 20 28 34 50 70 80  
156 RY 5 3 1 0 1 2 3 4

157 KK S14b  
158 KO 0 0 0.0 0 22  
159 BA 0.0624  
160 LG 0.105 0.25 5.556 0.239 25.56  
\* 10 Year Clark Unit Hydrograph Parameters  
161 UC .271 .228

\* The flow at C14b will be the design flow for the inlets at 7th Avenue and  
\* Cinnabar Avenue.  
\* C14 combines runoff from subbasin S14b and Route R14a.

162 KK C14b  
163 HC 2  
\*  
\* C14 combines runoff from subbasin C14b and Route R17.

164 KK C14  
165 HC 2  
\*  
\* Route R14 routes runoff from the intersection of 7th Avenue and Cinnabar  
\* Avenue along 7th Avenue to the dip section through the proposed lateral.

166 KK R14  
167 RS 1 FLOW -1  
168 RK 219 .0091 .013 CIRC 3

\* The peak flow from S13 will be the design flow for the inlets into the  
\* Cinnabar Avenue lateral at the dip section.

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

169 KK S13  
170 KO 0 0 0.0 0 22  
171 BA 0.0085  
172 LG 0.25 0.21 6.4 0.188 35.0  
\* 10 Year Clark Unit Hydrograph Parameters  
173 UC .117 .107

\* C13 combines runoff from subbasin S13 and Route R14. The flow at  
\* C13 will be the design flow for the lateral pipe along Cinnabar  
\* between the 7th Avenue and the dip section at approximately the  
\* 8th Avenue alignment.

174 KK C13  
175 HC 2  
\*  
\* Route R13 routes runoff from the dip section on Cinnabar  
\* Avenue along Cinnabar Avenue through the proposed lateral to 9th Avenue.

176 KK R13  
177 RS 1 FLOW -1  
178 RK 390 .0103 0.013 CIRC 4

\* The flow at S12 will be the design flow for the inlets along

\* Cinnabar Avenue between the dip section and 9th Avenue

179 KK S12  
180 KO 0 0 0.0 0 22  
181 BA 0.0018  
182 LG 0.25 0.21 6.4 0.188 35.0  
\* 10 Year Clark Unit Hydrograph Parameters  
183 UC .0096 .160

\* C12\* combines runoff from subbasin S14 and Route R17. The flow at  
\* C12\* will be the design flow for the lateral pipe along Cinnabar  
\* Avenue between the dip section and 9th Avenue.

184 KK C12\*  
185 HC 2  
\*  
\* C12 combines runoff from C12\* and R11

186 KK C12  
187 HC 2  
\*  
\* Route R12 routes runoff from the the intersection of Cinnabar and  
\* 9th Avenues along 9th Avenue to Mountain View.  
\* The route is through the proposed 9th Avenue storm drain.  
HEC-1 INPUT

1  
LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

188 KK R12  
189 RS 1 FLOW -1  
190 RK 613 .0163 .013 CIRC 7

\* The flow at S15 will be the design flow for inlets along 9th  
\* Avenue between Cinnabar Avenue and Mountain View Road.

191 KK S15  
192 KO 0 0 0.0 0 22  
193 BA 0.0068  
194 LG 0.25 0.25 5.305 0.254 35.0  
\* 10 Year Clark Unit Hydrograph Parameters  
195 UC .108 .110

\* CSD4 combines runoff from S15 and R12  
\* The flow will be the design flow for the 9th Avenue Storm  
\* drain between Cinnabar Avenue and Mountain View Road.

196 KK CSD4  
197 HC 2  
\*  
\* Route RSD4  
\* The route is through the proposed 9th Avenue storm drain between  
\* the Mountain View Road and the Purdue Avenue alignment.

198 KK RSD4  
199 RS 1 FLOW -1  
200 RK 478 .0084 .013 CIRC 7

\* The flow at S16 will be the design flows for inlets along  
\* 9th Avenue between Mountain view Road and the Purdue Avenue alignment.

201 KK S16  
202 KO 0 0 0.0 0 22  
203 BA 0.0197  
204 LG 0.25 0.25 4.676 0.316 58.634  
\* 10 Year Clark Unit Hydrograph Parameters  
205 UC .221 .256

\* CSD5 (Storm Drain Reach 5) combines runoff from S16 and R15  
\* The peak flow at CSD6 is the design flow for the 9th Avenue  
\* storm drain pipe between Mountain View Road and the Purdue Avenue alignment.

206 KK CSD5  
207 HC 2  
\*  
\* Route RSD5  
\* The route is through the proposed 9th Avenue storm drain between  
\* the Purdue Avenue alignment and Vogel Avenue.  
HEC-1 INPUT

1  
LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

208 KK RSD5  
209 RS 1 FLOW -1  
210 RK 213 .0188 .013 CIRC 7

\*  
 \*  
 \* The peak flow from S18 is the design flow for inlets into  
 \* the 9th Avenue storm drain between the Purude Avenue alignment and Vogel Avenue

211 KK S18  
 212 KO 0 0 0.0 0 22  
 213 BA 0.0015  
 214 LG 0.25 0.25 3.95 0.4 35.0  
 \* 10 Year Clark Unit Hydrograph Parameters  
 215 UC 0.083 0.128  
 \*

\*  
 \*  
 \* The peak flow from S19 is the design flow for inlets into  
 \* the 9th Avenue storm drain at Vogel Avenue.

216 KK S19  
 217 KO 0 0 0.0 0 22  
 218 BA 0.0046  
 219 LG 0.25 0.25 4.207 0.413 50.106  
 \* 10 Year Clark Unit Hydrograph Parameters  
 220 UC .183 .252  
 \*

\*  
 \* CSD6 (Storm Drain Reach 6) combines runoff from S18, S19 and RSD5  
 \* The peak flow at CSD6 is the design flow for the 9th Avenue  
 \* storm drain pipe between Mountain View Road and Vogel Avenue.

221 KK CSD6  
 222 HC 3  
 \*

\*  
 \*  
 \* Route RSD6  
 \* The route is through the proposed 9th Avenue storm drain between  
 \* Vogel Avenue and Hatcher Road.

223 KK RSD6  
 224 RS 1 FLOW -1  
 225 RK 764 .0105 .013 CIRC 7  
 \*

\*  
 \*  
 \* The peak flow from S20 is the design flow for inlets into  
 \* the 9th Avenue storm drain between Vogel Avenue and Hatcher Road.

226 KK S20  
 227 KO 0 0 0.0 0 22  
 228 BA 0.0050  
 229 LG 0.202 0.25 4.674 0.382 44.563  
 \* 10 Year Clark Unit Hydrograph Parameters  
 230 UC .154 .209  
 \*

\*  
 \*  
 \* CSD7 (Storm Drain Reach 7) combines runoff from S20 and RSD6  
 \* The peak flow at CSD7 is the design flow for the 9th Avenue  
 \* storm drain pipe between Vogel Avenue and Hatcher Road.

1

HEC-1 INPUT

PAGE 11

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

231 KK CSD7  
 232 HC 2  
 \*

\*  
 \*  
 \* Route RSD7  
 \* The route is through the proposed 9th Avenue storm drain between  
 \* Hatcher Road and the ACDC.

233 KK RSD7  
 234 RS 1 FLOW -1  
 235 RK 788 .0102 .013 CIRC 7  
 \*

\*  
 \*  
 \* The peak flow from S21 is the design flow for inlets into  
 \* the 9th Avenue storm drain between Hatcher Road and the ACDC.

236 KK S21  
 237 KO 0 0 0.0 0 22  
 238 BA 0.0067  
 239 LG 0.15 0.25 4.8 0.389 55.0  
 \* 10 Year Clark Unit Hydrograph Parameters  
 240 UC .154 .192  
 \*

\*  
 \*  
 \* CSD8 (Storm Drain Reach 8) combines runoff from S21 and RSD7  
 \* The peak flow at CSD8 is the design flow for the 9th Avenue  
 \* storm drain pipe between Hatcher and the ACDC, and is the  
 \* outflow into the ACDC.

241 KK CSD8  
 242 HC 2  
 \*

1

SCHEMATIC DIAGRAM OF STREAM NETWORK

INPUT LINE	(V) ROUTING	(-->) DIVERSION OR PUMP FLOW
NO.	(.) CONNECTOR	(<---) RETURN OF DIVERTED OR PUMPED FLOW
32	S7	
.	.	
38	S1	
.	V	
.	V	
43	WPD	
.	V	
.	V	
49	R1	
.	.	
54	.	S2
.	.	.
59	C2.....	
.	V	
.	V	
61	R2	
.	.	
64	.	S5
.	.	.
69	CSD1.....	
.	.	
71	.	S4
.	V	
.	V	
76	.	R4
.	.	.
79	.	S6
.	.	.
84	C6.....	
.	V	
.	V	
86	R6	
.	.	
89	.	S8
.	.	.
94	CSD2.....	
.	.	
96	.	S3
.	V	
.	V	
101	.	R3
.	.	.
104	.	S10
.	.	.
109	C10.....	
.	V	
.	V	
111	R10	
.	.	
114	.	S9
.	.	.
119	C9.....	
.	.	
121	C9.....	
.	V	
.	V	
123	R9	
.	.	
126	.	S11
.	.	.
131	CSD3.....	
.	.	
133	.	S17
.	V	
.	V	
138	R17	
.	.	
.	.	

141	.	.	S14a	.
	.	.	V	.
	.	.	V	.
146	.	.	EPD	.
	.	.	V	.
	.	.	V	.
152	.	.	R14a	.
	.	.	.	.
157	.	.	.	S14b
	.	.	.	.
162	.	.	C14b.....	.
	.	.	.	.
164	.	.	C14.....	.
	.	.	V	.
	.	.	V	.
166	.	.	R14	.
	.	.	.	.
169	.	.	.	S13
	.	.	.	.
174	.	.	C13.....	.
	.	.	V	.
	.	.	V	.
176	.	.	R13	.
	.	.	.	.
179	.	.	.	S12
	.	.	.	.
184	.	.	C12*.....	.
	.	.	.	.
186	.	.	C12.....	.
	.	.	V	.
	.	.	V	.
188	.	.	R12	.
	.	.	.	.
191	.	.	.	S15
	.	.	.	.
196	.	.	CSD4.....	.
	.	.	V	.
	.	.	V	.
198	.	.	RSD4	.
	.	.	.	.
201	.	.	.	S16
	.	.	.	.
206	.	.	CSD5.....	.
	.	.	V	.
	.	.	V	.
208	.	.	RSD5	.
	.	.	.	.
211	.	.	.	S18
	.	.	.	.
216	.	.	.	S19
	.	.	.	.
221	.	.	CSD6.....	.
	.	.	V	.
	.	.	V	.
223	.	.	RSD6	.
	.	.	.	.
226	.	.	.	S20
	.	.	.	.
231	.	.	CSD7.....	.
	.	.	V	.
	.	.	V	.
233	.	.	RSD7	.
	.	.	.	.
236	.	.	.	S21
	.	.	.	.
241	.	.	CSD8.....	.

(\*\*\*) RUNOFF ALSO COMPUTED AT THIS LOCATION

RUNOFF SUMMARY  
FLOW IN CUBIC FEET PER SECOND  
TIME IN HOURS, AREA IN SQUARE MILES

OPERATION	STATION	PEAK FLOW	TIME OF PEAK	AVERAGE FLOW FOR MAXIMUM PERIOD			BASIN AREA	MAXIMUM STAGE	TIME OF MAX STAGE
				6-HOUR	24-HOUR	72-HOUR			
+	HYDROGRAPH AT								
+	S7	12.	3.10	1.	0.	0.	.00		
+	HYDROGRAPH AT								
+	S1	520.	3.47	77.	46.	46.	.54		
+	ROUTED TO								
+	WPD	23.	4.95	22.	16.	16.	.54	1322.75	4.97
+	ROUTED TO								
+	R1	23.	4.98	22.	16.	16.	.54	1.15	5.02
+	HYDROGRAPH AT								
+	S2	57.	3.15	5.	3.	3.	.03		
+	2 COMBINED AT								
+	C2	70.	3.15	26.	19.	19.	.57		
+	ROUTED TO								
+	R2	70.	3.17	26.	19.	19.	.57		
+	HYDROGRAPH AT								
+	S5	2.	3.13	0.	0.	0.	.00		
+	2 COMBINED AT								
+	CSD1	72.	3.17	26.	19.	19.	.57		
+	HYDROGRAPH AT								
+	S4	4.	3.10	0.	0.	0.	.00		
+	ROUTED TO								
+	R4	4.	3.10	0.	0.	0.	.00		
+	HYDROGRAPH AT								
+	S6	6.	3.13	1.	0.	0.	.00		
+	3 COMBINED AT								
+	C6	81.	3.15	26.	19.	19.	.57		
+	ROUTED TO								
+	R6	81.	3.17	26.	19.	19.	.57		
+	HYDROGRAPH AT								
+	S8	5.	3.15	0.	0.	0.	.00		
+	2 COMBINED AT								
+	CSD2	86.	3.17	27.	20.	20.	.58		
+	HYDROGRAPH AT								
+	S3	96.	3.28	9.	6.	6.	.09		
+	ROUTED TO								
+	R3	96.	3.28	9.	6.	6.	.09		
+	HYDROGRAPH AT								
+	S10	12.	3.13	1.	1.	1.	.01		
+	2 COMBINED AT								
+	C10	104.	3.28	10.	6.	6.	.09		
+	ROUTED TO								
+	R10	104.	3.28	10.	6.	6.	.09		
+	HYDROGRAPH AT								
+	S9	32.	3.17	3.	2.	2.	.02		
+	2 COMBINED AT								
+	C9*	130.	3.27	13.	8.	8.	.11		
+	2 COMBINED AT								
+	C9	205.	3.22	39.	28.	28.	.69		
+	ROUTED TO								
+	R9	205.	3.22	39.	28.	28.	.69		
+	HYDROGRAPH AT								
+	S11	13.	3.13	1.	1.	1.	.01		
+	2 COMBINED AT								
+	CSD3	216.	3.22	40.	28.	28.	.69		
+	HYDROGRAPH AT								
+	S17	23.	3.15	2.	1.	1.	.01		



## **ATTACHMENTS**

- A. Vicinity Map
- B. Proposed Storm Drain Layout/ Map from CAR
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## Calculation Results Summary

=====  
 Scenario: Base

>>>> Info: Subsurface Network Rooted by: ACDC Outlet  
 >>>> Info: Subsurface Analysis iterations: 1  
 >>>> Info: Convergence was achieved.

>>>> Info: Subsurface Network Rooted by: Manhole 21  
 >>>> Info: Subsurface Analysis iterations: 1  
 >>>> Info: Convergence was achieved.

### CALCULATION SUMMARY FOR SURFACE NETWORKS

Label	Inlet Type	Inlet	Total Intercepted Flow (cfs)	Total Bypassed Flow (cfs)	Capture Efficiency (%)	Gutter Spread (ft)	Gutter Depth (ft)
Manhole 7: Q=380 cfs	Generic Inlet	Generic Default 100%	0.00	0.00	100.0	0.00	0.00
Manhole 11: Q=340 cfs	Generic Inlet	Generic Default 100%	0.00	0.00	100.0	0.00	0.00
Manhole 13: Q=220 cfs	Generic Inlet	Generic Default 100%	0.00	0.00	100.0	0.00	0.00
Manhole 23: Q=130 cfs	Generic Inlet	Generic Default 100%	0.00	0.00	100.0	0.00	0.00
Manhole 26A: Q=120 cfs	Generic Inlet	Generic Default 100%	0.00	0.00	100.0	0.00	0.00
Manhole 18: Q=90 cfs	Generic Inlet	Generic Default 100%	0.00	0.00	100.0	0.00	0.00
Manhole 19A: Q=5 cfs	Generic Inlet	Generic Default 100%	0.00	0.00	100.0	0.00	0.00
Manhole 20: Q=10 cfs	Generic Inlet	Generic Default 100%	0.00	0.00	100.0	0.00	0.00

### CALCULATION SUMMARY FOR SUBSURFACE NETWORK WITH ROOT: ACDC Outlet

Label	Number of Sections	Section Size	Section Shape	Length (ft)	Total System Flow (cfs)	Average Velocity (ft/s)	Hydraulic Grade Upstream (ft)	Hydraulic Grade Downstream (ft)
9th-1	1	72 inch	Circular	22.00	380.00	19.02	1,222.40	1,221.66
9th-2	1	72 inch	Circular	327.00	380.00	19.11	1,226.76	1,223.97
9th-3	1	66 inch	Circular	435.00	380.00	18.33	1,232.78	1,226.54
9th-4	1	66 inch	Circular	86.00	380.00	15.99	1,235.07	1,233.96
9th-5	1	66 inch	Circular	579.00	380.00	15.99	1,243.59	1,236.18
9th-6	1	66 inch	Circular	105.00	380.00	15.99	1,245.14	1,243.79
9th-7	1	66 inch	Circular	411.00	380.00	15.99	1,250.60	1,245.34

### Calculation Results Summary

9th-8	1	66 inch	Circular	261.00	340.00	14.31	1,253.47	1,250.80
9th-8b	1	66 inch	Circular	329.00	340.00	14.31	1,256.90	1,253.52
9th-9	1	66 inch	Circular	173.00	340.00	14.31	1,258.67	1,256.90
9th-9A	1	66 inch	Circular	74.00	340.00	14.31	1,259.59	1,258.83
9th-10	1	66 inch	Circular	37.00	340.00	14.31	1,259.97	1,259.59
9th-11	1	54 inch	Circular	254.00	220.00	13.83	1,266.01	1,262.83
Cinnabar-1	1	54 inch	Circular	418.00	120.00	7.55	1,264.39	1,262.83
9th-12	1	54 inch	Circular	397.00	220.00	19.07	1,271.77	1,266.16
Cinnabar-2	1	54 inch	Circular	246.00	120.00	7.55	1,265.35	1,264.43
Cheryl-1	1	48 inch	Circular	325.00	130.00	10.35	1,277.31	1,274.65
9th-13	1	42 inch	Circular	19.00	95.00	9.87	1,274.82	1,274.65
7th-1	1	48 inch	Circular	176.00	120.00	9.55	1,266.62	1,265.39
Cheryl-2	1	48 inch	Circular	55.00	130.00	10.35	1,277.76	1,277.31
9th-14	1	42 inch	Circular	269.00	95.00	15.32	1,276.99	1,274.90
7th-2	1	48 inch	Circular	123.00	120.00	9.55	1,267.88	1,267.02
Cheryl-3	1	48 inch	Circular	242.00	130.00	19.33	1,280.34	1,277.81
9th-15A	1	42 inch	Circular	52.00	95.00	15.09	1,277.91	1,277.08
9th-15	1	36 inch	Circular	330.00	95.00	14.63	1,284.43	1,278.00
9th-16	1	36 inch	Circular	325.00	95.00	13.44	1,291.10	1,284.43
9th-18	1	36 inch	Circular	113.00	5.00	0.71	1,292.79	1,292.79
9th-17	1	36 inch	Circular	205.00	90.00	12.73	1,296.52	1,292.79
9th-19	1	36 inch	Circular	24.00	5.00	0.71	1,292.79	1,292.79

Label	Total System Flow (cfs)	Ground Elevation (ft)	Hydraulic Grade Line In (ft)	Hydraulic Grade Line Out (ft)
ACDC Outlet	380.00	1,229.00	1,216.87	1,216.87
Manhole 1	380.00	1,230.31	1,223.97	1,222.40
Manhole 2	380.00	1,236.30	1,226.92	1,226.76
Manhole 3	380.00	1,241.21	1,233.96	1,232.78
Manhole 4	380.00	1,242.39	1,236.18	1,235.07
Manhole 5	380.00	1,249.60	1,243.79	1,243.59
Manhole 6	380.00	1,250.56	1,245.34	1,245.14
Manhole 7: Q=380 cfs	380.00	1,256.20	1,250.80	1,250.60
Manhole 8	340.00	1,258.87	1,253.52	1,253.47
Manhole 9	340.00	1,263.46	1,256.90	1,256.90
Manhole 9A	340.00	1,267.16	1,258.83	1,258.67
Manhole 10	340.00	1,266.95	1,259.59	1,259.59
Manhole 11: Q=340 cfs	340.00	1,267.49	1,262.83	1,259.97
Manhole 12	220.00	1,273.01	1,266.16	1,266.01
Manhole 24	120.00	1,270.38	1,264.43	1,264.39
Manhole 13: Q=220 cfs	220.00	1,280.35	1,274.65	1,271.77
Manhole 25	120.00	1,274.00	1,265.39	1,265.35
Manhole 21A	130.00	1,282.93	1,277.31	1,277.31

### Calculation Results Summary

Manhole 14	95.00	1,280.76	1,274.90	1,274.82
Manhole 26	120.00	1,270.79	1,267.02	1,266.62
Manhole 22	130.00	1,281.67	1,277.81	1,277.76
Manhole 15A	95.00	1,286.16	1,277.08	1,276.99
Manhole 26A: Q=120 cfs	120.00	1,269.97	1,267.95	1,267.88
Manhole 23: Q=130 cfs	130.00	1,286.00	1,280.44	1,280.34
Manhole 15	95.00	1,286.81	1,278.00	1,277.91
Manhole 16	95.00	1,291.88	1,284.43	1,284.43
Manhole 17	95.00	1,296.16	1,292.79	1,291.10
Manhole 19	5.00	1,293.96	1,292.79	1,292.79
Manhole 18: Q=90 cfs	90.00	1,299.30	1,296.64	1,296.52
Manhole 19A: Q=5 cfs	5.00	1,293.27	1,292.79	1,292.79

CALCULATION SUMMARY FOR SUBSURFACE NETWORK WITH ROOT: Manhole 21

Label	Number of Sections	Section Size	Section Shape	Length (ft)	Total System Flow (cfs)	Average Velocity (ft/s)	Hydraulic Grade Upstream (ft)	Hydraulic Grade Downstream (ft)
Cochise 1	1	18 inch	Circular	271.00	10.00	5.66	1,279.14	1,276.68

Label	Total System Flow (cfs)	Ground Elevation (ft)	Hydraulic Grade Line In (ft)	Hydraulic Grade Line Out (ft)
Manhole 21	10.00	1,284.65	1,275.18	1,275.18
Manhole 20: Q=10 cfs	10.00	1,283.70	1,279.16	1,279.14

=====  
Completed: 12/16/2005 03:54:48 PM

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HYDROLOGY											HYDRAULICS						
Subbasin ID	Area (Ac)	100-Year Runoff Coefficient	10-Year Runoff Coefficient	Upstream Elevation (ft)	Downstream Elevation (ft)	Flow Length (ft)	Slope %	Surface Type	10-Year Peak Flow (cfs)	Street	CB#	Station of Structure	Proposed Structure Type	Modeled	Cummulative Flow (cfs)	Catch Basin Interception (cfs)	Flow By (cfs)
50	0.75	0.95	0.85	1320.00	1303.19	780.00		Paved Street	4	9th Rt.					4		4.00
51	0.75	0.95	0.85	1320.00	1303.22	780.00		Paved Street	3	9th Rt.					7.00		7.00
52	0.30	0.95	0.85	1303.22	1298.07	250.00	0.02	Paved Street	2	9th Rt.					9.00		9.00
										9th Rt.	EXIST 1	STA. 62+19	Concrete Catch Basin, Type "M-1, L=6-Ft", Phx. Supp. Detail P-1569-1	Grade	9.00	3.29	5.71
84	0.52			1298.07	1293.67	351.00	0.01	Paved Street - School Site	3	9th Rt.					8.31		8.31
59	0.12	0.95	0.85	1298.07	1293.67	351.00	0.01	Paved Street	0.6	9th Rt.					8.91		8.91
										9th Rt.	CB14.1	STA.58+45.00 15.5' RT.	Concrete Catch Basin, Type "G", M.A.G. Detail 537 - Double	Grade	8.91	4.44	4.47
85	0.44			1293.67	1289.37	287.00	0.01	School Site	2	9th Rt.					6.67		6.67
60	1.30	0.92	0.85	1298.50	1280.56	1190.00	0.02	Paved Street	4.2	9th Rt.					10.87		10.87
										9th Rt.	CB13.3	STA.55+63.00 15' RT	Concrete Catch Basin, Type "G", M.A.G. Detail 537 - Double	Grade	10.87	4.04	6.83
										9th Rt.	CB12.2	STA.50+31.60 16.4' RT. B/C	Concrete Catch Basin, Type "M", Phx. Supp. Detail P-1569-1	Grade	6.83	1.03	5.80
68	2.70	0.70	0.56	1282.72	1274.50	530.00	0.02	Single -family & Multi-family	9.0	9th Rt.					14.80		14.80
From Cheryl									0.0	9th Rt.	CB11.5	STA.46+65.00 16.2' RT. B/C	Concrete Catch Basin, Type "M-2, L=17-Ft", Phx. Supp. Detail P-1569-1	Grade	14.80	13.06	1.74
70	1.20	0.95	0.85	1277.00	1267.79	420.00	0.02	Single -family & Multi-family	6	9th Rt.					7.74		7.74
										9th Rt.	CB11.4	STA.44+71.40 16.2' RT. B/C	Concrete Catch Basin, Type "M-2, L=17-Ft", Phx. Supp. Detail P-1569-1	Grade	7.74	7.74	0.00
										9th Rt.	CB11.2	STA.43+75.25 16.2' RT. B/C	Concrete Catch Basin, Type "M", Phx. Supp. Detail P-1569-1	Grade	0.00	0	0.00
73	0.54	0.95	0.85	1272.00	1258.48	890.00	0.02	Paved Street	2	9th Rt.					2.00		2.00
From Cinnabar										9th Rt.					9.30		9.30
74	3.26	0.75	0.60	1272.45	1258.48	680.00	0.02	Single -family & Multi-family	11	9th Rt.					20.30		20.30
										9th Rt.	CB10.2	STA.41+27.00 16.3' RT. B/C	Concrete Catch Basin, Type "M", Phx. Supp. Detail P-1569-1	Grade	20.30	1.7	18.60
										9th Rt.	CB9.2	STA.37+98.00 16.3' RT. B/C	Concrete Catch Basin, Type "M-1, L=10-Ft", Phx. Supp. Detail P-1569-1	Grade	18.60	6.58	12.02
S16 (Partial)	11.70	n/a	n/a	n/a	n/a	n/a	n/a	n/a	25	9th Rt.					37.02		37.02
77	0.30	0.95	0.85	1258.83	1251.87	510.00	0.01	Paved Street	1	9th Rt.					38.02		38.02
										9th Rt.	CB8.5	STA.32+54.03 16.1' RT. B/C	Concrete Catch Basin, Type "M-1, L=10-Ft", Phx. Supp. Detail P-1569-1	Grade	38.02	10.99	27.03
79	0.32	0.95	0.85	1260.00	1250.03	560.00	0.02	Pavement, Driveways, Rock Yards	1	9th Rt.					28.03		28.03
S18	3.10	n/a	n/a	n/a	n/a	n/a	n/a	n/a	3	9th Rt.					31.03		31.03
										9th Rt.	CB8.4	STA.31+25.43 16.1' RT. B/C	Concrete Catch Basin, Type "M-1, L=17-Ft", Phx. Supp. Detail P-1569-1	Grade	31.03	12.56	18.47
80	2.20	0.95	0.85	1260.00	1242.61	1160.00	0.01	Paved Street	9	9th Rt.					27.47		27.47
										9th Rt.	CB8.2	STA.30+21.00 16.1' RT. B/C	Concrete Catch Basin, Type "N, Single", Phx. Supp. Detail P-1570	Grade	27.47	8.20	19.27
										9th Rt.	CB7.1	STA.24+70.88 16.3' RT. B/C	Concrete Catch Basin, Type "M-2, L=17-Ft", Phx. Supp. Detail P-1569-1	Grade	19.27	17.17	2.10
83	0.71	0.95	0.85	1241.35	1238.31	260.00	0.01	Paved Street	4	9th Rt.					6.10		6.10
										9th Rt.	CB5.1	STA.21+36.28 19.7' RT. B/C	Concrete Catch Basin, Type "M-1, L=6-Ft", Phx. Supp. Detail P-1569-1	Grade	6.10	3.10	3.00

65	1.10	0.95	0.85	1296.20	1285.70	550.00	0.02	Pavement, Driveways, Rock Yards	5	Cheryl					5.00		5.00
66	0.10	0.95	0.85	1286.68	1285.12	75.00	0.02	Paved Street	1	Cheryl					6.00		6.00
										Cheryl	CB18.2	STA.22+77.00 18.4' RT. B/C	Concrete Catch Basin, Type "N, Single", Phx. Supp. Detail P-1570	Grade	6.00	3.32	2.68
										Cheryl	CB18.1	STA.22+50.00 18.5' LT. B/C	Concrete Catch Basin, Type "M-1, L=3-Ft", Phx. Supp. Detail P-1569-1	Grade	2.68	1.21	1.47
64	4.16	0.75	0.60	1296.50	1281.42	216.00	0.07	Pavement, Driveways, Rock Yards	15	Cheryl					16.47		16.47
										Cheryl	CB17.4	STA.20+35.00 17.7' RT.	ABT Inc. TF-14 Heavy Duty Grated Trench Drain w/1901 Catch Basin, Per Special Provisions (Or Approved Equivalent)	Grade	16.47	9.35	7.12
										Cheryl	CB17.2	STA.19+43.90 18.5' LT. B/C	Concrete Catch Basin, Type "M", Phx. Supp. Detail P-1569-1	Grade	7.12	0.96	6.16
										Cheryl	CB17.3	STA.19+77.82 86.3' RT.	Concrete Catch Basin, Type "G", M.A.G. Detail 537 - Double	Sag / Sump	6.16	6.16	0.00
67	0.25	0.95	0.85	1285.94	1280.70	160.00	0.03	Paved Street	2	Cheryl					2.00		2.00
										Cheryl	CB17.1	STA.17+16.90 18.5' LT. B/C	Concrete Catch Basin, Type "M-2, L=10-Ft", Phx. Supp. Detail P-1569-1	Grade	2.00	2.00	0.00

C14b	92.48	n/a	85	7th					85.00		85.00						
										7th	CB21.6	STA.105+62.40 23.2' RT.	Concrete Catch Basin, Type "G", M.A.G. Detail 537 - Double	Ditch	85.00	25.07	59.93
										7th	CB21.5	STA.104+00.00 21.9' RT.	Concrete Catch Basin, Type "G", M.A.G. Detail 537 - Double	Grade	59.93	11.64	48.29
										7th	CB21.4	STA.102+77.09 80.3' RT.	Concrete Catch Basin, Type "G", M.A.G. Detail 537 - Double	Sag / Sump	48.29	12.00	36.29
										7th	CB21.3	STA.102+68.68 91.5' RT.	Concrete Catch Basin, Type "G", M.A.G. Detail 537 - Double	Sag / Sump	36.29	12.00	24.29
										7th	CB21.2	STA.102+61.91 103.8' RT.	Concrete Catch Basin, Type "G", M.A.G. Detail 537 - Double	Sag / Sump	24.29	12.00	12.29
										7th	CB21.1	STA.102+55.85 116.4' RT.	Concrete Catch Basin, Type "G", M.A.G. Detail 537 - Double	Sag / Sump	12.29	12.29	0.00

71	5.50	0.75	0.60	1285.25	1270.65	710.00	0.02	Single -family & Multi-family	19	Cinnabar					19.00		19.00
72	0.25	0.95	0.85	1273.75	1270.00	250.00	0.02	Paved Street	2	Cinnabar					21.00		21.00
										Cinnabar	CB20.1	STA.20+74.00 16.4' RT. B/C	Concrete Catch Basin, Type "G", M.A.G. Detail 537 - Double	Grade	21.00	6.17	14.83
										Cinnabar	CB19.1	STA.17+50.00 18.3' RT. B/C	Concrete Catch Basin, Type "N, Triple", Phx. Supp. Detail P-1570	Grade	14.83	7.53	7.30

53	0.33	0.95	0.85	1302.77	1298.10	170.00	0.03	Paved Street	2	9th Lt.					2.00		2.00
										9th Lt.	EXIST 2	STA. 62+19	Concrete Catch Basin, Type "N, Triple", Phx. Supp. Detail P-1570	Grade	2.00	1.72	0.28
54	0.11	0.95	0.85	1298.10	1293.71	230.00	0.02	Pavement	1	9th Lt.					1.28		1.28
55	0.10	0.95	0.85	1296.46	1292.36	142.00	0.03	Paved Street	1	North					2.28		2.28
										North	CB15.1	STA.16+26.25 18.5' RT. B/C	Concrete Catch Basin, Type "M", Phx. Supp. Detail P-1569-1	Grade	2.28	0.58	1.70
										North	CB15.2	STA.15+25.92 20.3' RT.	Concrete Catch Basin, Type "G", M.A.G. Detail 537 - Double	Sag / Sump	1.70	1.7	0.00

58	0.34	0.95	0.85	1295.34	1291.65	266.00	0.01	Pavement, Driveways, Rock Yards	2	9th Lt.					2.00		2.00
										9th Lt.	CB13.5	STA.57+73.00 16.4' LT. B/C	Concrete Catch Basin, Type "N, Triple", Phx. Supp. Detail P-1570	Grade	2.00	1.66	0.34
										9th Lt.	CB13.4	STA.57+47.10 37.5' LT. B/C	Concrete Catch Basin, Type "N, Single", Phx. Supp. Detail P-1570	Grade	0.34	0.34	0.00
57	2.40	0.75	0.60	1292.36	1283.44	360.00	0.02	Single -family & Multi-family	8	Cochise					8.00		8.00
56	0.20	0.95	0.95	1291.65	1283.44	332.00	0.02	Paved Street	1	Cochise					9.00		9.00
62	0.20	0.95	0.95	1291.22	1283.22	352.00	0.02	Paved Street	1	Cochise					10.00		10.00
										Cochise	CB16.1	STA.13+12.00 18' RT.	Concrete Catch Basin, Type "G", M.A.G. Detail 537 - Double	Grade	10.00	3.83	6.17
										Cochise	CB16.2	STA.10+40.80 15.2' LT. B/C	Concrete Catch Basin, Type "N, Single", Phx. Supp. Detail P-1570	Grade	6.17	3.37	2.80

61	0.50	0.95	0.85	1291.22	1287.11	270.00	0.02	Pavement, Driveways, Rock Yards	3	9th Lt.					3.00		3.00
										9th Lt.	CB13.2	STA.54+43.00 16.4' LT. B/C	Concrete Catch Basin, Type "N, Triple", Phx. Supp. Detail P-1570	Grade	3.00	2.32	0.68
										9th Lt.	CB13.1	STA.54+15.94 37.5' LT. B/C	Concrete Catch Basin, Type "N, Single", Phx. Supp. Detail P-1570	Grade	0.68	0.66	0.02
63	0.60	0.95	0.85	1286.23	1280.50	270.00	0.02	Pavement, Driveways, Rock Yards	3	9th Lt.					3.02		3.02
										9th Lt.	CB12.3	STA.51+19.00 16.5' LT. B/C	Concrete Catch Basin, Type "N, Triple", Phx. Supp. Detail P-1570	Grade	3.02	2.34	0.68
										9th Lt.	CB12.1	STA.50+21.60 16.3' LT. B/C	Concrete Catch Basin, Type "M", Phx. Supp. Detail P-1569-1	Grade	0.68	0.35	0.33
69	1.10	0.95	0.85	1279.58	1267.50	630.00	0.02	Pavement, Driveways, Rock Yards	5	9th Lt.					5.33		5.33
										9th Lt.	CB11.3	STA.44+54.10 16.3' LT. B/C	Concrete Catch Basin, Type "M-1, L=17-Ft", Phx. Supp. Detail P-1569-1	Grade	5.33	4.6	0.73
										9th Lt.	CB11.1	STA.43+75.25 16.3' LT. B/C	Concrete Catch Basin, Type "M", Phx. Supp. Detail P-1569-1	Grade	0.73	0.36	0.37
75	0.37	0.95	0.85	1267.03	1263.40	300.00	0.01	Pavement, Driveways, Rock Yards	2	9th Lt.					2.37		2.37
										9th Lt.	CB10.3	STA.41+27.00 16.9' LT. B/C	Concrete Catch Basin, Type "M-1, L=10-Ft", Phx. Supp. Detail P-1569-1	Grade	2.37	2.24	0.13
										9th Lt.	CB10.1	STA.40+43.80 16.9' LT. B/C	Concrete Catch Basin, Type "M", Phx. Supp. Detail P-1569-1	Grade	0.13	0.13	0.00
76	0.23	0.95	0.85	1263.12	1258.06	300.00	0.02	Pavement, Driveways, Rock Yards	1	9th Lt.					1.00		1.00
										9th Lt.	CB9.1	STA.37+98.00 16.5' LT. B/C	Concrete Catch Basin, Type "M-1, L=10-Ft", Phx. Supp. Detail P-1569-1	Grade	1.00	1	0.00
78	1.00	0.95	0.85	1258.13	1250.11	660.00	0.01	Pavement, Driveways, Rock Yards	4	9th Lt.					4.00		4.00
										9th Lt.	CB8.3	STA.31+25.43 16.6' LT. B/C	Concrete Catch Basin, Type "M-1, L=17-Ft", Phx. Supp. Detail P-1569-1	Grade	4.00	3.96	0.04
										9th Lt.	CB8.1	STA.30+21.00 16.6' LT. B/C	Concrete Catch Basin, Type "N, Single", Phx. Supp. Detail P-1570	Grade	0.04	0.04	0.00
81	1.00	0.95	0.85	1249.58	1242.80	580.00	0.01	Pavement, Driveways, Rock Yards	5	9th Lt.					5.00		5.00
										9th Lt.	CB7.3	STA.26+00.00 17.2' LT. B/C	Concrete Catch Basin, Type "N, Triple", Phx. Supp. Detail P-1570	Grade	5.00	3.45	1.55
										9th Lt.	CB7.2	STA.25+00.00 16.4' LT. B/C	Concrete Catch Basin, Type "N, Triple", Phx. Supp. Detail P-1570	Grade	1.55	1.34	0.21
82	0.71	0.95	0.85	1241.36	1238.31	250.00	0.01	Paved Street	4	9th Lt.					4.21		4.21
										9th Lt.	CB5.2	STA.21+46.36 20.1' LT. B/C	Concrete Catch Basin, Type "M-1, L=6-Ft", Phx. Supp. Detail P-1569-1	Grade	4.21	2.54	1.67

## Worksheet for EXIST 1

### Project Description

Flow Element: Curb Inlet On Grade  
Solve For: Efficiency

### Input Data

Discharge:	9.00	ft <sup>3</sup> /s
Slope:	0.02000	ft/ft
Gutter Width:	1.50	ft
Gutter Cross Slope:	0.04	ft/ft
Road Cross Slope:	0.02	ft/ft
Manning Coefficient:	0.015	
Curb Opening Length:	7.20	ft
Local Depression:	2.00	in
Local Depression Width:	1.50	ft

### Results

Efficiency:	36.54	%
Intercepted Flow:	3.29	ft <sup>3</sup> /s
Bypass Flow:	5.71	ft <sup>3</sup> /s
Spread:	13.96	ft
Depth:	0.31	ft
Flow Area:	1.97	ft <sup>2</sup>
Gutter Depression:	0.03	ft
Total Depression:	0.20	ft
Velocity:	4.56	ft/s
Equivalent Cross Slope:	0.05735	ft/ft
Length Factor:	0.22	
Total Interception Length:	32.25	ft

## Worksheet for CB14.1

### Project Description

Flow Element: Grate Inlet On Grade  
Solve For: Efficiency

### Input Data

Discharge:	8.91	ft <sup>3</sup> /s
Slope:	0.01000	ft/ft
Gutter Width:	2.00	ft
Gutter Cross Slope:	0.04	ft/ft
Road Cross Slope:	0.02	ft/ft
Manning Coefficient:	0.015	
Grate Width:	2.00	ft
Grate Length:	4.00	ft
Grate Type:	P-50 mm (P-1-7/8")	
Clogging:	50.00	%

### Options

Grate Flow Option: ExcludeNone

### Results

Efficiency:	37.21	%
Intercepted Flow:	3.32	ft <sup>3</sup> /s
Bypass Flow:	5.59	ft <sup>3</sup> /s
Spread:	15.77	ft
Depth:	0.36	ft
Flow Area:	2.53	ft <sup>2</sup>
Gutter Depression:	0.04	ft
Total Depression:	0.04	ft
Velocity:	3.52	ft/s
Splash Over Velocity:	8.13	ft/s
Frontal Flow Factor:	1.00	
Side Flow Factor:	0.06	
Grate Flow Ratio:	0.33	
Active Grate Length:	2.00	ft

## Worksheet for CB13.3

### Project Description

Flow Element: Grate Inlet On Grade  
Solve For: Efficiency

### Input Data

Discharge:	10.87	ft <sup>3</sup> /s
Slope:	0.02000	ft/ft
Gutter Width:	2.00	ft
Gutter Cross Slope:	0.04	ft/ft
Road Cross Slope:	0.02	ft/ft
Manning Coefficient:	0.015	
Grate Width:	2.00	ft
Grate Length:	4.00	ft
Grate Type:	P-50 mm (P-1-7/8")	
Clogging:	50.00	%

### Options

Grate Flow Option: ExcludeNone

### Results

Efficiency:	37.19	%
Intercepted Flow:	4.04	ft <sup>3</sup> /s
Bypass Flow:	6.83	ft <sup>3</sup> /s
Spread:	14.90	ft
Depth:	0.34	ft
Flow Area:	2.26	ft <sup>2</sup>
Gutter Depression:	0.04	ft
Total Depression:	0.04	ft
Velocity:	4.80	ft/s
Splash Over Velocity:	8.13	ft/s
Frontal Flow Factor:	1.00	
Side Flow Factor:	0.04	
Grate Flow Ratio:	0.35	
Active Grate Length:	2.00	ft

## Worksheet for CB12.2

### Project Description

Flow Element: Curb Inlet On Grade  
Solve For: Efficiency

### Input Data

Discharge:	6.83	ft <sup>3</sup> /s
Slope:	0.02000	ft/ft
Gutter Width:	1.50	ft
Gutter Cross Slope:	0.04	ft/ft
Road Cross Slope:	0.02	ft/ft
Manning Coefficient:	0.015	
Curb Opening Length:	2.40	ft
Local Depression:	2.00	in
Local Depression Width:	1.50	ft

### Results

Efficiency:	15.11	%
Intercepted Flow:	1.03	ft <sup>3</sup> /s
Bypass Flow:	5.80	ft <sup>3</sup> /s
Spread:	12.56	ft
Depth:	0.28	ft
Flow Area:	1.60	ft <sup>2</sup>
Gutter Depression:	0.03	ft
Total Depression:	0.20	ft
Velocity:	4.26	ft/s
Equivalent Cross Slope:	0.06130	ft/ft
Length Factor:	0.09	
Total Interception Length:	27.59	ft

## Worksheet for CB11.5

### Project Description

Flow Element: Curb Inlet On Grade  
Solve For: Efficiency

### Input Data

Discharge:	14.80	ft <sup>3</sup> /s
Slope:	0.02000	ft/ft
Gutter Width:	1.50	ft
Gutter Cross Slope:	0.04	ft/ft
Road Cross Slope:	0.02	ft/ft
Manning Coefficient:	0.015	
Curb Opening Length:	29.60	ft
Local Depression:	2.00	in
Local Depression Width:	1.50	ft

### Results

Efficiency:	88.21	%
Intercepted Flow:	13.06	ft <sup>3</sup> /s
Bypass Flow:	1.74	ft <sup>3</sup> /s
Spread:	16.87	ft
Depth:	0.37	ft
Flow Area:	2.87	ft <sup>2</sup>
Gutter Depression:	0.03	ft
Total Depression:	0.20	ft
Velocity:	5.15	ft/s
Equivalent Cross Slope:	0.05110	ft/ft
Length Factor:	0.70	
Total Interception Length:	42.58	ft

## Worksheet for CB11.4

### Project Description

Flow Element: Curb Inlet On Grade  
Solve For: Efficiency

### Input Data

Discharge:	7.74	ft <sup>3</sup> /s
Slope:	0.02000	ft/ft
Gutter Width:	1.50	ft
Gutter Cross Slope:	0.04	ft/ft
Road Cross Slope:	0.02	ft/ft
Manning Coefficient:	0.015	
Curb Opening Length:	29.60	ft
Local Depression:	2.00	in
Local Depression Width:	1.50	ft

### Results

Efficiency:	99.98	%
Intercepted Flow:	7.74	ft <sup>3</sup> /s
Bypass Flow:	0.00	ft <sup>3</sup> /s
Spread:	13.19	ft
Depth:	0.29	ft
Flow Area:	1.76	ft <sup>2</sup>
Gutter Depression:	0.03	ft
Total Depression:	0.20	ft
Velocity:	4.39	ft/s
Equivalent Cross Slope:	0.05874	ft/ft
Length Factor:	0.99	
Total Interception Length:	29.83	ft

## Worksheet for CB11.2

### Project Description

Flow Element: Curb Inlet On Grade  
Solve For: Efficiency

### Input Data

Discharge:	0.01	ft <sup>3</sup> /s
Slope:	0.02000	ft/ft
Gutter Width:	1.50	ft
Gutter Cross Slope:	0.04	ft/ft
Road Cross Slope:	0.02	ft/ft
Manning Coefficient:	0.015	
Curb Opening Length:	2.40	ft
Local Depression:	2.00	in
Local Depression Width:	1.50	ft

### Results

Efficiency:	100.00	%
Intercepted Flow:	0.01	ft <sup>3</sup> /s
Bypass Flow:	0.00	ft <sup>3</sup> /s
Spread:	0.70	ft
Depth:	0.03	ft
Flow Area:	0.01	ft <sup>2</sup>
Gutter Depression:	0.03	ft
Total Depression:	0.20	ft
Velocity:	0.99	ft/s
Equivalent Cross Slope:	0.15271	ft/ft
Length Factor:	2.33	
Total Interception Length:	1.03	ft

## Worksheet for CB10.2

### Project Description

Flow Element: Curb Inlet On Grade

Solve For: Efficiency

### Input Data

Discharge:	20.30	ft <sup>3</sup> /s
Slope:	0.02000	ft/ft
Gutter Width:	1.50	ft
Gutter Cross Slope:	0.04	ft/ft
Road Cross Slope:	0.02	ft/ft
Manning Coefficient:	0.015	
Curb Opening Length:	2.40	ft
Local Depression:	2.00	in
Local Depression Width:	1.50	ft

### Results

Efficiency:	8.36	%
Intercepted Flow:	1.70	ft <sup>3</sup> /s
Bypass Flow:	18.60	ft <sup>3</sup> /s
Spread:	19.02	ft
Depth:	0.41	ft
Flow Area:	3.64	ft <sup>2</sup>
Gutter Depression:	0.03	ft
Total Depression:	0.20	ft
Velocity:	5.57	ft/s
Equivalent Cross Slope:	0.04767	ft/ft
Length Factor:	0.05	
Total Interception Length:	50.70	ft

## Worksheet for CB9.2

### Project Description

Flow Element: Curb Inlet On Grade  
Solve For: Efficiency

### Input Data

Discharge:	18.60	ft <sup>3</sup> /s
Slope:	0.02000	ft/ft
Gutter Width:	1.50	ft
Gutter Cross Slope:	0.04	ft/ft
Road Cross Slope:	0.02	ft/ft
Manning Coefficient:	0.015	
Curb Opening Length:	10.40	ft
Local Depression:	2.00	in
Local Depression Width:	1.50	ft

### Results

Efficiency:	35.36	%
Intercepted Flow:	6.58	ft <sup>3</sup> /s
Bypass Flow:	12.02	ft <sup>3</sup> /s
Spread:	18.40	ft
Depth:	0.40	ft
Flow Area:	3.41	ft <sup>2</sup>
Gutter Depression:	0.03	ft
Total Depression:	0.20	ft
Velocity:	5.45	ft/s
Equivalent Cross Slope:	0.04858	ft/ft
Length Factor:	0.22	
Total Interception Length:	48.32	ft

## Worksheet for CB8.5

### Project Description

Flow Element: Curb Inlet On Grade  
Solve For: Efficiency

### Input Data

Discharge:	38.02	ft <sup>3</sup> /s
Slope:	0.01000	ft/ft
Gutter Width:	1.50	ft
Gutter Cross Slope:	0.04	ft/ft
Road Cross Slope:	0.02	ft/ft
Manning Coefficient:	0.015	
Curb Opening Length:	10.40	ft
Local Depression:	2.00	in
Local Depression Width:	1.50	ft

### Results

Efficiency:	28.91	%
Intercepted Flow:	10.99	ft <sup>3</sup> /s
Bypass Flow:	27.03	ft <sup>3</sup> /s
Spread:	27.48	ft
Depth:	0.58	ft
Flow Area:	7.57	ft <sup>2</sup>
Gutter Depression:	0.03	ft
Total Depression:	0.20	ft
Velocity:	5.02	ft/s
Equivalent Cross Slope:	0.03926	ft/ft
Length Factor:	0.17	
Total Interception Length:	60.22	ft

## Worksheet for CB8.4

### Project Description

Flow Element: Curb Inlet On Grade  
Solve For: Efficiency

### Input Data

Discharge:	31.03	ft <sup>3</sup> /s
Slope:	0.02000	ft/ft
Gutter Width:	1.50	ft
Gutter Cross Slope:	0.04	ft/ft
Road Cross Slope:	0.02	ft/ft
Manning Coefficient:	0.015	
Curb Opening Length:	16.00	ft
Local Depression:	2.00	in
Local Depression Width:	1.50	ft

### Results

Efficiency:	40.48	%
Intercepted Flow:	12.56	ft <sup>3</sup> /s
Bypass Flow:	18.47	ft <sup>3</sup> /s
Spread:	22.33	ft
Depth:	0.48	ft
Flow Area:	5.01	ft <sup>2</sup>
Gutter Depression:	0.03	ft
Total Depression:	0.20	ft
Velocity:	6.19	ft/s
Equivalent Cross Slope:	0.04364	ft/ft
Length Factor:	0.25	
Total Interception Length:	63.89	ft

## Worksheet for CB8.2

### Project Description

Flow Element: Grate Inlet On Grade  
Solve For: Efficiency

### Input Data

Discharge:	27.47	ft <sup>3</sup> /s
Slope:	0.01000	ft/ft
Gutter Width:	1.50	ft
Gutter Cross Slope:	0.04	ft/ft
Road Cross Slope:	0.02	ft/ft
Manning Coefficient:	0.015	
Grate Width:	2.00	ft
Grate Length:	3.00	ft
Grate Type:	P-50 mm (P-1-7/8")	
Clogging:	50.00	%

### Options

Grate Flow Option: ExcludeNone

### Results

Efficiency:	29.87	%
Intercepted Flow:	8.20	ft <sup>3</sup> /s
Bypass Flow:	19.27	ft <sup>3</sup> /s
Spread:	24.31	ft
Depth:	0.52	ft
Flow Area:	5.93	ft <sup>2</sup>
Gutter Depression:	0.03	ft
Total Depression:	0.03	ft
Velocity:	4.63	ft/s
Splash Over Velocity:	6.99	ft/s
Frontal Flow Factor:	1.00	
Side Flow Factor:	0.02	
Grate Flow Ratio:	0.28	
Active Grate Length:	1.50	ft

## Worksheet for CB7.1

### Project Description

Flow Element: Curb Inlet On Grade  
Solve For: Efficiency

### Input Data

Discharge:	19.27	ft <sup>3</sup> /s
Slope:	0.01000	ft/ft
Gutter Width:	1.50	ft
Gutter Cross Slope:	0.04	ft/ft
Road Cross Slope:	0.02	ft/ft
Manning Coefficient:	0.015	
Curb Opening Length:	29.60	ft
Local Depression:	2.00	in
Local Depression Width:	1.50	ft

### Results

Efficiency:	89.09	%
Intercepted Flow:	17.17	ft <sup>3</sup> /s
Bypass Flow:	2.10	ft <sup>3</sup> /s
Spread:	21.27	ft
Depth:	0.46	ft
Flow Area:	4.55	ft <sup>2</sup>
Gutter Depression:	0.03	ft
Total Depression:	0.20	ft
Velocity:	4.24	ft/s
Equivalent Cross Slope:	0.04481	ft/ft
Length Factor:	0.71	
Total Interception Length:	41.81	ft

## Worksheet for CB5.1

### Project Description

Flow Element: Curb Inlet On Grade  
Solve For: Efficiency

### Input Data

Discharge:	6.10	ft <sup>3</sup> /s
Slope:	0.01000	ft/ft
Gutter Width:	1.50	ft
Gutter Cross Slope:	0.04	ft/ft
Road Cross Slope:	0.02	ft/ft
Manning Coefficient:	0.015	
Curb Opening Length:	7.20	ft
Local Depression:	2.00	in
Local Depression Width:	1.50	ft

### Results

Efficiency:	50.80	%
Intercepted Flow:	3.10	ft <sup>3</sup> /s
Bypass Flow:	3.00	ft <sup>3</sup> /s
Spread:	13.74	ft
Depth:	0.31	ft
Flow Area:	1.91	ft <sup>2</sup>
Gutter Depression:	0.03	ft
Total Depression:	0.20	ft
Velocity:	3.19	ft/s
Equivalent Cross Slope:	0.05793	ft/ft
Length Factor:	0.33	
Total Interception Length:	22.11	ft

## Worksheet for CB18.2

### Project Description

Flow Element: Grate Inlet On Grade  
Solve For: Efficiency

### Input Data

Discharge:	6.00	ft <sup>3</sup> /s
Slope:	0.02000	ft/ft
Gutter Width:	1.50	ft
Gutter Cross Slope:	0.04	ft/ft
Road Cross Slope:	0.02	ft/ft
Manning Coefficient:	0.015	
Grate Width:	2.00	ft
Grate Length:	3.00	ft
Grate Type:	P-50 mm (P-1-7/8")	
Clogging:	50.00	%

### Options

Grate Flow Option: ExcludeNone

### Results

Efficiency:	55.41	%
Intercepted Flow:	3.32	ft <sup>3</sup> /s
Bypass Flow:	2.68	ft <sup>3</sup> /s
Spread:	11.95	ft
Depth:	0.27	ft
Flow Area:	1.45	ft <sup>2</sup>
Gutter Depression:	0.03	ft
Total Depression:	0.03	ft
Velocity:	4.13	ft/s
Splash Over Velocity:	6.99	ft/s
Frontal Flow Factor:	1.00	
Side Flow Factor:	0.03	
Grate Flow Ratio:	0.54	
Active Grate Length:	1.50	ft

## Worksheet for CB18.1

### Project Description

Flow Element: Curb Inlet On Grade  
Solve For: Efficiency

### Input Data

Discharge:	2.68	ft <sup>3</sup> /s
Slope:	0.02000	ft/ft
Gutter Width:	1.50	ft
Gutter Cross Slope:	0.04	ft/ft
Road Cross Slope:	0.02	ft/ft
Manning Coefficient:	0.015	
Curb Opening Length:	4.60	ft
Local Depression:	2.00	in
Local Depression Width:	1.50	ft

### Results

Efficiency:	45.30	%
Intercepted Flow:	1.21	ft <sup>3</sup> /s
Bypass Flow:	1.47	ft <sup>3</sup> /s
Spread:	8.73	ft
Depth:	0.21	ft
Flow Area:	0.79	ft <sup>2</sup>
Gutter Depression:	0.03	ft
Total Depression:	0.20	ft
Velocity:	3.41	ft/s
Equivalent Cross Slope:	0.07774	ft/ft
Length Factor:	0.28	
Total Interception Length:	16.15	ft

## Worksheet for CB17.4

### Project Description

Flow Element: Grate Inlet On Grade  
Solve For: Efficiency

### Input Data

Discharge:	16.47	ft <sup>3</sup> /s
Slope:	0.05000	ft/ft
Gutter Width:	1.50	ft
Gutter Cross Slope:	0.04	ft/ft
Road Cross Slope:	0.02	ft/ft
Manning Coefficient:	0.015	
Grate Width:	1.00	ft
Grate Length:	16.00	ft
Grate Type:	P-50 mm (P-1-7/8")	
Clogging:	50.00	%

### Options

Grate Flow Option: ExcludeNone

### Results

Efficiency:	56.75	%
Intercepted Flow:	9.35	ft <sup>3</sup> /s
Bypass Flow:	7.12	ft <sup>3</sup> /s
Spread:	14.76	ft
Depth:	0.33	ft
Flow Area:	2.20	ft <sup>2</sup>
Gutter Depression:	0.03	ft
Total Depression:	0.03	ft
Velocity:	7.47	ft/s
Splash Over Velocity:	21.38	ft/s
Frontal Flow Factor:	1.00	
Side Flow Factor:	0.47	
Grate Flow Ratio:	0.18	
Active Grate Length:	8.00	ft

## Worksheet for CB17.2

### Project Description

Flow Element: Curb Inlet On Grade  
Solve For: Efficiency

### Input Data

Discharge:	7.12	ft <sup>3</sup> /s
Slope:	0.03000	ft/ft
Gutter Width:	1.50	ft
Gutter Cross Slope:	0.04	ft/ft
Road Cross Slope:	0.02	ft/ft
Manning Coefficient:	0.015	
Curb Opening Length:	2.40	ft
Local Depression:	2.00	in
Local Depression Width:	1.50	ft

### Results

Efficiency:	13.52	%
Intercepted Flow:	0.96	ft <sup>3</sup> /s
Bypass Flow:	6.16	ft <sup>3</sup> /s
Spread:	11.81	ft
Depth:	0.27	ft
Flow Area:	1.42	ft <sup>2</sup>
Gutter Depression:	0.03	ft
Total Depression:	0.20	ft
Velocity:	5.02	ft/s
Equivalent Cross Slope:	0.06379	ft/ft
Length Factor:	0.08	
Total Interception Length:	30.96	ft

## Worksheet for CB17.3

### Project Description

Flow Element: Grate Inlet In Sag  
Solve For: Spread

### Input Data

Discharge:	6.16	ft <sup>3</sup> /s
Gutter Width:	2.00	ft
Gutter Cross Slope:	0.04	ft/ft
Road Cross Slope:	0.02	ft/ft
Grate Width:	2.00	ft
Grate Length:	4.00	ft
Local Depression:	6.00	in
Local Depression Width:	10.00	ft
Grate Type:	P-50 mm (P-1-7/8")	
Clogging:	50.00	%

### Results

Spread:	6.69	ft
Depth:	0.11	ft
Gutter Depression:	0.04	ft
Total Depression:	0.54	ft
Open Grate Area:	3.60	ft <sup>2</sup>
Active Grate Weir Length:	6.00	ft

## Worksheet for CB17.1

### Project Description

Flow Element: Curb Inlet On Grade

Solve For: Efficiency

### Input Data

Discharge:	2.00	ft <sup>3</sup> /s
Slope:	0.03000	ft/ft
Gutter Width:	1.50	ft
Gutter Cross Slope:	0.04	ft/ft
Road Cross Slope:	0.02	ft/ft
Manning Coefficient:	0.015	
Curb Opening Length:	18.40	ft
Local Depression:	2.00	in
Local Depression Width:	1.50	ft

### Results

Efficiency:	100.00	%
Intercepted Flow:	2.00	ft <sup>3</sup> /s
Bypass Flow:	0.00	ft <sup>3</sup> /s
Spread:	7.17	ft
Depth:	0.18	ft
Flow Area:	0.54	ft <sup>2</sup>
Gutter Depression:	0.03	ft
Total Depression:	0.20	ft
Velocity:	3.72	ft/s
Equivalent Cross Slope:	0.08852	ft/ft
Length Factor:	1.23	
Total Interception Length:	14.92	ft

## Worksheet for CB21.6

### Project Description

Flow Element: Ditch Inlet On Grade  
Solve For: Efficiency

### Input Data

Manning Coefficient:	0.025	
Slope:	0.04000	ft/ft
Left Side Slope:	6.00	ft/ft (H:V)
Right Side Slope:	6.00	ft/ft (H:V)
Bottom Width:	2.00	ft
Discharge:	85.00	ft <sup>3</sup> /s
Grate Width:	2.00	ft
Grate Length:	4.00	ft
Grate Type:	P-50 mm (P-1-7/8")	
Clogging:	50.00	%

### Results

Efficiency:	29.50	%
Intercepted Flow:	25.07	ft <sup>3</sup> /s
Bypass Flow:	59.93	ft <sup>3</sup> /s
Flow Area:	9.78	ft <sup>2</sup>
Wetted Perimeter:	15.63	ft
Top Width:	15.45	ft
Velocity:	8.69	ft/s
Splash Over Velocity:	8.13	ft/s
Frontal Flow Factor:	0.95	
Side Flow Factor:	0.10	
Grate Flow Ratio:	0.23	
Active Grate Length:	2.00	ft
Critical Depth:	1.50	ft
Critical Slope:	0.00987	ft/ft
Froude Number:	1.93	
Flow Type:	Supercritical	
Specific Energy:	2.30	ft
Velocity Head:	1.17	ft
Depth:	1.12	ft

## Worksheet for CB21.5

### Project Description

Flow Element: Grate Inlet On Grade

Solve For: Efficiency

### Input Data

Discharge:	59.93	ft <sup>3</sup> /s
Slope:	0.04000	ft/ft
Gutter Width:	2.00	ft
Gutter Cross Slope:	0.04	ft/ft
Road Cross Slope:	0.02	ft/ft
Manning Coefficient:	0.015	
Grate Width:	2.00	ft
Grate Length:	4.00	ft
Grate Type:	P-50 mm (P-1-7/8")	
Clogging:	50.00	%

### Options

Grate Flow Option: ExcludeNone

### Results

Efficiency:	19.43	%
Intercepted Flow:	11.64	ft <sup>3</sup> /s
Bypass Flow:	48.29	ft <sup>3</sup> /s
Spread:	25.06	ft
Depth:	0.54	ft
Flow Area:	6.32	ft <sup>2</sup>
Gutter Depression:	0.04	ft
Total Depression:	0.04	ft
Velocity:	9.48	ft/s
Splash Over Velocity:	8.13	ft/s
Frontal Flow Factor:	0.88	
Side Flow Factor:	0.01	
Grate Flow Ratio:	0.21	
Active Grate Length:	2.00	ft

## Worksheet for CB21.4 - 21.1

### Project Description

Flow Element: Grate Inlet In Sag  
Solve For: Spread

### Input Data

Discharge:	48.29	ft <sup>3</sup> /s
Gutter Width:	2.00	ft
Gutter Cross Slope:	0.04	ft/ft
Road Cross Slope:	0.02	ft/ft
Grate Width:	2.00	ft
Grate Length:	16.00	ft
Local Depression:	18.00	in
Local Depression Width:	10.00	ft
Grate Type:	P-50 mm (P-1-7/8")	
Clogging:	50.00	%

### Results

Spread:	7.83	ft
Depth:	0.00	ft
Gutter Depression:	0.04	ft
Total Depression:	1.54	ft
Open Grate Area:	14.40	ft <sup>2</sup>
Active Grate Weir Length:	18.00	ft

## Worksheet for CB20.1

### Project Description

Flow Element: Grate Inlet On Grade

Solve For: Efficiency

### Input Data

Discharge:	21.00	ft <sup>3</sup> /s
Slope:	0.02000	ft/ft
Gutter Width:	2.00	ft
Gutter Cross Slope:	0.04	ft/ft
Road Cross Slope:	0.02	ft/ft
Manning Coefficient:	0.015	
Grate Width:	2.00	ft
Grate Length:	4.00	ft
Grate Type:	P-50 mm (P-1-7/8")	
Clogging:	50.00	%

### Options

Grate Flow Option: ExcludeNone

### Results

Efficiency:	29.40	%
Intercepted Flow:	6.17	ft <sup>3</sup> /s
Bypass Flow:	14.83	ft <sup>3</sup> /s
Spread:	19.19	ft
Depth:	0.43	ft
Flow Area:	3.72	ft <sup>2</sup>
Gutter Depression:	0.04	ft
Total Depression:	0.04	ft
Velocity:	5.64	ft/s
Splash Over Velocity:	8.13	ft/s
Frontal Flow Factor:	1.00	
Side Flow Factor:	0.03	
Grate Flow Ratio:	0.27	
Active Grate Length:	2.00	ft

## Worksheet for CB19.1

### Project Description

Flow Element: Grate Inlet On Grade  
Solve For: Efficiency

### Input Data

Discharge:	14.83	ft <sup>3</sup> /s
Slope:	0.02000	ft/ft
Gutter Width:	1.50	ft
Gutter Cross Slope:	0.04	ft/ft
Road Cross Slope:	0.02	ft/ft
Manning Coefficient:	0.015	
Grate Width:	2.00	ft
Grate Length:	9.00	ft
Grate Type:	P-50 mm (P-1-7/8")	
Clogging:	50.00	%

### Options

Grate Flow Option: ExcludeNone

### Results

Efficiency:	50.80	%
Intercepted Flow:	7.53	ft <sup>3</sup> /s
Bypass Flow:	7.30	ft <sup>3</sup> /s
Spread:	16.89	ft
Depth:	0.37	ft
Flow Area:	2.88	ft <sup>2</sup>
Gutter Depression:	0.03	ft
Total Depression:	0.03	ft
Velocity:	5.16	ft/s
Splash Over Velocity:	12.28	ft/s
Frontal Flow Factor:	1.00	
Side Flow Factor:	0.18	
Grate Flow Ratio:	0.40	
Active Grate Length:	4.50	ft

## Worksheet for EXIST 2

### Project Description

Flow Element: Grate Inlet On Grade  
Solve For: Efficiency

### Input Data

Discharge:	2.00	ft <sup>3</sup> /s
Slope:	0.03000	ft/ft
Gutter Width:	1.50	ft
Gutter Cross Slope:	0.04	ft/ft
Road Cross Slope:	0.02	ft/ft
Manning Coefficient:	0.015	
Grate Width:	2.00	ft
Grate Length:	9.00	ft
Grate Type:	P-50 mm (P-1-7/8")	
Clogging:	50.00	%

### Options

Grate Flow Option: ExcludeNone

### Results

Efficiency:	85.84	%
Intercepted Flow:	1.72	ft <sup>3</sup> /s
Bypass Flow:	0.28	ft <sup>3</sup> /s
Spread:	7.17	ft
Depth:	0.18	ft
Flow Area:	0.54	ft <sup>2</sup>
Gutter Depression:	0.03	ft
Total Depression:	0.03	ft
Velocity:	3.72	ft/s
Splash Over Velocity:	12.28	ft/s
Frontal Flow Factor:	1.00	
Side Flow Factor:	0.29	
Grate Flow Ratio:	0.80	
Active Grate Length:	4.50	ft

## Worksheet for CB15.1

### Project Description

Flow Element: Curb Inlet On Grade  
Solve For: Efficiency

### Input Data

Discharge:	2.28	ft <sup>3</sup> /s
Slope:	0.03000	ft/ft
Gutter Width:	1.50	ft
Gutter Cross Slope:	0.04	ft/ft
Road Cross Slope:	0.02	ft/ft
Manning Coefficient:	0.015	
Curb Opening Length:	2.40	ft
Local Depression:	2.00	in
Local Depression Width:	1.50	ft

### Results

Efficiency:	25.22	%
Intercepted Flow:	0.58	ft <sup>3</sup> /s
Bypass Flow:	1.70	ft <sup>3</sup> /s
Spread:	7.56	ft
Depth:	0.18	ft
Flow Area:	0.60	ft <sup>2</sup>
Gutter Depression:	0.03	ft
Total Depression:	0.20	ft
Velocity:	3.83	ft/s
Equivalent Cross Slope:	0.08552	ft/ft
Length Factor:	0.15	
Total Interception Length:	16.10	ft

## Worksheet for CB15.2

### Project Description

Flow Element: Grate Inlet In Sag

Solve For: Spread

### Input Data

Discharge:	1.70	ft <sup>3</sup> /s
Gutter Width:	2.00	ft
Gutter Cross Slope:	0.04	ft/ft
Road Cross Slope:	0.02	ft/ft
Grate Width:	2.00	ft
Grate Length:	4.00	ft
Local Depression:	6.00	in
Local Depression Width:	10.00	ft
Grate Type:	P-50 mm (P-1-7/8")	
Clogging:	50.00	%

### Results

Spread:	5.46	ft
Depth:	0.00	ft
Gutter Depression:	0.04	ft
Total Depression:	0.54	ft
Open Grate Area:	3.60	ft <sup>2</sup>
Active Grate Weir Length:	6.00	ft

## Worksheet for CB13.5

### Project Description

Flow Element: Grate Inlet On Grade  
Solve For: Efficiency

### Input Data

Discharge:	2.00	ft <sup>3</sup> /s
Slope:	0.01000	ft/ft
Gutter Width:	1.50	ft
Gutter Cross Slope:	0.04	ft/ft
Road Cross Slope:	0.02	ft/ft
Manning Coefficient:	0.015	
Grate Width:	2.00	ft
Grate Length:	9.00	ft
Grate Type:	P-50 mm (P-1-7/8")	
Clogging:	50.00	%

### Options

Grate Flow Option: ExcludeNone

### Results

Efficiency:	83.08	%
Intercepted Flow:	1.66	ft <sup>3</sup> /s
Bypass Flow:	0.34	ft <sup>3</sup> /s
Spread:	8.92	ft
Depth:	0.21	ft
Flow Area:	0.82	ft <sup>2</sup>
Gutter Depression:	0.03	ft
Total Depression:	0.03	ft
Velocity:	2.44	ft/s
Splash Over Velocity:	12.28	ft/s
Frontal Flow Factor:	1.00	
Side Flow Factor:	0.46	
Grate Flow Ratio:	0.69	
Active Grate Length:	4.50	ft

## Worksheet for CB13.4

### Project Description

Flow Element: Grate Inlet On Grade  
Solve For: Efficiency

### Input Data

Discharge:	0.34	ft <sup>3</sup> /s
Slope:	0.01000	ft/ft
Gutter Width:	1.50	ft
Gutter Cross Slope:	0.04	ft/ft
Road Cross Slope:	0.02	ft/ft
Manning Coefficient:	0.015	
Grate Width:	2.00	ft
Grate Length:	3.00	ft
Grate Type:	P-50 mm (P-1-7/8")	
Clogging:	50.00	%

### Options

Grate Flow Option: ExcludeNone

### Results

Efficiency:	102.71	%
Intercepted Flow:	0.35	ft <sup>3</sup> /s
Bypass Flow:	-0.01	ft <sup>3</sup> /s
Spread:	4.27	ft
Depth:	0.12	ft
Flow Area:	0.21	ft <sup>2</sup>
Gutter Depression:	0.03	ft
Total Depression:	0.03	ft
Velocity:	1.65	ft/s
Splash Over Velocity:	6.99	ft/s
Frontal Flow Factor:	1.00	
Side Flow Factor:	0.12	
Grate Flow Ratio:	1.03	
Active Grate Length:	1.50	ft

## Worksheet for CB16.1

### Project Description

Flow Element: Grate Inlet On Grade  
Solve For: Efficiency

### Input Data

Discharge:	10.00	ft <sup>3</sup> /s
Slope:	0.02000	ft/ft
Gutter Width:	2.00	ft
Gutter Cross Slope:	0.04	ft/ft
Road Cross Slope:	0.02	ft/ft
Manning Coefficient:	0.015	
Grate Width:	2.00	ft
Grate Length:	4.00	ft
Grate Type:	P-50 mm (P-1-7/8")	
Clogging:	50.00	%

### Options

Grate Flow Option: ExcludeNone

### Results

Efficiency:	38.29	%
Intercepted Flow:	3.83	ft <sup>3</sup> /s
Bypass Flow:	6.17	ft <sup>3</sup> /s
Spread:	14.43	ft
Depth:	0.33	ft
Flow Area:	2.12	ft <sup>2</sup>
Gutter Depression:	0.04	ft
Total Depression:	0.04	ft
Velocity:	4.71	ft/s
Splash Over Velocity:	8.13	ft/s
Frontal Flow Factor:	1.00	
Side Flow Factor:	0.04	
Grate Flow Ratio:	0.36	
Active Grate Length:	2.00	ft

## Worksheet for CB16.2

### Project Description

Flow Element: Grate Inlet On Grade  
Solve For: Efficiency

### Input Data

Discharge:	6.17	ft <sup>3</sup> /s
Slope:	0.02000	ft/ft
Gutter Width:	1.50	ft
Gutter Cross Slope:	0.04	ft/ft
Road Cross Slope:	0.02	ft/ft
Manning Coefficient:	0.015	
Grate Width:	2.00	ft
Grate Length:	3.00	ft
Grate Type:	P-50 mm (P-1-7/8")	
Clogging:	50.00	%

### Options

Grate Flow Option: ExcludeNone

### Results

Efficiency:	54.60	%
Intercepted Flow:	3.37	ft <sup>3</sup> /s
Bypass Flow:	2.80	ft <sup>3</sup> /s
Spread:	12.09	ft
Depth:	0.27	ft
Flow Area:	1.48	ft <sup>2</sup>
Gutter Depression:	0.03	ft
Total Depression:	0.03	ft
Velocity:	4.16	ft/s
Splash Over Velocity:	6.99	ft/s
Frontal Flow Factor:	1.00	
Side Flow Factor:	0.03	
Grate Flow Ratio:	0.53	
Active Grate Length:	1.50	ft

## Worksheet for CB13.2

### Project Description

Flow Element: Grate Inlet On Grade  
Solve For: Efficiency

### Input Data

Discharge:	3.00	ft <sup>3</sup> /s
Slope:	0.02000	ft/ft
Gutter Width:	1.50	ft
Gutter Cross Slope:	0.04	ft/ft
Road Cross Slope:	0.02	ft/ft
Manning Coefficient:	0.015	
Grate Width:	2.00	ft
Grate Length:	9.00	ft
Grate Type:	P-50 mm (P-1-7/8")	
Clogging:	50.00	%

### Options

Grate Flow Option: ExcludeNone

### Results

Efficiency:	77.49	%
Intercepted Flow:	2.32	ft <sup>3</sup> /s
Bypass Flow:	0.68	ft <sup>3</sup> /s
Spread:	9.13	ft
Depth:	0.21	ft
Flow Area:	0.86	ft <sup>2</sup>
Gutter Depression:	0.03	ft
Total Depression:	0.03	ft
Velocity:	3.50	ft/s
Splash Over Velocity:	12.28	ft/s
Frontal Flow Factor:	1.00	
Side Flow Factor:	0.31	
Grate Flow Ratio:	0.67	
Active Grate Length:	4.50	ft

## Worksheet for CB13.1

### Project Description

Flow Element: Grate Inlet On Grade  
Solve For: Efficiency

### Input Data

Discharge:	0.68	ft <sup>3</sup> /s
Slope:	0.02000	ft/ft
Gutter Width:	1.50	ft
Gutter Cross Slope:	0.04	ft/ft
Road Cross Slope:	0.02	ft/ft
Manning Coefficient:	0.015	
Grate Width:	2.00	ft
Grate Length:	3.00	ft
Grate Type:	P-50 mm (P-1-7/8")	
Clogging:	50.00	%

### Options

Grate Flow Option: ExcludeNone

### Results

Efficiency:	97.42	%
Intercepted Flow:	0.66	ft <sup>3</sup> /s
Bypass Flow:	0.02	ft <sup>3</sup> /s
Spread:	5.01	ft
Depth:	0.13	ft
Flow Area:	0.27	ft <sup>2</sup>
Gutter Depression:	0.03	ft
Total Depression:	0.03	ft
Velocity:	2.49	ft/s
Splash Over Velocity:	6.99	ft/s
Frontal Flow Factor:	1.00	
Side Flow Factor:	0.06	
Grate Flow Ratio:	0.97	
Active Grate Length:	1.50	ft

## Worksheet for CB12.3

### Project Description

Flow Element: Grate Inlet On Grade  
Solve For: Efficiency

### Input Data

Discharge:	3.02	ft <sup>3</sup> /s
Slope:	0.02000	ft/ft
Gutter Width:	1.50	ft
Gutter Cross Slope:	0.04	ft/ft
Road Cross Slope:	0.02	ft/ft
Manning Coefficient:	0.015	
Grate Width:	2.00	ft
Grate Length:	9.00	ft
Grate Type:	P-50 mm (P-1-7/8")	
Clogging:	50.00	%

### Options

Grate Flow Option: ExcludeNone

### Results

Efficiency:	77.38	%
Intercepted Flow:	2.34	ft <sup>3</sup> /s
Bypass Flow:	0.68	ft <sup>3</sup> /s
Spread:	9.15	ft
Depth:	0.22	ft
Flow Area:	0.86	ft <sup>2</sup>
Gutter Depression:	0.03	ft
Total Depression:	0.03	ft
Velocity:	3.50	ft/s
Splash Over Velocity:	12.28	ft/s
Frontal Flow Factor:	1.00	
Side Flow Factor:	0.31	
Grate Flow Ratio:	0.67	
Active Grate Length:	4.50	ft

## Worksheet for CB12.1

### Project Description

Flow Element: Curb Inlet On Grade  
Solve For: Efficiency

### Input Data

Discharge:	0.68	ft <sup>3</sup> /s
Slope:	0.02000	ft/ft
Gutter Width:	1.50	ft
Gutter Cross Slope:	0.04	ft/ft
Road Cross Slope:	0.02	ft/ft
Manning Coefficient:	0.015	
Curb Opening Length:	2.40	ft
Local Depression:	2.00	in
Local Depression Width:	1.50	ft

### Results

Efficiency:	50.98	%
Intercepted Flow:	0.35	ft <sup>3</sup> /s
Bypass Flow:	0.33	ft <sup>3</sup> /s
Spread:	4.98	ft
Depth:	0.13	ft
Flow Area:	0.27	ft <sup>2</sup>
Gutter Depression:	0.03	ft
Total Depression:	0.20	ft
Velocity:	2.50	ft/s
Equivalent Cross Slope:	0.11086	ft/ft
Length Factor:	0.33	
Total Interception Length:	7.34	ft

## Worksheet for CB11.3

### Project Description

Flow Element: Curb Inlet On Grade  
Solve For: Efficiency

### Input Data

Discharge:	5.33	ft <sup>3</sup> /s
Slope:	0.02000	ft/ft
Gutter Width:	1.50	ft
Gutter Cross Slope:	0.04	ft/ft
Road Cross Slope:	0.02	ft/ft
Manning Coefficient:	0.015	
Curb Opening Length:	16.00	ft
Local Depression:	2.00	in
Local Depression Width:	1.50	ft

### Results

Efficiency:	86.24	%
Intercepted Flow:	4.60	ft <sup>3</sup> /s
Bypass Flow:	0.73	ft <sup>3</sup> /s
Spread:	11.42	ft
Depth:	0.26	ft
Flow Area:	1.33	ft <sup>2</sup>
Gutter Depression:	0.03	ft
Total Depression:	0.20	ft
Velocity:	4.01	ft/s
Equivalent Cross Slope:	0.06519	ft/ft
Length Factor:	0.67	
Total Interception Length:	23.96	ft

## Worksheet for CB11.1

### Project Description

Flow Element: Curb Inlet On Grade  
Solve For: Efficiency

### Input Data

Discharge:	0.73	ft <sup>3</sup> /s
Slope:	0.02000	ft/ft
Gutter Width:	1.50	ft
Gutter Cross Slope:	0.04	ft/ft
Road Cross Slope:	0.02	ft/ft
Manning Coefficient:	0.015	
Curb Opening Length:	2.40	ft
Local Depression:	2.00	in
Local Depression Width:	1.50	ft

### Results

Efficiency:	49.27	%
Intercepted Flow:	0.36	ft <sup>3</sup> /s
Bypass Flow:	0.37	ft <sup>3</sup> /s
Spread:	5.13	ft
Depth:	0.14	ft
Flow Area:	0.29	ft <sup>2</sup>
Gutter Depression:	0.03	ft
Total Depression:	0.20	ft
Velocity:	2.54	ft/s
Equivalent Cross Slope:	0.10893	ft/ft
Length Factor:	0.31	
Total Interception Length:	7.64	ft

## Worksheet for CB10.3

### Project Description

Flow Element: Curb Inlet On Grade  
Solve For: Efficiency

### Input Data

Discharge:	2.37	ft <sup>3</sup> /s
Slope:	0.01000	ft/ft
Gutter Width:	1.50	ft
Gutter Cross Slope:	0.04	ft/ft
Road Cross Slope:	0.02	ft/ft
Manning Coefficient:	0.015	
Curb Opening Length:	10.40	ft
Local Depression:	2.00	in
Local Depression Width:	1.50	ft

### Results

Efficiency:	94.44	%
Intercepted Flow:	2.24	ft <sup>3</sup> /s
Bypass Flow:	0.13	ft <sup>3</sup> /s
Spread:	9.55	ft
Depth:	0.22	ft
Flow Area:	0.93	ft <sup>2</sup>
Gutter Depression:	0.03	ft
Total Depression:	0.20	ft
Velocity:	2.54	ft/s
Equivalent Cross Slope:	0.07230	ft/ft
Length Factor:	0.80	
Total Interception Length:	13.01	ft

## Worksheet for CB10.1

### Project Description

Flow Element: Curb Inlet On Grade  
Solve For: Efficiency

### Input Data

Discharge:	0.13	ft <sup>3</sup> /s
Slope:	0.01000	ft/ft
Gutter Width:	1.50	ft
Gutter Cross Slope:	0.04	ft/ft
Road Cross Slope:	0.02	ft/ft
Manning Coefficient:	0.015	
Curb Opening Length:	2.40	ft
Local Depression:	2.00	in
Local Depression Width:	1.50	ft

### Results

Efficiency:	99.30	%
Intercepted Flow:	0.13	ft <sup>3</sup> /s
Bypass Flow:	0.00	ft <sup>3</sup> /s
Spread:	2.70	ft
Depth:	0.08	ft
Flow Area:	0.10	ft <sup>2</sup>
Gutter Depression:	0.03	ft
Total Depression:	0.20	ft
Velocity:	1.36	ft/s
Equivalent Cross Slope:	0.14210	ft/ft
Length Factor:	0.94	
Total Interception Length:	2.56	ft

## Worksheet for CB9.1

### Project Description

Flow Element: Curb Inlet On Grade  
Solve For: Efficiency

### Input Data

Discharge:	1.00	ft <sup>3</sup> /s
Slope:	0.02000	ft/ft
Gutter Width:	1.50	ft
Gutter Cross Slope:	0.04	ft/ft
Road Cross Slope:	0.02	ft/ft
Manning Coefficient:	0.015	
Curb Opening Length:	10.40	ft
Local Depression:	2.00	in
Local Depression Width:	1.50	ft

### Results

Efficiency:	100.00	%
Intercepted Flow:	1.00	ft <sup>3</sup> /s
Bypass Flow:	0.00	ft <sup>3</sup> /s
Spread:	5.86	ft
Depth:	0.15	ft
Flow Area:	0.37	ft <sup>2</sup>
Gutter Depression:	0.03	ft
Total Depression:	0.20	ft
Velocity:	2.72	ft/s
Equivalent Cross Slope:	0.10058	ft/ft
Length Factor:	1.14	
Total Interception Length:	9.15	ft

## Worksheet for CB8.3

### Project Description

Flow Element: Curb Inlet On Grade  
Solve For: Efficiency

### Input Data

Discharge:	4.00	ft <sup>3</sup> /s
Slope:	0.01000	ft/ft
Gutter Width:	1.50	ft
Gutter Cross Slope:	0.04	ft/ft
Road Cross Slope:	0.02	ft/ft
Manning Coefficient:	0.015	
Curb Opening Length:	16.00	ft
Local Depression:	2.00	in
Local Depression Width:	1.50	ft

### Results

Efficiency:	98.92	%
Intercepted Flow:	3.96	ft <sup>3</sup> /s
Bypass Flow:	0.04	ft <sup>3</sup> /s
Spread:	11.68	ft
Depth:	0.27	ft
Flow Area:	1.39	ft <sup>2</sup>
Gutter Depression:	0.03	ft
Total Depression:	0.20	ft
Velocity:	2.88	ft/s
Equivalent Cross Slope:	0.06423	ft/ft
Length Factor:	0.92	
Total Interception Length:	17.41	ft

## Worksheet for CB8.1

### Project Description

Flow Element: Grate Inlet On Grade  
Solve For: Efficiency

### Input Data

Discharge:	0.04	ft <sup>3</sup> /s
Slope:	0.01000	ft/ft
Gutter Width:	1.50	ft
Gutter Cross Slope:	0.04	ft/ft
Road Cross Slope:	0.02	ft/ft
Manning Coefficient:	0.015	
Grate Width:	2.00	ft
Grate Length:	3.00	ft
Grate Type:	P-50 mm (P-1-7/8")	
Clogging:	50.00	%

### Options

Grate Flow Option: ExcludeNone

### Results

Efficiency:	100.00	%
Intercepted Flow:	0.04	ft <sup>3</sup> /s
Bypass Flow:	0.00	ft <sup>3</sup> /s
Spread:	1.34	ft
Depth:	0.06	ft
Flow Area:	0.04	ft <sup>2</sup>
Gutter Depression:	0.03	ft
Total Depression:	0.03	ft
Velocity:	1.08	ft/s
Splash Over Velocity:	6.99	ft/s
Frontal Flow Factor:	1.00	
Side Flow Factor:	0.23	
Grate Flow Ratio:	1.00	
Active Grate Length:	1.50	ft

## Worksheet for CB7.3

### Project Description

Flow Element: Grate Inlet On Grade  
Solve For: Efficiency

### Input Data

Discharge:	5.00	ft <sup>3</sup> /s
Slope:	0.01000	ft/ft
Gutter Width:	1.50	ft
Gutter Cross Slope:	0.04	ft/ft
Road Cross Slope:	0.02	ft/ft
Manning Coefficient:	0.015	
Grate Width:	2.00	ft
Grate Length:	9.00	ft
Grate Type:	P-50 mm (P-1-7/8")	
Clogging:	50.00	%

### Options

Grate Flow Option: ExcludeNone

### Results

Efficiency:	69.08	%
Intercepted Flow:	3.45	ft <sup>3</sup> /s
Bypass Flow:	1.55	ft <sup>3</sup> /s
Spread:	12.73	ft
Depth:	0.29	ft
Flow Area:	1.64	ft <sup>2</sup>
Gutter Depression:	0.03	ft
Total Depression:	0.03	ft
Velocity:	3.04	ft/s
Splash Over Velocity:	12.28	ft/s
Frontal Flow Factor:	1.00	
Side Flow Factor:	0.36	
Grate Flow Ratio:	0.51	
Active Grate Length:	4.50	ft

## Worksheet for CB7.2

### Project Description

Flow Element: Grate Inlet On Grade  
Solve For: Efficiency

### Input Data

Discharge:	1.55	ft <sup>3</sup> /s
Slope:	0.01000	ft/ft
Gutter Width:	1.50	ft
Gutter Cross Slope:	0.04	ft/ft
Road Cross Slope:	0.02	ft/ft
Manning Coefficient:	0.015	
Grate Width:	2.00	ft
Grate Length:	9.00	ft
Grate Type:	P-50 mm (P-1-7/8")	
Clogging:	50.00	%

### Options

Grate Flow Option: ExcludeNone

### Results

Efficiency:	86.64	%
Intercepted Flow:	1.34	ft <sup>3</sup> /s
Bypass Flow:	0.21	ft <sup>3</sup> /s
Spread:	8.07	ft
Depth:	0.19	ft
Flow Area:	0.67	ft <sup>2</sup>
Gutter Depression:	0.03	ft
Total Depression:	0.03	ft
Velocity:	2.30	ft/s
Splash Over Velocity:	12.28	ft/s
Frontal Flow Factor:	1.00	
Side Flow Factor:	0.49	
Grate Flow Ratio:	0.74	
Active Grate Length:	4.50	ft

## Worksheet for CB5.2

### Project Description

Flow Element: Curb Inlet On Grade  
Solve For: Efficiency

### Input Data

Discharge:	4.21	ft <sup>3</sup> /s
Slope:	0.01000	ft/ft
Gutter Width:	1.50	ft
Gutter Cross Slope:	0.04	ft/ft
Road Cross Slope:	0.02	ft/ft
Manning Coefficient:	0.015	
Curb Opening Length:	7.20	ft
Local Depression:	2.00	in
Local Depression Width:	1.50	ft

### Results

Efficiency:	60.34	%
Intercepted Flow:	2.54	ft <sup>3</sup> /s
Bypass Flow:	1.67	ft <sup>3</sup> /s
Spread:	11.91	ft
Depth:	0.27	ft
Flow Area:	1.44	ft <sup>2</sup>
Gutter Depression:	0.03	ft
Total Depression:	0.20	ft
Velocity:	2.92	ft/s
Equivalent Cross Slope:	0.06341	ft/ft
Length Factor:	0.40	
Total Interception Length:	17.92	ft

## **ATTACHMENTS**

- A. Vicinity Map
- B. Proposed Storm Drain Layout/ Map from CAR
- C. Hydrology Maps
- D. Precipitation Data
- E. Soil and Landuse Data
- F. Clark Unit Hydrograph Data
- G. Hydraulic Routing Data
- H. HEC-1 Input/Output
- I. StormCAD Output
- J. Hydrology / Hydraulics Supporting Data
- K. Electronic Files