TO: FILE
LID 3.9

ARCADIA AREA DRAINAGE PROJECT

PROJECT NO. 94.21
EXISTING HYDROLOGY

VOLUME II

FLOO
SEP 12 1995
REMARKS

FLOOD CONTROL DISTRICT OF
MARICOPA COUNTY, ARIZONA
2801 WEST DURANGO STREET
PHOENIX, ARIZONA 85009

September 8, 1995

HUITT-ZOLLARS, INC.
6245 North 24th Parkway, Suite 102
Phoenix, Arizona 85016
(602) 381-0125

A-1

HEC-1 MODEL 10-YEAR EXISTING CONDITIONS

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1****************************************                    ****************************************
*                                      *                    *                                      *
*  FLOOD HYDROGRAPH PACKAGE  (HEC-1)   *                    *   U.S. ARMY CORPS OF ENGINEERS       *
*            MAY   1991                *                    *   HYDROLOGIC ENGINEERING CENTER      *
*          VERSION 4.0.1E              *                    *         609 SECOND STREET            *
*                                      *                    *      DAVIS, CALIFORNIA 95616         *
*  RUN DATE  09/01/95  TIME  04:59:57  *                    *          (916) 551-1748              *
*                                      *                    *                                      *
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                                    X     X  XXXXXXX   XXXXX          X
                                    X     X  X        X     X        XX
                                    X     X  X        X              X
                                    XXXXXXX  XXXX     X        XXXXX X
                                    X     X  X        X              X
                                    X     X  X        X     X        X
                                    X     X  XXXXXXX   XXXXX        XXX
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THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE.
THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION
NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,
DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION
KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

HEC-1 INPUT PAGE 1

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LINE          ID.......1.......2.......3.......4.......5.......6.......7.......8.......9......10

              *       ARCADIA AREA HYDROLOGY STUDY - EXISTING CONDITIONS.
              *       PREPARED BY: HUITT-ZOLLARS INC. 8-31-95
              *       PREPARED FOR: FCDMC CONTRACT # 94-21
    1         ID
    2         ID   DDM MCUHP1 ARCADIA AREA 10-yr 6hr
    3         IT       5                    300
    4         IO       5
              *DIAGRAM
              *

    5         KK    SUB1
    6         KM   SUB-BASIN SUB1
    7         KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
    8         KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
    9         KM     L =  .28  Kb = .100  Adj. Slope = 2120.0
   10         BA    .037
   11         IN      15
   12         KM   RAINFALL DEPTH OF 2.00 WAS SPACIALLY REDUCED AS SHOWN BY THE PB RECORD
   13         PB   1.924
   14         KM   THE FOLLOWING PC RECORD USED A 6-HOUR STORM WITH A PATTERN No. OF 2.20
   15         PC    .000    .010    .017    .026    .037    .046    .056    .065    .075    .085
   16         PC    .097    .111    .131    .175    .263    .455    .689    .829    .893    .933
   17         PC    .949    .962    .975    .988   1.000
   18         LG    .142    .322   4.550    .310  52.000
   19         UC    .150    .107
   20         UA       0       3       5       8      12      20      43      75      90      96
   21         UA     100
              *

   22         KK    R1-2
   23         KM        ROUTE FLOW FROM SUB1 TO SUB2
   24         RK  3183.8   .0166     .07       0    TRAP       0       3     YES
              *

   25         KK    SUB2
   26         KM   SUB-BASIN SUB2
   27         KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
   28         KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
   29         KM     L =  .60  Kb = .041  Adj. Slope =   88.0
   30         BA    .119
   31         LG    .342    .250   4.650    .440   9.000
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 32          UC    .596    .466
 33          UA       0       5      16      30      65      77      84      90      94      97
 34          UA     100
             *

 35          KK    DIV2
 36          KM        DIVERT FOR IRRIGATED LAWNS SUB2
 37          DT      D2     .80
 38          DI       0       1
 39          DQ       0    .382
             *
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LINE         ID.......1.......2.......3.......4.......5.......6.......7.......8.......9......10

 40          KK    C1-2
 41          KM        COMBINE HYDROGRAPHS SUB1 AND SUB2 AT CP2
 42          HC       2
             *

 43          KK    R2-3
 44          KM        ROUTE FLOW FROM SUB2 TO SUB3
 45          RK  1367.5    .009    .016            TRAP      60       1     YES
             *

 46          KK    SUB3
 47          KM   SUB-BASIN SUB3
 48          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
 49          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
 50          KM     L =  .26  Kb = .058  Adj. Slope =   47.0
 51          BA    .067
 52          LG    .298    .250   4.250    .510  16.000
 53          UC    .533    .293
 54          UA       0       5      16      30      65      77      84      90      94      97
 55          UA     100
             *

 56          KK    DIV3
 57          KM        DIVERT FOR IRRIGATED LAWNS SUB3
 58          DT      D3     .88
 59          DI       0       1
 60          DQ       0    .573
             *

 61          KK    C2-3
 62          KM        COMBINE HYDROGRAPHS SUB2 & SUB3 AT CP3
 63          HC       2
             *

 64          KK    R3-4
 65          KM        ROUTE FLOW FROM CP3 TO CP4
 66          RK    1320    .008    .016            TRAP      44       1     YES
             *

 67          KK    SUB4
 68          KM   SUB-BASIN SUB4
 69          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
 70          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
 71          KM     L =  .25  Kb = .058  Adj. Slope =   42.0
 72          BA    .065
 73          LG    .300    .250   4.800    .360  15.000
 74          UC    .467    .249
 75          UA       0       5      16      30      65      77      84      90      94      97
 76          UA     100
             *
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LINE         ID.......1.......2.......3.......4.......5.......6.......7.......8.......9......10

 77          KK    DIV4
 78          KM        DIVERT FOR IRRIGATED LAWNS SUB4
 79          DT      D4     1.0
 80          DI       0       1
 81          DQ       0     .55
             *

 82          KK    C3-4
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 83          KM        COMBINE HYDROGRAPHS SUB3 & SUB4 AT CP4
 84          HC       2
             *

 85          KK  DIVIBW
 86          KM        DIVERT LAFAYETTE DRAIN INTERCETION TO INDIAN BEND WASH
 87          DT    DIBW
 88          DI      25      63     101     193     241     306
 89          DQ    12.5    31.5    50.5    96.5     121    55.1
             *

 90          KK    R4-5
 91          KM        ROUTE FLOW FROM CP4 TO CP5
 92          RK  2307.4    .005    .016            TRAP      44       1     YES
             *

 93          KK    SUB5
 94          KM   SUB-BASIN SUB5
 95          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
 96          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
 97          KM     L =  .44  Kb = .058  Adj. Slope =   24.0
 98          BA    .067
 99          LG    .300    .250   4.800    .360  15.000
100          UC    .846    .744
101          UA       0       5      16      30      65      77      84      90      94      97
102          UA     100
             *

103          KK    DIV5
104          KM        DIVERT FOR IRRIGATED LAWNS SUB5
105          DT      D5     .94
106          DI       0       1
107          DQ       0     .50
             *

108          KK    C4-5
109          KM        COMBINE HYDROGRAPHS SUB4 & SUB5 AT CP5
110          HC       2
             *

111          KK    SUB6
112          KM   SUB-BASIN SUB6
113          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
114          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
115          KM     L =  .26  Kb = .102  Adj. Slope = 2367.0
116          BA    .090
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LINE         ID.......1.......2.......3.......4.......5.......6.......7.......8.......9......10

117          LG    .113    .341   4.700    .250  50.000
118          UC    .142    .057
119          UA       0       3       5       8      12      20      43      75      90      96
120          UA     100
             *

121          KK    R6-7
122          KM        ROUTE FLOW FROM SUB6 TO SUB7
123          RK  2972.0    .013     .07            TRAP       0       3     YES
             *

124          KK    SUB7
125          KM   SUB-BASIN SUB7
126          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
127          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
128          KM     L =  .56  Kb = .052  Adj. Slope =   71.0
129          BA    .153
130          LG    .295    .269   5.400    .280  18.000
131          UC    .546    .346
132          UA       0       5      16      30      65      77      84      90      94      97
133          UA     100
             *

134          KK    DIV7
135          KM        DIVERT FOR IRRIGATED LAWNS SUB7
136          DT      D7    2.30
137          DI       0       1
138          DQ       0    .427
             *
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139          KK    C6-7
140          KM        COMBINE HYDROGRAPHS SUB6 & SUB7 AT CP7
141          HC       2
             *

142          KK    R7-8
143          KM        ROUTE FLOW FROM SUB7 TO SUB8
144          RK  2302.1    .001    .016            TRAP      40       1     YES
             *

145          KK    SUB8
146          KM   SUB-BASIN SUB8
147          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
148          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
149          KM     L =  .44  Kb = .057  Adj. Slope =   52.0
150          BA    .068
151          LG    .300    .250   4.350    .480  15.000
152          UC    .696    .594
153          UA       0       5      16      30      65      77      84      90      94      97
154          UA     100
             *
                                                HEC-1 INPUT                                          PAGE  5

LINE         ID.......1.......2.......3.......4.......5.......6.......7.......8.......9......10

155          KK    DIV8
156          KM        DIVERT FOR IRRIGATED LAWNS SUB8
157          DT      D8     .99
158          DI       0       1
159          DQ       0      .6
             *

160          KK    C7-8
161          KM        COMBINE HYDROGRAPHS SUB7 & SUB8 AT CP8
162          HC       2
             *

163          KK    R8-9
164          KM        ROUTE FLOW FROM SUB8 TO SUB9
165          RK  1314.7    .010    .016            TRAP      20       1     YES
             *

166          KK    SUB9
167          KM   SUB-BASIN SUB9
168          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
169          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
170          KM     L =  .25  Kb = .058  Adj. Slope =   55.0
171          BA    .065
172          LG    .300    .250   4.500    .430  15.000
173          UC    .454    .241
174          UA       0       5      16      30      65      77      84      90      94      97
175          UA     100
             *

176          KK    DIV9
177          KM        DIVERT FOR IRRIGATED LAWNS SUB9
178          DT      D9     .94
179          DI       0       1
180          DQ       0      .6
             *

181          KK    C8-9
182          KM        COMBINE HYDROGRAPHS SUB8 & SUB9   AT CP9
183          HC       2
             *

184          KK    R9-5
185          KM        ROUTE FLOW FROM SUB9 TO  SUB5
186          RK  1784.7    .007    .016            TRAP      40       1     YES
             *

187          KK    C9-5
188          KM        COMBINE HYDROGRAPH SUB9  & SUB5  AT CP5
189          HC       2
             *
             *
             *
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LINE          ID.......1.......2.......3.......4.......5.......6.......7.......8.......9......10

 190          KK   R5-10
 191          KM        ROUTE FLOW ALONG CHANNEL FROM SUB5 TO  SUB10
 192          RS       1    FLOW      -1
 193          SV       0       1       3      13      50     110     162
 194          SQ       0      75     250     500    1200    2400    4000
              *

 195          KK   SUB10
 196          KM   SUB-BASIN SUB10
 197          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
 198          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
 199          KM     L =  .34  Kb = .056  Adj. Slope =   37.0
 200          BA    .093
 201          LG    .299    .250   4.800    .360  15.000
 202          UC    .579    .330
 203          UA       0       5      16      30      65      77      84      90      94      97
 204          UA     100
              *

 205          KK   DIV10
 206          KM        DIVERT FOR IRRIGATED LAWNS SUB10
 207          DT     D10    1.17
 208          DI       0       1
 209          DQ       0    .445
              *

 210          KK   C5-10
 211          KM        COMBINE HYDROGRAPH SUB5  & SUB10 AT CP10
 212          HC       2
              *
              *
              *

 213          KK  R10-15
 214          KM        ROUTE FLOW ALONG CHANNEL FROM SUB10 TO SUB15
 215          RS       1    FLOW      -1
 216          SV       0       2       5       8      46     156     247
 217          SQ       0      75     250     500    1200    2400    4000
              *

 218          KK   SUB11
 219          KM   SUB-BASIN SUB11
 220          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
 221          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
 222          KM     L =  .56  Kb = .106  Adj. Slope = 1740.0
 223          BA    .093
 224          LG    .115    .350   4.550    .270  39.000
 225          UC    .237    .183
 226          UA       0       3       5       8      12      20      43      75      90      96
 227          UA     100
              *
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LINE          ID.......1.......2.......3.......4.......5.......6.......7.......8.......9......10

 228          KK  R11-12
 229          KM        ROUTE FLOW FROM SUB11 TO   SUB12
 230          RK    1632    .058     .07            TRAP       0       3     YES
              *

 231          KK   SUB12
 232          KM   SUB-BASIN SUB12
 233          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
 234          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
 235          KM     L =  .31  Kb = .064  Adj. Slope =  304.0
 236          BA    .120
 237          LG    .269    .279   5.700    .200   9.000
 238          UC    .246    .102
 239          UA       0       5      16      30      65      77      84      90      94      97
 240          UA     100
              *

 241          KK   DIV12
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```
242          KM        DIVERT FOR IRRIGATED LAWNS SUB12
243          DT     D12     .31
244          DI       0       1
245          DQ       0    .079
             *

246          KK  C11-12
247          KM        COMBINE HYDROGRAPH SUB11 & SUB12 AT CP12
248          HC       2
             *

249          KK  R12-13
250          KM        ROUTE FLOW FROM SUB12 TO SUB13
251          RK  1362.2    .020    .016            TRAP      60       1     YES      50
             *

252          KK   SUB13
253          KM   SUB-BASIN SUB13
254          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
255          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
256          KM     L =  .26  Kb = .054  Adj. Slope =  107.0
257          BA    .129
258          LG    .300    .230   6.200    .200  15.000
259          UC    .283    .100
260          UA       0       5      16      30      65      77      84      90      94      97
261          UA     100
             *

262          KK   DIV13
263          KM        DIVERT FOR IRRIGATED LAWNS SUB13
264          DT     D13     .98
265          DI       0       1
266          DQ       0      .2
             *
                                          HEC-1 INPUT                                          PAGE  8

LINE         ID.......1.......2.......3.......4.......5.......6.......7.......8.......9......10

267          KK  C12-13
268          KM        COMBINE HYDROGRAPHS SUB12 & SUB13 AT CP13
269          HC       2
             *

270          KK  R13-14
271          KM        ROUTE FL OW FROM SUB13 TO SUB14
272          RK  1314.7    .014    .016            TRAP      60       1     YES
             *

273          KK   SUB14
274          KM   SUB-BASIN SUB14
275          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
276          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
277          KM     L =  .25  Kb = .054  Adj. Slope =   74.0
278          BA    .126
279          LG    .300    .250   4.100    .550  15.000
280          UC    .433    .157
281          UA       0       5      16      30      65      77      84      90      94      97
282          UA     100
             *

283          KK   DIV14
284          KM        DIVERT FOR IRRIGATED LAWNS SUB14
285          DT     D14    1.57
286          DI       0       1
287          DQ       0      .6
             *

288          KK  C13-14
289          KM        COMBINE HYDROGRAPHS SUB13 & SUB14 AT CP14
290          HC       2
             *

291          KK  R14-15
292          KM        ROUTE FLOW FROM SUB 14 TO SUB15
293          RK  1985.3    .011    .016            TRAP      60       1     YES
             *

294          KK   SUB15
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295          KM   SUB-BASIN SUB15
296          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
297          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
298          KM     L =  .38  Kb = .054  Adj. Slope =   56.0
299          BA    .126
300          LG    .297    .250   4.650    .390  16.000
301          UC    .529    .274
302          UA      0       5      16      30      65      77      84      90      94      97
303          UA    100
             *
1                                          HEC-1 INPUT                                                    PAGE  9

LINE         ID.......1.......2.......3.......4.......5.......6.......7.......8.......9......10

304          KK   DIV15
305          KM        DIVERT FOR IRRIGATED LAWNS SUB15
306          DT     D15    2.05
307          DI       0       1
308          DQ       0    .585
             *

309          KK  C15-10
310          KM        COMBINE SUB14, SUB10 WITH SUB15
311          HC       3
             *      1       2
             *

312          KK   D56ST
313          KM        DIVERT FLOW THAT CROSSES 56TH ST. BRIDGE
314          DT   D56ST
315          DI       0     400     650     790    1040    1139    1334    1484    1689    1900
316          DQ       0       0     240     318     400     489     584     684     789     900
             *
             *      3       0
             *

317          KK  R15-20
318          KM        ROUTE FLOW ALONG CHANNEL FROM SUB15 TO SUB20
319          RS       1    FLOW      -1
320          SV       0      14      18      25      35      72     111
321          SQ       0      75     250     500    1200    2400    4000
             *

322          KK   SUB16
323          KM   SUB-BASIN SUB16
324          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
325          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
326          KM     L =  .65  Kb = .102  Adj. Slope = 2052.0
327          BA    .129
328          LG    .104    .350   4.700    .240  47.000
329          UC    .233    .167
330          UA      0       3       5       8      12      20      43      75      90      96
331          UA    100
             *

332          KK  R16-17
333          KM        ROUTE FLOW FROM SUB16 TO SUB17
334          RK    1668    .058     .07            TRAP       0       3     YES
             *

335          KK   SUB17
336          KM   SUB-BASIN SUB17
337          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
338          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
339          KM     L =  .32  Kb = .058  Adj. Slope =  183.0
340          BA    .073
341          LG    .298    .252   4.350    .400  10.000
342          UC    .329    .193
                                           HEC-1 INPUT                                                    PAGE 10

LINE         ID.......1.......2.......3.......4.......5.......6.......7.......8.......9......10

343          UA      0       5      16      30      65      77      84      90      94      97
344          UA    100
             *

345          KK   DIV17
346          KM        DIVERT FOR IRRIGATED LAWNS SUB17
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347          DT     D17     .11
348          DI       0       1
349          DQ       0    .074
             *

350          KK  C16-17
351          KM       COMBINE HYDROGRAPH SUB16 & SUB17 AT CP17
352          HC       2
             *

353          KK  R17-18
354          KM       ROUTE FLOW FROM SUB17 TO SUB18
355          RK  1378.1    .019    .016            TRAP      40       1     YES
             *

356          KK   SUB18
357          KM   SUB-BASIN SUB18
358          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
359          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
360          KM     L =  .26  Kb = .058  Adj. Slope =  102.0
361          BA    .067
362          LG    .300    .250   4.150    .530  15.000
363          UC    .404    .215
364          UA       0       5      16      30      65      77      84      90      94      97
365          UA     100
             *

366          KK   DIV18
367          KM       DIVERT FOR IRRIGATED LAWNS SUB18
368          DT     D18     .81
369          DI       0       1
370          DQ       0      .6
             *

371          KK  C17-18
372          KM       COMBINE  HYDROGRAPH SUB17 & SUB18 AT CP18
373          HC       2
             *

374          KK  R18-19
375          KM       ROUTE FLOW SUB18 TO SUB19
376          RK  1335.8    .014    .016            TRAP      40       1     YES
             *
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LINE         ID.......1.......2.......3.......4.......5.......6.......7.......8.......9......10

377          KK   SUB19
378          KM   SUB-BASIN SUB19
379          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
380          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
381          KM     L =  .25  Kb = .057  Adj. Slope =   77.0
382          BA    .075
383          LG    .300    .250   3.950    .580  15.000
384          UC    .450    .220
385          UA       0       5      16      30      65      77      84      90      94      97
386          UA     100
             *

387          KK   DIV19
388          KM       DIVERT FOR IRRIGATED LAWNS SUB19
389          DT     D19     .91
390          DI       0       1
391          DQ       0      .6
             *

392          KK  C18-19
393          KM       COMBINE HYDROGRAPH SUB18 & SUB19 AT CP19
394          HC       2
             *

395          KK  R19-20
396          KM       ROUTE FLOW FROM SUB19 TO SUB20
397          RK  1473.1    .010    .016            TRAP      30       1     YES
             *

398          KK   SUB20
399          KM   SUB-BASIN SUB20
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400          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
401          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
402          KM     L =  .28  Kb = .054  Adj. Slope =   54.0
403          BA    .129
404          LG    .300    .250   4.450    .450  15.000
405          UC    .479    .190
406          UA      0       5      16      30      65      77      84      90      94      97
407          UA    100
             *

408          KK   DIV20
409          KM        DIVERT FOR IRRIGATED LAWNS SUB20
410          DT     D20    1.86
411          DI       0       1
412          DQ       0      .6
             *

413          KK  C20-15
414          KM        COMBINE SUB19, SUB15 WITH SUB20
415          HC       3
             *      1       2
             *
             *      3       0
             *
```



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LINE         ID.......1.......2.......3.......4.......5.......6.......7.......8.......9......10

416          KK  R20-25
417          KM        ROUTE FLOW ALONG CHANNEL FROM SUB20 TO SUB25
418          RS       1    FLOW      -1
419          SV       0      23      27      35      37      84     122
420          SQ       0      75     250     500    1200    2400    4000
             *

421          KK   SUB21
422          KM   SUB-BASIN SUB21
423          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
424          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
425          KM     L =  .56  Kb = .102  Adj. Slope = 2352.0
426          BA    .124
427          LG    .104    .350   4.700    .240  46.000
428          UC    .208    .134
429          UA      0       3       5       8      12      20      43      75      90      96
430          UA    100
             *

431          KK  R21-22
432          KM        ROUTE FLOW FROM SUB21 TO SUB22
433          RK    2735    .026     .07            TRAP       0       3     YES
             *

434          KK   SUB22
435          KM   SUB-BASIN SUB22
436          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
437          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
438          KM     L =  .52  Kb = .060  Adj. Slope =  134.0
439          BA    .112
440          LG    .281    .266   4.000    .480  11.000
441          UC    .571    .410
442          UA      0       5      16      30      65      77      84      90      94      97
443          UA    100
             *

444          KK   DIV22
445          KM        DIVERT FOR IRRIGATED LAWNS SUB22
446          DT     D22     .12
447          DI       0       1
448          DQ       0    .063
             *

449          KK  C21-22
450          KM        COMBINE HYDROGRAPH SUB21 & SUB22 AT CP22
451          HC       2
             *

452          KK  R22-23
453          KM        ROUTE FLOW FROM SUB22 TO SUB23
```

```
454          RK  1240.8    .025    .016            TRAP      20       1     YES
             *
                                        HEC-1 INPUT                                                    PAGE 13
LINE         ID.......1.......2.......3.......4.......5.......6.......7.......8.......9......10

455          KK   SUB23
456          KM   SUB-BASIN SUB23
457          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
458          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
459          KM     L =  .23  Kb = .058  Adj. Slope =  132.0
460          BA    .060
461          LG    .300    .250   3.950    .580  15.000
462          UC    .350    .177
463          UA      0       5      16      30      65      77      84      90      94      97
464          UA     100
             *

465          KK   DIV23
466          KM        DIVERT FOR IRRIGATED LAWNS SUB23
467          DT     D23     .72
468          DI       0       1
469          DQ       0    .593
             *

470          KK  C22-23
471          KM        COMBINE HYDROGRAPH SUB22 & SUB23 AT CP23
472          HC       2
             *

473          KK  R23-24
474          KM        ROUTE FLOW FROM SUB 23 TO SUB24
475          RK  1088.9    .015    .016            TRAP      32       1     YES
             *

476          KK   SUB24
477          KM   SUB-BASIN SUB24
478          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
479          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
480          KM     L =  .28  Kb = .057  Adj. Slope =   78.0
481          BA    .077
482          LG    .300    .250   3.950    .580  15.000
483          UC    .479    .255
484          UA      0       5      16      30      65      77      84      90      94      97
485          UA     100
             *

486          KK   DIV24
487          KM        DIVERT FOR IRRIGATED LAWNS SUB24
488          DT     D24     .93
489          DI       0       1
490          DQ       0      .6
             *

491          KK  C23-24
492          KM        COMBINE HYDROGRAPH SUB23 & SUB24 AT CP24
493          HC       2
             *
                                        HEC-1 INPUT                                                    PAGE 14
LINE         ID.......1.......2.......3.......4.......5.......6.......7.......8.......9......10

494          KK  R24-25
495          KM        ROUTE FLOW FROM SUB24 TO SUB25
496          RK  1346.4    .009    .016            TRAP      40       1     YES
             *

497          KK   SUB25
498          KM   SUB-BASIN SUB25
499          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
500          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
501          KM     L =  .25  Kb = .057  Adj. Slope =   46.0
502          BA    .076
503          LG    .300    .250   3.950    .580  15.000
504          UC    .550    .273
505          UA      0       5      16      30      65      77      84      90      94      97
506          UA     100
```

```
*
KK   DIV25
KM        DIVERT FOR IRRIGATED LAWNS SUB25
DT     D25      .93
DI       0        1
DQ       0       .6
*
KK  C25-20
KM        COMBINE SUB19, SUB 20 WITH SUB25
HC       3
*      1        2
*
*      3        0
*
KK  R25-29
KM        ROUTE FLOW ALONG CHANNEL FROM SUB25 TO SUB29
RS       1    FLOW      -1
SV       0        2        6       13       23       35       36
SQ       0       75      250      500     1200     2400     4000
*
KK   SUB26
KM   SUB-BASIN SUB26
KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
KM     L =  .52  Kb = .067  Adj. Slope =  840.0
BA    .053
LG    .272    .295   4.250    .520  17.000
UC    .304    .312
UA       0       5       16       30       65       77       84       90       94       97
UA     100
*
```



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LINE          ID.......1.......2.......3.......4.......5.......6.......7.......8.......9......10

KK   DIV26
KM        DIVERT FOR GOLF   COURSE
DT     D26      .31
DI       0        1
DQ       0     .312
*
KK  R26-27
KM        ROUTE FLOW FROM SUB26 TO SUB27
RK  1293.6     .024     .016            TRAP      35        1      YES
*
KK   SUB27
KM   SUB-BASIN SUB27
KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
KM     L =  .25  Kb = .058  Adj. Slope =  122.0
BA    .061
LG    .300    .250   3.950    .580  15.000
UC    .379    .205
UA       0       5       16       30       65       77       84       90       94       97
UA     100
*
KK   DIV27
KM        DIVERT FOR IRRIGATED LAWNS SUB27
DT     D27      .74
DI       0      1.0
DQ       0      .60
*
KK  C26-27
KM        COMBINE HYDROGRAPH SUB 26 & SUB27 AT CP27
HC       2
*
KK  R27-28
KM        ROUTE FLOW FROM SUB 27 TO SUB28
RK  1436.2     .017     .016            TRAP      35        1      YES
```

```
            *
559         KK   SUB28
560         KM   SUB-BASIN SUB28
561         KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
562         KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
563         KM     L =  .27  Kb = .057  Adj. Slope =   89.0
564         BA    .078
565         LG    .300    .250   3.950    .580  15.000
566         UC    .446    .227
567         UA       0       5      16      30      65      77      84      90      94      97
568         UA     100
            *
                                          HEC-1 INPUT                                          PAGE 16

LINE        ID.......1.......2.......3.......4.......5.......6.......7.......8.......9......10

569         KK   DIV28
570         KM        DIVERT FOR IRRIGATED LAWNS SUB28
571         DT     D28     .95
572         DI       0       1
573         DQ       0     .60
            *

574         KK  C27-28
575         KM        COMBINE HYDROGRAPH SUB27 & SUB28 AT CP28
576         HC       2
            *

577         KK  R28-29
578         KM        ROUTE FLOW FROM SUB 28 TO SUB29
579         RK  1161.6    .009    .016            TRAP      35       1     YES
            *

580         KK   SUB29
581         KM   SUB-BASIN SUB29
582         KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
583         KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
584         KM     L =  .22  Kb = .058  Adj. Slope =   47.0
585         BA    .058
586         LG    .299    .250   3.950    .580  15.000
587         UC    .508    .264
588         UA       0       5      16      30      65      77      84      90      94      97
589         UA     100
            *

590         KK   DIV29
591         KM        DIVERT FOR IRRIGATED LAWNS SUB29
592         DT     D29     .70
593         DI       0       1
594         DQ       0    .587
            *

595         KK  C29-25
596         KM        COMBINE SUB28, SUB25 WITH SUB29
597         HC       3
            *      1       2
            *

598         KK   DOCCC
599         KM        DIVERT AZ CANAL FLOW TO OCCC
600         DT   DOCCC
601         DI       0     200     400     800    1000    1001    1200    4000
602         DQ       0     200     400     800    1000    1000    1000    1000
            *
            *      3       0
            *
1                                         HEC-1 INPUT                                          PAGE 17

LINE        ID.......1.......2.......3.......4.......5.......6.......7.......8.......9......10

603         KK  R29-33
604         KM        ROUTE FLOW ALONG CHANNEL FROM SUB29 TO SUB33
605         RS       1    FLOW      -1
606         SV       0       2       4       7      18      36      60
607         SQ       0      75     250     500    1200    2400    4000
            *
```

```
608          KK   SUB38
609          KM   SUB-BASIN SUB38
610          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
611          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
612          KM     L = 1.28  Kb = .090  Adj. Slope = 1079.0
613          BA    .252
614          LG    .131    .340   4.550    .280  37.000
615          UC    .408    .366
616          UA      0       3       5       8      12      20      43      75      90      96
617          UA    100
             *

618          KK  D38-39
619          KM       DIVERT 16CFS FROM SUB38 TO SUB39
620          DT  D38-39
621          DI      0       5      10      16      50     100     200     400     600
622          DQ      0       5      10      16      16      16      16      16      16
             *

623          KK  R38-30
624          KM       ROUTE FLOW FROM SUB38 TO   SUB30
625          RK   1200    .035    .016            TRAP      30       1     YES
             *

626          KK   SUB30
627          KM   SUB-BASIN SUB30
628          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
629          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
630          KM     L =  .48  Kb = .067  Adj. Slope =  571.0
631          BA    .064
632          LG    .272    .267   4.000    .460  10.000
633          UC    .313    .271
634          UA      0       5      16      30      65      77      84      90      94      97
635          UA    100
             *

636          KK  C30-38
637          KM       COMBINE SUB38 & SUB30 AT CP30
638          HC      2
             *

639          KK  R30-31
640          KM       ROUTE FLOW FROM SUB30 TO SUB31
641          RK   1304   .0225    .025            TRAP      20       1     YES
             *
```



```
LINE         ID.......1.......2.......3.......4.......5.......6.......7.......8.......9......10

642          KK   SUB31
643          KM   SUB-BASIN SUB31
644          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
645          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
646          KM     L =  .25  Kb = .058  Adj. Slope =  118.0
647          BA    .061
648          LG    .300    .260   3.670    .690  15.000
649          UC    .433    .238
650          UA      0       5      16      30      65      77      84      90      94      97
651          UA    100
             *

652          KK   DIV31
653          KM       DIVERT FOR IRRIGATED LAWNS SUB31
654          DT     D31     .45
655          DI      0       1
656          DQ      0    .400
             *

657          KK  C30-31
658          KM       COMBINE SUB30 & SUB31 AT CP31
659          HC      2
             *

660          KK  R31-32
661          KM       ROUTE FLOW FROM SUB31 TO SUB32
662          RK   1260    .019    .016       0    TRAP      30       1     YES
             *
```

```
663          KK   SUB32
664          KM   SUB-BASIN SUB32
665          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
666          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
667          KM     L =  .27  Kb = .058  Adj. Slope =   77.0
668          BA    .065
669          LG    .300    .250   3.950    .580  15.000
670          UC    .479    .272
671          UA       0       5      16      30      65      77      84      90      94      97
672          UA     100
             *

673          KK   DIV32
674          KM        DIVERT FOR IRRIGATED LAWNS SUB32
675          DT     D32     .79
676          DI     0.0     1.0
677          DQ       0     .60
             *

678          KK  C31-32
679          KM        COMBINE HYDROGRAPH SUB31 & SUB32 AT CP32
680          HC       2
             *
```



```
LINE         ID.......1.......2.......3.......4.......5.......6.......7.......8.......9......10

681          KK  R32-33
682          KM        ROUTE FLOW FROM SUB32 TO SUB33
683          RK    1447   .0144     .07            TRAP       0       3     YES
             *

684          KK   SUB33
685          KM   SUB-BASIN SUB33
686          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
687          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
688          KM     L =  .22  Kb = .058  Adj. Slope =   65.0
689          BA    .062
690          LG    .277    .250   3.950    .580  22.000
691          UC    .408    .199
692          UA       0       5      16      30      65      77      84      90      94      97
693          UA     100
             *

694          KK   DIV33
695          KM        DIVERT FOR IRRIGATED LAWNS SUB33
696          DT     D33     .62
697          DI       0       1
698          DQ       0     .37
             *

699          KK  C33-29
700          KM        COMBINE SUB32, SUB29 WITH SUB33
701          HC       3
             *      1       2
             *
             *      3       0
             *

702          KK  R33-35
703          KM        ROUTE FLOW ALONG CHANNEL FROM SUB33 TO SUB35
704          RS       1    FLOW      -1
705          SV       0       5      10      22      50      93     142
706          SQ       0      75     250     500    1200    2400    4000
             *

707          KK   SUB34
708          KM   SUB-BASIN SUB34
709          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
710          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
711          KM     L =  .57  Kb = .050  Adj. Slope =   87.0
712          BA    .167
713          LG    .284    .250   3.950    .590  20.000
714          UC    .617    .383
715          UA       0       5      16      30      65      77      84      90      94      97
716          UA     100
             *
```

```
LINE          ID.......1.......2.......3.......4.......5.......6.......7.......8.......9......10

  717         KK   DIV34
  718         KM        DIVERT FOR IRRIGATED LAWNS SUB34
  719         DT     D34    1.53
  720         DI       0       1
  721         DQ       0    .366
              *

  722         KK  R34-35
  723         KM        ROUTE FLOW FROM SUB34 TO SUB35
  724         RK  1531.2    .018    .016            TRAP      40       1     YES
              *

  725         KK   SUB35
  726         KM   SUB-BASIN SUB35
  727         KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
  728         KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
  729         KM     L =  .29  Kb = .048  Adj. Slope =   51.0
  730         BA    .128
  731         LG    .223    .250   3.950    .600  39.000
  732         UC    .400    .160
  733         UA       0       5      16      30      65      77      84      90      94      97
  734         UA     100
              *

  735         KK   DIV35
  736         KM        DIVERT FOR IRRIGATED LAWNS SUB35
  737         DT     D35     .53
  738         DI     0.0     1.0
  739         DQ     0.0    .095
              *

  740         KK  C35-33
  741         KM        COMBINE SUB34, SUB33 WITH SUB35
  742         HC       3
              *
              *      3       0
              *

  743         KK  R35-36
  744         KM        ROUTE FLOW ALONG CHANNEL FROM SUB35 TO SUB36
  745         RS       1    FLOW      -1
  746         SV       0       4       9      28      67     131     179
  747         SQ       0      75     250     500    1200    2400    4000
              *

  748         KK   SUB40
  749         KM   SUB-BASIN SUB40
  750         KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
  751         KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
  752         KM     L =  .31  Kb = .090  Adj. Slope = 1822.0
  753         BA    .074
  754         LG    .203    .314   4.000    .420  11.000
  755         UC    .188    .100
  756         UA       0       3       5       8      12      20      43      75      90      96
```



```
LINE          ID.......1.......2.......3.......4.......5.......6.......7.......8.......9......10

  757         UA     100
              *

  758         KK  R40-41
  759         KM        ROUTE FLOW FROM SUB40 TO SUB41
  760         RK    1452   .0221     .05            TRAP       6       2     YES
              *

  761         KK   SUB41
  762         KM   SUB-BASIN SUB41
  763         KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
  764         KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
  765         KM     L =  .54  Kb = .053  Adj. Slope =  110.0
  766         BA    .156
  767         LG    .281    .252   4.350    .420  16.000
  768         UC    .508    .308
```

```
769        UA       0       5      16      30      65      77      84      90      94      97
770        UA     100
           *

771        KK  C40-41
772        KM        COMBINE HYDROGRAPH SUB40 & SUB41 AT CP41
773        HC       2
           *

774        KK  R41-39
775        KM        ROUTE FLOW FROM SUB41 TO   SUB39
776        RK    2865   .0341     .05            TRAP       4       3     YES
           *

777        KK   SUB37
778        KM   SUB-BASIN SUB37
779        KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
780        KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
781        KM     L =  .30  Kb = .059  Adj. Slope =  247.0
782        BA    .049
783        LG    .300    .250   3.950    .490   5.000
784        UC    .321    .223
785        UA       0       5      16      30      65      77      84      90      94      97
786        UA     100
           *

787        KK  R37-39
788        KM        ROUTE FLOW FROM SUB37 TO   SUB39
789        RK    3500    .018    .016            TRAP      70       1     YES
           *

790        KK   SUB39
791        KM   SUB-BASIN SUB39
792        KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
793        KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
794        KM     L =  .84  Kb = .050  Adj. Slope =   79.0
795        BA    .224
796        LG    .233    .259   4.300    .450  29.000
797        UC    .667    .481
```



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LINE       ID.......1.......2.......3.......4.......5.......6.......7.......8.......9......10

798        UA       0       5      16      30      65      77      84      90      94      97
799        UA     100
           *

800        KK  D39-36
801        KM        DIVERT FLOW OF CAMELBACK RD. OVERTOPPING AND RUNNING TO    SUB36
802        DT  D39-36
803        DI       0    99.5     160     200     300     500     700    1000
804        DQ       0       0       0      40     140     340     540     840
           *

805        KK   DCBR1
806        KM        DIVERT 55 CFS FROM WATERSHED STORM DRAIN OUTLETS TO 40TH STREET SYSTEM
807        DT   DCBR1
808        DI       0      20      50      55     100     200     500    1000    2000    3000
809        DQ       0      20      50      55      55      55      55      55      55      55
           *

810        KK   DCBR2
811        KM        DIVERT 60 CFS FOR STORM DRAIN THAT OUTLETS INTO AZ. CANAL IN SUBBASIN 36
812        DT   DCBR2
813        DI       0      20      50      60     150     300     600    1000    2000    3000
814        DQ       0      20      50      60      60      60      60      60      60      60
           *

815        KK  RD3839
816        KM        RECALL DIVERSION FROM SUBBASIN 38
817        DR  D38-39
           *

818        KK  C37-41
819        KM        COMBINE HYDROGRAPHS SUB41, SUB37 & SUB39 AT CP39 AND RECALLED DIVERSION
820        HC       4
           *

821        KK  R39-36
```

```
822          KM        ROUTE FLOW FROM SUB39 TO   SUB36
823          RK    1250    .006    .016            TRAP      26       1     YES
             *

824          KK   SUB36
825          KM   SUB-BASIN SUB36
826          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
827          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
828          KM     L =  .28  Kb = .052  Adj. Slope =   14.0
829          BA    .089
830          LG    .232    .250   3.950    .590  41.000
831          UC    .646    .327
832          UA       0       5      16      30      65      77      84      90      94      97
833          UA     100
             *
```



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LINE         ID.......1.......2.......3.......4.......5.......6.......7.......8.......9......10

834          KK   DIV36
835          KM        DIVERT FOR IRRIGATED LAWNS SUB36
836          DT     D36     .61
837          DI     0.0     1.0
838          DQ     0.0    .150
             *

839          KK  RDCBR2
840          KM        RECALL DIVERSION FOR STORM DRAIN ALONG CAMELBACK RD.
841          DR   DCBR2
             *

842          KK  RD39366
843          KM        RECALL DIVERSION FROM SUB 39 TO    SUB36
844          DR  D39-36
             *

845          KK  C36-35
846          KM        COMBINE SUB39, SUB35, 2 RECALLED DIVERSIONS AND SUB36
847          HC       5
             *

848          KK   D40ST
849          KM        DIVERT FLOW FOR 40TH ST.
850          DT   D40ST
851          DI       0      10     100     300     500     700     900    1100    1300    1500
852          DQ       0       0      90     290     490     690     890    1090    1290    1490
             *
             *      3       0
             *

853          KK  R36-42
854          KM        ROUTE FLOW FROM SUB36 TO SUB42
855          RS       1    FLOW      -1
856          SV       0       3       6      10      34      60     130
857          SQ       0      75     250     500    1200    2400    4000
             *

858          KK   SUB42
859          KM   SUB-BASIN SUB42
860          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
861          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
862          KM     L =  .51  Kb = .044  Adj. Slope =   29.0
863          BA    .206
864          LG    .247    .250   5.600    .250  27.000
865          UC    .587    .294
866          UA       0       5      16      30      65      77      84      90      94      97
867          UA     100
             *
```



```
LINE         ID.......1.......2.......3.......4.......5.......6.......7.......8.......9......10

868          KK   DIV42
869          KM        DIVERT FOR IRRIGATED LAWNS SUB42
870          DT     D42     .75
871          DI       0       1
872          DQ       0    .072
```

```
                    *      1       2
                    *

873                 KK  C42-36
874                 KM        COMBINE HYDROGRAPH SUB42 WITH SUB36
875                 HC       2
                    *
                    *      3       0
                    *
876                 ZZ
```

1

SCHEMATIC DIAGRAM OF STREAM NETWORK

```
INPUT
 LINE      (V) ROUTING          (--->) DIVERSION OR PUMP FLOW

 NO.       (.) CONNECTOR        (<---) RETURN OF DIVERTED OR PUMPED FLOW

  5          SUB1
                V
                V
 22          R1-2
                .
                .
 25             .        SUB2
                .           .
                .           .
 37             .           .-------->      D2
 35             .        DIV2
                .           .
                .           .
 40          C1-2............
                V
                V
 43          R2-3
                .
                .
 46             .        SUB3
                .           .
                .           .
 58             .           .-------->      D3
 56             .        DIV3
                .           .
                .           .
 61          C2-3............
                V
                V
 64          R3-4
                .
                .
 67             .        SUB4
                .           .
                .           .
 79             .           .-------->      D4
 77             .        DIV4
                .           .
                .           .
 82          C3-4............
                .
                .
 87             .-------->   DIBW
 85       DIVIBW
                V
                V
 90          R4-5
                .
                .
 93             .        SUB5
                .           .
                .           .
105             .           .-------->      D5
103             .        DIV5
                .           .
                .           .
108          C4-5............
                .
                .
111             .        SUB6
                .           V
                .           V
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121          .        R6-7
             .          .
             .          .
124          .          .        SUB7
             .          .          .
             .          .          .
136          .          .          .-------->      D7
134          .          .        DIV7
             .          .          .
             .          .          .
139          .        C6-7............
             .          V
             .          V
142          .        R7-8
             .          .
             .          .
145          .          .        SUB8
             .          .          .
             .          .          .
157          .          .          .-------->      D8
155          .          .        DIV8
             .          .          .
             .          .          .
160          .        C7-8............
             .          V
             .          V
163          .        R8-9
             .          .
             .          .
166          .          .        SUB9
             .          .          .
             .          .          .
178          .          .          .-------->      D9
176          .          .        DIV9
             .          .          .
             .          .          .
181          .        C8-9............
             .          V
             .          V
184          .        R9-5
             .          .
             .          .
187       C9-5............
             V
             V
190       R5-10
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             .
195          .       SUB10
             .          .
             .          .
207          .          .-------->     D10
205          .       DIV10
             .          .
             .          .
210       C5-10...........
             V
             V
213      R10-15
             .
             .
218          .       SUB11
             .          V
             .          V
228          .      R11-12
             .          .
             .          .
231          .          .       SUB12
             .          .          .
             .          .          .
243          .          .          .-------->     D12
241          .          .       DIV12
             .          .          .
             .          .          .
246          .      C11-12...........
             .          V
             .          V
249          .      R12-13
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252          .           .       SUB13
             .           .           .
             .           .           .
264          .           .           .-------->     D13
262          .           .       DIV13
             .           .           .
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267          .      C12-13............
             .           V
             .           V
270          .      R13-14
             .           .
             .           .
273          .           .       SUB14
             .           .           .
             .           .           .
285          .           .           .-------->     D14
283          .           .       DIV14
             .           .           .
             .           .           .
288          .      C13-14............
             .           V
             .           V
291          .      R14-15
             .           .
             .           .
294          .           .       SUB15
             .           .           .
             .           .           .
306          .           .           .-------->     D15
304          .           .       DIV15
             .           .           .
             .           .           .
309     C15-10........................
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             .
314          .-------->  D56ST
312      D56ST
             V
             V
317     R15-20
             .
             .
322          .       SUB16
             .           V
             .           V
332          .      R16-17
             .           .
             .           .
335          .           .       SUB17
             .           .           .
             .           .           .
347          .           .           .-------->     D17
345          .           .       DIV17
             .           .           .
             .           .           .
350          .      C16-17............
             .           V
             .           V
353          .      R17-18
             .           .
             .           .
356          .           .       SUB18
             .           .           .
             .           .           .
368          .           .           .-------->     D18
366          .           .       DIV18
             .           .           .
             .           .           .
371          .      C17-18............
             .           V
             .           V
374          .      R18-19
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             .           .
377          .           .       SUB19
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389          .          .          .-------->    D19
387          .          .      DIV19
             .          .          .
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392          .     C18-19...........
             .          V
             .          V
395          .     R19-20
             .          .
             .          .
398          .          .      SUB20
             .          .          .
             .          .          .
410          .          .          .-------->    D20
408          .          .      DIV20
             .          .          .
             .          .          .
413     C20-15......................
             V
             V
416     R20-25
             .
             .
421          .      SUB21
             .          V
             .          V
431          .     R21-22
             .          .
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434          .          .      SUB22
             .          .          .
             .          .          .
446          .          .          .-------->    D22
444          .          .      DIV22
             .          .          .
             .          .          .
449          .     C21-22...........
             .          V
             .          V
452          .     R22-23
             .          .
             .          .
455          .          .      SUB23
             .          .          .
             .          .          .
467          .          .          .-------->    D23
465          .          .      DIV23
             .          .          .
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470          .     C22-23...........
             .          V
             .          V
473          .     R23-24
             .          .
             .          .
476          .          .      SUB24
             .          .          .
             .          .          .
488          .          .          .-------->    D24
486          .          .      DIV24
             .          .          .
             .          .          .
491          .     C23-24...........
             .          V
             .          V
494          .     R24-25
             .          .
             .          .
497          .          .      SUB25
             .          .          .
             .          .          .
509          .          .          .-------->    D25
507          .          .      DIV25
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512     C25-20......................
             V
             V
515     R25-29
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520       .      SUB26
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          .          .
532       .          .-------->     D26
530       .      DIV26
          .          V
          .          V
535       .      R26-27
          .          .
          .          .
538       .          .       SUB27
          .          .           .
          .          .           .
550       .          .           .-------->     D27
548       .          .       DIV27
          .          .           .
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553       .      C26-27............
          .          V
          .          V
556       .      R27-28
          .          .
          .          .
559       .          .       SUB28
          .          .           .
          .          .           .
571       .          .           .-------->     D28
569       .          .       DIV28
          .          .           .
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574       .      C27-28............
          .          V
          .          V
577       .      R28-29
          .          .
          .          .
580       .          .       SUB29
          .          .           .
          .          .           .
592       .          .           .-------->     D29
590       .          .       DIV29
          .          .           .
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595    C29-25........................
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          .
600       .-------->   DOCCC
598    DOCCC
          V
          V
603    R29-33
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608       .      SUB38
          .          .
          .          .
620       .          .-------->  D38-39
618       .      D38-39
          .          V
          .          V
623       .      R38-30
          .          .
          .          .
626       .          .       SUB30
          .          .           .
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636       .      C30-38............
          .          V
          .          V
639       .      R30-31
          .          .
          .          .
642       .          .       SUB31
          .          .           .
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654       .          .           .-------->     D31
652       .          .       DIV31
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657             .     C30-31...........
                .          V
                .          V
660             .     R31-32
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663             .          .     SUB32
                .          .          .
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675             .          .          .-------->     D32
673             .          .     DIV32
                .          .          .
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678             .     C31-32...........
                .          V
                .          V
681             .     R32-33
                .          .
                .          .
684             .          .     SUB33
                .          .          .
                .          .          .
696             .          .          .-------->     D33
694             .          .     DIV33
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699        C33-29......................
                V
                V
702        R33-35
                .
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707             .     SUB34
                .          .
                .          .
719             .          .-------->     D34
717             .     DIV34
                .          V
                .          V
722             .     R34-35
                .          .
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725             .          .     SUB35
                .          .          .
                .          .          .
737             .          .          .-------->     D35
735             .          .     DIV35
                .          .          .
                .          .          .
740        C35-33......................
                V
                V
743        R35-36
                .
                .
748             .     SUB40
                .          V
                .          V
758             .     R40-41
                .          .
                .          .
761             .          .     SUB41
                .          .          .
                .          .          .
771             .     C40-41...........
                .          V
                .          V
774             .     R41-39
                .          .
                .          .
777             .          .     SUB37
                .          .          V
                .          .          V
787             .          .     R37-39
                .          .          .
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790             .          .          .     SUB39
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802             .          .          .          .-------> D39-36
800             .          .          .     D39-36
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807             .          .          .          .------->  DCBR1
805             .          .          .      DCBR1
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                .          .          .          .
812             .          .          .          .------->  DCBR2
810             .          .          .      DCBR2
                .          .          .          .
                .          .          .          .
817             .          .          .          .          .<-------  D38-39
815             .          .          .          .     RD3839
                .          .          .          .          .
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818             .     C37-41.......................................
                .          V
                .          V
821             .     R39-36
                .          .
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824             .          .      SUB36
                .          .          .
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836             .          .          .------->     D36
834             .          .      DIV36
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841             .          .          .          .<-------   DCBR2
839             .          .          .     RDCBR2
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844             .          .          .          .          .<-------  D39-36
842             .          .          .          .     RD3936
                .          .          .          .          .
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845        C36-35.............................................
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850             .------->  D40ST
848        D40ST
                V
                V
853        R36-42
                .
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858             .      SUB42
                .          .
                .          .
870             .          .------->     D42
868             .      DIV42
                .          .
                .          .
873        C42-36............
```

(***) RUNOFF ALSO COMPUTED AT THIS LOCATION

```
1*****************************************
*                                       *
*  FLOOD HYDROGRAPH PACKAGE  (HEC-1)    *
*            MAY   1991                 *
*         VERSION 4.0.1E                *
*                                       *
*  RUN DATE  09/01/95  TIME  04:59:57   *
*                                       *
*****************************************
```

```
*****************************************
*                                       *
*    U.S. ARMY CORPS OF ENGINEERS       *
*    HYDROLOGIC ENGINEERING CENTER      *
*          609 SECOND STREET            *
*       DAVIS, CALIFORNIA 95616         *
*           (916) 551-1748              *
*                                       *
*****************************************
```

DDM MCUHP1 ARCADIA AREA 10-yr 6hr

```
4 IO          OUTPUT CONTROL VARIABLES
                    IPRNT          5  PRINT CONTROL
                    IPLOT          0  PLOT CONTROL
```

```
                QSCAL          0.  HYDROGRAPH PLOT SCALE

IT          HYDROGRAPH TIME DATA
                 NMIN            5  MINUTES IN COMPUTATION INTERVAL
                IDATE      1     0  STARTING DATE
                ITIME         0000  STARTING TIME
                   NQ          300  NUMBER OF HYDROGRAPH ORDINATES
               NDDATE      2     0  ENDING DATE
               NDTIME         0055  ENDING TIME
               ICENT           19  CENTURY MARK

            COMPUTATION INTERVAL    0.08 HOURS
                 TOTAL TIME BASE   24.92 HOURS

     ENGLISH UNITS
          DRAINAGE AREA          SQUARE MILES
          PRECIPITATION DEPTH    INCHES
          LENGTH, ELEVATION      FEET
          FLOW                   CUBIC FEET PER SECOND
          STORAGE VOLUME         ACRE-FEET
          SURFACE AREA           ACRES
          TEMPERATURE            DEGREES FAHRENHEIT
```

RUNOFF SUMMARY
FLOW IN CUBIC FEET PER SECOND
TIME IN HOURS, AREA IN SQUARE MILES

OPERATION	STATION	PEAK FLOW	TIME OF PEAK	AVERAGE FLOW FOR MAXIMUM PERIOD 6-HOUR	24-HOUR	72-HOUR	BASIN AREA	MAXIMUM STAGE	TIME OF MAX STAGE
HYDROGRAPH AT	SUB1	30.	4.08	5.	1.	1.	0.04		
ROUTED TO	R1-2	30.	4.25	5.	1.	1.	0.04		
HYDROGRAPH AT	SUB2	22.	4.33	4.	1.	1.	0.12		
DIVERSION TO	D2	8.	4.33	2.	0.	0.	0.12		
HYDROGRAPH AT	DIV2	14.	4.33	3.	1.	1.	0.12		
2 COMBINED AT	C1-2	43.	4.25	7.	2.	2.	0.16		
ROUTED TO	R2-3	42.	4.25	7.	2.	2.	0.16		
HYDROGRAPH AT	SUB3	18.	4.25	3.	1.	1.	0.07		
DIVERSION TO	D3	10.	4.25	2.	0.	0.	0.07		
HYDROGRAPH AT	DIV3	8.	4.25	1.	0.	0.	0.07		
2 COMBINED AT	C2-3	50.	4.25	9.	2.	2.	0.22		
ROUTED TO	R3-4	49.	4.33	9.	2.	2.	0.22		
HYDROGRAPH AT	SUB4	24.	4.17	4.	1.	1.	0.06		
DIVERSION TO	D4	13.	4.17	2.	1.	0.	0.06		
HYDROGRAPH AT	DIV4	11.	4.17	2.	0.	0.	0.06		
2 COMBINED AT	C3-4	60.	4.33	10.	3.	2.	0.29		

DIVERSION TO	DIBW	30.	4.33	7.	2.	2.	0.29
HYDROGRAPH AT	DIVIBW	30.	4.33	4.	1.	1.	0.29
ROUTED TO	R4-5	29.	4.42	4.	1.	1.	0.29
HYDROGRAPH AT	SUB5	14.	4.50	4.	1.	1.	0.07
DIVERSION TO	D5	7.	4.50	2.	0.	0.	0.07
HYDROGRAPH AT	DIV5	7.	4.50	2.	0.	0.	0.07
2 COMBINED AT	C4-5	36.	4.42	6.	1.	1.	0.35
HYDROGRAPH AT	SUB6	80.	4.00	12.	3.	3.	0.09
ROUTED TO	R6-7	78.	4.17	12.	3.	3.	0.09
HYDROGRAPH AT	SUB7	58.	4.25	10.	3.	2.	0.15
DIVERSION TO	D7	25.	4.25	4.	1.	1.	0.15
HYDROGRAPH AT	DIV7	33.	4.25	6.	1.	1.	0.15
2 COMBINED AT	C6-7	109.	4.17	17.	4.	4.	0.24
ROUTED TO	R7-8	107.	4.25	17.	4.	4.	0.24
HYDROGRAPH AT	SUB8	13.	4.42	3.	1.	1.	0.07
DIVERSION TO	D8	8.	4.42	2.	0.	0.	0.07
HYDROGRAPH AT	DIV8	5.	4.42	1.	0.	0.	0.07
2 COMBINED AT	C7-8	112.	4.25	19.	5.	5.	0.31
ROUTED TO	R8-9	110.	4.33	19.	5.	5.	0.31
HYDROGRAPH AT	SUB9	22.	4.17	3.	1.	1.	0.06
DIVERSION TO	D9	13.	4.17	2.	0.	0.	0.06
HYDROGRAPH AT	DIV9	9.	4.17	1.	0.	0.	0.06
2 COMBINED AT	C8-9	118.	4.33	20.	5.	5.	0.38
ROUTED TO	R9-5	118.	4.33	20.	5.	5.	0.38
2 COMBINED AT	C9-5	152.	4.33	26.	6.	6.	0.73
ROUTED TO	R5-10	137.	4.50	26.	6.	6.	0.73

HYDROGRAPH AT	SUB10	31.	4.25	5.	1.	1.	0.09
DIVERSION TO	D10	14.	4.25	2.	1.	1.	0.09
HYDROGRAPH AT	DIV10	17.	4.25	3.	1.	1.	0.09
2 COMBINED AT	C5-10	151.	4.50	28.	7.	7.	0.82
ROUTED TO	R10-15	127.	4.75	28.	7.	7.	0.82
HYDROGRAPH AT	SUB11	64.	4.08	10.	3.	2.	0.09
ROUTED TO	R11-12	63.	4.17	10.	3.	2.	0.09
HYDROGRAPH AT	SUB12	77.	4.08	8.	2.	2.	0.12
DIVERSION TO	D12	6.	4.08	1.	0.	0.	0.12
HYDROGRAPH AT	DIV12	71.	4.08	7.	2.	2.	0.12
2 COMBINED AT	C11-12	131.	4.08	17.	4.	4.	0.21
ROUTED TO	R12-13	126.	4.17	17.	4.	4.	0.21
HYDROGRAPH AT	SUB13	89.	4.08	10.	2.	2.	0.13
DIVERSION TO	D13	18.	4.08	2.	0.	0.	0.13
HYDROGRAPH AT	DIV13	71.	4.08	8.	2.	2.	0.13
2 COMBINED AT	C12-13	197.	4.08	25.	6.	6.	0.34
ROUTED TO	R13-14	191.	4.08	25.	6.	6.	0.34
HYDROGRAPH AT	SUB14	39.	4.17	5.	1.	1.	0.13
DIVERSION TO	D14	23.	4.17	3.	1.	1.	0.13
HYDROGRAPH AT	DIV14	15.	4.17	2.	1.	1.	0.13
2 COMBINED AT	C13-14	207.	4.17	27.	7.	7.	0.47
ROUTED TO	R14-15	206.	4.17	27.	7.	7.	0.47
HYDROGRAPH AT	SUB15	44.	4.25	7.	2.	2.	0.13
DIVERSION TO	D15	26.	4.25	4.	1.	1.	0.13
HYDROGRAPH AT	DIV15	18.	4.25	3.	1.	1.	0.13
3 COMBINED AT	C15-10	257.	4.25	58.	15.	14.	1.42
DIVERSION TO							

+	D56ST	0.	4.25	0.	0.	0.	1.42
HYDROGRAPH AT	D56ST	257.	4.25	58.	15.	14.	1.42
ROUTED TO	R15-20	128.	5.00	52.	15.	14.	1.42
HYDROGRAPH AT	SUB16	99.	4.08	16.	4.	4.	0.13
+ ROUTED TO	R16-17	98.	4.17	16.	4.	4.	0.13
HYDROGRAPH AT	SUB17	28.	4.08	3.	1.	1.	0.07
DIVERSION TO	D17	2.	4.08	0.	0.	0.	0.07
+ HYDROGRAPH AT	DIV17	26.	4.08	3.	1.	1.	0.07
2 COMBINED AT	C16-17	123.	4.17	19.	5.	5.	0.20
ROUTED TO	R17-18	123.	4.17	19.	5.	5.	0.20
+ HYDROGRAPH AT	SUB18	20.	4.17	3.	1.	1.	0.07
DIVERSION TO	D18	12.	4.17	2.	0.	0.	0.07
HYDROGRAPH AT	DIV18	8.	4.17	1.	0.	0.	0.07
+ 2 COMBINED AT	C17-18	130.	4.17	20.	5.	5.	0.27
ROUTED TO	R18-19	128.	4.17	20.	5.	5.	0.27
HYDROGRAPH AT	SUB19	20.	4.17	3.	1.	1.	0.08
DIVERSION TO	D19	12.	4.17	2.	0.	0.	0.08
HYDROGRAPH AT	DIV19	8.	4.17	1.	0.	0.	0.08
+ 2 COMBINED AT	C18-19	137.	4.17	22.	5.	5.	0.34
ROUTED TO	R19-20	134.	4.25	22.	5.	5.	0.34
HYDROGRAPH AT	SUB20	45.	4.17	6.	2.	2.	0.13
+ DIVERSION TO	D20	27.	4.17	4.	1.	1.	0.13
HYDROGRAPH AT	DIV20	18.	4.17	3.	1.	1.	0.13
3 COMBINED AT	C20-15	191.	4.25	73.	21.	20.	1.89
ROUTED TO	R20-25	61.	6.67	52.	21.	20.	1.89
+ HYDROGRAPH AT	SUB21	100.	4.08	15.	4.	4.	0.12
ROUTED TO	R21-22	98.	4.17	15.	4.	4.	0.12

HYDROGRAPH AT	SUB22	24.	4.25	4.	1.	1.	0.11
DIVERSION TO	D22	2.	4.25	0.	0.	0.	0.11
HYDROGRAPH AT	DIV22	23.	4.25	4.	1.	1.	0.11
2 COMBINED AT	C21-22	119.	4.17	19.	5.	5.	0.24
ROUTED TO	R22-23	117.	4.17	19.	5.	5.	0.24
HYDROGRAPH AT	SUB23	18.	4.08	2.	1.	1.	0.06
DIVERSION TO	D23	11.	4.08	1.	0.	0.	0.06
HYDROGRAPH AT	DIV23	7.	4.08	1.	0.	0.	0.06
2 COMBINED AT	C22-23	124.	4.17	20.	5.	5.	0.30
ROUTED TO	R23-24	123.	4.25	20.	5.	5.	0.30
HYDROGRAPH AT	SUB24	19.	4.17	3.	1.	1.	0.08
DIVERSION TO	D24	12.	4.17	2.	0.	0.	0.08
HYDROGRAPH AT	DIV24	8.	4.17	1.	0.	0.	0.08
2 COMBINED AT	C23-24	130.	4.25	22.	5.	5.	0.37
ROUTED TO	R24-25	130.	4.25	22.	5.	5.	0.37
HYDROGRAPH AT	SUB25	18.	4.25	3.	1.	1.	0.08
DIVERSION TO	D25	11.	4.25	2.	0.	0.	0.08
HYDROGRAPH AT	DIV25	7.	4.25	1.	0.	0.	0.08
3 COMBINED AT	C25-20	158.	4.25	69.	26.	25.	2.34
ROUTED TO	R25-29	126.	4.50	69.	26.	25.	2.34
HYDROGRAPH AT	SUB26	14.	4.17	2.	1.	1.	0.05
DIVERSION TO	D26	4.	4.17	1.	0.	0.	0.05
HYDROGRAPH AT	DIV26	9.	4.17	2.	0.	0.	0.05
ROUTED TO	R26-27	9.	4.17	2.	0.	0.	0.05
HYDROGRAPH AT	SUB27	17.	4.17	2.	1.	1.	0.06
DIVERSION TO	D27	10.	4.17	1.	0.	0.	0.06

HYDROGRAPH AT	DIV27	7.	4.17	1.	0.	0.	0.06
2 COMBINED AT	C26-27	16.	4.17	3.	1.	1.	0.11
ROUTED TO	R27-28	16.	4.25	3.	1.	1.	0.11
HYDROGRAPH AT	SUB28	21.	4.17	3.	1.	1.	0.08
DIVERSION TO	D28	12.	4.17	2.	0.	0.	0.08
HYDROGRAPH AT	DIV28	8.	4.17	1.	0.	0.	0.08
2 COMBINED AT	C27-28	24.	4.17	4.	1.	1.	0.19
ROUTED TO	R28-29	24.	4.25	4.	1.	1.	0.19
HYDROGRAPH AT	SUB29	14.	4.17	2.	1.	1.	0.06
DIVERSION TO	D29	8.	4.17	1.	0.	0.	0.06
HYDROGRAPH AT	DIV29	6.	4.17	1.	0.	0.	0.06
3 COMBINED AT	C29-25	147.	4.50	73.	28.	27.	2.59
DIVERSION TO	DOCCC	147.	0.08	73.	28.	27.	2.59
HYDROGRAPH AT	DOCCC	0.	0.08	0.	0.	0.	2.59
ROUTED TO	R29-33	0.	0.08	0.	0.	0.	2.59
HYDROGRAPH AT	SUB38	131.	4.33	26.	7.	6.	0.25
DIVERSION TO	D38-39	16.	4.33	9.	2.	2.	0.25
HYDROGRAPH AT	D38-39	115.	4.33	17.	4.	4.	0.25
ROUTED TO	R38-30	115.	4.33	17.	4.	4.	0.25
HYDROGRAPH AT	SUB30	19.	4.17	3.	1.	1.	0.06
2 COMBINED AT	C30-38	131.	4.25	19.	5.	5.	0.32
ROUTED TO	R30-31	131.	4.33	19.	5.	5.	0.32
HYDROGRAPH AT	SUB31	13.	4.17	2.	1.	1.	0.06
DIVERSION TO	D31	5.	4.17	1.	0.	0.	0.06
HYDROGRAPH AT	DIV31	8.	4.17	1.	0.	0.	0.06
2 COMBINED AT	C30-31	137.	4.33	21.	5.	5.	0.38
ROUTED TO							

	R31-32	137.	4.33	21.	5.	5.	0.38
HYDROGRAPH AT	SUB32	16.	4.17	3.	1.	1.	0.06
DIVERSION TO	D32	10.	4.17	2.	0.	0.	0.06
HYDROGRAPH AT	DIV32	6.	4.17	1.	0.	0.	0.06
2 COMBINED AT	C31-32	142.	4.33	22.	5.	5.	0.44
ROUTED TO	R32-33	140.	4.42	22.	5.	5.	0.44
HYDROGRAPH AT	SUB33	21.	4.17	3.	1.	1.	0.06
DIVERSION TO	D33	8.	4.17	1.	0.	0.	0.06
HYDROGRAPH AT	DIV33	13.	4.17	2.	1.	1.	0.06
3 COMBINED AT	C33-29	150.	4.33	24.	6.	6.	3.09
ROUTED TO	R33-35	84.	4.83	24.	6.	6.	3.09
HYDROGRAPH AT	SUB34	40.	4.25	8.	2.	2.	0.17
DIVERSION TO	D34	15.	4.25	3.	1.	1.	0.17
HYDROGRAPH AT	DIV34	25.	4.25	5.	1.	1.	0.17
ROUTED TO	R34-35	25.	4.33	5.	1.	1.	0.17
HYDROGRAPH AT	SUB35	65.	4.08	11.	3.	3.	0.13
DIVERSION TO	D35	6.	4.08	1.	0.	0.	0.13
HYDROGRAPH AT	DIV35	59.	4.08	10.	3.	2.	0.13
3 COMBINED AT	C35-33	117.	4.42	38.	10.	10.	3.39
ROUTED TO	R35-36	99.	5.00	38.	10.	10.	3.39
HYDROGRAPH AT	SUB40	36.	4.08	3.	1.	1.	0.07
ROUTED TO	R40-41	33.	4.17	3.	1.	1.	0.07
HYDROGRAPH AT	SUB41	51.	4.25	8.	2.	2.	0.16
2 COMBINED AT	C40-41	83.	4.17	12.	3.	3.	0.23
ROUTED TO	R41-39	81.	4.25	12.	3.	3.	0.23
HYDROGRAPH AT	SUB37	13.	4.17	1.	0.	0.	0.05
ROUTED TO	R37-39	13.	4.33	1.	0.	0.	0.05

HYDROGRAPH AT	SUB39	72.	4.33	17.	4.	4.	0.22
DIVERSION TO	D39-36	0.	4.33	0.	0.	0.	0.22
HYDROGRAPH AT	D39-36	72.	4.33	17.	4.	4.	0.22
DIVERSION TO	DCBR1	55.	4.33	16.	4.	4.	0.22
HYDROGRAPH AT	DCBR1	17.	4.33	1.	0.	0.	0.22
DIVERSION TO	DCBR2	17.	0.08	1.	0.	0.	0.22
HYDROGRAPH AT	DCBR2	0.	0.08	0.	0.	0.	0.22
HYDROGRAPH AT	RD3839	16.	3.58	9.	2.	2.	0.00
4 COMBINED AT	C37-41	108.	4.25	23.	6.	6.	0.50
ROUTED TO	R39-36	105.	4.33	23.	6.	6.	0.50
HYDROGRAPH AT	SUB36	37.	4.25	8.	2.	2.	0.09
DIVERSION TO	D36	6.	4.25	1.	0.	0.	0.09
HYDROGRAPH AT	DIV36	31.	4.25	7.	2.	2.	0.09
HYDROGRAPH AT	RDCBR2	17.	4.33	1.	0.	0.	0.00
HYDROGRAPH AT	RD3936	0.	0.08	0.	0.	0.	0.00
5 COMBINED AT	C36-35	211.	4.33	67.	18.	17.	3.98
DIVERSION TO	D40ST	201.	1.58	57.	14.	14.	3.98
HYDROGRAPH AT	D40ST	10.	1.58	10.	3.	3.	3.98
ROUTED TO	R36-42	10.	5.50	10.	3.	3.	3.98
HYDROGRAPH AT	SUB42	103.	4.25	18.	5.	4.	0.21
DIVERSION TO	D42	7.	4.25	1.	0.	0.	0.21
HYDROGRAPH AT	DIV42	96.	4.25	17.	4.	4.	0.21
2 COMBINED AT	C42-36	106.	4.25	27.	8.	7.	4.19

SUMMARY OF KINEMATIC WAVE - MUSKINGUM-CUNGE ROUTING
(FLOW IS DIRECT RUNOFF WITHOUT BASE FLOW)

ISTAQ	ELEMENT	DT (MIN)	PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	INTERPOLATED TO COMPUTATION INTERVAL DT (MIN)	PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)

```
R1-2  MANE        5.12    29.86   255.56     1.19     5.00    29.83   255.00       1.19

ONTINUITY SUMMARY (AC-FT) - INFLOW=0.2317E+01 EXCESS=0.0000E+00 OUTFLOW=0.2339E+01 BASIN STORAGE=0.2955E-05 PERCENT ERROR=  -0.9

R2-3  MANE        1.45    43.23   257.99     0.44     5.00    42.18   255.00       0.44

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.3655E+01 EXCESS=0.0000E+00 OUTFLOW=0.3660E+01 BASIN STORAGE=0.4521E-04 PERCENT ERROR=  -0.1

R3-4  MANE        1.25    49.76   257.74     0.36     5.00    49.35   260.00       0.36

ONTINUITY SUMMARY (AC-FT) - INFLOW=0.4313E+01 EXCESS=0.0000E+00 OUTFLOW=0.4316E+01 BASIN STORAGE=0.7821E-04 PERCENT ERROR=  -0.1

R4-5  MANE        3.13    29.49   266.69     0.12     5.00    29.44   265.00       0.12

ONTINUITY SUMMARY (AC-FT) - INFLOW=0.1804E+01 EXCESS=0.0000E+00 OUTFLOW=0.1829E+01 BASIN STORAGE=0.9862E-04 PERCENT ERROR=  -1.4

R6-7  MANE        4.21    77.69   250.70     1.20     5.00    77.60   250.00       1.20

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.5728E+01 EXCESS=0.0000E+00 OUTFLOW=0.5763E+01 BASIN STORAGE=0.3073E-05 PERCENT ERROR=  -0.6

R7-8  MANE        3.05   108.33   256.54     0.67     5.00   106.68   255.00       0.67

ONTINUITY SUMMARY (AC-FT) - INFLOW=0.8700E+01 EXCESS=0.0000E+00 OUTFLOW=0.8733E+01 BASIN STORAGE=0.3825E-03 PERCENT ERROR=  -0.4

R8-9  MANE        0.72   111.31   256.96     0.56     5.00   110.11   260.00       0.56

ONTINUITY SUMMARY (AC-FT) - INFLOW=0.9358E+01 EXCESS=0.0000E+00 OUTFLOW=0.9362E+01 BASIN STORAGE=0.1244E-03 PERCENT ERROR=   0.0

R9-5  MANE        1.35   117.65   260.62     0.50     5.00   117.60   260.00       0.50

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.1006E+02 EXCESS=0.0000E+00 OUTFLOW=0.1006E+02 BASIN STORAGE=0.4150E-03 PERCENT ERROR=  -0.1

R11-12  MANE      1.50    63.53   248.96     1.01     5.00    63.33   250.00       1.01

ONTINUITY SUMMARY (AC-FT) - INFLOW=0.5003E+01 EXCESS=0.0000E+00 OUTFLOW=0.5008E+01 BASIN STORAGE=0.3009E-07 PERCENT ERROR=  -0.1

R12-13  MANE      0.08   130.23   247.18     0.76     5.00   126.42   250.00       0.76

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.8613E+01 EXCESS=0.0000E+00 OUTFLOW=0.8615E+01 BASIN STORAGE=0.1763E-04 PERCENT ERROR=   0.0

R13-14  MANE      0.72   196.22   246.73     0.69     5.00   191.12   245.00       0.69

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.1251E+02 EXCESS=0.0000E+00 OUTFLOW=0.1253E+02 BASIN STORAGE=0.4645E-04 PERCENT ERROR=  -0.1

R14-15  MANE      1.14   206.40   250.26     0.55     5.00   206.39   250.00       0.54

ONTINUITY SUMMARY (AC-FT) - INFLOW=0.1360E+02 EXCESS=0.0000E+00 OUTFLOW=0.1362E+02 BASIN STORAGE=0.2039E-03 PERCENT ERROR=  -0.1

R16-17  MANE      1.26    99.18   247.90     1.16     5.00    97.94   250.00       1.16

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.7951E+01 EXCESS=0.0000E+00 OUTFLOW=0.7960E+01 BASIN STORAGE=0.3775E-07 PERCENT ERROR=  -0.1

R17-18  MANE      0.73   123.15   251.44     0.88     5.00   122.58   250.00       0.88
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ONTINUITY SUMMARY (AC-FT) - INFLOW=0.9499E+01 EXCESS=0.0000E+00 OUTFLOW=0.9507E+01 BASIN STORAGE=0.8525E-05 PERCENT ERROR=  -0.1

          R18-19  MANE        0.77    129.87    251.81      0.71      5.00    128.46    250.00        0.71

 CONTINUITY SUMMARY (AC-FT) - INFLOW=0.1014E+02 EXCESS=0.0000E+00 OUTFLOW=0.1015E+02 BASIN STORAGE=0.2370E-04 PERCENT ERROR=  -0.1

          R19-20  MANE        0.87    136.15    251.61      0.59      5.00    133.74    255.00        0.59

 ONTINUITY SUMMARY (AC-FT) - INFLOW=0.1077E+02 EXCESS=0.0000E+00 OUTFLOW=0.1078E+02 BASIN STORAGE=0.5153E-04 PERCENT ERROR=  -0.1

          R21-22  MANE        2.84     98.77    251.48      1.14      5.00     98.09    250.00        1.14

 ONTINUITY SUMMARY (AC-FT) - INFLOW=0.7538E+01 EXCESS=0.0000E+00 OUTFLOW=0.7563E+01 BASIN STORAGE=0.6540E-06 PERCENT ERROR=  -0.3

          R22-23  MANE        0.51    118.81    251.33      0.77      5.00    117.09    250.00        0.77

 CONTINUITY SUMMARY (AC-FT) - INFLOW=0.9660E+01 EXCESS=0.0000E+00 OUTFLOW=0.9663E+01 BASIN STORAGE=0.3678E-05 PERCENT ERROR=   0.0

          R23-24  MANE        0.58    124.03    251.55      0.64      5.00    122.65    255.00        0.64

 ONTINUITY SUMMARY (AC-FT) - INFLOW=0.1017E+02 EXCESS=0.0000E+00 OUTFLOW=0.1018E+02 BASIN STORAGE=0.1162E-04 PERCENT ERROR=   0.0

          R24-25  MANE        0.86    130.02    255.96      0.54      5.00    129.88    255.00        0.54

 ONTINUITY SUMMARY (AC-FT) - INFLOW=0.1082E+02 EXCESS=0.0000E+00 OUTFLOW=0.1083E+02 BASIN STORAGE=0.5241E-04 PERCENT ERROR=  -0.1

          R26-27  MANE        1.54      9.39    253.29      0.31      5.00      9.30    250.00        0.31

 CONTINUITY SUMMARY (AC-FT) - INFLOW=0.8650E+00 EXCESS=0.0000E+00 OUTFLOW=0.8663E+00 BASIN STORAGE=0.4718E-05 PERCENT ERROR=  -0.1

          R27-28  MANE        1.57     16.01    253.52      0.23      5.00     15.72    255.00        0.23

 ONTINUITY SUMMARY (AC-FT) - INFLOW=0.1368E+01 EXCESS=0.0000E+00 OUTFLOW=0.1370E+01 BASIN STORAGE=0.1754E-04 PERCENT ERROR=  -0.1

          R28-29  MANE        1.32     23.63    253.34      0.20      5.00     23.57    255.00        0.20

 ONTINUITY SUMMARY (AC-FT) - INFLOW=0.2007E+01 EXCESS=0.0000E+00 OUTFLOW=0.2009E+01 BASIN STORAGE=0.3101E-04 PERCENT ERROR=  -0.1

          R38-30  MANE        0.46    115.45    260.41      0.62      5.00    115.45    260.00        0.62

 CONTINUITY SUMMARY (AC-FT) - INFLOW=0.8266E+01 EXCESS=0.0000E+00 OUTFLOW=0.8271E+01 BASIN STORAGE=0.1684E-05 PERCENT ERROR=  -0.1

          R30-31  MANE        0.71    130.57    256.83      0.57      5.00    130.55    260.00        0.57

 ONTINUITY SUMMARY (AC-FT) - INFLOW=0.9565E+01 EXCESS=0.0000E+00 OUTFLOW=0.9571E+01 BASIN STORAGE=0.6502E-05 PERCENT ERROR=  -0.1

          R31-32  MANE        0.63    136.86    260.55      0.51      5.00    136.65    260.00        0.51

 ONTINUITY SUMMARY (AC-FT) - INFLOW=0.1024E+02 EXCESS=0.0000E+00 OUTFLOW=0.1024E+02 BASIN STORAGE=0.1268E-04 PERCENT ERROR=  -0.1

          R32-33  MANE        1.75    142.07    263.47      0.46      5.00    140.42    265.00        0.46
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CONTINUITY SUMMARY (AC-FT) - INFLOW=0.1078E+02 EXCESS=0.0000E+00 OUTFLOW=0.1079E+02 BASIN STORAGE=0.7930E-05 PERCENT ERROR=  -0.1

          R34-35  MANE        1.37     25.33    258.78      0.30      5.00     25.21    260.00       0.30

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.2663E+01 EXCESS=0.0000E+00 OUTFLOW=0.2666E+01 BASIN STORAGE=0.1271E-04 PERCENT ERROR=  -0.1

          R40-41  MANE        1.59     35.40    248.29      0.42      5.00     33.32    250.00       0.42

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.1646E+01 EXCESS=0.0000E+00 OUTFLOW=0.1653E+01 BASIN STORAGE=0.2684E-06 PERCENT ERROR=  -0.4

          R41-39  MANE        2.31     81.10    255.73      0.48      5.00     81.05    255.00       0.48

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.5889E+01 EXCESS=0.0000E+00 OUTFLOW=0.5896E+01 BASIN STORAGE=0.1671E-05 PERCENT ERROR=  -0.1

          R37-39  MANE        4.96     12.94    257.79      0.28      5.00     12.51    260.00       0.28

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.7106E+00 EXCESS=0.0000E+00 OUTFLOW=0.7236E+00 BASIN STORAGE=0.1983E-03 PERCENT ERROR=  -1.9

          R39-36  MANE        0.95    107.48    256.92      0.42      5.00    105.30    260.00       0.42

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.1136E+02 EXCESS=0.0000E+00 OUTFLOW=0.1136E+02 BASIN STORAGE=0.1130E-03 PERCENT ERROR=   0.0


*** NORMAL END OF HEC-1 ***
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A-2

HEC-1 MODEL 25-YEAR EXISTING CONDITIONS

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1****************************************
*                                      *
*  FLOOD HYDROGRAPH PACKAGE  (HEC-1)   *
*            MAY   1991                *
*         VERSION 4.0.1E               *
*                                      *
*  RUN DATE  09/01/95  TIME  05:20:25  *
*                                      *
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****************************************
*                                      *
*   U.S. ARMY CORPS OF ENGINEERS       *
*   HYDROLOGIC ENGINEERING CENTER      *
*         609 SECOND STREET            *
*      DAVIS, CALIFORNIA 95616         *
*          (916) 551-1748              *
*                                      *
****************************************
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X     X  XXXXXXX   XXXXX          X
X     X  X        X     X        XX
X     X  X        X              X
XXXXXXX  XXXX     X        XXXXX X
X     X  X        X              X
X     X  X        X     X        X
X     X  XXXXXXX   XXXXX        XXX
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THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE.
THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION
NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,
DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION
KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

HEC-1 INPUT PAGE 1

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LINE          ID.......1.......2.......3.......4.......5.......6.......7.......8.......9......10

              *       ARCADIA AREA HYDROLOGY STUDY - EXISTING CONDITIONS.
              *       PREPARED BY: HUITT-ZOLLARS INC. 8-31-95
              *       PREPARED FOR: FCDMC CONTRACT # 94-21
    1         ID
    2         ID   DDM MCUHP1 ARCADIA AREA 25-yr 6hr
    3         IT       5                    300
    4         IO       5
              *DIAGRAM
              *

    5         KK    SUB1
    6         KM   SUB-BASIN SUB1
    7         KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
    8         KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
    9         KM     L =  .28  Kb = .100  Adj. Slope = 2120.0
   10         BA    .037
   11         IN      15
   12         KM   RAINFALL DEPTH OF 2.00 WAS SPACIALLY REDUCED AS SHOWN BY THE PB RECORD
   13         PB   2.388
   14         KM   THE FOLLOWING PC RECORD USED A 6-HOUR STORM WITH A PATTERN No. OF 2.20
   15         PC    .000    .010    .017    .026    .037    .046    .056    .065    .075    .085
   16         PC    .097    .111    .131    .175    .263    .455    .689    .829    .893    .933
   17         PC    .949    .962    .975    .988   1.000
   18         LG    .142    .322   4.550    .310  52.000
   19         UC    .150    .107
   20         UA       0       3       5       8      12      20      43      75      90      96
   21         UA     100
              *

   22         KK    R1-2
   23         KM        ROUTE FLOW FROM SUB1 TO SUB2
   24         RK  3183.8   .0166     .07       0    TRAP       0       3     YES
              *

   25         KK    SUB2
   26         KM   SUB-BASIN SUB2
   27         KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
   28         KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
   29         KM     L =  .60  Kb = .041  Adj. Slope =   88.0
   30         BA    .119
   31         LG    .342    .250   4.650    .440   9.000
```

```
 32          UC    .596    .466
 33          UA       0       5      16      30      65      77      84      90      94      97
 34          UA     100
             *

 35          KK    DIV2
 36          KM        DIVERT FOR IRRIGATED LAWNS SUB2
 37          DT      D2     .80
 38          DI       0       1
 39          DQ       0    .382
             *
```



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LINE         ID.......1.......2.......3.......4.......5.......6.......7.......8.......9......10

 40          KK    C1-2
 41          KM        COMBINE HYDROGRAPHS SUB1 AND SUB2 AT CP2
 42          HC       2
             *

 43          KK    R2-3
 44          KM        ROUTE FLOW FROM SUB2 TO SUB3
 45          RK  1367.5    .009    .016            TRAP      60       1     YES
             *

 46          KK    SUB3
 47          KM   SUB-BASIN SUB3
 48          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
 49          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
 50          KM     L =  .26  Kb = .058  Adj. Slope =   47.0
 51          BA    .067
 52          LG    .298    .250   4.250    .510  16.000
 53          UC    .533    .293
 54          UA       0       5      16      30      65      77      84      90      94      97
 55          UA     100
             *

 56          KK    DIV3
 57          KM        DIVERT FOR IRRIGATED LAWNS SUB3
 58          DT      D3     .88
 59          DI       0       1
 60          DQ       0    .573
             *

 61          KK    C2-3
 62          KM        COMBINE HYDROGRAPHS SUB2 & SUB3 AT CP3
 63          HC       2
             *

 64          KK    R3-4
 65          KM        ROUTE FLOW FROM CP3 TO CP4
 66          RK    1320    .008    .016            TRAP      44       1     YES
             *

 67          KK    SUB4
 68          KM   SUB-BASIN SUB4
 69          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
 70          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
 71          KM     L =  .25  Kb = .058  Adj. Slope =   42.0
 72          BA    .065
 73          LG    .300    .250   4.800    .360  15.000
 74          UC    .467    .249
 75          UA       0       5      16      30      65      77      84      90      94      97
 76          UA     100
             *
```



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LINE         ID.......1.......2.......3.......4.......5.......6.......7.......8.......9......10

 77          KK    DIV4
 78          KM        DIVERT FOR IRRIGATED LAWNS SUB4
 79          DT      D4     1.0
 80          DI       0       1
 81          DQ       0     .55
             *

 82          KK    C3-4
```

```
 83          KM        COMBINE HYDROGRAPHS SUB3 & SUB4 AT CP4
 84          HC       2
             *

 85          KK  DIVIBW
 86          KM        DIVERT LAFAYETTE DRAIN INTERCETION TO INDIAN BEND WASH
 87          DT    DIBW
 88          DI      25      63     101     193     241     306
 89          DQ    12.5    31.5    50.5    96.5     121    55.1
             *

 90          KK    R4-5
 91          KM        ROUTE FLOW FROM CP4 TO CP5
 92          RK  2307.4    .005    .016            TRAP      44       1     YES
             *

 93          KK    SUB5
 94          KM   SUB-BASIN SUB5
 95          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
 96          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
 97          KM     L =  .44  Kb = .058  Adj. Slope =   24.0
 98          BA    .067
 99          LG    .300    .250   4.800    .360  15.000
100          UC    .846    .744
101          UA       0       5      16      30      65      77      84      90      94      97
102          UA     100
             *

103          KK    DIV5
104          KM        DIVERT FOR IRRIGATED LAWNS SUB5
105          DT      D5     .94
106          DI       0       1
107          DQ       0     .50
             *

108          KK    C4-5
109          KM        COMBINE HYDROGRAPHS SUB4 & SUB5 AT CP5
110          HC       2
             *

111          KK    SUB6
112          KM   SUB-BASIN SUB6
113          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
114          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
115          KM     L =  .26  Kb = .102  Adj. Slope = 2367.0
116          BA    .090
```



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LINE         ID.......1.......2.......3.......4.......5.......6.......7.......8.......9......10

117          LG    .113    .341   4.700    .250  50.000
118          UC    .142    .057
119          UA       0       3       5       8      12      20      43      75      90      96
120          UA     100
             *

121          KK    R6-7
122          KM        ROUTE FLOW FROM SUB6 TO SUB7
123          RK  2972.0    .013     .07            TRAP       0       3     YES
             *

124          KK    SUB7
125          KM   SUB-BASIN SUB7
126          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
127          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
128          KM     L =  .56  Kb = .052  Adj. Slope =   71.0
129          BA    .153
130          LG    .295    .269   5.400    .280  18.000
131          UC    .546    .346
132          UA       0       5      16      30      65      77      84      90      94      97
133          UA     100
             *

134          KK    DIV7
135          KM        DIVERT FOR IRRIGATED LAWNS SUB7
136          DT      D7    2.30
137          DI       0       1
138          DQ       0    .427
             *
```

```
139          KK    C6-7
140          KM        COMBINE HYDROGRAPHS SUB6 & SUB7 AT CP7
141          HC       2
             *

142          KK    R7-8
143          KM        ROUTE FLOW FROM SUB7 TO SUB8
144          RK  2302.1    .001    .016            TRAP      40       1     YES
             *

145          KK    SUB8
146          KM   SUB-BASIN SUB8
147          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
148          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
149          KM     L =  .44  Kb = .057  Adj. Slope =   52.0
150          BA    .068
151          LG    .300    .250   4.350    .480  15.000
152          UC    .696    .594
153          UA       0       5      16      30      65      77      84      90      94      97
154          UA     100
             *
1                                          HEC-1 INPUT                                          PAGE  5

LINE         ID.......1.......2.......3.......4.......5.......6.......7.......8.......9......10

155          KK    DIV8
156          KM        DIVERT FOR IRRIGATED LAWNS SUB8
157          DT      D8     .99
158          DI       0       1
159          DQ       0      .6
             *

160          KK    C7-8
161          KM        COMBINE HYDROGRAPHS SUB7 & SUB8 AT CP8
162          HC       2
             *

163          KK    R8-9
164          KM        ROUTE FLOW FROM SUB8 TO SUB9
165          RK  1314.7    .010    .016            TRAP      20       1     YES
             *

166          KK    SUB9
167          KM   SUB-BASIN SUB9
168          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
169          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
170          KM     L =  .25  Kb = .058  Adj. Slope =   55.0
171          BA    .065
172          LG    .300    .250   4.500    .430  15.000
173          UC    .454    .241
174          UA       0       5      16      30      65      77      84      90      94      97
175          UA     100
             *

176          KK    DIV9
177          KM        DIVERT FOR IRRIGATED LAWNS SUB9
178          DT      D9     .94
179          DI       0       1
180          DQ       0      .6
             *

181          KK    C8-9
182          KM        COMBINE HYDROGRAPHS SUB8 & SUB9   AT CP9
183          HC       2
             *

184          KK    R9-5
185          KM        ROUTE FLOW FROM SUB9 TO  SUB5
186          RK  1784.7    .007    .016            TRAP      40       1     YES
             *

187          KK    C9-5
188          KM        COMBINE HYDROGRAPH SUB9  & SUB5  AT CP5
189          HC       2
             *
             *      3       0
             *
```

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LINE          ID.......1.......2.......3.......4.......5.......6.......7.......8.......9......10

 190          KK   R5-10
 191          KM        ROUTE FLOW ALONG CHANNEL FROM SUB5 TO  SUB10
 192          RS       1    FLOW      -1
 193          SV       0       1       3      13      50     110     162
 194          SQ       0      75     250     500    1200    2400    4000
              *

 195          KK   SUB10
 196          KM   SUB-BASIN SUB10
 197          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
 198          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
 199          KM     L =  .34  Kb = .056  Adj. Slope =   37.0
 200          BA    .093
 201          LG    .299    .250   4.800    .360  15.000
 202          UC    .579    .330
 203          UA       0       5      16      30      65      77      84      90      94      97
 204          UA     100
              *

 205          KK   DIV10
 206          KM        DIVERT FOR IRRIGATED LAWNS SUB10
 207          DT     D10    1.17
 208          DI       0       1
 209          DQ       0    .445
              *

 210          KK   C5-10
 211          KM        COMBINE HYDROGRAPH SUB5  & SUB10 AT CP10
 212          HC       2
              *
              *      3       0
              *

 213          KK  R10-15
 214          KM        ROUTE FLOW ALONG CHANNEL FROM SUB10 TO SUB15
 215          RS       1    FLOW      -1
 216          SV       0       2       5       8      46     156     247
 217          SQ       0      75     250     500    1200    2400    4000
              *

 218          KK   SUB11
 219          KM   SUB-BASIN SUB11
 220          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
 221          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
 222          KM     L =  .56  Kb = .106  Adj. Slope = 1740.0
 223          BA    .093
 224          LG    .115    .350   4.550    .270  39.000
 225          UC    .237    .183
 226          UA       0       3       5       8      12      20      43      75      90      96
 227          UA     100
              *
```



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LINE          ID.......1.......2.......3.......4.......5.......6.......7.......8.......9......10

 228          KK  R11-12
 229          KM        ROUTE FLOW FROM SUB11 TO   SUB12
 230          RK    1632    .058     .07            TRAP       0       3     YES
              *

 231          KK   SUB12
 232          KM   SUB-BASIN SUB12
 233          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
 234          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
 235          KM     L =  .31  Kb = .064  Adj. Slope =  304.0
 236          BA    .120
 237          LG    .269    .279   5.700    .200   9.000
 238          UC    .246    .102
 239          UA       0       5      16      30      65      77      84      90      94      97
 240          UA     100
              *

 241          KK   DIV12
```

```
242          KM        DIVERT FOR IRRIGATED LAWNS SUB12
243          DT     D12     .31
244          DI       0       1
245          DQ       0    .079
             *

246          KK  C11-12
247          KM        COMBINE HYDROGRAPH SUB11 & SUB12 AT CP12
248          HC       2
             *

249          KK  R12-13
250          KM        ROUTE FLOW FROM SUB12 TO SUB13
251          RK  1362.2    .020    .016            TRAP      60       1     YES      50
             *

252          KK   SUB13
253          KM   SUB-BASIN SUB13
254          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
255          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
256          KM     L =  .26  Kb = .054  Adj. Slope =  107.0
257          BA    .129
258          LG    .300    .230   6.200    .200  15.000
259          UC    .283    .100
260          UA       0       5      16      30      65      77      84      90      94      97
261          UA     100
             *

262          KK   DIV13
263          KM        DIVERT FOR IRRIGATED LAWNS SUB13
264          DT     D13     .98
265          DI       0       1
266          DQ       0      .2
             *
                                          HEC-1 INPUT                                          PAGE  8

LINE         ID.......1.......2.......3.......4.......5.......6.......7.......8.......9......10

267          KK  C12-13
268          KM        COMBINE HYDROGRAPHS SUB12 & SUB13 AT CP13
269          HC       2
             *

270          KK  R13-14
271          KM        ROUTE FL OW FROM SUB13 TO SUB14
272          RK  1314.7    .014    .016            TRAP      60       1     YES
             *

273          KK   SUB14
274          KM   SUB-BASIN SUB14
275          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
276          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
277          KM     L =  .25  Kb = .054  Adj. Slope =   74.0
278          BA    .126
279          LG    .300    .250   4.100    .550  15.000
280          UC    .433    .157
281          UA       0       5      16      30      65      77      84      90      94      97
282          UA     100
             *

283          KK   DIV14
284          KM        DIVERT FOR IRRIGATED LAWNS SUB14
285          DT     D14    1.57
286          DI       0       1
287          DQ       0      .6
             *

288          KK  C13-14
289          KM        COMBINE HYDROGRAPHS SUB13 & SUB14 AT CP14
290          HC       2
             *

291          KK  R14-15
292          KM        ROUTE FLOW FROM SUB 14 TO SUB15
293          RK  1985.3    .011    .016            TRAP      60       1     YES
             *

294          KK   SUB15
```

```
295          KM   SUB-BASIN SUB15
296          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
297          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
298          KM     L =  .38  Kb = .054  Adj. Slope =   56.0
299          BA    .126
300          LG    .297    .250   4.650    .390  16.000
301          UC    .529    .274
302          UA      0       5      16      30      65      77      84      90      94      97
303          UA    100
             *
1                                        HEC-1 INPUT                                          PAGE  9

LINE         ID.......1.......2.......3.......4.......5.......6.......7.......8.......9......10


304          KK   DIV15
305          KM        DIVERT FOR IRRIGATED LAWNS SUB15
306          DT     D15    2.05
307          DI       0       1
308          DQ       0    .585
             *

309          KK  C15-10
310          KM        COMBINE SUB14, SUB10 WITH SUB15
311          HC       3
             *      1       2
             *

312          KK   D56ST
313          KM        DIVERT FLOW THAT CROSSES 56TH ST. BRIDGE
314          DT   D56ST
315          DI       0     400     650     790    1040    1139    1334    1484    1689    1900
316          DQ       0       0     240     318     400     489     584     684     789     900
             *
             *      3       0
             *

317          KK  R15-20
318          KM        ROUTE FLOW ALONG CHANNEL FROM SUB15 TO SUB20
319          RS       1    FLOW      -1
320          SV       0      14      18      25      35      72     111
321          SQ       0      75     250     500    1200    2400    4000
             *

322          KK   SUB16
323          KM   SUB-BASIN SUB16
324          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
325          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
326          KM     L =  .65  Kb = .102  Adj. Slope = 2052.0
327          BA    .129
328          LG    .104    .350   4.700    .240  47.000
329          UC    .233    .167
330          UA      0       3       5       8      12      20      43      75      90      96
331          UA    100
             *

332          KK  R16-17
333          KM        ROUTE FLOW FROM SUB16 TO SUB17
334          RK    1668    .058     .07            TRAP       0       3     YES
             *

335          KK   SUB17
336          KM   SUB-BASIN SUB17
337          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
338          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
339          KM     L =  .32  Kb = .058  Adj. Slope =  183.0
340          BA    .073
341          LG    .298    .252   4.350    .400  10.000
342          UC    .329    .193
                                         HEC-1 INPUT                                          PAGE 10

LINE         ID.......1.......2.......3.......4.......5.......6.......7.......8.......9......10

343          UA      0       5      16      30      65      77      84      90      94      97
344          UA    100
             *

345          KK   DIV17
346          KM        DIVERT FOR IRRIGATED LAWNS SUB17
```

```
347          DT     D17     .11
348          DI       0       1
349          DQ       0    .074
             *

350          KK  C16-17
351          KM        COMBINE HYDROGRAPH SUB16 & SUB17 AT CP17
352          HC       2
             *

353          KK  R17-18
354          KM        ROUTE FLOW FROM SUB17 TO SUB18
355          RK  1378.1    .019    .016            TRAP      40       1     YES
             *

356          KK   SUB18
357          KM   SUB-BASIN SUB18
358          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
359          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
360          KM     L =  .26  Kb = .058  Adj. Slope =  102.0
361          BA    .067
362          LG    .300    .250   4.150    .530  15.000
363          UC    .404    .215
364          UA       0       5      16      30      65      77      84      90      94      97
365          UA     100
             *

366          KK   DIV18
367          KM        DIVERT FOR IRRIGATED LAWNS SUB18
368          DT     D18     .81
369          DI       0       1
370          DQ       0      .6
             *

371          KK  C17-18
372          KM        COMBINE  HYDROGRAPH SUB17 & SUB18 AT CP18
373          HC       2
             *

374          KK  R18-19
375          KM        ROUTE FLOW SUB18 TO SUB19
376          RK  1335.8    .014    .016            TRAP      40       1     YES
             *
```



```
LINE         ID.......1.......2.......3.......4.......5.......6.......7.......8.......9......10

377          KK   SUB19
378          KM   SUB-BASIN SUB19
379          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
380          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
381          KM     L =  .25  Kb = .057  Adj. Slope =   77.0
382          BA    .075
383          LG    .300    .250   3.950    .580  15.000
384          UC    .450    .220
385          UA       0       5      16      30      65      77      84      90      94      97
386          UA     100
             *

387          KK   DIV19
388          KM        DIVERT FOR IRRIGATED LAWNS SUB19
389          DT     D19     .91
390          DI       0       1
391          DQ       0      .6
             *

392          KK  C18-19
393          KM        COMBINE HYDROGRAPH SUB18 & SUB19 AT CP19
394          HC       2
             *

395          KK  R19-20
396          KM        ROUTE FLOW FROM SUB19 TO SUB20
397          RK  1473.1    .010    .016            TRAP      30       1     YES
             *

398          KK   SUB20
399          KM   SUB-BASIN SUB20
```

```
400          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
401          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
402          KM     L =  .28  Kb = .054  Adj. Slope =   54.0
403          BA    .129
404          LG    .300    .250   4.450    .450  15.000
405          UC    .479    .190
406          UA       0       5      16      30      65      77      84      90      94      97
407          UA     100
             *

408          KK   DIV20
409          KM        DIVERT FOR IRRIGATED LAWNS SUB20
410          DT     D20    1.86
411          DI       0       1
412          DQ       0      .6
             *

413          KK  C20-15
414          KM        COMBINE SUB19, SUB15 WITH SUB20
415          HC       3
             *      1       2
             *
             *      3       0
             *
                                          HEC-1 INPUT                                          PAGE 12

LINE         ID.......1.......2.......3.......4.......5.......6.......7.......8.......9......10

416          KK  R20-25
417          KM        ROUTE FLOW ALONG CHANNEL FROM SUB20 TO SUB25
418          RS       1    FLOW      -1
419          SV       0      23      27      35      37      84     122
420          SQ       0      75     250     500    1200    2400    4000
             *

421          KK   SUB21
422          KM   SUB-BASIN SUB21
423          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
424          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
425          KM     L =  .56  Kb = .102  Adj. Slope = 2352.0
426          BA    .124
427          LG    .104    .350   4.700    .240  46.000
428          UC    .208    .134
429          UA       0       3       5       8      12      20      43      75      90      96
430          UA     100
             *

431          KK  R21-22
432          KM        ROUTE FLOW FROM SUB21 TO SUB22
433          RK    2735    .026     .07            TRAP       0       3     YES
             *

434          KK   SUB22
435          KM   SUB-BASIN SUB22
436          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
437          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
438          KM     L =  .52  Kb = .060  Adj. Slope =  134.0
439          BA    .112
440          LG    .281    .266   4.000    .480  11.000
441          UC    .571    .410
442          UA       0       5      16      30      65      77      84      90      94      97
443          UA     100
             *

444          KK   DIV22
445          KM        DIVERT FOR IRRIGATED LAWNS SUB22
446          DT     D22     .12
447          DI       0       1
448          DQ       0    .063
             *

449          KK  C21-22
450          KM        COMBINE HYDROGRAPH SUB21 & SUB22 AT CP22
451          HC       2
             *

452          KK  R22-23
453          KM        ROUTE FLOW FROM SUB22 TO SUB23
```

```
454          RK  1240.8    .025    .016            TRAP      20       1     YES
             *
```



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LINE         ID.......1.......2.......3.......4.......5.......6.......7.......8.......9......10

455          KK   SUB23
456          KM   SUB-BASIN SUB23
457          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
458          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
459          KM     L =  .23  Kb = .058  Adj. Slope =  132.0
460          BA    .060
461          LG    .300    .250   3.950    .580  15.000
462          UC    .350    .177
463          UA       0       5      16      30      65      77      84      90      94      97
464          UA     100
             *

465          KK   DIV23
466          KM        DIVERT FOR IRRIGATED LAWNS SUB23
467          DT     D23     .72
468          DI       0       1
469          DQ       0    .593
             *

470          KK  C22-23
471          KM        COMBINE HYDROGRAPH SUB22 & SUB23 AT CP23
472          HC       2
             *

473          KK  R23-24
474          KM        ROUTE FLOW FROM SUB 23 TO SUB24
475          RK  1088.9    .015    .016            TRAP      32       1     YES      25
             *

476          KK   SUB24
477          KM   SUB-BASIN SUB24
478          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
479          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
480          KM     L =  .28  Kb = .057  Adj. Slope =   78.0
481          BA    .077
482          LG    .300    .250   3.950    .580  15.000
483          UC    .479    .255
484          UA       0       5      16      30      65      77      84      90      94      97
485          UA     100
             *

486          KK   DIV24
487          KM        DIVERT FOR IRRIGATED LAWNS SUB24
488          DT     D24     .93
489          DI       0       1
490          DQ       0      .6
             *

491          KK  C23-24
492          KM        COMBINE HYDROGRAPH SUB23 & SUB24 AT CP24
493          HC       2
             *
```



```
LINE         ID.......1.......2.......3.......4.......5.......6.......7.......8.......9......10

494          KK  R24-25
495          KM        ROUTE FLOW FROM SUB24 TO SUB25
496          RK  1346.4    .009    .016            TRAP      40       1     YES
             *

497          KK   SUB25
498          KM   SUB-BASIN SUB25
499          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
500          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
501          KM     L =  .25  Kb = .057  Adj. Slope =   46.0
502          BA    .076
503          LG    .300    .250   3.950    .580  15.000
504          UC    .550    .273
505          UA       0       5      16      30      65      77      84      90      94      97
506          UA     100
```

```
*

KK   DIV25
KM        DIVERT FOR IRRIGATED LAWNS SUB25
DT     D25      .93
DI       0        1
DQ       0       .6
*

KK  C25-20
KM        COMBINE SUB19, SUB 20 WITH SUB25
HC       3
*      1        2
*
*      3        0
*

KK  R25-29
KM        ROUTE FLOW ALONG CHANNEL FROM SUB25 TO SUB29
RS       1    FLOW      -1
SV       0        2        6       13       23       35       36
SQ       0       75      250      500     1200     2400     4000
*

KK   SUB26
KM   SUB-BASIN SUB26
KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
KM     L =  .52  Kb = .067  Adj. Slope =  840.0
BA    .053
LG    .272    .295   4.250    .520  17.000
UC    .304    .312
UA       0       5       16       30       65       77       84       90       94       97
UA     100
*
```



```
LINE          ID.......1.......2.......3.......4.......5.......6.......7.......8.......9......10

KK   DIV26
KM        DIVERT FOR GOLF   COURSE
DT     D26      .31
DI       0        1
DQ       0     .312
*

KK  R26-27
KM        ROUTE FLOW FROM SUB26 TO SUB27
RK  1293.6    .024    .016            TRAP      35       1     YES
*

KK   SUB27
KM   SUB-BASIN SUB27
KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
KM     L =  .25  Kb = .058  Adj. Slope =  122.0
BA    .061
LG    .300    .250   3.950    .580  15.000
UC    .379    .205
UA       0       5       16       30       65       77       84       90       94       97
UA     100
*

KK   DIV27
KM        DIVERT FOR IRRIGATED LAWNS SUB27
DT     D27      .74
DI       0      1.0
DQ       0      .60
*

KK  C26-27
KM        COMBINE HYDROGRAPH SUB 26 & SUB27 AT CP27
HC       2
*

KK  R27-28
KM        ROUTE FLOW FROM SUB 27 TO SUB28
RK  1436.2    .017    .016            TRAP      35       1     YES
```

```
*
KK   SUB28
KM   SUB-BASIN SUB28
KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
KM     L =  .27  Kb = .057  Adj. Slope =   89.0
BA    .078
LG    .300    .250   3.950    .580  15.000
UC    .446    .227
UA      0       5      16      30      65      77      84      90      94      97
UA    100
*
```



```
LINE          ID.......1.......2.......3.......4.......5.......6.......7.......8.......9......10

KK   DIV28
KM        DIVERT FOR IRRIGATED LAWNS SUB28
DT     D28     .95
DI       0       1
DQ       0     .60
*

KK  C27-28
KM        COMBINE HYDROGRAPH SUB27 & SUB28 AT CP28
HC       2
*

KK  R28-29
KM        ROUTE FLOW FROM SUB 28 TO SUB29
RK  1161.6    .009    .016            TRAP      35       1     YES
*

KK   SUB29
KM   SUB-BASIN SUB29
KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
KM     L =  .22  Kb = .058  Adj. Slope =   47.0
BA    .058
LG    .299    .250   3.950    .580  15.000
UC    .508    .264
UA      0       5      16      30      65      77      84      90      94      97
UA    100
*

KK   DIV29
KM        DIVERT FOR IRRIGATED LAWNS SUB29
DT     D29     .70
DI       0       1
DQ       0    .587
*

KK  C29-25
KM        COMBINE SUB28, SUB25 WITH SUB29
HC       3
*      1       2
*

KK   DOCCC
KM        DIVERT AZ CANAL FLOW TO OCCC
DT   DOCCC
DI       0     200     400     800    1000    1001    1200    4000
DQ       0     200     400     800    1000    1000    1000    1000
*
*      3       0
*
```



```
LINE          ID.......1.......2.......3.......4.......5.......6.......7.......8.......9......10

KK  R29-33
KM        ROUTE FLOW ALONG CHANNEL FROM SUB29 TO SUB33
RS       1    FLOW      -1
SV       0       2       4       7      18      36      60
SQ       0      75     250     500    1200    2400    4000
*
```

```
608          KK   SUB38
609          KM   SUB-BASIN SUB38
610          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
611          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
612          KM     L = 1.28  Kb = .090  Adj. Slope = 1079.0
613          BA    .252
614          LG    .131    .340   4.550    .280  37.000
615          UC    .408    .366
616          UA       0       3       5       8      12      20      43      75      90      96
617          UA     100
             *

618          KK  D38-39
619          KM        DIVERT 16CFS FROM SUB38 TO SUB39
620          DT  D38-39
621          DI       0       5      10      16      50     100     200     400     600
622          DQ       0       5      10      16      16      16      16      16      16
             *

623          KK  R38-30
624          KM        ROUTE FLOW FROM SUB38 TO   SUB30
625          RK    1200    .035    .016            TRAP      30       1     YES
             *

626          KK   SUB30
627          KM   SUB-BASIN SUB30
628          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
629          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
630          KM     L =  .48  Kb = .067  Adj. Slope =  571.0
631          BA    .064
632          LG    .272    .267   4.000    .460  10.000
633          UC    .313    .271
634          UA       0       5      16      30      65      77      84      90      94      97
635          UA     100
             *

636          KK  C30-38
637          KM        COMBINE SUB38 & SUB30 AT CP30
638          HC       2
             *

639          KK  R30-31
640          KM        ROUTE FLOW FROM SUB30 TO SUB31
641          RK    1304   .0225    .025            TRAP      20       1     YES
             *
```



```
LINE         ID.......1.......2.......3.......4.......5.......6.......7.......8.......9......10

642          KK   SUB31
643          KM   SUB-BASIN SUB31
644          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
645          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
646          KM     L =  .25  Kb = .058  Adj. Slope =  118.0
647          BA    .061
648          LG    .300    .260   3.670    .690  15.000
649          UC    .433    .238
650          UA       0       5      16      30      65      77      84      90      94      97
651          UA     100
             *

652          KK   DIV31
653          KM        DIVERT FOR IRRIGATED LAWNS SUB31
654          DT     D31     .45
655          DI       0       1
656          DQ       0    .400
             *

657          KK  C30-31
658          KM        COMBINE SUB30 & SUB31 AT CP31
659          HC       2
             *

660          KK  R31-32
661          KM        ROUTE FLOW FROM SUB31 TO SUB32
662          RK    1260    .019    .016       0    TRAP      30       1     YES
             *
```

```
663          KK   SUB32
664          KM   SUB-BASIN SUB32
665          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
666          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
667          KM     L =  .27  Kb = .058  Adj. Slope =   77.0
668          BA    .065
669          LG    .300    .250   3.950    .580  15.000
670          UC    .479    .272
671          UA       0       5      16      30      65      77      84      90      94      97
672          UA     100
             *

673          KK   DIV32
674          KM        DIVERT FOR IRRIGATED LAWNS SUB32
675          DT     D32     .79
676          DI     0.0     1.0
677          DQ       0     .60
             *

678          KK  C31-32
679          KM        COMBINE HYDROGRAPH SUB31 & SUB32 AT CP32
680          HC       2
             *
```



```
LINE         ID.......1.......2.......3.......4.......5.......6.......7.......8.......9......10

681          KK  R32-33
682          KM        ROUTE FLOW FROM SUB32 TO SUB33
683          RK    1447   .0144     .07            TRAP       0       3     YES
             *

684          KK   SUB33
685          KM   SUB-BASIN SUB33
686          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
687          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
688          KM     L =  .22  Kb = .058  Adj. Slope =   65.0
689          BA    .062
690          LG    .277    .250   3.950    .580  22.000
691          UC    .408    .199
692          UA       0       5      16      30      65      77      84      90      94      97
693          UA     100
             *

694          KK   DIV33
695          KM        DIVERT FOR IRRIGATED LAWNS SUB33
696          DT     D33     .62
697          DI       0       1
698          DQ       0     .37
             *

699          KK  C33-29
700          KM        COMBINE SUB32, SUB29 WITH SUB33
701          HC       3
             *      1       2
             *
             *      3       0
             *

702          KK  R33-35
703          KM        ROUTE FLOW ALONG CHANNEL FROM SUB33 TO SUB35
704          RS       1    FLOW      -1
705          SV       0       5      10      22      50      93     142
706          SQ       0      75     250     500    1200    2400    4000
             *

707          KK   SUB34
708          KM   SUB-BASIN SUB34
709          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
710          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
711          KM     L =  .57  Kb = .050  Adj. Slope =   87.0
712          BA    .167
713          LG    .284    .250   3.950    .590  20.000
714          UC    .617    .383
715          UA       0       5      16      30      65      77      84      90      94      97
716          UA     100
             *
```

```
LINE          ID.......1.......2.......3.......4.......5.......6.......7.......8.......9......10

 717          KK   DIV34
 718          KM        DIVERT FOR IRRIGATED LAWNS SUB34
 719          DT     D34    1.53
 720          DI       0       1
 721          DQ       0    .366
              *

 722          KK  R34-35
 723          KM        ROUTE FLOW FROM SUB34 TO SUB35
 724          RK  1531.2    .018    .016            TRAP      40       1     YES
              *

 725          KK   SUB35
 726          KM   SUB-BASIN SUB35
 727          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
 728          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
 729          KM     L =  .29  Kb = .048  Adj. Slope =   51.0
 730          BA    .128
 731          LG    .223    .250   3.950    .600  39.000
 732          UC    .400    .160
 733          UA       0       5      16      30      65      77      84      90      94      97
 734          UA     100
              *

 735          KK   DIV35
 736          KM        DIVERT FOR IRRIGATED LAWNS SUB35
 737          DT     D35     .53
 738          DI     0.0     1.0
 739          DQ     0.0    .095
              *

 740          KK  C35-33
 741          KM        COMBINE SUB34, SUB33 WITH SUB35
 742          HC       3
              *
              *      3       0
              *

 743          KK  R35-36
 744          KM        ROUTE FLOW ALONG CHANNEL FROM SUB35 TO SUB36
 745          RS       1    FLOW      -1
 746          SV       0       4       9      28      67     131     179
 747          SQ       0      75     250     500    1200    2400    4000
              *

 748          KK   SUB40
 749          KM   SUB-BASIN SUB40
 750          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
 751          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
 752          KM     L =  .31  Kb = .090  Adj. Slope = 1822.0
 753          BA    .074
 754          LG    .203    .314   4.000    .420  11.000
 755          UC    .188    .100
 756          UA       0       3       5       8      12      20      43      75      90      96
```



```
LINE          ID.......1.......2.......3.......4.......5.......6.......7.......8.......9......10

 757          UA     100
              *

 758          KK  R40-41
 759          KM        ROUTE FLOW FROM SUB40 TO SUB41
 760          RK    1452   .0221     .05            TRAP       6       2     YES
              *

 761          KK   SUB41
 762          KM   SUB-BASIN SUB41
 763          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
 764          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
 765          KM     L =  .54  Kb = .053  Adj. Slope =  110.0
 766          BA    .156
 767          LG    .281    .252   4.350    .420  16.000
 768          UC    .508    .308
```

```
769          UA       0       5      16      30      65      77      84      90      94      97
770          UA     100
             *

771          KK  C40-41
772          KM        COMBINE HYDROGRAPH SUB40 & SUB41 AT CP41
773          HC       2
             *

774          KK  R41-39
775          KM        ROUTE FLOW FROM SUB41 TO   SUB39
776          RK    2865   .0341     .05            TRAP       4       3     YES
             *

777          KK   SUB37
778          KM   SUB-BASIN SUB37
779          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
780          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
781          KM     L =  .30  Kb = .059  Adj. Slope =  247.0
782          BA    .049
783          LG    .300    .250   3.950    .490   5.000
784          UC    .321    .223
785          UA       0       5      16      30      65      77      84      90      94      97
786          UA     100
             *

787          KK  R37-39
788          KM        ROUTE FLOW FROM SUB37 TO   SUB39
789          RK    3500    .018    .016            TRAP      70       1     YES
             *

790          KK   SUB39
791          KM   SUB-BASIN SUB39
792          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
793          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
794          KM     L =  .84  Kb = .050  Adj. Slope =   79.0
795          BA    .224
796          LG    .233    .259   4.300    .450  29.000
797          UC    .667    .481
```



```
LINE         ID.......1.......2.......3.......4.......5.......6.......7.......8.......9......10

798          UA       0       5      16      30      65      77      84      90      94      97
799          UA     100
             *

800          KK  D39-36
801          KM        DIVERT FLOW OF CAMELBACK RD. OVERTOPPING AND RUNNING TO SUB36
802          DT  D39-36
803          DI       0    99.5     160     200     300     500     700    1000
804          DQ       0       0       0      40     140     340     540     840
             *

805          KK   DCBR1
806          KM        DIVERT 55 CFS FROM WATERSHED STORM DRAIN OUTLETS TO 40TH STREET SYSTEM
807          DT   DCBR1
808          DI       0      20      50      55     100     200     500    1000    2000    3000
809          DQ       0      20      50      55      55      55      55      55      55      55
             *

810          KK   DCBR2
811          KM        DIVERT 60 CFS FOR STORM DRAIN THAT OUTLETS INTO AZ. CANAL IN SUBBASIN 36
812          DT   DCBR2
813          DI       0      20      50      60     150     300     600    1000    2000    3000
814          DQ       0      20      50      60      60      60      60      60      60      60
             *

815          KK  RD3839
816          KM        RECALL DIVERSION FROM SUBBASIN 38
817          DR  D38-39
             *

818          KK  C37-41
819          KM        COMBINE HYDROGRAPHS SUB41, SUB37 & SUB39 AT CP39 AND RECALLED DIVERSION
820          HC       4
             *

821          KK  R39-36
```

```
822          KM        ROUTE FLOW FROM SUB39 TO   SUB36
823          RK    1250    .006    .016            TRAP      26       1     YES
             *

824          KK   SUB36
825          KM   SUB-BASIN SUB36
826          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
827          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
828          KM     L =  .28  Kb = .052  Adj. Slope =   14.0
829          BA    .089
830          LG    .232    .250   3.950    .590  41.000
831          UC    .646    .327
832          UA       0       5      16      30      65      77      84      90      94      97
833          UA     100
             *
```



```
LINE         ID.......1.......2.......3.......4.......5.......6.......7.......8.......9......10

834          KK   DIV36
835          KM        DIVERT FOR IRRIGATED LAWNS SUB36
836          DT     D36     .61
837          DI     0.0     1.0
838          DQ     0.0    .150
             *

839          KK  RDCBR2
840          KM        RECALL DIVERSION FOR STORM DRAIN ALONG CAMELBACK RD.
841          DR   DCBR2
             *

842          KK  RD39366
843          KM        RECALL DIVERSION FROM SUB 39 TO    SUB36
844          DR  D39-36
             *

845          KK  C36-35
846          KM        COMBINE SUB39, SUB35, 2 RECALLED DIVERSIONS AND SUB36
847          HC       5
             *

848          KK   D40ST
849          KM        DIVERT FLOW FOR 40TH ST.
850          DT   D40ST
851          DI       0      10     100     300     500     700     900    1100    1300    1500
852          DQ       0       0      90     290     490     690     890    1090    1290    1490
             *
             *      3       0
             *

853          KK  R36-42
854          KM        ROUTE FLOW FROM SUB36 TO SUB42
855          RS       1    FLOW      -1
856          SV       0       3       6      10      34      60     130
857          SQ       0      75     250     500    1200    2400    4000
             *

858          KK   SUB42
859          KM   SUB-BASIN SUB42
860          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
861          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
862          KM     L =  .51  Kb = .044  Adj. Slope =   29.0
863          BA    .206
864          LG    .247    .250   5.600    .250  27.000
865          UC    .587    .294
866          UA       0       5      16      30      65      77      84      90      94      97
867          UA     100
             *
```



```
LINE         ID.......1.......2.......3.......4.......5.......6.......7.......8.......9......10

868          KK   DIV42
869          KM        DIVERT FOR IRRIGATED LAWNS SUB42
870          DT     D42     .75
871          DI       0       1
872          DQ       0    .072
```

```
                    *      1       2
                    *
873                 KK  C42-36
874                 KM        COMBINE HYDROGRAPH SUB42 WITH SUB36
875                 HC       2
                    *
                    *      3       0
                    *
876                 ZZ
```

1

SCHEMATIC DIAGRAM OF STREAM NETWORK

```
NPUT
LINE     (V) ROUTING          (--->) DIVERSION OR PUMP FLOW

NO.      (.) CONNECTOR        (<---) RETURN OF DIVERTED OR PUMPED FLOW

 5         SUB1
              V
              V
 22        R1-2
              .
              .
 25           .        SUB2
              .           .
              .           .
 37           .           .------->      D2
 35           .        DIV2
              .           .
              .           .
 40        C1-2............
              V
              V
 43        R2-3
              .
              .
 46           .        SUB3
              .           .
              .           .
 58           .           .------->      D3
 56           .        DIV3
              .           .
              .           .
 61        C2-3............
              V
              V
 64        R3-4
              .
              .
 67           .        SUB4
              .           .
              .           .
 79           .           .------->      D4
 77           .        DIV4
              .           .
              .           .
 82        C3-4............
              .
              .
 87           .------->    DIBW
 85      DIVIBW
              V
              V
 90        R4-5
              .
              .
 93           .        SUB5
              .           .
              .           .
105           .           .------->      D5
103           .        DIV5
              .           .
              .           .
108        C4-5............
              .
              .
111           .        SUB6
              .           V
              .           V
```

```
121          .        R6-7
             .          .
             .          .
124          .          .        SUB7
             .          .          .
             .          .          .
136          .          .          .-------->      D7
134          .          .        DIV7
             .          .          .
             .          .          .
139          .        C6-7............
             .          V
             .          V
142          .        R7-8
             .          .
             .          .
145          .          .        SUB8
             .          .          .
             .          .          .
157          .          .          .-------->      D8
155          .          .        DIV8
             .          .          .
             .          .          .
160          .        C7-8............
             .          V
             .          V
163          .        R8-9
             .          .
             .          .
166          .          .        SUB9
             .          .          .
             .          .          .
178          .          .          .-------->      D9
176          .          .        DIV9
             .          .          .
             .          .          .
181          .        C8-9............
             .          V
             .          V
184          .        R9-5
             .          .
             .          .
187       C9-5............
             V
             V
190       R5-10
             .
             .
195          .       SUB10
             .          .
             .          .
207          .          .-------->     D10
205          .       DIV10
             .          .
             .          .
210       C5-10...........
             V
             V
213      R10-15
             .
             .
218          .       SUB11
             .          V
             .          V
228          .      R11-12
             .          .
             .          .
231          .          .       SUB12
             .          .          .
             .          .          .
243          .          .          .-------->     D12
241          .          .       DIV12
             .          .          .
             .          .          .
246          .      C11-12...........
             .          V
             .          V
249          .      R12-13
             .          .
```

```
252          .           .       SUB13
             .           .           .
             .           .           .
264          .           .           .-------->     D13
262          .           .       DIV13
             .           .           .
             .           .           .
267          .      C12-13............
             .           V
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270          .      R13-14
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273          .           .       SUB14
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285          .           .           .-------->     D14
283          .           .       DIV14
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288          .      C13-14............
             .           V
             .           V
291          .      R14-15
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294          .           .       SUB15
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306          .           .           .-------->     D15
304          .           .       DIV15
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309     C15-10........................
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314          .-------->  D56ST
312      D56ST
             V
             V
317     R15-20
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322          .       SUB16
             .           V
             .           V
332          .      R16-17
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335          .           .       SUB17
             .           .           .
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347          .           .           .-------->     D17
345          .           .       DIV17
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350          .      C16-17............
             .           V
             .           V
353          .      R17-18
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356          .           .       SUB18
             .           .           .
             .           .           .
368          .           .           .-------->     D18
366          .           .       DIV18
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371          .      C17-18............
             .           V
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374          .      R18-19
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377          .           .       SUB19
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389          .          .          .-------->    D19
387          .          .      DIV19
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392          .     C18-19............
             .          V
             .          V
395          .     R19-20
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398          .          .      SUB20
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410          .          .          .-------->    D20
408          .          .      DIV20
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413     C20-15........................
             V
             V
416     R20-25
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421          .      SUB21
             .          V
             .          V
431          .     R21-22
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434          .          .      SUB22
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446          .          .          .-------->    D22
444          .          .      DIV22
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449          .     C21-22............
             .          V
             .          V
452          .     R22-23
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455          .          .      SUB23
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467          .          .          .-------->    D23
465          .          .      DIV23
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470          .     C22-23............
             .          V
             .          V
473          .     R23-24
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476          .          .      SUB24
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488          .          .          .-------->    D24
486          .          .      DIV24
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491          .     C23-24............
             .          V
             .          V
494          .     R24-25
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497          .          .      SUB25
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509          .          .          .-------->    D25
507          .          .      DIV25
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512     C25-20........................
             V
             V
515     R25-29
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520       .      SUB26
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532       .          .-------->     D26
530       .      DIV26
          .          V
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535       .     R26-27
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538       .          .       SUB27
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550       .          .           .-------->     D27
548       .          .       DIV27
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553       .     C26-27............
          .          V
          .          V
556       .     R27-28
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559       .          .       SUB28
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571       .          .           .-------->     D28
569       .          .       DIV28
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574       .     C27-28............
          .          V
          .          V
577       .     R28-29
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580       .          .       SUB29
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592       .          .           .-------->     D29
590       .          .       DIV29
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595    C29-25........................
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600       .-------->   DOCCC
598     DOCCC
          V
          V
603    R29-33
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608       .      SUB38
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620       .          .-------->  D38-39
618       .     D38-39
          .          V
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623       .     R38-30
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626       .          .       SUB30
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636       .     C30-38............
          .          V
          .          V
639       .     R30-31
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642       .          .       SUB31
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654       .          .           .-------->     D31
652       .          .       DIV31
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657             .     C30-31...........
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660             .     R31-32
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663             .          .     SUB32
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675             .          .          .-------->     D32
673             .          .     DIV32
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678             .     C31-32...........
                .          V
                .          V
681             .     R32-33
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684             .          .     SUB33
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696             .          .          .-------->     D33
694             .          .     DIV33
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699        C33-29......................
                V
                V
702        R33-35
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707             .     SUB34
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719             .          .-------->     D34
717             .     DIV34
                .          V
                .          V
722             .     R34-35
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725             .          .     SUB35
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737             .          .          .-------->     D35
735             .          .     DIV35
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740        C35-33......................
                V
                V
743        R35-36
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748             .     SUB40
                .          V
                .          V
758             .     R40-41
                .          .
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761             .          .     SUB41
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771             .     C40-41...........
                .          V
                .          V
774             .     R41-39
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777             .          .     SUB37
                .          .          V
                .          .          V
787             .          .     R37-39
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790             .          .          .     SUB39
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802             .          .          .          .-------> D39-36
800             .          .          .     D39-36
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807             .          .          .          .------->  DCBR1
805             .          .          .      DCBR1
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812             .          .          .          .------->  DCBR2
810             .          .          .      DCBR2
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817             .          .          .          .          .<-------  D38-39
815             .          .          .          .     RD3839
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818             .     C37-41.......................................
                .          V
                .          V
821             .     R39-36
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824             .          .      SUB36
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836             .          .          .------->     D36
834             .          .      DIV36
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841             .          .          .          .<-------  DCBR2
839             .          .          .     RDCBR2
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844             .          .          .          .          .<-------  D39-36
842             .          .          .          .     RD3936
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845        C36-35.............................................
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850             .------->  D40ST
848         D40ST
                V
                V
853        R36-42
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858             .      SUB42
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                .          .
870             .          .------->     D42
868             .      DIV42
                .          .
                .          .
873        C42-36............
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(***) RUNOFF ALSO COMPUTED AT THIS LOCATION

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1****************************************
*                                      *
*   FLOOD HYDROGRAPH PACKAGE  (HEC-1)  *
*             MAY   1991               *
*          VERSION 4.0.1E              *
*                                      *
*  RUN DATE  09/01/95  TIME  05:20:25  *
*                                      *
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****************************************
*                                      *
*    U.S. ARMY CORPS OF ENGINEERS      *
*    HYDROLOGIC ENGINEERING CENTER     *
*          609 SECOND STREET           *
*       DAVIS, CALIFORNIA 95616        *
*           (916) 551-1748             *
*                                      *
****************************************
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DDM MCUHP1 ARCADIA AREA 25-yr 6hr

```
  4 IO          OUTPUT CONTROL VARIABLES
                      IPRNT          5  PRINT CONTROL
                      IPLOT          0  PLOT CONTROL
```

```
                QSCAL          0.  HYDROGRAPH PLOT SCALE

IT          HYDROGRAPH TIME DATA
                 NMIN          5  MINUTES IN COMPUTATION INTERVAL
                IDATE      1   0  STARTING DATE
                ITIME       0000  STARTING TIME
                   NQ        300  NUMBER OF HYDROGRAPH ORDINATES
               NDDATE      2   0  ENDING DATE
               NDTIME       0055  ENDING TIME
               ICENT         19  CENTURY MARK

            COMPUTATION INTERVAL    0.08 HOURS
                 TOTAL TIME BASE   24.92 HOURS

     ENGLISH UNITS
          DRAINAGE AREA          SQUARE MILES
          PRECIPITATION DEPTH    INCHES
          LENGTH, ELEVATION      FEET
          FLOW                   CUBIC FEET PER SECOND
          STORAGE VOLUME         ACRE-FEET
          SURFACE AREA           ACRES
          TEMPERATURE            DEGREES FAHRENHEIT
```

RUNOFF SUMMARY
FLOW IN CUBIC FEET PER SECOND
TIME IN HOURS, AREA IN SQUARE MILES

OPERATION	STATION	PEAK FLOW	TIME OF PEAK	AVERAGE FLOW FOR MAXIMUM PERIOD 6-HOUR	24-HOUR	72-HOUR	BASIN AREA	MAXIMUM STAGE	TIME OF MAX STAGE
HYDROGRAPH AT	SUB1	40.	4.08	6.	2.	2.	0.04		
+ ROUTED TO	R1-2	39.	4.17	6.	2.	2.	0.04		
HYDROGRAPH AT	SUB2	45.	4.33	8.	2.	2.	0.12		
DIVERSION TO	D2	17.	4.58	2.	0.	0.	0.12		
+ HYDROGRAPH AT	DIV2	37.	4.58	7.	2.	2.	0.12		
2 COMBINED AT	C1-2	66.	4.25	13.	3.	3.	0.16		
ROUTED TO	R2-3	65.	4.25	13.	3.	3.	0.16		
+ HYDROGRAPH AT	SUB3	33.	4.25	5.	1.	1.	0.07		
DIVERSION TO	D3	19.	4.50	2.	0.	0.	0.07		
HYDROGRAPH AT	DIV3	25.	4.50	4.	1.	1.	0.07		
+ 2 COMBINED AT	C2-3	84.	4.42	16.	4.	4.	0.22		
ROUTED TO	R3-4	84.	4.50	16.	4.	4.	0.22		
HYDROGRAPH AT	SUB4	41.	4.17	6.	2.	1.	0.06		
+ DIVERSION TO	D4	22.	4.42	2.	1.	0.	0.06		
HYDROGRAPH AT	DIV4	33.	4.42	4.	1.	1.	0.06		
2 COMBINED AT	C3-4	115.	4.42	20.	5.	5.	0.29		

DIVERSION TO	DIBW	57.	4.42	12.	3.	3.	0.29
HYDROGRAPH AT	DIVIBW	57.	4.42	9.	2.	2.	0.29
ROUTED TO	R4-5	57.	4.50	9.	2.	2.	0.29
HYDROGRAPH AT	SUB5	24.	4.50	6.	2.	2.	0.07
DIVERSION TO	D5	12.	5.00	2.	0.	0.	0.07
HYDROGRAPH AT	DIV5	17.	5.00	4.	1.	1.	0.07
2 COMBINED AT	C4-5	69.	4.50	13.	3.	3.	0.35
HYDROGRAPH AT	SUB6	107.	4.00	15.	4.	4.	0.09
ROUTED TO	R6-7	103.	4.17	15.	4.	4.	0.09
HYDROGRAPH AT	SUB7	93.	4.25	16.	4.	4.	0.15
DIVERSION TO	D7	40.	4.58	5.	1.	1.	0.15
HYDROGRAPH AT	DIV7	62.	4.58	11.	3.	3.	0.15
2 COMBINED AT	C6-7	154.	4.17	27.	7.	6.	0.24
ROUTED TO	R7-8	152.	4.25	27.	7.	6.	0.24
HYDROGRAPH AT	SUB8	24.	4.42	5.	1.	1.	0.07
DIVERSION TO	D8	14.	4.83	2.	0.	0.	0.07
HYDROGRAPH AT	DIV8	17.	4.83	3.	1.	1.	0.07
2 COMBINED AT	C7-8	160.	4.25	30.	8.	7.	0.31
ROUTED TO	R8-9	158.	4.25	30.	8.	7.	0.31
HYDROGRAPH AT	SUB9	38.	4.17	6.	1.	1.	0.06
DIVERSION TO	D9	23.	4.33	2.	0.	0.	0.06
HYDROGRAPH AT	DIV9	32.	4.33	4.	1.	1.	0.06
2 COMBINED AT	C8-9	187.	4.33	34.	9.	8.	0.38
ROUTED TO	R9-5	181.	4.33	34.	9.	8.	0.38
2 COMBINED AT	C9-5	241.	4.42	47.	12.	11.	0.73
ROUTED TO	R5-10	224.	4.50	47.	12.	11.	0.73

HYDROGRAPH AT	SUB10	52.	4.25	9.	2.	2.	0.09
DIVERSION TO	D10	23.	4.50	2.	1.	1.	0.09
HYDROGRAPH AT	DIV10	40.	4.50	6.	2.	2.	0.09
2 COMBINED AT	C5-10	264.	4.50	53.	13.	13.	0.82
ROUTED TO	R10-15	228.	4.75	53.	13.	13.	0.82
HYDROGRAPH AT	SUB11	89.	4.08	14.	3.	3.	0.09
ROUTED TO	R11-12	88.	4.17	14.	3.	3.	0.09
HYDROGRAPH AT	SUB12	112.	4.08	13.	3.	3.	0.12
DIVERSION TO	D12	9.	4.08	1.	0.	0.	0.12
HYDROGRAPH AT	DIV12	103.	4.08	12.	3.	3.	0.12
2 COMBINED AT	C11-12	188.	4.08	26.	6.	6.	0.21
ROUTED TO	R12-13	184.	4.17	26.	6.	6.	0.21
HYDROGRAPH AT	SUB13	127.	4.08	15.	4.	4.	0.13
DIVERSION TO	D13	25.	4.08	2.	0.	0.	0.13
HYDROGRAPH AT	DIV13	101.	4.08	13.	3.	3.	0.13
2 COMBINED AT	C12-13	285.	4.08	39.	10.	9.	0.34
ROUTED TO	R13-14	281.	4.17	39.	10.	9.	0.34
HYDROGRAPH AT	SUB14	73.	4.17	9.	2.	2.	0.13
DIVERSION TO	D14	44.	4.25	3.	1.	1.	0.13
HYDROGRAPH AT	DIV14	61.	4.25	6.	2.	1.	0.13
2 COMBINED AT	C13-14	326.	4.25	45.	11.	11.	0.47
ROUTED TO	R14-15	320.	4.25	45.	11.	11.	0.47
HYDROGRAPH AT	SUB15	74.	4.25	12.	3.	3.	0.13
DIVERSION TO	D15	43.	4.50	4.	1.	1.	0.13
HYDROGRAPH AT	DIV15	56.	4.50	7.	2.	2.	0.13
3 COMBINED AT	C15-10	466.	4.42	105.	26.	26.	1.42
DIVERSION TO							

+	D56ST	63.	4.42	3.	1.	1.	1.42
HYDROGRAPH AT	D56ST	403.	4.42	102.	26.	25.	1.42
ROUTED TO	R15-20	313.	4.83	94.	26.	25.	1.42
HYDROGRAPH AT +	SUB16	134.	4.08	21.	5.	5.	0.13
ROUTED TO	R16-17	132.	4.17	21.	5.	5.	0.13
HYDROGRAPH AT	SUB17	48.	4.08	6.	1.	1.	0.07
DIVERSION TO +	D17	4.	4.17	0.	0.	0.	0.07
HYDROGRAPH AT	DIV17	46.	4.17	6.	1.	1.	0.07
2 COMBINED AT	C16-17	178.	4.17	27.	7.	7.	0.20
ROUTED TO +	R17-18	177.	4.17	27.	7.	7.	0.20
HYDROGRAPH AT	SUB18	37.	4.17	5.	1.	1.	0.07
DIVERSION TO	D18	22.	4.33	2.	0.	0.	0.07
HYDROGRAPH AT +	DIV18	31.	4.33	3.	1.	1.	0.07
2 COMBINED AT	C17-18	196.	4.25	30.	8.	7.	0.27
ROUTED TO	R18-19	195.	4.25	31.	8.	7.	0.27
HYDROGRAPH AT +	SUB19	38.	4.17	5.	1.	1.	0.08
DIVERSION TO	D19	23.	4.33	2.	0.	0.	0.08
HYDROGRAPH AT	DIV19	33.	4.33	4.	1.	1.	0.08
2 COMBINED AT +	C18-19	216.	4.33	34.	9.	8.	0.34
ROUTED TO	R19-20	215.	4.33	34.	9.	8.	0.34
HYDROGRAPH AT	SUB20	79.	4.17	11.	3.	3.	0.13
DIVERSION TO +	D20	47.	4.33	4.	1.	1.	0.13
HYDROGRAPH AT	DIV20	68.	4.33	7.	2.	2.	0.13
3 COMBINED AT	C20-15	443.	4.50	132.	36.	35.	1.89
ROUTED TO +	R20-25	287.	5.17	106.	36.	35.	1.89
HYDROGRAPH AT	SUB21	135.	4.08	20.	5.	5.	0.12
ROUTED TO	R21-22	133.	4.17	20.	5.	5.	0.12

HYDROGRAPH AT	SUB22	47.	4.33	8.	2.	2.	0.11
DIVERSION TO	D22	3.	4.42	0.	0.	0.	0.11
HYDROGRAPH AT	DIV22	45.	4.42	8.	2.	2.	0.11
2 COMBINED AT	C21-22	174.	4.17	28.	7.	7.	0.24
ROUTED TO	R22-23	171.	4.17	28.	7.	7.	0.24
HYDROGRAPH AT	SUB23	34.	4.08	4.	1.	1.	0.06
DIVERSION TO	D23	20.	4.25	1.	0.	0.	0.06
HYDROGRAPH AT	DIV23	29.	4.25	3.	1.	1.	0.06
2 COMBINED AT	C22-23	198.	4.25	31.	8.	8.	0.30
ROUTED TO	R23-24	195.	4.25	31.	8.	8.	0.30
HYDROGRAPH AT	SUB24	37.	4.17	6.	1.	1.	0.08
DIVERSION TO	D24	22.	4.42	2.	0.	0.	0.08
HYDROGRAPH AT	DIV24	30.	4.42	4.	1.	1.	0.08
2 COMBINED AT	C23-24	209.	4.25	35.	9.	8.	0.37
ROUTED TO	R24-25	209.	4.33	35.	9.	8.	0.37
HYDROGRAPH AT	SUB25	35.	4.25	5.	1.	1.	0.08
DIVERSION TO	D25	21.	4.42	2.	0.	0.	0.08
HYDROGRAPH AT	DIV25	30.	4.42	4.	1.	1.	0.08
3 COMBINED AT	C25-20	329.	5.08	138.	46.	44.	2.34
ROUTED TO	R25-29	301.	5.33	136.	46.	44.	2.34
HYDROGRAPH AT	SUB26	25.	4.17	4.	1.	1.	0.05
DIVERSION TO	D26	8.	4.33	1.	0.	0.	0.05
HYDROGRAPH AT	DIV26	22.	4.33	3.	1.	1.	0.05
ROUTED TO	R26-27	22.	4.33	3.	1.	1.	0.05
HYDROGRAPH AT	SUB27	32.	4.17	4.	1.	1.	0.06
DIVERSION TO	D27	19.	4.33	1.	0.	0.	0.06

HYDROGRAPH AT	DIV27	26.	4.33	3.	1.	1.	0.06
2 COMBINED AT	C26-27	47.	4.33	6.	2.	2.	0.11
ROUTED TO	R27-28	46.	4.33	6.	2.	2.	0.11
HYDROGRAPH AT	SUB28	39.	4.17	6.	1.	1.	0.08
DIVERSION TO	D28	24.	4.33	2.	0.	0.	0.08
HYDROGRAPH AT	DIV28	34.	4.33	4.	1.	1.	0.08
2 COMBINED AT	C27-28	79.	4.33	10.	3.	2.	0.19
ROUTED TO	R28-29	75.	4.42	10.	3.	2.	0.19
HYDROGRAPH AT	SUB29	27.	4.25	4.	1.	1.	0.06
DIVERSION TO	D29	16.	4.42	1.	0.	0.	0.06
HYDROGRAPH AT	DIV29	23.	4.42	3.	1.	1.	0.06
3 COMBINED AT	C29-25	310.	5.33	148.	49.	47.	2.59
DIVERSION TO	DOCCC	310.	0.08	148.	49.	47.	2.59
HYDROGRAPH AT	DOCCC	0.	0.08	0.	0.	0.	2.59
ROUTED TO	R29-33	0.	0.08	0.	0.	0.	2.59
HYDROGRAPH AT	SUB38	186.	4.25	36.	9.	9.	0.25
DIVERSION TO	D38-39	16.	4.25	10.	3.	3.	0.25
HYDROGRAPH AT	D38-39	170.	4.25	26.	6.	6.	0.25
ROUTED TO	R38-30	170.	4.33	26.	6.	6.	0.25
HYDROGRAPH AT	SUB30	35.	4.17	5.	1.	1.	0.06
2 COMBINED AT	C30-38	200.	4.25	31.	8.	7.	0.32
ROUTED TO	R30-31	199.	4.33	31.	8.	7.	0.32
HYDROGRAPH AT	SUB31	26.	4.17	4.	1.	1.	0.06
DIVERSION TO	D31	10.	4.33	1.	0.	0.	0.06
HYDROGRAPH AT	DIV31	19.	4.33	3.	1.	1.	0.06
2 COMBINED AT	C30-31	219.	4.33	33.	8.	8.	0.38
ROUTED TO							

	R31-32	217.	4.33	34.	8.	8.	0.38
HYDROGRAPH AT	SUB32	30.	4.17	5.	1.	1.	0.06
DIVERSION TO	D32	18.	4.42	2.	0.	0.	0.06
HYDROGRAPH AT	DIV32	25.	4.42	3.	1.	1.	0.06
2 COMBINED AT	C31-32	236.	4.33	37.	9.	9.	0.44
ROUTED TO	R32-33	235.	4.42	37.	9.	9.	0.44
HYDROGRAPH AT	SUB33	37.	4.17	5.	1.	1.	0.06
DIVERSION TO	D33	14.	4.33	1.	0.	0.	0.06
HYDROGRAPH AT	DIV33	30.	4.33	4.	1.	1.	0.06
3 COMBINED AT	C33-29	260.	4.42	41.	10.	10.	3.09
ROUTED TO	R33-35	177.	4.67	40.	10.	10.	3.09
HYDROGRAPH AT	SUB34	71.	4.25	14.	3.	3.	0.17
DIVERSION TO	D34	26.	4.58	3.	1.	1.	0.17
HYDROGRAPH AT	DIV34	56.	4.58	11.	3.	3.	0.17
ROUTED TO	R34-35	52.	4.67	11.	3.	3.	0.17
HYDROGRAPH AT	SUB35	98.	4.08	16.	4.	4.	0.13
DIVERSION TO	D35	9.	4.08	1.	0.	0.	0.13
HYDROGRAPH AT	DIV35	89.	4.08	15.	4.	4.	0.13
3 COMBINED AT	C35-33	258.	4.67	65.	17.	16.	3.39
ROUTED TO	R35-36	212.	4.92	64.	17.	16.	3.39
HYDROGRAPH AT	SUB40	58.	4.08	6.	1.	1.	0.07
ROUTED TO	R40-41	56.	4.08	6.	1.	1.	0.07
HYDROGRAPH AT	SUB41	87.	4.25	14.	4.	3.	0.16
2 COMBINED AT	C40-41	139.	4.17	20.	5.	5.	0.23
ROUTED TO	R41-39	137.	4.25	20.	5.	5.	0.23
HYDROGRAPH AT	SUB37	26.	4.17	3.	1.	1.	0.05
ROUTED TO	R37-39	26.	4.25	3.	1.	1.	0.05

HYDROGRAPH AT	SUB39	114.	4.33	25.	6.	6.	0.22
DIVERSION TO	D39-36	0.	4.33	0.	0.	0.	0.22
HYDROGRAPH AT	D39-36	114.	4.33	25.	6.	6.	0.22
DIVERSION TO	DCBR1	55.	4.33	19.	5.	5.	0.22
HYDROGRAPH AT	DCBR1	59.	4.33	6.	2.	2.	0.22
DIVERSION TO	DCBR2	59.	0.08	6.	2.	2.	0.22
HYDROGRAPH AT	DCBR2	0.	0.08	0.	0.	0.	0.22
HYDROGRAPH AT	RD3839	16.	3.50	10.	3.	3.	0.00
4 COMBINED AT	C37-41	179.	4.25	33.	8.	8.	0.50
ROUTED TO	R39-36	177.	4.25	33.	8.	8.	0.50
HYDROGRAPH AT	SUB36	55.	4.25	11.	3.	3.	0.09
DIVERSION TO	D36	8.	4.25	1.	0.	0.	0.09
HYDROGRAPH AT	DIV36	46.	4.25	10.	3.	2.	0.09
HYDROGRAPH AT	RDCBR2	59.	4.33	6.	2.	2.	0.00
HYDROGRAPH AT	RD3936	0.	0.08	0.	0.	0.	0.00
5 COMBINED AT	C36-35	388.	4.42	112.	29.	28.	3.98
DIVERSION TO	D40ST	378.	1.17	102.	26.	25.	3.98
HYDROGRAPH AT	D40ST	10.	1.17	10.	4.	3.	3.98
ROUTED TO	R36-42	10.	5.42	10.	4.	3.	3.98
HYDROGRAPH AT	SUB42	151.	4.25	27.	7.	6.	0.21
DIVERSION TO	D42	11.	4.25	2.	0.	0.	0.21
HYDROGRAPH AT	DIV42	140.	4.25	25.	6.	6.	0.21
2 COMBINED AT	C42-36	150.	4.25	35.	10.	9.	4.19

SUMMARY OF KINEMATIC WAVE - MUSKINGUM-CUNGE ROUTING
(FLOW IS DIRECT RUNOFF WITHOUT BASE FLOW)

ISTAQ	ELEMENT	DT	PEAK	TIME TO PEAK	VOLUME	DT	INTERPOLATED TO COMPUTATION INTERVAL PEAK	TIME TO PEAK	VOLUME
		(MIN)	(CFS)	(MIN)	(IN)	(MIN)	(CFS)	(MIN)	(IN)

```
R1-2  MANE        4.72    40.33   252.41    1.58    5.00   39.32   250.00      1.58

ONTINUITY SUMMARY (AC-FT) - INFLOW=0.3094E+01 EXCESS=0.0000E+00 OUTFLOW=0.3114E+01 BASIN STORAGE=0.2535E-05 PERCENT ERROR=  -0.6

R2-3  MANE        1.22    65.51   256.95    0.77    5.00   64.73   255.00      0.77

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.6379E+01 EXCESS=0.0000E+00 OUTFLOW=0.6385E+01 BASIN STORAGE=0.5716E-04 PERCENT ERROR=  -0.1

R3-4  MANE        1.11    84.30   268.05    0.69    5.00   83.99   270.00      0.69

ONTINUITY SUMMARY (AC-FT) - INFLOW=0.8152E+01 EXCESS=0.0000E+00 OUTFLOW=0.8158E+01 BASIN STORAGE=0.7938E-04 PERCENT ERROR=  -0.1

R4-5  MANE        2.44    56.83   269.45    0.28    5.00   56.79   270.00      0.28

ONTINUITY SUMMARY (AC-FT) - INFLOW=0.4279E+01 EXCESS=0.0000E+00 OUTFLOW=0.4296E+01 BASIN STORAGE=0.8838E-04 PERCENT ERROR=  -0.4

R6-7  MANE        3.83   104.93   246.66    1.59    5.00  103.37   250.00      1.60

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.7608E+01 EXCESS=0.0000E+00 OUTFLOW=0.7652E+01 BASIN STORAGE=0.3389E-05 PERCENT ERROR=  -0.6

R7-8  MANE        2.68   151.83   254.00    1.03    5.00  151.53   255.00      1.03

ONTINUITY SUMMARY (AC-FT) - INFLOW=0.1334E+02 EXCESS=0.0000E+00 OUTFLOW=0.1336E+02 BASIN STORAGE=0.4182E-03 PERCENT ERROR=  -0.1

R8-9  MANE        0.65   160.07   256.13    0.91    5.00  158.36   255.00      0.91

ONTINUITY SUMMARY (AC-FT) - INFLOW=0.1508E+02 EXCESS=0.0000E+00 OUTFLOW=0.1509E+02 BASIN STORAGE=0.1204E-03 PERCENT ERROR=   0.0

R9-5  MANE        1.19   185.00   261.74    0.84    5.00  181.23   260.00      0.84

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.1692E+02 EXCESS=0.0000E+00 OUTFLOW=0.1693E+02 BASIN STORAGE=0.3826E-03 PERCENT ERROR=   0.0

R11-12  MANE      1.40    88.52   248.37    1.38    5.00   87.98   250.00      1.38

ONTINUITY SUMMARY (AC-FT) - INFLOW=0.6857E+01 EXCESS=0.0000E+00 OUTFLOW=0.6864E+01 BASIN STORAGE=0.2846E-07 PERCENT ERROR=  -0.1

R12-13  MANE      0.07   187.41   246.96    1.12    5.00  184.12   250.00      1.12

ONTINUITY SUMMARY (AC-FT) - INFLOW=0.1277E+02 EXCESS=0.0000E+00 OUTFLOW=0.1277E+02 BASIN STORAGE=0.1787E-04 PERCENT ERROR=   0.0

R13-14  MANE      0.62   284.81   246.34    1.05    5.00  281.00   250.00      1.06

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.1922E+02 EXCESS=0.0000E+00 OUTFLOW=0.1923E+02 BASIN STORAGE=0.4879E-04 PERCENT ERROR=  -0.1

R14-15  MANE      1.07   323.90   256.87    0.90    5.00  320.46   255.00      0.89

ONTINUITY SUMMARY (AC-FT) - INFLOW=0.2232E+02 EXCESS=0.0000E+00 OUTFLOW=0.2235E+02 BASIN STORAGE=0.1786E-03 PERCENT ERROR=  -0.1

R16-17  MANE      1.17   134.12   247.60    1.55    5.00  132.05   250.00      1.54

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.1062E+02 EXCESS=0.0000E+00 OUTFLOW=0.1063E+02 BASIN STORAGE=0.3845E-07 PERCENT ERROR=  -0.1

R17-18  MANE      0.71   177.05   251.07    1.25    5.00  176.68   250.00      1.25
```

ONTINUITY SUMMARY (AC-FT) - INFLOW=0.1344E+02 EXCESS=0.0000E+00 OUTFLOW=0.1345E+02 BASIN STORAGE=0.9988E-05 PERCENT ERROR= -0.1

R18-19	MANE	0.71	195.74	256.00	1.06	5.00	195.16	255.00	1.06

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.1518E+02 EXCESS=0.0000E+00 OUTFLOW=0.1519E+02 BASIN STORAGE=0.2797E-04 PERCENT ERROR= -0.1

R19-20	MANE	0.79	215.65	260.41	0.93	5.00	215.39	260.00	0.93

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.1697E+02 EXCESS=0.0000E+00 OUTFLOW=0.1698E+02 BASIN STORAGE=0.4839E-04 PERCENT ERROR= -0.1

R21-22	MANE	2.64	133.61	249.40	1.53	5.00	133.06	250.00	1.53

ONTINUITY SUMMARY (AC-FT) - INFLOW=0.1009E+02 EXCESS=0.0000E+00 OUTFLOW=0.1012E+02 BASIN STORAGE=0.5867E-06 PERCENT ERROR= -0.2

R22-23	MANE	0.51	173.23	250.96	1.12	5.00	171.25	250.00	1.12

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.1410E+02 EXCESS=0.0000E+00 OUTFLOW=0.1410E+02 BASIN STORAGE=0.3289E-05 PERCENT ERROR= 0.0

R23-24	MANE	0.06	197.77	256.26	0.98	5.00	194.85	255.00	0.98

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.1554E+02 EXCESS=0.0000E+00 OUTFLOW=0.1554E+02 BASIN STORAGE=0.1976E-04 PERCENT ERROR= 0.0

R24-25	MANE	0.73	209.31	256.70	0.87	5.00	209.18	260.00	0.87

ONTINUITY SUMMARY (AC-FT) - INFLOW=0.1737E+02 EXCESS=0.0000E+00 OUTFLOW=0.1739E+02 BASIN STORAGE=0.4999E-04 PERCENT ERROR= -0.1

R26-27	MANE	1.08	21.75	261.23	0.60	5.00	21.75	260.00	0.60

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.1692E+01 EXCESS=0.0000E+00 OUTFLOW=0.1695E+01 BASIN STORAGE=0.3902E-05 PERCENT ERROR= -0.1

R27-28	MANE	1.02	47.24	262.00	0.52	5.00	45.50	260.00	0.52

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.3133E+01 EXCESS=0.0000E+00 OUTFLOW=0.3138E+01 BASIN STORAGE=0.1919E-04 PERCENT ERROR= -0.1

R28-29	MANE	0.95	78.40	262.35	0.49	5.00	74.86	265.00	0.49

ONTINUITY SUMMARY (AC-FT) - INFLOW=0.4973E+01 EXCESS=0.0000E+00 OUTFLOW=0.4978E+01 BASIN STORAGE=0.3518E-04 PERCENT ERROR= -0.1

R38-30	MANE	0.44	170.13	256.22	0.95	5.00	169.99	260.00	0.95

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.1277E+02 EXCESS=0.0000E+00 OUTFLOW=0.1278E+02 BASIN STORAGE=0.1695E-05 PERCENT ERROR= 0.0

R30-31	MANE	0.71	200.16	256.72	0.90	5.00	199.39	260.00	0.90

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.1516E+02 EXCESS=0.0000E+00 OUTFLOW=0.1517E+02 BASIN STORAGE=0.5753E-05 PERCENT ERROR= 0.0

R31-32	MANE	0.50	218.11	261.12	0.83	5.00	217.34	260.00	0.83

ONTINUITY SUMMARY (AC-FT) - INFLOW=0.1661E+02 EXCESS=0.0000E+00 OUTFLOW=0.1661E+02 BASIN STORAGE=0.1306E-04 PERCENT ERROR= 0.0

R32-33	MANE	1.49	235.58	264.16	0.77	5.00	235.41	265.00	0.77

```
ONTINUITY SUMMARY (AC-FT) - INFLOW=0.1816E+02 EXCESS=0.0000E+00 OUTFLOW=0.1818E+02 BASIN STORAGE=0.8356E-05 PERCENT ERROR=  -0.1

          R34-35  MANE        1.05     54.98    277.59      0.60      5.00     51.59    280.00        0.60

ONTINUITY SUMMARY (AC-FT) - INFLOW=0.5299E+01 EXCESS=0.0000E+00 OUTFLOW=0.5304E+01 BASIN STORAGE=0.1207E-04 PERCENT ERROR=  -0.1

          R40-41  MANE        1.46     57.48    246.83      0.75      5.00     56.01    245.00        0.75

 CONTINUITY SUMMARY (AC-FT) - INFLOW=0.2937E+01 EXCESS=0.0000E+00 OUTFLOW=0.2945E+01 BASIN STORAGE=0.3098E-06 PERCENT ERROR=  -0.3

          R41-39  MANE        1.91    137.95    254.58      0.81      5.00    137.23    255.00        0.81

ONTINUITY SUMMARY (AC-FT) - INFLOW=0.9968E+01 EXCESS=0.0000E+00 OUTFLOW=0.9980E+01 BASIN STORAGE=0.1540E-05 PERCENT ERROR=  -0.1

          R37-39  MANE        3.96     25.84    253.83      0.58      5.00     25.83    255.00        0.59

ONTINUITY SUMMARY (AC-FT) - INFLOW=0.1508E+01 EXCESS=0.0000E+00 OUTFLOW=0.1526E+01 BASIN STORAGE=0.1932E-03 PERCENT ERROR=  -1.2

          R39-36  MANE        0.72    178.47    255.98      0.62      5.00    177.32    255.00        0.62

 CONTINUITY SUMMARY (AC-FT) - INFLOW=0.1673E+02 EXCESS=0.0000E+00 OUTFLOW=0.1674E+02 BASIN STORAGE=0.1132E-03 PERCENT ERROR=   0.0


** NORMAL END OF HEC-1 ***
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A-3

HEC-1 MODEL 50-YEAR EXISTING CONDITIONS

```
1*****************************************
*                                       *
*  FLOOD HYDROGRAPH PACKAGE  (HEC-1)    *
*            MAY   1991                 *
*         VERSION 4.0.1E                *
*                                       *
*  RUN DATE  09/01/95  TIME  05:32:32   *
*                                       *
*****************************************
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*****************************************
*                                       *
*    U.S. ARMY CORPS OF ENGINEERS       *
*    HYDROLOGIC ENGINEERING CENTER      *
*          609 SECOND STREET            *
*       DAVIS, CALIFORNIA 95616         *
*          (916) 551-1748               *
*                                       *
*****************************************
```

```
X     X  XXXXXXX   XXXXX          X
X     X  X        X     X        XX
X     X  X        X              X
XXXXXXX  XXXX     X        XXXXX X
X     X  X        X              X
X     X  X        X     X        X
X     X  XXXXXXX   XXXXX         XXX
```

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE.
THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION
NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,
DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION
KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

```
1                                   HEC-1 INPUT                                          PAGE  1

LINE          ID.......1.......2.......3.......4.......5.......6.......7.......8.......9......10

              *       ARCADIA AREA HYDROLOGY STUDY - EXISTING CONDITIONS.
              *       PREPARED BY: HUITT-ZOLLARS INC. 8-31-95
              *       PREPARED FOR: FCDMC CONTRACT # 94-21
   1          ID
   2          ID   DDM MCUHP1 ARCADIA AREA 50-yr 6hr
   3          IT       5                    300
   4          IO       5
              *DIAGRAM
              *

   5          KK    SUB1
   6          KM   SUB-BASIN SUB1
   7          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
   8          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
   9          KM     L =  .28  Kb = .100  Adj. Slope = 2120.0
  10          BA    .037
  11          IN      15
  12          KM   RAINFALL DEPTH OF 2.00 WAS SPACIALLY REDUCED AS SHOWN BY THE PB RECORD
  13          PB   2.707
  14          KM   THE FOLLOWING PC RECORD USED A 6-HOUR STORM WITH A PATTERN No. OF 2.20
  15          PC    .000    .010    .017    .026    .037    .046    .056    .065    .075    .085
  16          PC    .097    .111    .131    .175    .263    .455    .689    .829    .893    .933
  17          PC    .949    .962    .975    .988   1.000
  18          LG    .142    .322   4.550    .310  52.000
  19          UC    .150    .107
  20          UA       0       3       5       8      12      20      43      75      90      96
  21          UA     100
              *

  22          KK    R1-2
  23          KM        ROUTE FLOW FROM SUB1 TO SUB2
  24          RK  3183.8   .0166     .07       0    TRAP       0       3     YES
              *

  25          KK    SUB2
  26          KM   SUB-BASIN SUB2
  27          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
  28          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
  29          KM     L =  .60  Kb = .041  Adj. Slope =   88.0
  30          BA    .119
  31          LG    .342    .250   4.650    .440   9.000
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```
 32          UC    .596    .466
 33          UA      0       5      16      30      65      77      84      90      94      97
 34          UA    100
             *

 35          KK    DIV2
 36          KM        DIVERT FOR IRRIGATED LAWNS SUB2
 37          DT      D2     .80
 38          DI       0       1
 39          DQ       0    .382
             *
```



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LINE         ID.......1.......2.......3.......4.......5.......6.......7.......8.......9......10

 40          KK    C1-2
 41          KM        COMBINE HYDROGRAPHS SUB1 AND SUB2 AT CP2
 42          HC       2
             *

 43          KK    R2-3
 44          KM        ROUTE FLOW FROM SUB2 TO SUB3
 45          RK  1367.5    .009    .016            TRAP      60       1     YES
             *

 46          KK    SUB3
 47          KM   SUB-BASIN SUB3
 48          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
 49          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
 50          KM     L =  .26  Kb = .058  Adj. Slope =   47.0
 51          BA    .067
 52          LG    .298    .250   4.250    .510  16.000
 53          UC    .533    .293
 54          UA      0       5      16      30      65      77      84      90      94      97
 55          UA    100
             *

 56          KK    DIV3
 57          KM        DIVERT FOR IRRIGATED LAWNS SUB3
 58          DT      D3     .88
 59          DI       0       1
 60          DQ       0    .573
             *

 61          KK    C2-3
 62          KM        COMBINE HYDROGRAPHS SUB2 & SUB3 AT CP3
 63          HC       2
             *

 64          KK    R3-4
 65          KM        ROUTE FLOW FROM CP3 TO CP4
 66          RK    1320    .008    .016            TRAP      44       1     YES
             *

 67          KK    SUB4
 68          KM   SUB-BASIN SUB4
 69          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
 70          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
 71          KM     L =  .25  Kb = .058  Adj. Slope =   42.0
 72          BA    .065
 73          LG    .300    .250   4.800    .360  15.000
 74          UC    .467    .249
 75          UA      0       5      16      30      65      77      84      90      94      97
 76          UA    100
             *
```



```
LINE         ID.......1.......2.......3.......4.......5.......6.......7.......8.......9......10

 77          KK    DIV4
 78          KM        DIVERT FOR IRRIGATED LAWNS SUB4
 79          DT      D4     1.0
 80          DI       0       1
 81          DQ       0     .55
             *

 82          KK    C3-4
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```
 83          KM        COMBINE HYDROGRAPHS SUB3 & SUB4 AT CP4
 84          HC       2
             *

 85          KK  DIVIBW
 86          KM        DIVERT LAFAYETTE DRAIN INTERCETION TO INDIAN BEND WASH
 87          DT    DIBW
 88          DI      25      63     101     193     241     306
 89          DQ    12.5    31.5    50.5    96.5     121    55.1
             *

 90          KK    R4-5
 91          KM        ROUTE FLOW FROM CP4 TO CP5
 92          RK  2307.4    .005    .016            TRAP      44       1     YES
             *

 93          KK    SUB5
 94          KM   SUB-BASIN SUB5
 95          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
 96          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
 97          KM     L =  .44  Kb = .058  Adj. Slope =   24.0
 98          BA    .067
 99          LG    .300    .250   4.800    .360  15.000
100          UC    .846    .744
101          UA       0       5      16      30      65      77      84      90      94      97
102          UA     100
             *

103          KK    DIV5
104          KM        DIVERT FOR IRRIGATED LAWNS SUB5
105          DT      D5     .94
106          DI       0       1
107          DQ       0     .50
             *

108          KK    C4-5
109          KM        COMBINE HYDROGRAPHS SUB4 & SUB5 AT CP5
110          HC       2
             *

111          KK    SUB6
112          KM   SUB-BASIN SUB6
113          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
114          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
115          KM     L =  .26  Kb = .102  Adj. Slope = 2367.0
116          BA    .090
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LINE         ID.......1.......2.......3.......4.......5.......6.......7.......8.......9......10

117          LG    .113    .341   4.700    .250  50.000
118          UC    .142    .057
119          UA       0       3       5       8      12      20      43      75      90      96
120          UA     100
             *

121          KK    R6-7
122          KM        ROUTE FLOW FROM SUB6 TO SUB7
123          RK  2972.0    .013     .07            TRAP       0       3     YES
             *

124          KK    SUB7
125          KM   SUB-BASIN SUB7
126          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
127          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
128          KM     L =  .56  Kb = .052  Adj. Slope =   71.0
129          BA    .153
130          LG    .295    .269   5.400    .280  18.000
131          UC    .546    .346
132          UA       0       5      16      30      65      77      84      90      94      97
133          UA     100
             *

134          KK    DIV7
135          KM        DIVERT FOR IRRIGATED LAWNS SUB7
136          DT      D7    2.30
137          DI       0       1
138          DQ       0    .427
             *
```

```
139          KK    C6-7
140          KM        COMBINE HYDROGRAPHS SUB6 & SUB7 AT CP7
141          HC       2
             *

142          KK    R7-8
143          KM        ROUTE FLOW FROM SUB7 TO SUB8
144          RK  2302.1    .001    .016            TRAP      40       1     YES
             *

145          KK    SUB8
146          KM   SUB-BASIN SUB8
147          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
148          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
149          KM     L =  .44  Kb = .057  Adj. Slope =   52.0
150          BA    .068
151          LG    .300    .250   4.350    .480  15.000
152          UC    .696    .594
153          UA       0       5      16      30      65      77      84      90      94      97
154          UA     100
             *
1                                          HEC-1 INPUT                                          PAGE  5

LINE         ID.......1.......2.......3.......4.......5.......6.......7.......8.......9......10

155          KK    DIV8
156          KM        DIVERT FOR IRRIGATED LAWNS SUB8
157          DT      D8     .99
158          DI       0       1
159          DQ       0      .6
             *

160          KK    C7-8
161          KM        COMBINE HYDROGRAPHS SUB7 & SUB8 AT CP8
162          HC       2
             *

163          KK    R8-9
164          KM        ROUTE FLOW FROM SUB8 TO SUB9
165          RK  1314.7    .010    .016            TRAP      20       1     YES
             *

166          KK    SUB9
167          KM   SUB-BASIN SUB9
168          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
169          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
170          KM     L =  .25  Kb = .058  Adj. Slope =   55.0
171          BA    .065
172          LG    .300    .250   4.500    .430  15.000
173          UC    .454    .241
174          UA       0       5      16      30      65      77      84      90      94      97
175          UA     100
             *

176          KK    DIV9
177          KM        DIVERT FOR IRRIGATED LAWNS SUB9
178          DT      D9     .94
179          DI       0       1
180          DQ       0      .6
             *

181          KK    C8-9
182          KM        COMBINE HYDROGRAPHS SUB8 & SUB9   AT CP9
183          HC       2
             *

184          KK    R9-5
185          KM        ROUTE FLOW FROM SUB9 TO  SUB5
186          RK  1784.7    .007    .016            TRAP      40       1     YES
             *

187          KK    C9-5
188          KM        COMBINE HYDROGRAPH SUB9  & SUB5  AT CP5
189          HC       2
             *
             *     3       0
             *
```

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LINE          ID.......1.......2.......3.......4.......5.......6.......7.......8.......9......10

 190          KK   R5-10
 191          KM        ROUTE FLOW ALONG CHANNEL FROM SUB5 TO  SUB10
 192          RS       1    FLOW      -1
 193          SV       0       1       3      13      50     110     162
 194          SQ       0      75     250     500    1200    2400    4000
              *

 195          KK   SUB10
 196          KM   SUB-BASIN SUB10
 197          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
 198          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
 199          KM     L =  .34  Kb = .056  Adj. Slope =   37.0
 200          BA    .093
 201          LG    .299    .250   4.800    .360  15.000
 202          UC    .579    .330
 203          UA       0       5      16      30      65      77      84      90      94      97
 204          UA     100
              *

 205          KK   DIV10
 206          KM        DIVERT FOR IRRIGATED LAWNS SUB10
 207          DT     D10    1.17
 208          DI       0       1
 209          DQ       0    .445
              *

 210          KK   C5-10
 211          KM        COMBINE HYDROGRAPH SUB5  & SUB10 AT CP10
 212          HC       2
              *
              *      3       0
              *

 213          KK  R10-15
 214          KM        ROUTE FLOW ALONG CHANNEL FROM SUB10 TO SUB15
 215          RS       1    FLOW      -1
 216          SV       0       2       5       8      46     156     247
 217          SQ       0      75     250     500    1200    2400    4000
              *

 218          KK   SUB11
 219          KM   SUB-BASIN SUB11
 220          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
 221          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
 222          KM     L =  .56  Kb = .106  Adj. Slope = 1740.0
 223          BA    .093
 224          LG    .115    .350   4.550    .270  39.000
 225          UC    .237    .183
 226          UA       0       3       5       8      12      20      43      75      90      96
 227          UA     100
              *
```



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LINE          ID.......1.......2.......3.......4.......5.......6.......7.......8.......9......10

 228          KK  R11-12
 229          KM        ROUTE FLOW FROM SUB11 TO   SUB12
 230          RK    1632    .058     .07            TRAP       0       3     YES
              *

 231          KK   SUB12
 232          KM   SUB-BASIN SUB12
 233          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
 234          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
 235          KM     L =  .31  Kb = .064  Adj. Slope =  304.0
 236          BA    .120
 237          LG    .269    .279   5.700    .200   9.000
 238          UC    .246    .102
 239          UA       0       5      16      30      65      77      84      90      94      97
 240          UA     100
              *

 241          KK   DIV12
```

```
242          KM        DIVERT FOR IRRIGATED LAWNS SUB12
243          DT     D12     .31
244          DI       0       1
245          DQ       0    .079
             *

246          KK  C11-12
247          KM        COMBINE HYDROGRAPH SUB11 & SUB12 AT CP12
248          HC       2
             *

249          KK  R12-13
250          KM        ROUTE FLOW FROM SUB12 TO SUB13
251          RK  1362.2    .020    .016            TRAP      60       1     YES      50
             *

252          KK   SUB13
253          KM   SUB-BASIN SUB13
254          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
255          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
256          KM     L =  .26  Kb = .054  Adj. Slope =  107.0
257          BA    .129
258          LG    .300    .230   6.200    .200  15.000
259          UC    .283    .100
260          UA       0       5      16      30      65      77      84      90      94      97
261          UA     100
             *

262          KK   DIV13
263          KM        DIVERT FOR IRRIGATED LAWNS SUB13
264          DT     D13     .98
265          DI       0       1
266          DQ       0      .2
             *
                                          HEC-1 INPUT                                          PAGE  8

LINE         ID.......1.......2.......3.......4.......5.......6.......7.......8.......9......10

267          KK  C12-13
268          KM        COMBINE HYDROGRAPHS SUB12 & SUB13 AT CP13
269          HC       2
             *

270          KK  R13-14
271          KM        ROUTE FL OW FROM SUB13 TO SUB14
272          RK  1314.7    .014    .016            TRAP      60       1     YES
             *

273          KK   SUB14
274          KM   SUB-BASIN SUB14
275          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
276          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
277          KM .   L =  .25  Kb = .054  Adj. Slope =   74.0
278          BA    .126
279          LG    .300    .250   4.100    .550  15.000
280          UC    .433    .157
281          UA       0       5      16      30      65      77      84      90      94      97
282          UA     100
             *

283          KK   DIV14
284          KM        DIVERT FOR IRRIGATED LAWNS SUB14
285          DT     D14    1.57
286          DI       0       1
287          DQ       0      .6
             *

288          KK  C13-14
289          KM        COMBINE HYDROGRAPHS SUB13 & SUB14 AT CP14
290          HC       2
             *

291          KK  R14-15
292          KM        ROUTE FLOW FROM SUB 14 TO SUB15
293          RK  1985.3    .011    .016            TRAP      60       1     YES
             *

294          KK   SUB15
```

```
295          KM   SUB-BASIN SUB15
296          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
297          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
298          KM     L =  .38  Kb = .054  Adj. Slope =   56.0
299          BA    .126
300          LG    .297    .250   4.650    .390  16.000
301          UC    .529    .274
302          UA       0       5      16      30      65      77      84      90      94      97
303          UA     100
             *
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LINE         ID.......1.......2.......3.......4.......5.......6.......7.......8.......9......10

304          KK   DIV15
305          KM        DIVERT FOR IRRIGATED LAWNS SUB15
306          DT     D15    2.05
307          DI       0       1
308          DQ       0    .585
             *

309          KK  C15-10
310          KM        COMBINE SUB14, SUB10 WITH SUB15
311          HC       3
             *      1       2
             *

312          KK   D56ST
313          KM        DIVERT FLOW THAT CROSSES 56TH ST. BRIDGE
314          DT   D56ST
315          DI       0     400     650     790    1040    1139    1334    1484    1689    1900
316          DQ       0       0     240     318     400     489     584     684     789     900
             *
             *      3       0
             *

317          KK  R15-20
318          KM        ROUTE FLOW ALONG CHANNEL FROM SUB15 TO SUB20
319          RS       1    FLOW      -1
320          SV       0      14      18      25      35      72     111
321          SQ       0      75     250     500    1200    2400    4000
             *

322          KK   SUB16
323          KM   SUB-BASIN SUB16
324          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
325          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
326          KM     L =  .65  Kb = .102  Adj. Slope = 2052.0
327          BA    .129
328          LG    .104    .350   4.700    .240  47.000
329          UC    .233    .167
330          UA       0       3       5       8      12      20      43      75      90      96
331          UA     100
             *

332          KK  R16-17
333          KM        ROUTE FLOW FROM SUB16 TO SUB17
334          RK    1668    .058     .07            TRAP       0       3     YES
             *

335          KK   SUB17
336          KM   SUB-BASIN SUB17
337          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
338          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
339          KM     L =  .32  Kb = .058  Adj. Slope =  183.0
340          BA    .073
341          LG    .298    .252   4.350    .400  10.000
342          UC    .329    .193
```



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LINE         ID.......1.......2.......3.......4.......5.......6.......7.......8.......9......10

343          UA       0       5      16      30      65      77      84      90      94      97
344          UA     100
             *

345          KK   DIV17
346          KM        DIVERT FOR IRRIGATED LAWNS SUB17
```

```
347          DT     D17     .11
348          DI       0       1
349          DQ       0    .074
             *

350          KK  C16-17
351          KM        COMBINE HYDROGRAPH SUB16 & SUB17 AT CP17
352          HC       2
             *

353          KK  R17-18
354          KM        ROUTE FLOW FROM SUB17 TO SUB18
355          RK  1378.1    .019    .016            TRAP      40       1     YES
             *

356          KK   SUB18
357          KM   SUB-BASIN SUB18
358          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
359          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
360          KM     L =  .26  Kb = .058  Adj. Slope =  102.0
361          BA    .067
362          LG    .300    .250   4.150    .530  15.000
363          UC    .404    .215
364          UA       0       5      16      30      65      77      84      90      94      97
365          UA     100
             *

366          KK   DIV18
367          KM        DIVERT FOR IRRIGATED LAWNS SUB18
368          DT     D18     .81
369          DI       0       1
370          DQ       0      .6
             *

371          KK  C17-18
372          KM        COMBINE  HYDROGRAPH SUB17 & SUB18 AT CP18
373          HC       2
             *

374          KK  R18-19
375          KM        ROUTE FLOW SUB18 TO SUB19
376          RK  1335.8    .014    .016            TRAP      40       1     YES
             *
```



```
LINE         ID.......1.......2.......3.......4.......5.......6.......7.......8.......9......10

377          KK   SUB19
378          KM   SUB-BASIN SUB19
379          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
380          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
381          KM     L =  .25  Kb = .057  Adj. Slope =   77.0
382          BA    .075
383          LG    .300    .250   3.950    .580  15.000
384          UC    .450    .220
385          UA       0       5      16      30      65      77      84      90      94      97
386          UA     100
             *

387          KK   DIV19
388          KM        DIVERT FOR IRRIGATED LAWNS SUB19
389          DT     D19     .91
390          DI       0       1
391          DQ       0      .6
             *

392          KK  C18-19
393          KM        COMBINE HYDROGRAPH SUB18 & SUB19 AT CP19
394          HC       2
             *

395          KK  R19-20
396          KM        ROUTE FLOW FROM SUB19 TO SUB20
397          RK  1473.1    .010    .016            TRAP      30       1     YES
             *

398          KK   SUB20
399          KM   SUB-BASIN SUB20
```

```
400          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
401          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
402          KM     L =  .28  Kb = .054  Adj. Slope =   54.0
403          BA    .129
404          LG    .300    .250   4.450    .450  15.000
405          UC    .479    .190
406          UA      0       5      16      30      65      77      84      90      94      97
407          UA    100
             *

408          KK   DIV20
409          KM        DIVERT FOR IRRIGATED LAWNS SUB20
410          DT     D20    1.86
411          DI       0       1
412          DQ       0      .6
             *

413          KK  C20-15
414          KM        COMBINE SUB19, SUB15 WITH SUB20
415          HC       3
             *      1       2
             *
             *      3       0
             *
```



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LINE         ID.......1.......2.......3.......4.......5.......6.......7.......8.......9......10

416          KK  R20-25
417          KM        ROUTE FLOW ALONG CHANNEL FROM SUB20 TO SUB25
418          RS       1    FLOW      -1
419          SV       0      23      27      35      37      84     122
420          SQ       0      75     250     500    1200    2400    4000
             *

421          KK   SUB21
422          KM   SUB-BASIN SUB21
423          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
424          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
425          KM     L =  .56  Kb = .102  Adj. Slope = 2352.0
426          BA    .124
427          LG    .104    .350   4.700    .240  46.000
428          UC    .208    .134
429          UA      0       3       5       8      12      20      43      75      90      96
430          UA    100
             *

431          KK  R21-22
432          KM        ROUTE FLOW FROM SUB21 TO SUB22
433          RK    2735    .026     .07            TRAP       0       3     YES
             *

434          KK   SUB22
435          KM   SUB-BASIN SUB22
436          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
437          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
438          KM     L =  .52  Kb = .060  Adj. Slope =  134.0
439          BA    .112
440          LG    .281    .266   4.000    .480  11.000
441          UC    .571    .410
442          UA      0       5      16      30      65      77      84      90      94      97
443          UA    100
             *

444          KK   DIV22
445          KM        DIVERT FOR IRRIGATED LAWNS SUB22
446          DT     D22     .12
447          DI       0       1
448          DQ       0    .063
             *

449          KK  C21-22
450          KM        COMBINE HYDROGRAPH SUB21 & SUB22 AT CP22
451          HC       2
             *

452          KK  R22-23
453          KM        ROUTE FLOW FROM SUB22 TO SUB23
```

```
454          RK  1240.8    .025    .016            TRAP      20       1     YES
             *
                                        HEC-1 INPUT                                                    PAGE 13

LINE         ID.......1.......2.......3.......4.......5.......6.......7.......8.......9......10


455          KK   SUB23
456          KM   SUB-BASIN SUB23
457          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
458          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
459          KM     L =  .23  Kb = .058  Adj. Slope =  132.0
460          BA    .060
461          LG    .300    .250   3.950    .580  15.000
462          UC    .350    .177
463          UA       0       5      16      30      65      77      84      90      94      97
464          UA     100
             *

465          KK   DIV23
466          KM        DIVERT FOR IRRIGATED LAWNS SUB23
467          DT     D23     .72
468          DI       0       1
469          DQ       0    .593
             *

470          KK  C22-23
471          KM        COMBINE HYDROGRAPH SUB22 & SUB23 AT CP23
472          HC       2
             *

473          KK  R23-24
474          KM        ROUTE FLOW FROM SUB 23 TO SUB24
475          RK  1088.9    .015    .016            TRAP      32       1     YES
             *

476          KK   SUB24
477          KM   SUB-BASIN SUB24
478          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
479          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
480          KM     L =  .28  Kb = .057  Adj. Slope =   78.0
481          BA    .077
482          LG    .300    .250   3.950    .580  15.000
483          UC    .479    .255
484          UA       0       5      16      30      65      77      84      90      94      97
485          UA     100
             *

486          KK   DIV24
487          KM        DIVERT FOR IRRIGATED LAWNS SUB24
488          DT     D24     .93
489          DI       0       1
490          DQ       0      .6
             *

491          KK  C23-24
492          KM        COMBINE HYDROGRAPH SUB23 & SUB24 AT CP24
493          HC       2
             *
1                                       HEC-1 INPUT                                                    PAGE 14

LINE         ID.......1.......2.......3.......4.......5.......6.......7.......8.......9......10


494          KK  R24-25
495          KM        ROUTE FLOW FROM SUB24 TO SUB25
496          RK  1346.4    .009    .016            TRAP      40       1     YES
             *

497          KK   SUB25
498          KM   SUB-BASIN SUB25
499          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
500          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
501          KM     L =  .25  Kb = .057  Adj. Slope =   46.0
502          BA    .076
503          LG    .300    .250   3.950    .580  15.000
504          UC    .550    .273
505          UA       0       5      16      30      65      77      84      90      94      97
506          UA     100
```

```
*

KK   DIV25
KM        DIVERT FOR IRRIGATED LAWNS SUB25
DT     D25     .93
DI       0       1
DQ       0      .6
*

KK  C25-20
KM        COMBINE SUB19, SUB 20 WITH SUB25
HC       3
*      1       2
*
*      3       0
*

KK  R25-29
KM        ROUTE FLOW ALONG CHANNEL FROM SUB25 TO SUB29
RS       1    FLOW      -1
SV       0       2       6      13      23      35      36
SQ       0      75     250     500    1200    2400    4000
*

KK   SUB26
KM   SUB-BASIN SUB26
KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
KM     L =  .52  Kb = .067  Adj. Slope =  840.0
BA    .053
LG    .272    .295   4.250    .520  17.000
UC    .304    .312
UA       0       5      16      30      65      77      84      90      94      97
UA     100
*
```



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LINE          ID.......1.......2.......3.......4.......5.......6.......7.......8.......9......10

KK   DIV26
KM        DIVERT FOR GOLF   COURSE
DT     D26     .31
DI       0       1
DQ       0    .312
*

KK  R26-27
KM        ROUTE FLOW FROM SUB26 TO SUB27
RK  1293.6    .024    .016            TRAP      35       1     YES
*

KK   SUB27
KM   SUB-BASIN SUB27
KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
KM     L =  .25  Kb = .058  Adj. Slope =  122.0
BA    .061
LG    .300    .250   3.950    .580  15.000
UC    .379    .205
UA       0       5      16      30      65      77      84      90      94      97
UA     100
*

KK   DIV27
KM        DIVERT FOR IRRIGATED LAWNS SUB27
DT     D27     .74
DI       0     1.0
DQ       0     .60
*

KK  C26-27
KM        COMBINE HYDROGRAPH SUB 26 & SUB27 AT CP27
HC       2
*

KK  R27-28
KM        ROUTE FLOW FROM SUB 27 TO SUB28
RK  1436.2    .017    .016            TRAP      35       1     YES
```

```
*

KK   SUB28
KM   SUB-BASIN SUB28
KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
KM     L =  .27  Kb = .057  Adj. Slope =   89.0
BA    .078
LG    .300    .250   3.950    .580  15.000
UC    .446    .227
UA      0       5      16      30      65      77      84      90      94      97
UA    100
*
```



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LINE          ID.......1.......2.......3.......4.......5.......6.......7.......8.......9......10

KK   DIV28
KM        DIVERT FOR IRRIGATED LAWNS SUB28
DT     D28     .95
DI       0       1
DQ       0     .60
*

KK  C27-28
KM        COMBINE HYDROGRAPH SUB27 & SUB28 AT CP28
HC       2
*

KK  R28-29
KM        ROUTE FLOW FROM SUB 28 TO SUB29
RK  1161.6    .009    .016            TRAP      35       1     YES
*

KK   SUB29
KM   SUB-BASIN SUB29
KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
KM     L =  .22  Kb = .058  Adj. Slope =   47.0
BA    .058
LG    .299    .250   3.950    .580  15.000
UC    .508    .264
UA      0       5      16      30      65      77      84      90      94      97
UA    100
*

KK   DIV29
KM        DIVERT FOR IRRIGATED LAWNS SUB29
DT     D29     .70
DI       0       1
DQ       0    .587
*

KK  C29-25
KM        COMBINE SUB28, SUB25 WITH SUB29
HC       3
*      1       2
*

KK   DOCCC
KM        DIVERT AZ CANAL FLOW TO OCCC
DT   DOCCC
DI       0     200     400     800    1000    1001    1200    4000
DQ       0     200     400     800    1000    1000    1000    1000
*
*      3       0
*
```



```
LINE          ID.......1.......2.......3.......4.......5.......6.......7.......8.......9......10

KK  R29-33
KM        ROUTE FLOW ALONG CHANNEL FROM SUB29 TO SUB33
RS       1    FLOW      -1
SV       0       2       4       7      18      36      60
SQ       0      75     250     500    1200    2400    4000
*
```

```
608          KK   SUB38
609          KM   SUB-BASIN SUB38
610          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
611          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
612          KM     L = 1.28  Kb = .090  Adj. Slope = 1079.0
613          BA    .252
614          LG    .131    .340   4.550    .280  37.000
615          UC    .408    .366
616          UA       0       3       5       8      12      20      43      75      90      96
617          UA     100
             *

618          KK  D38-39
619          KM        DIVERT 16CFS FROM SUB38 TO SUB39
620          DT  D38-39
621          DI       0       5      10      16      50     100     200     400     600
622          DQ       0       5      10      16      16      16      16      16      16
             *

623          KK  R38-30
624          KM        ROUTE FLOW FROM SUB38 TO   SUB30
625          RK    1200    .035    .016            TRAP      30       1     YES
             *

626          KK   SUB30
627          KM   SUB-BASIN SUB30
628          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
629          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
630          KM     L =  .48  Kb = .067  Adj. Slope =  571.0
631          BA    .064
632          LG    .272    .267   4.000    .460  10.000
633          UC    .313    .271
634          UA       0       5      16      30      65      77      84      90      94      97
635          UA     100
             *

636          KK  C30-38
637          KM        COMBINE SUB38 & SUB30 AT CP30
638          HC       2
             *

639          KK  R30-31
640          KM        ROUTE FLOW FROM SUB30 TO SUB31
641          RK    1304   .0225    .025            TRAP      20       1     YES
             *
```



```
LINE         ID.......1.......2.......3.......4.......5.......6.......7.......8.......9......10

642          KK   SUB31
643          KM   SUB-BASIN SUB31
644          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
645          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
646          KM     L =  .25  Kb = .058  Adj. Slope =  118.0
647          BA    .061
648          LG    .300    .260   3.670    .690  15.000
649          UC    .433    .238
650          UA       0       5      16      30      65      77      84      90      94      97
651          UA     100
             *

652          KK   DIV31
653          KM        DIVERT FOR IRRIGATED LAWNS SUB31
654          DT     D31     .45
655          DI       0       1
656          DQ       0    .400
             *

657          KK  C30-31
658          KM        COMBINE SUB30 & SUB31 AT CP31
659          HC       2
             *

660          KK  R31-32
661          KM        ROUTE FLOW FROM SUB31 TO SUB32
662          RK    1260    .019    .016       0    TRAP      30       1     YES
             *
```

```
663          KK   SUB32
664          KM   SUB-BASIN SUB32
665          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
666          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
667          KM     L =  .27  Kb = .058  Adj. Slope =   77.0
668          BA    .065
669          LG    .300    .250   3.950    .580  15.000
670          UC    .479    .272
671          UA       0       5      16      30      65      77      84      90      94      97
672          UA     100
             *

673          KK   DIV32
674          KM        DIVERT FOR IRRIGATED LAWNS SUB32
675          DT     D32     .79
676          DI     0.0     1.0
677          DQ       0     .60
             *

678          KK  C31-32
679          KM        COMBINE HYDROGRAPH SUB31 & SUB32 AT CP32
680          HC       2
             *
```



```
LINE         ID.......1.......2.......3.......4.......5.......6.......7.......8.......9......10

681          KK  R32-33
682          KM        ROUTE FLOW FROM SUB32 TO SUB33
683          RK    1447   .0144     .07            TRAP       0       3     YES
             *

684          KK   SUB33
685          KM   SUB-BASIN SUB33
686          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
687          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
688          KM     L =  .22  Kb = .058  Adj. Slope =   65.0
689          BA    .062
690          LG    .277    .250   3.950    .580  22.000
691          UC    .408    .199
692          UA       0       5      16      30      65      77      84      90      94      97
693          UA     100
             *

694          KK   DIV33
695          KM        DIVERT FOR IRRIGATED LAWNS SUB33
696          DT     D33     .62
697          DI       0       1
698          DQ       0     .37
             *

699          KK  C33-29
700          KM        COMBINE SUB32, SUB29 WITH SUB33
701          HC       3
             *      1       2
             *
             *      3       0
             *

702          KK  R33-35
703          KM        ROUTE FLOW ALONG CHANNEL FROM SUB33 TO SUB35
704          RS       1    FLOW      -1
705          SV       0       5      10      22      50      93     142
706          SQ       0      75     250     500    1200    2400    4000
             *

707          KK   SUB34
708          KM   SUB-BASIN SUB34
709          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
710          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
711          KM     L =  .57  Kb = .050  Adj. Slope =   87.0
712          BA    .167
713          LG    .284    .250   3.950    .590  20.000
714          UC    .617    .383
715          UA       0       5      16      30      65      77      84      90      94      97
716          UA     100
             *
```

```
LINE          ID.......1.......2.......3.......4.......5.......6.......7.......8.......9......10

  717         KK   DIV34
  718         KM        DIVERT FOR IRRIGATED LAWNS SUB34
  719         DT     D34    1.53
  720         DI       0       1
  721         DQ       0    .366
              *

  722         KK  R34-35
  723         KM        ROUTE FLOW FROM SUB34 TO SUB35
  724         RK  1531.2    .018    .016            TRAP      40       1     YES
              *

  725         KK   SUB35
  726         KM   SUB-BASIN SUB35
  727         KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
  728         KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
  729         KM     L =  .29  Kb = .048  Adj. Slope =   51.0
  730         BA    .128
  731         LG    .223    .250   3.950    .600  39.000
  732         UC    .400    .160
  733         UA       0       5      16      30      65      77      84      90      94      97
  734         UA     100
              *

  735         KK   DIV35
  736         KM        DIVERT FOR IRRIGATED LAWNS SUB35
  737         DT     D35     .53
  738         DI     0.0     1.0
  739         DQ     0.0    .095
              *

  740         KK  C35-33
  741         KM        COMBINE SUB34, SUB33 WITH SUB35
  742         HC       3
              *
              *      3       0
              *

  743         KK  R35-36
  744         KM        ROUTE FLOW ALONG CHANNEL FROM SUB35 TO SUB36
  745         RS       1    FLOW      -1
  746         SV       0       4       9      28      67     131     179
  747         SQ       0      75     250     500    1200    2400    4000
              *

  748         KK   SUB40
  749         KM   SUB-BASIN SUB40
  750         KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
  751         KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
  752         KM     L =  .31  Kb = .090  Adj. Slope = 1822.0
  753         BA    .074
  754         LG    .203    .314   4.000    .420  11.000
  755         UC    .188    .100
  756         UA       0       3       5       8      12      20      43      75      90      96
```



```
LINE          ID.......1.......2.......3.......4.......5.......6.......7.......8.......9......10

  757         UA     100
              *

  758         KK  R40-41
  759         KM        ROUTE FLOW FROM SUB40 TO SUB41
  760         RK    1452   .0221     .05            TRAP       6       2     YES
              *

  761         KK   SUB41
  762         KM   SUB-BASIN SUB41
  763         KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
  764         KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
  765         KM     L =  .54  Kb = .053  Adj. Slope =  110.0
  766         BA    .156
  767         LG    .281    .252   4.350    .420  16.000
  768         UC    .508    .308
```

```
769          UA       0       5      16      30      65      77      84      90      94      97
770          UA     100
             *

771          KK  C40-41
772          KM        COMBINE HYDROGRAPH SUB40 & SUB41 AT CP41
773          HC       2
             *

774          KK  R41-39
775          KM        ROUTE FLOW FROM SUB41 TO   SUB39
776          RK    2865   .0341     .05            TRAP       4       3     YES
             *

777          KK   SUB37
778          KM   SUB-BASIN SUB37
779          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
780          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
781          KM     L =  .30  Kb = .059  Adj. Slope =  247.0
782          BA    .049
783          LG    .300    .250   3.950    .490   5.000
784          UC    .321    .223
785          UA       0       5      16      30      65      77      84      90      94      97
786          UA     100
             *

787          KK  R37-39
788          KM        ROUTE FLOW FROM SUB37 TO   SUB39
789          RK    3500    .018    .016            TRAP      70       1     YES
             *

790          KK   SUB39
791          KM   SUB-BASIN SUB39
792          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
793          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
794          KM     L =  .84  Kb = .050  Adj. Slope =   79.0
795          BA    .224
796          LG    .233    .259   4.300    .450  29.000
797          UC    .667    .481
```



```
LINE         ID.......1.......2.......3.......4.......5.......6.......7.......8.......9......10

798          UA       0       5      16      30      65      77      84      90      94      97
799          UA     100
             *

800          KK  D39-36
801          KM        DIVERT FLOW OF CAMELBACK RD. OVERTOPPING AND RUNNING TO SUB36
802          DT  D39-36
803          DI       0    99.5     160     200     300     500     700    1000
804          DQ       0       0       0      40     140     340     540     840
             *

805          KK   DCBR1
806          KM        DIVERT 55 CFS FROM WATERSHED STORM DRAIN OUTLETS TO 40TH STREET SYSTEM
807          DT   DCBR1
808          DI       0      20      50      55     100     200     500    1000    2000    3000
809          DQ       0      20      50      55      55      55      55      55      55      55
             *

810          KK   DCBR2
811          KM        DIVERT 60 CFS FOR STROM DRAIN THAT OUTLETS INTO AZ. CANAL IN SUBBASIN 36
812          DT   DCBR2
813          DI       0      20      50      60     150     300     600    1000    2000    3000
814          DQ       0      20      50      60      60      60      60      60      60      60
             *

815          KK  RD3839
816          KM        RECALL DIVERSION FROM SUBBASIN 38
817          DR  D38-39
             *

818          KK  C37-41
819          KM        COMBINE HYDROGRAPHS SUB41, SUB37 & SUB39 AT CP39 AND RECALL DIVERSION
820          HC       4
             *

821          KK  R39-36
```

```
822          KM        ROUTE FLOW FROM SUB39 TO   SUB36
823          RK    1250    .006    .016            TRAP      26       1     YES
             *

824          KK   SUB36
825          KM   SUB-BASIN SUB36
826          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
827          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
828          KM     L =  .28  Kb = .052  Adj. Slope =   14.0
829          BA    .089
830          LG    .232    .250   3.950    .590  41.000
831          UC    .646    .327
832          UA       0       5      16      30      65      77      84      90      94      97
833          UA     100
             *
```



```
LINE         ID.......1.......2.......3.......4.......5.......6.......7.......8.......9......10

834          KK   DIV36
835          KM        DIVERT FOR IRRIGATED LAWNS SUB36
836          DT     D36     .61
837          DI     0.0     1.0
838          DQ     0.0    .150
             *

839          KK  RDCBR2
840          KM        RECALL DIVERSION FOR STORM DRAIN ALONG CAMELBACK RD.
841          DR   DCBR2
             *

842          KK  RD39366
843          KM        RECALL DIVERSION FROM SUB 39 TO    SUB36
844          DR  D39-36
             *

845          KK  C36-35
846          KM        COMBINE SUB39, SUB35, 2 RECALLED DIVERSIONS AND SUB36
847          HC       5
             *

848          KK   D40ST
849          KM        DIVERT FLOW FOR 40TH ST.
850          DT   D40ST
851          DI       0      10     100     300     500     700     900    1100    1300    1500
852          DQ       0       0      90     290     490     690     890    1090    1290    1490
             *
             *     3       0
             *

853          KK  R36-42
854          KM        ROUTE FLOW FROM SUB36 TO SUB42
855          RS       1    FLOW      -1
856          SV       0       3       6      10      34      60     130
857          SQ       0      75     250     500    1200    2400    4000
             *

858          KK   SUB42
859          KM   SUB-BASIN SUB42
860          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
861          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
862          KM     L =  .51  Kb = .044  Adj. Slope =   29.0
863          BA    .206
864          LG    .247    .250   5.600    .250  27.000
865          UC    .587    .294
866          UA       0       5      16      30      65      77      84      90      94      97
867          UA     100
             *
```



```
LINE         ID.......1.......2.......3.......4.......5.......6.......7.......8.......9......10

868          KK   DIV42
869          KM        DIVERT FOR IRRIGATED LAWNS SUB42
870          DT     D42     .75
871          DI       0       1
872          DQ       0    .072
```

```
                    *      1       2
                    *

873                 KK  C42-36
874                 KM        COMBINE HYDROGRAPH SUB42 WITH SUB36
875                 HC       2
                    *
                    *      3       0
                    *
876                 ZZ
```

SCHEMATIC DIAGRAM OF STREAM NETWORK

```
PUT
LINE      (V) ROUTING          (--->) DIVERSION OR PUMP FLOW

NO.       (.) CONNECTOR        (<---) RETURN OF DIVERTED OR PUMPED FLOW

 5          SUB1
               V
               V
 22         R1-2
               .
               .
 25            .        SUB2
               .           .
               .           .
 37            .           .------->      D2
 35            .        DIV2
               .           .
               .           .
 40         C1-2............
               V
               V
 43         R2-3
               .
               .
 46            .        SUB3
               .           .
               .           .
 58            .           .------->      D3
 56            .        DIV3
               .           .
               .           .
 61         C2-3............
               V
               V
 64         R3-4
               .
               .
 67            .        SUB4
               .           .
               .           .
 79            .           .------->      D4
 77            .        DIV4
               .           .
               .           .
 82         C3-4............
               .
               .
 87            .------->    DIBW
 85       DIVIBW
               V
               V
 90         R4-5
               .
               .
 93            .        SUB5
               .           .
               .           .
105            .           .------->      D5
103            .        DIV5
               .           .
               .           .
108         C4-5............
               .
               .
111            .        SUB6
               .           V
               .           V
```

```
121          .        R6-7
             .          .
             .          .
124          .          .        SUB7
             .          .          .
             .          .          .
136          .          .          .-------->     D7
134          .          .        DIV7
             .          .          .
             .          .          .
139          .        C6-7............
             .          V
             .          V
142          .        R7-8
             .          .
             .          .
145          .          .        SUB8
             .          .          .
             .          .          .
157          .          .          .-------->     D8
155          .          .        DIV8
             .          .          .
             .          .          .
160          .        C7-8............
             .          V
             .          V
163          .        R8-9
             .          .
             .          .
166          .          .        SUB9
             .          .          .
             .          .          .
178          .          .          .-------->     D9
176          .          .        DIV9
             .          .          .
             .          .          .
181          .        C8-9............
             .          V
             .          V
184          .        R9-5
             .          .
             .          .
187       C9-5............
             V
             V
190      R5-10
             .
             .
195          .       SUB10
             .          .
             .          .
207          .          .-------->     D10
205          .       DIV10
             .          .
             .          .
210      C5-10............
             V
             V
213      R10-15
             .
             .
218          .       SUB11
             .          V
             .          V
228          .      R11-12
             .          .
             .          .
231          .          .        SUB12
             .          .          .
             .          .          .
243          .          .          .-------->     D12
241          .          .        DIV12
             .          .          .
             .          .          .
246          .      C11-12............
             .          V
             .          V
249          .      R12-13
             .          .
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                .          .
252             .          .       SUB13
                .          .          .
                .          .          .
264             .          .          .-------->     D13
262             .          .       DIV13
                .          .          .
                .          .          .
267             .     C12-13............
                .          V
                .          V
270             .     R13-14
                .          .
                .          .
273             .          .       SUB14
                .          .          .
                .          .          .
285             .          .          .-------->     D14
283             .          .       DIV14
                .          .          .
                .          .          .
288             .     C13-14............
                .          V
                .          V
291             .     R14-15
                .          .
                .          .
294             .          .       SUB15
                .          .          .
                .          .          .
306             .          .          .-------->     D15
304             .          .       DIV15
                .          .          .
                .          .          .
309        C15-10........................
                .
                .
314             .-------->   D56ST
312        D56ST
                V
                V
317        R15-20
                .
                .
322             .      SUB16
                .          V
                .          V
332             .     R16-17
                .          .
                .          .
335             .          .       SUB17
                .          .          .
                .          .          .
347             .          .          .-------->     D17
345             .          .       DIV17
                .          .          .
                .          .          .
350             .     C16-17............
                .          V
                .          V
353             .     R17-18
                .          .
                .          .
356             .          .       SUB18
                .          .          .
                .          .          .
368             .          .          .-------->     D18
366             .          .       DIV18
                .          .          .
                .          .          .
371             .     C17-18............
                .          V
                .          V
374             .     R18-19
                .          .
                .          .
377             .          .       SUB19
                .          .          .
                .          .          .
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```
389          .          .          .-------->    D19
387          .          .      DIV19
             .          .          .
             .          .          .
392          .     C18-19...........
             .          V
             .          V
395          .     R19-20
             .          .
             .          .
398          .          .      SUB20
             .          .          .
             .          .          .
410          .          .          .-------->    D20
408          .          .      DIV20
             .          .          .
             .          .          .
413     C20-15.......................
             V
             V
416     R20-25
             .
             .
421          .      SUB21
             .          V
             .          V
431          .     R21-22
             .          .
             .          .
434          .          .      SUB22
             .          .          .
             .          .          .
446          .          .          .-------->    D22
444          .          .      DIV22
             .          .          .
             .          .          .
449          .     C21-22...........
             .          V
             .          V
452          .     R22-23
             .          .
             .          .
455          .          .      SUB23
             .          .          .
             .          .          .
467          .          .          .-------->    D23
465          .          .      DIV23
             .          .          .
             .          .          .
470          .     C22-23...........
             .          V
             .          V
473          .     R23-24
             .          .
             .          .
476          .          .      SUB24
             .          .          .
             .          .          .
488          .          .          .-------->    D24
486          .          .      DIV24
             .          .          .
             .          .          .
491          .     C23-24...........
             .          V
             .          V
494          .     R24-25
             .          .
             .          .
497          .          .      SUB25
             .          .          .
             .          .          .
509          .          .          .-------->    D25
507          .          .      DIV25
             .          .          .
             .          .          .
512     C25-20.......................
             V
             V
515     R25-29
```

```
          .
          .
520       .      SUB26
          .          .
          .          .
532       .          .-------->    D26
530       .      DIV26
          .          V
          .          V
535       .      R26-27
          .          .
          .          .
538       .          .      SUB27
          .          .          .
          .          .          .
550       .          .          .-------->    D27
548       .          .      DIV27
          .          .          .
          .          .          .
553       .      C26-27............
          .          V
          .          V
556       .      R27-28
          .          .
          .          .
559       .          .      SUB28
          .          .          .
          .          .          .
571       .          .          .-------->    D28
569       .          .      DIV28
          .          .          .
          .          .          .
574       .      C27-28............
          .          V
          .          V
577       .      R28-29
          .          .
          .          .
580       .          .      SUB29
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592       .          .          .-------->    D29
590       .          .      DIV29
          .          .          .
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595     C29-25........................
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600       .-------->   DOCCC
598     DOCCC
          V
          V
603     R29-33
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608       .      SUB38
          .          .
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620       .          .-------->  D38-39
618       .      D38-39
          .          V
          .          V
623       .      R38-30
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626       .          .      SUB30
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636       .      C30-38............
          .          V
          .          V
639       .      R30-31
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642       .          .      SUB31
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654       .          .          .-------->    D31
652       .          .      DIV31
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657             .     C30-31...........
                .          V
                .          V
660             .     R31-32
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663             .          .     SUB32
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                .          .          .
675             .          .          .-------->     D32
673             .          .     DIV32
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678             .     C31-32...........
                .          V
                .          V
681             .     R32-33
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684             .          .     SUB33
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                .          .          .
696             .          .          .-------->     D33
694             .          .     DIV33
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699        C33-29.......................
                V
                V
702        R33-35
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707             .     SUB34
                .          .
                .          .
719             .          .-------->     D34
717             .     DIV34
                .          V
                .          V
722             .     R34-35
                .          .
                .          .
725             .          .     SUB35
                .          .          .
                .          .          .
737             .          .          .-------->     D35
735             .          .     DIV35
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                .          .          .
740        C35-33.......................
                V
                V
743        R35-36
                .
                .
748             .     SUB40
                .          V
                .          V
758             .     R40-41
                .          .
                .          .
761             .          .     SUB41
                .          .          .
                .          .          .
771             .     C40-41...........
                .          V
                .          V
774             .     R41-39
                .          .
                .          .
777             .          .     SUB37
                .          .          V
                .          .          V
787             .          .    R37-39
                .          .          .
                .          .          .
790             .          .          .     SUB39
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802             .          .          .          .-------> D39-36
800             .          .          .     D39-36
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807             .          .          .          .------->  DCBR1
805             .          .          .      DCBR1
                .          .          .          .
                .          .          .          .
812             .          .          .          .------->  DCBR2
810             .          .          .      DCBR2
                .          .          .          .
                .          .          .          .
817             .          .          .          .          .<-------  D38-39
815             .          .          .          .     RD3839
                .          .          .          .          .
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818             .     C37-41.......................................
                .          V
                .          V
821             .     R39-36
                .          .
                .          .
824             .          .      SUB36
                .          .          .
                .          .          .
836             .          .          .------->     D36
834             .          .      DIV36
                .          .          .
                .          .          .
841             .          .          .          .<-------  DCBR2
839             .          .          .     RDCBR2
                .          .          .          .
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844             .          .          .          .          .<-------  D39-36
842             .          .          .          .     RD3936
                .          .          .          .          .
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845        C36-35.............................................
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850             .------->  D40ST
848        D40ST
                V
                V
853        R36-42
                .
                .
858             .     SUB42
                .          .
                .          .
870             .          .------->     D42
868             .     DIV42
                .          .
                .          .
873        C42-36............
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(***) RUNOFF ALSO COMPUTED AT THIS LOCATION

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****************************************
*                                      *
*   FLOOD HYDROGRAPH PACKAGE  (HEC-1)  *
*             MAY   1991               *
*          VERSION 4.0.1E              *
*                                      *
*  RUN DATE  09/01/95  TIME  05:32:32  *
*                                      *
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****************************************
*                                      *
*    U.S. ARMY CORPS OF ENGINEERS      *
*    HYDROLOGIC ENGINEERING CENTER     *
*          609 SECOND STREET           *
*       DAVIS, CALIFORNIA 95616        *
*           (916) 551-1748             *
*                                      *
****************************************
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DDM MCUHP1 ARCADIA AREA 50-yr 6hr

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  4 IO          OUTPUT CONTROL VARIABLES
                      IPRNT           5  PRINT CONTROL
                      IPLOT           0  PLOT CONTROL
```

```
                QSCAL          0.  HYDROGRAPH PLOT SCALE

IT          HYDROGRAPH TIME DATA
                 NMIN            5  MINUTES IN COMPUTATION INTERVAL
                IDATE      1     0  STARTING DATE
                ITIME         0000  STARTING TIME
                   NQ          300  NUMBER OF HYDROGRAPH ORDINATES
               NDDATE      2     0  ENDING DATE
               NDTIME         0055  ENDING TIME
               ICENT           19  CENTURY MARK

          COMPUTATION INTERVAL    0.08 HOURS
               TOTAL TIME BASE   24.92 HOURS

     ENGLISH UNITS
          DRAINAGE AREA          SQUARE MILES
          PRECIPITATION DEPTH    INCHES
          LENGTH, ELEVATION      FEET
          FLOW                   CUBIC FEET PER SECOND
          STORAGE VOLUME         ACRE-FEET
          SURFACE AREA           ACRES
          TEMPERATURE            DEGREES FAHRENHEIT
```

RUNOFF SUMMARY
FLOW IN CUBIC FEET PER SECOND
TIME IN HOURS, AREA IN SQUARE MILES

OPERATION	STATION	PEAK FLOW	TIME OF PEAK	AVERAGE FLOW FOR MAXIMUM PERIOD 6-HOUR	24-HOUR	72-HOUR	BASIN AREA	MAXIMUM STAGE	TIME OF MAX STAGE
HYDROGRAPH AT	SUB1	47.	4.08	7.	2.	2.	0.04		
+ ROUTED TO	R1-2	47.	4.17	7.	2.	2.	0.04		
HYDROGRAPH AT	SUB2	61.	4.33	11.	3.	3.	0.12		
DIVERSION TO	D2	23.	4.42	2.	0.	0.	0.12		
+ HYDROGRAPH AT	DIV2	60.	4.42	10.	2.	2.	0.12		
2 COMBINED AT	C1-2	94.	4.42	17.	4.	4.	0.16		
ROUTED TO	R2-3	93.	4.42	17.	4.	4.	0.16		
+ HYDROGRAPH AT	SUB3	44.	4.25	7.	2.	2.	0.07		
DIVERSION TO	D3	25.	4.33	2.	0.	0.	0.07		
HYDROGRAPH AT	DIV3	42.	4.33	5.	1.	1.	0.07		
+ 2 COMBINED AT	C2-3	132.	4.42	22.	6.	5.	0.22		
ROUTED TO	R3-4	131.	4.42	22.	6.	5.	0.22		
HYDROGRAPH AT	SUB4	52.	4.17	8.	2.	2.	0.06		
+ DIVERSION TO	D4	29.	4.33	2.	1.	0.	0.06		
HYDROGRAPH AT	DIV4	48.	4.33	6.	1.	1.	0.06		
2 COMBINED AT	C3-4	174.	4.42	28.	7.	7.	0.29		

DIVERSION TO	DIBW	87.	4.42	15.	4.	4.	0.29
HYDROGRAPH AT	DIVIBW	87.	4.42	12.	3.	3.	0.29
ROUTED TO	R4-5	86.	4.42	12.	3.	3.	0.29
HYDROGRAPH AT	SUB5	31.	4.50	8.	2.	2.	0.07
DIVERSION TO	D5	16.	4.75	2.	0.	0.	0.07
HYDROGRAPH AT	DIV5	28.	4.75	6.	2.	1.	0.07
2 COMBINED AT	C4-5	102.	4.42	18.	5.	4.	0.35
HYDROGRAPH AT	SUB6	125.	4.00	18.	5.	4.	0.09
ROUTED TO	R6-7	120.	4.17	18.	5.	4.	0.09
HYDROGRAPH AT	SUB7	116.	4.25	20.	5.	5.	0.15
DIVERSION TO	D7	50.	4.42	5.	1.	1.	0.15
HYDROGRAPH AT	DIV7	100.	4.42	16.	4.	4.	0.15
2 COMBINED AT	C6-7	184.	4.17	34.	8.	8.	0.24
ROUTED TO	R7-8	181.	4.25	33.	8.	8.	0.24
HYDROGRAPH AT	SUB8	32.	4.42	7.	2.	2.	0.07
DIVERSION TO	D8	19.	4.58	2.	0.	0.	0.07
HYDROGRAPH AT	DIV8	30.	4.58	5.	1.	1.	0.07
2 COMBINED AT	C7-8	193.	4.25	39.	10.	9.	0.31
ROUTED TO	R8-9	192.	4.25	39.	10.	9.	0.31
HYDROGRAPH AT	SUB9	49.	4.17	7.	2.	2.	0.06
DIVERSION TO	D9	28.	4.25	2.	0.	0.	0.06
HYDROGRAPH AT	DIV9	48.	4.25	5.	1.	1.	0.06
2 COMBINED AT	C8-9	240.	4.25	44.	11.	11.	0.38
ROUTED TO	R9-5	234.	4.33	44.	11.	11.	0.38
2 COMBINED AT	C9-5	326.	4.33	62.	16.	15.	0.73
ROUTED TO	R5-10	280.	4.67	62.	16.	15.	0.73

HYDROGRAPH AT	SUB10	66.	4.25	11.	3.	3.	0.09
+ DIVERSION TO	D10	29.	4.42	2.	1.	1.	0.09
HYDROGRAPH AT	DIV10	62.	4.42	9.	2.	2.	0.09
2 COMBINED AT	C5-10	329.	4.50	71.	18.	17.	0.82
+ ROUTED TO	R10-15	310.	4.75	71.	18.	17.	0.82
HYDROGRAPH AT	SUB11	106.	4.08	16.	4.	4.	0.09
ROUTED TO	R11-12	105.	4.17	16.	4.	4.	0.09
+ HYDROGRAPH AT	SUB12	137.	4.00	16.	4.	4.	0.12
DIVERSION TO	D12	11.	4.08	1.	0.	0.	0.12
HYDROGRAPH AT	DIV12	135.	4.08	15.	4.	4.	0.12
2 COMBINED AT	C11-12	236.	4.08	32.	8.	8.	0.21
+ ROUTED TO	R12-13	229.	4.08	31.	8.	8.	0.21
HYDROGRAPH AT	SUB13	153.	4.08	18.	5.	4.	0.13
DIVERSION TO	D13	30.	4.08	2.	0.	0.	0.13
+ HYDROGRAPH AT	DIV13	135.	4.08	17.	4.	4.	0.13
2 COMBINED AT	C12-13	364.	4.08	48.	12.	12.	0.34
+ ROUTED TO	R13-14	362.	4.17	48.	12.	12.	0.34
HYDROGRAPH AT	SUB14	96.	4.17	12.	3.	3.	0.13
DIVERSION TO	D14	49.	4.17	3.	1.	1.	0.13
+ HYDROGRAPH AT	DIV14	96.	4.17	9.	2.	2.	0.13
2 COMBINED AT	C13-14	458.	4.17	57.	14.	14.	0.47
ROUTED TO	R14-15	444.	4.17	57.	14.	14.	0.47
+ HYDROGRAPH AT	SUB15	95.	4.25	15.	4.	4.	0.13
DIVERSION TO	D15	55.	4.33	4.	1.	1.	0.13
HYDROGRAPH AT	DIV15	91.	4.33	11.	3.	3.	0.13
+ 3 COMBINED AT	C15-10	645.	4.33	138.	35.	34.	1.42
DIVERSION TO							

+	D56ST	235.	4.33	18.	5.	4.	1.42
HYDROGRAPH AT	D56ST	410.	4.33	120.	30.	29.	1.42
ROUTED TO	R15-20	363.	4.92	112.	30.	29.	1.42
HYDROGRAPH AT	SUB16	158.	4.08	25.	6.	6.	0.13
+ ROUTED TO	R16-17	155.	4.17	25.	6.	6.	0.13
HYDROGRAPH AT	SUB17	62.	4.08	8.	2.	2.	0.07
DIVERSION TO	D17	4.	4.17	0.	0.	0.	0.07
+ HYDROGRAPH AT	DIV17	61.	4.17	7.	2.	2.	0.07
2 COMBINED AT	C16-17	216.	4.17	33.	8.	8.	0.20
ROUTED TO	R17-18	215.	4.17	33.	8.	8.	0.20
+ HYDROGRAPH AT	SUB18	49.	4.17	7.	2.	2.	0.07
DIVERSION TO	D18	24.	4.17	2.	0.	0.	0.07
HYDROGRAPH AT	DIV18	49.	4.17	5.	1.	1.	0.07
+ 2 COMBINED AT	C17-18	264.	4.17	38.	9.	9.	0.27
ROUTED TO	R18-19	257.	4.17	38.	9.	9.	0.27
HYDROGRAPH AT	SUB19	51.	4.17	7.	2.	2.	0.08
+ DIVERSION TO	D19	29.	4.25	2.	0.	0.	0.08
HYDROGRAPH AT	DIV19	49.	4.25	5.	1.	1.	0.08
2 COMBINED AT	C18-19	300.	4.17	43.	11.	10.	0.34
+ ROUTED TO	R19-20	300.	4.25	43.	11.	10.	0.34
HYDROGRAPH AT	SUB20	103.	4.17	14.	4.	3.	0.13
DIVERSION TO	D20	58.	4.25	4.	1.	1.	0.13
+ HYDROGRAPH AT	DIV20	98.	4.25	10.	3.	2.	0.13
3 COMBINED AT	C20-15	552.	4.42	162.	44.	42.	1.89
ROUTED TO	R20-25	377.	5.17	134.	44.	42.	1.89
+ HYDROGRAPH AT	SUB21	159.	4.08	24.	6.	6.	0.12
ROUTED TO	R21-22	158.	4.17	24.	6.	6.	0.12

HYDROGRAPH AT	SUB22	63.	4.25	11.	3.	3.	0.11
DIVERSION TO	D22	4.	4.33	0.	0.	0.	0.11
HYDROGRAPH AT	DIV22	63.	4.33	11.	3.	3.	0.11
2 COMBINED AT	C21-22	213.	4.17	35.	9.	8.	0.24
ROUTED TO	R22-23	211.	4.17	35.	9.	8.	0.24
HYDROGRAPH AT	SUB23	45.	4.08	6.	1.	1.	0.06
DIVERSION TO	D23	23.	4.17	1.	0.	0.	0.06
HYDROGRAPH AT	DIV23	44.	4.17	4.	1.	1.	0.06
2 COMBINED AT	C22-23	255.	4.17	39.	10.	9.	0.30
ROUTED TO	R23-24	250.	4.17	39.	10.	9.	0.30
HYDROGRAPH AT	SUB24	50.	4.17	7.	2.	2.	0.08
DIVERSION TO	D24	27.	4.25	2.	0.	0.	0.08
HYDROGRAPH AT	DIV24	49.	4.25	6.	1.	1.	0.08
2 COMBINED AT	C23-24	297.	4.25	45.	11.	11.	0.37
ROUTED TO	R24-25	293.	4.25	45.	11.	11.	0.37
HYDROGRAPH AT	SUB25	47.	4.25	7.	2.	2.	0.08
DIVERSION TO	D25	28.	4.33	2.	0.	0.	0.08
HYDROGRAPH AT	DIV25	45.	4.33	5.	1.	1.	0.08
3 COMBINED AT	C25-20	442.	4.83	178.	56.	54.	2.34
ROUTED TO	R25-29	413.	5.25	177.	56.	54.	2.34
HYDROGRAPH AT	SUB26	34.	4.17	5.	1.	1.	0.05
DIVERSION TO	D26	9.	4.17	1.	0.	0.	0.05
HYDROGRAPH AT	DIV26	34.	4.17	5.	1.	1.	0.05
ROUTED TO	R26-27	33.	4.25	5.	1.	1.	0.05
HYDROGRAPH AT	SUB27	43.	4.17	6.	1.	1.	0.06
DIVERSION TO	D27	22.	4.17	1.	0.	0.	0.06

HYDROGRAPH AT	DIV27	43.	4.17	4.	1.	1.	0.06
2 COMBINED AT	C26-27	74.	4.17	9.	2.	2.	0.11
ROUTED TO	R27-28	73.	4.25	9.	2.	2.	0.11
HYDROGRAPH AT	SUB28	53.	4.17	8.	2.	2.	0.08
DIVERSION TO	D28	30.	4.25	2.	0.	0.	0.08
HYDROGRAPH AT	DIV28	51.	4.25	6.	1.	1.	0.08
2 COMBINED AT	C27-28	123.	4.25	15.	4.	4.	0.19
ROUTED TO	R28-29	119.	4.25	15.	4.	4.	0.19
HYDROGRAPH AT	SUB29	37.	4.25	6.	1.	1.	0.06
DIVERSION TO	D29	21.	4.25	1.	0.	0.	0.06
HYDROGRAPH AT	DIV29	37.	4.25	4.	1.	1.	0.06
3 COMBINED AT	C29-25	430.	5.08	195.	61.	59.	2.59
DIVERSION TO	DOCCC	430.	0.08	195.	61.	59.	2.59
HYDROGRAPH AT	DOCCC	0.	0.08	0.	0.	0.	2.59
ROUTED TO	R29-33	0.	0.08	0.	0.	0.	2.59
HYDROGRAPH AT	SUB38	223.	4.25	43.	11.	10.	0.25
DIVERSION TO	D38-39	16.	4.25	11.	3.	3.	0.25
HYDROGRAPH AT	D38-39	207.	4.25	32.	8.	8.	0.25
ROUTED TO	R38-30	207.	4.33	32.	8.	8.	0.25
HYDROGRAPH AT	SUB30	46.	4.17	6.	2.	2.	0.06
2 COMBINED AT	C30-38	247.	4.25	39.	10.	9.	0.32
ROUTED TO	R30-31	246.	4.33	39.	10.	9.	0.32
HYDROGRAPH AT	SUB31	36.	4.17	5.	1.	1.	0.06
DIVERSION TO	D31	14.	4.25	1.	0.	0.	0.06
HYDROGRAPH AT	DIV31	34.	4.25	4.	1.	1.	0.06
2 COMBINED AT	C30-31	279.	4.25	43.	11.	10.	0.38
ROUTED TO							

+	R31-32	277.	4.33	43.	11.	10.	0.38
HYDROGRAPH AT	SUB32	41.	4.17	6.	2.	2.	0.06
DIVERSION TO	D32	22.	4.25	2.	0.	0.	0.06
HYDROGRAPH AT +	DIV32	41.	4.25	5.	1.	1.	0.06
2 COMBINED AT	C31-32	315.	4.33	48.	12.	12.	0.44
ROUTED TO	R32-33	315.	4.33	48.	12.	12.	0.44
HYDROGRAPH AT +	SUB33	48.	4.17	7.	2.	2.	0.06
DIVERSION TO	D33	17.	4.25	1.	0.	0.	0.06
HYDROGRAPH AT	DIV33	44.	4.25	6.	1.	1.	0.06
3 COMBINED AT +	C33-29	355.	4.33	54.	13.	13.	3.09
ROUTED TO	R33-35	242.	4.67	53.	13.	13.	3.09
HYDROGRAPH AT	SUB34	94.	4.25	18.	5.	4.	0.17
DIVERSION TO +	D34	35.	4.42	3.	1.	1.	0.17
HYDROGRAPH AT	DIV34	91.	4.42	15.	4.	4.	0.17
ROUTED TO	R34-35	86.	4.50	15.	4.	4.	0.17
HYDROGRAPH AT +	SUB35	122.	4.08	19.	5.	5.	0.13
DIVERSION TO	D35	12.	4.08	1.	0.	0.	0.13
HYDROGRAPH AT	DIV35	110.	4.08	18.	5.	4.	0.13
3 COMBINED AT +	C35-33	371.	4.50	85.	22.	21.	3.39
ROUTED TO	R35-36	274.	4.92	85.	22.	21.	3.39
HYDROGRAPH AT	SUB40	74.	4.08	8.	2.	2.	0.07
ROUTED TO +	R40-41	71.	4.08	8.	2.	2.	0.07
HYDROGRAPH AT	SUB41	112.	4.25	18.	5.	4.	0.16
2 COMBINED AT	C40-41	178.	4.17	26.	6.	6.	0.23
ROUTED TO +	R41-39	175.	4.25	26.	6.	6.	0.23
HYDROGRAPH AT	SUB37	35.	4.08	4.	1.	1.	0.05
ROUTED TO	R37-39	35.	4.25	4.	1.	1.	0.05

HYDROGRAPH AT	SUB39	143.	4.33	31.	8.	8.	0.22
DIVERSION TO	D39-36	0.	4.33	0.	0.	0.	0.22
HYDROGRAPH AT	D39-36	143.	4.33	31.	8.	8.	0.22
DIVERSION TO	DCBR1	55.	4.33	21.	5.	5.	0.22
HYDROGRAPH AT	DCBR1	88.	4.33	11.	3.	3.	0.22
DIVERSION TO	DCBR2	60.	4.33	9.	2.	2.	0.22
HYDROGRAPH AT	DCBR2	28.	4.33	2.	0.	0.	0.22
HYDROGRAPH AT	RD3839	16.	3.42	11.	3.	3.	0.00
4 COMBINED AT	C37-41	249.	4.25	43.	11.	10.	0.50
ROUTED TO	R39-36	245.	4.25	43.	11.	10.	0.50
HYDROGRAPH AT	SUB36	68.	4.25	14.	3.	3.	0.09
DIVERSION TO	D36	10.	4.50	1.	0.	0.	0.09
HYDROGRAPH AT	DIV36	59.	4.50	13.	3.	3.	0.09
HYDROGRAPH AT	RDCBR2	60.	4.17	9.	2.	2.	0.00
HYDROGRAPH AT	RD3936	0.	0.08	0.	0.	0.	0.00
5 COMBINED AT	C36-35	551.	4.50	146.	38.	37.	3.98
DIVERSION TO	D40ST	541.	1.00	136.	34.	33.	3.98
HYDROGRAPH AT	D40ST	10.	1.00	10.	4.	3.	3.98
ROUTED TO	R36-42	10.	5.33	10.	4.	3.	3.98
HYDROGRAPH AT	SUB42	184.	4.25	32.	8.	8.	0.21
DIVERSION TO	D42	13.	4.25	2.	0.	0.	0.21
HYDROGRAPH AT	DIV42	170.	4.25	31.	8.	7.	0.21
2 COMBINED AT	C42-36	180.	4.25	40.	11.	11.	4.19

SUMMARY OF KINEMATIC WAVE - MUSKINGUM-CUNGE ROUTING
(FLOW IS DIRECT RUNOFF WITHOUT BASE FLOW)

ISTAQ	ELEMENT	DT	PEAK	TIME TO PEAK	VOLUME	INTERPOLATED TO COMPUTATION INTERVAL DT	PEAK	TIME TO PEAK	VOLUME
		(MIN)	(CFS)	(MIN)	(IN)	(MIN)	(CFS)	(MIN)	(IN)

```
R1-2  MANE        4.67    47.25   253.09     1.85     5.00    46.74   250.00       1.85

NTINUITY SUMMARY (AC-FT) - INFLOW=0.3628E+01 EXCESS=0.0000E+00 OUTFLOW=0.3649E+01 BASIN STORAGE=0.1966E-05 PERCENT ERROR=  -0.6

R2-3  MANE        1.17    93.43   266.92     1.01     5.00    93.19   265.00       1.01

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.8385E+01 EXCESS=0.0000E+00 OUTFLOW=0.8391E+01 BASIN STORAGE=0.5170E-04 PERCENT ERROR=  -0.1

R3-4  MANE        0.99   131.63   265.81     0.93     5.00   131.37   265.00       0.93

NTINUITY SUMMARY (AC-FT) - INFLOW=0.1100E+02 EXCESS=0.0000E+00 OUTFLOW=0.1101E+02 BASIN STORAGE=0.8129E-04 PERCENT ERROR=  -0.1

R4-5  MANE        2.03    86.69   268.25     0.40     5.00    86.37   265.00       0.40

NTINUITY SUMMARY (AC-FT) - INFLOW=0.6093E+01 EXCESS=0.0000E+00 OUTFLOW=0.6116E+01 BASIN STORAGE=0.1016E-03 PERCENT ERROR=  -0.4

R6-7  MANE        3.79   122.97   246.69     1.87     5.00   120.28   250.00       1.87

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.8938E+01 EXCESS=0.0000E+00 OUTFLOW=0.8973E+01 BASIN STORAGE=0.3022E-05 PERCENT ERROR=  -0.4

R7-8  MANE        2.56   181.61   253.55     1.29     5.00   181.33   255.00       1.29

NTINUITY SUMMARY (AC-FT) - INFLOW=0.1669E+02 EXCESS=0.0000E+00 OUTFLOW=0.1673E+02 BASIN STORAGE=0.4143E-03 PERCENT ERROR=  -0.2

R8-9  MANE        0.66   192.89   256.29     1.16     5.00   191.58   255.00       1.17

NTINUITY SUMMARY (AC-FT) - INFLOW=0.1931E+02 EXCESS=0.0000E+00 OUTFLOW=0.1931E+02 BASIN STORAGE=0.1271E-03 PERCENT ERROR=   0.0

R9-5  MANE        0.96   239.38   257.01     1.10     5.00   233.77   260.00       1.10

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.2197E+02 EXCESS=0.0000E+00 OUTFLOW=0.2198E+02 BASIN STORAGE=0.3889E-03 PERCENT ERROR=  -0.1

R11-12  MANE      1.25   105.69   247.66     1.65     5.00   104.71   250.00       1.65

NTINUITY SUMMARY (AC-FT) - INFLOW=0.8171E+01 EXCESS=0.0000E+00 OUTFLOW=0.8180E+01 BASIN STORAGE=0.3409E-07 PERCENT ERROR=  -0.1

R12-13  MANE      0.07   235.08   246.76     1.38     5.00   228.60   245.00       1.38

NTINUITY SUMMARY (AC-FT) - INFLOW=0.1567E+02 EXCESS=0.0000E+00 OUTFLOW=0.1567E+02 BASIN STORAGE=0.1778E-04 PERCENT ERROR=   0.0

R13-14  MANE      0.56   363.69   246.42     1.31     5.00   361.80   250.00       1.31

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.2387E+02 EXCESS=0.0000E+00 OUTFLOW=0.2390E+02 BASIN STORAGE=0.4868E-04 PERCENT ERROR=  -0.1

R14-15  MANE      0.87   453.61   252.07     1.15     5.00   443.58   250.00       1.14

NTINUITY SUMMARY (AC-FT) - INFLOW=0.2856E+02 EXCESS=0.0000E+00 OUTFLOW=0.2858E+02 BASIN STORAGE=0.1890E-03 PERCENT ERROR=  -0.1

R16-17  MANE      1.13   158.05   247.29     1.82     5.00   155.25   250.00       1.82

NTINUITY SUMMARY (AC-FT) - INFLOW=0.1251E+02 EXCESS=0.0000E+00 OUTFLOW=0.1252E+02 BASIN STORAGE=0.2605E-07 PERCENT ERROR=  -0.1

R17-18  MANE      0.57   215.53   250.86     1.51     5.00   215.19   250.00       1.51
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ONTINUITY SUMMARY (AC-FT) - INFLOW=0.1623E+02 EXCESS=0.0000E+00 OUTFLOW=0.1624E+02 BASIN STORAGE=0.8204E-05 PERCENT ERROR=  -0.1

          R18-19  MANE        0.69    262.19    251.60      1.31      5.00    257.06    250.00        1.31

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.1881E+02 EXCESS=0.0000E+00 OUTFLOW=0.1882E+02 BASIN STORAGE=0.2774E-04 PERCENT ERROR=  -0.1

          R19-20  MANE        0.70    300.31    251.46      1.17      5.00    299.86    255.00        1.18

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.2153E+02 EXCESS=0.0000E+00 OUTFLOW=0.2155E+02 BASIN STORAGE=0.4787E-04 PERCENT ERROR=  -0.1

          R21-22  MANE        2.46    158.48    250.08      1.80      5.00    158.36    250.00        1.81

ONTINUITY SUMMARY (AC-FT) - INFLOW=0.1190E+02 EXCESS=0.0000E+00 OUTFLOW=0.1193E+02 BASIN STORAGE=0.5923E-06 PERCENT ERROR=  -0.3

          R22-23  MANE        0.46    212.88    250.86      1.38      5.00    210.74    250.00        1.38

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.1732E+02 EXCESS=0.0000E+00 OUTFLOW=0.1732E+02 BASIN STORAGE=0.4017E-05 PERCENT ERROR=   0.0

          R23-24  MANE        0.49    254.37    250.91      1.24      5.00    249.83    250.00        1.24

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.1950E+02 EXCESS=0.0000E+00 OUTFLOW=0.1951E+02 BASIN STORAGE=0.1421E-04 PERCENT ERROR=   0.0

          R24-25  MANE        0.76    295.74    256.40      1.12      5.00    293.14    255.00        1.12

ONTINUITY SUMMARY (AC-FT) - INFLOW=0.2230E+02 EXCESS=0.0000E+00 OUTFLOW=0.2231E+02 BASIN STORAGE=0.5054E-04 PERCENT ERROR=  -0.1

          R26-27  MANE        0.99     33.75    252.38      0.83      5.00     32.79    255.00        0.83

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.2353E+01 EXCESS=0.0000E+00 OUTFLOW=0.2356E+01 BASIN STORAGE=0.4631E-05 PERCENT ERROR=  -0.1

          R27-28  MANE        0.84     73.71    252.26      0.75      5.00     72.84    255.00        0.75

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.4548E+01 EXCESS=0.0000E+00 OUTFLOW=0.4554E+01 BASIN STORAGE=0.1552E-04 PERCENT ERROR=  -0.1

          R28-29  MANE        0.82    122.87    256.68      0.72      5.00    118.77    255.00        0.72

ONTINUITY SUMMARY (AC-FT) - INFLOW=0.7355E+01 EXCESS=0.0000E+00 OUTFLOW=0.7362E+01 BASIN STORAGE=0.3387E-04 PERCENT ERROR=  -0.1

          R38-30  MANE        0.37    207.13    255.80      1.19      5.00    206.99    260.00        1.19

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.1600E+02 EXCESS=0.0000E+00 OUTFLOW=0.1600E+02 BASIN STORAGE=0.1445E-05 PERCENT ERROR=   0.0

          R30-31  MANE        0.65    247.23    256.64      1.14      5.00    246.01    260.00        1.14

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.1918E+02 EXCESS=0.0000E+00 OUTFLOW=0.1918E+02 BASIN STORAGE=0.7531E-05 PERCENT ERROR=   0.0

          R31-32  MANE        0.58    278.47    256.39      1.06      5.00    277.35    260.00        1.06

ONTINUITY SUMMARY (AC-FT) - INFLOW=0.2134E+02 EXCESS=0.0000E+00 OUTFLOW=0.2135E+02 BASIN STORAGE=0.1483E-04 PERCENT ERROR=   0.0

          R32-33  MANE        1.48    315.38    259.83      1.01      5.00    315.38    260.00        1.01
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NTINUITY SUMMARY (AC-FT) - INFLOW=0.2371E+02 EXCESS=0.0000E+00 OUTFLOW=0.2372E+02 BASIN STORAGE=0.8545E-05 PERCENT ERROR=  -0.1

          R34-35  MANE        0.89     90.26    266.63      0.83      5.00     86.42    270.00        0.83

NTINUITY SUMMARY (AC-FT) - INFLOW=0.7405E+01 EXCESS=0.0000E+00 OUTFLOW=0.7412E+01 BASIN STORAGE=0.9983E-05 PERCENT ERROR=  -0.1

          R40-41  MANE        1.38     72.97    247.81      0.98      5.00     71.46    245.00        0.97

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.3841E+01 EXCESS=0.0000E+00 OUTFLOW=0.3850E+01 BASIN STORAGE=0.2740E-06 PERCENT ERROR=  -0.2

          R41-39  MANE        1.77    177.84    253.41      1.05      5.00    174.90    255.00        1.05

NTINUITY SUMMARY (AC-FT) - INFLOW=0.1284E+02 EXCESS=0.0000E+00 OUTFLOW=0.1286E+02 BASIN STORAGE=0.1640E-05 PERCENT ERROR=  -0.2

          R37-39  MANE        3.52     34.81    252.29      0.81      5.00     34.66    255.00        0.81

NTINUITY SUMMARY (AC-FT) - INFLOW=0.2099E+01 EXCESS=0.0000E+00 OUTFLOW=0.2114E+01 BASIN STORAGE=0.1973E-03 PERCENT ERROR=  -0.7

          R39-36  MANE        0.71    248.36    256.16      0.80      5.00    245.41    255.00        0.80

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.2134E+02 EXCESS=0.0000E+00 OUTFLOW=0.2135E+02 BASIN STORAGE=0.1102E-03 PERCENT ERROR=   0.0


** NORMAL END OF HEC-1 ***
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A-4

HEC-1 MODEL 100-YEAR EXISTING CONDITIONS

```
1*****************************************                    *****************************************
                                         *                    *                                       *
  FLOOD HYDROGRAPH PACKAGE  (HEC-1)      *                    *    U.S. ARMY CORPS OF ENGINEERS       *
             MAY   1991                  *                    *    HYDROLOGIC ENGINEERING CENTER      *
*          VERSION 4.0.1E                *                    *          609 SECOND STREET            *
*                                        *                    *       DAVIS, CALIFORNIA 95616         *
 RUN DATE  09/01/95  TIME  05:44:09      *                    *          (916) 551-1748               *
                                         *                    *                                       *
*****************************************                    *****************************************

                                  X     X  XXXXXXX   XXXXX          X
                                  X     X  X        X     X        XX
                                  X     X  X        X              X
                                  XXXXXXX  XXXX     X       XXXXX  X
                                  X     X  X        X              X
                                  X     X  X        X     X        X
                                  X     X  XXXXXXX   XXXXX        XXX

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE.
THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION
NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,
DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL   LOSS RATE:GREEN AND AMPT INFILTRATION
KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

                                          HEC-1 INPUT                                          PAGE  1

LINE          ID.......1.......2.......3.......4.......5.......6.......7.......8.......9......10

              *       ARCADIA AREA HYDROLOGY STUDY - EXISTING CONDITIONS.
              *       PREPARED BY: HUITT-ZOLLARS INC. 8-31-95
              *       PREPARED FOR: FCDMC CONTRACT # 94-21
    1         ID
    2         ID   DDM MCUHP1 ARCADIA AREA 100yr 6hr
    3         IT       5                    300
    4         IO       5
              *DIAGRAM
              *

    5         KK    SUB1
    6         KM   SUB-BASIN SUB1
    7         KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
    8         KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
    9         KM     L =  .28  Kb = .100  Adj. Slope = 2120.0
   10         BA    .037
   11         IN      15
   12         KM   RAINFALL DEPTH OF 2.00 WAS SPACIALLY REDUCED AS SHOWN BY THE PB RECORD
   13         PB   3.084
   14         KM   THE FOLLOWING PC RECORD USED A 6-HOUR STORM WITH A PATTERN No. OF 2.20
   15         PC    .000    .010    .017    .026    .037    .046    .056    .065    .075    .085
   16         PC    .097    .111    .131    .175    .263    .455    .689    .829    .893    .933
   17         PC    .949    .962    .975    .988   1.000
   18         LG    .142    .322   4.550    .310  52.000
   19         UC    .150    .107
   20         UA       0       3       5       8      12      20      43      75      90      96
   21         UA     100
              *

   22         KK    R1-2
   23         KM       ROUTE FLOW FROM SUB1 TO SUB2
   24         RK  3183.8   .0166     .07       0    TRAP       0       3     YES
              *

   25         KK    SUB2
   26         KM   SUB-BASIN SUB2
   27         KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
   28         KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
   29         KM     L =  .60  Kb = .041  Adj. Slope =   88.0
   30         BA    .119
   31         LG    .342    .250   4.650    .440   9.000
```

```
 32          UC    .596    .466
 33          UA       0       5      16      30      65      77      84      90      94      97
 34          UA     100
             *

 35          KK    DIV2
 36          KM        DIVERT FOR IRRIGATED LAWNS SUB2
 37          DT      D2     .80
 38          DI       0       1
 39          DQ       0    .382
             *
```



```
LINE         ID.......1.......2.......3.......4.......5.......6.......7.......8.......9......10

 40          KK    C1-2
 41          KM        COMBINE HYDROGRAPHS SUB1 AND SUB2 AT CP2
 42          HC       2
             *

 43          KK    R2-3
 44          KM        ROUTE FLOW FROM SUB2 TO SUB3
 45          RK  1367.5    .009    .016            TRAP      60       1     YES
             *

 46          KK    SUB3
 47          KM   SUB-BASIN SUB3
 48          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
 49          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
 50          KM     L =  .26  Kb = .058  Adj. Slope =   47.0
 51          BA    .067
 52          LG    .298    .250   4.250    .510  16.000
 53          UC    .533    .293
 54          UA       0       5      16      30      65      77      84      90      94      97
 55          UA     100
             *

 56          KK    DIV3
 57          KM        DIVERT FOR IRRIGATED LAWNS SUB3
 58          DT      D3     .88
 59          DI       0       1
 60          DQ       0    .573
             *

 61          KK    C2-3
 62          KM        COMBINE HYDROGRAPHS SUB2 & SUB3 AT CP3
 63          HC       2
             *

 64          KK    R3-4
 65          KM        ROUTE FLOW FROM CP3 TO CP4
 66          RK    1320    .008    .016            TRAP      44       1     YES
             *

 67          KK    SUB4
 68          KM   SUB-BASIN SUB4
 69          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
 70          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
 71          KM     L =  .25  Kb = .058  Adj. Slope =   42.0
 72          BA    .065
 73          LG    .300    .250   4.800    .360  15.000
 74          UC    .467    .249
 75          UA       0       5      16      30      65      77      84      90      94      97
 76          UA     100
             *
```



```
LINE         ID.......1.......2.......3.......4.......5.......6.......7.......8.......9......10

 77          KK    DIV4
 78          KM        DIVERT FOR IRRIGATED LAWNS SUB4
 79          DT      D4     1.0
 80          DI       0       1
 81          DQ       0     .55
             *

 82          KK    C3-4
```

```
 83          KM        COMBINE HYDROGRAPHS SUB3 & SUB4 AT CP4
 84          HC       2
             *

 85          KK  DIVIBW
 86          KM        DIVERT LAFAYETTE DRAIN INTERCETION TO INDIAN BEND WASH
 87          DT    DIBW
 88          DI      25      63     101     193     241     306
 89          DQ    12.5    31.5    50.5    96.5     121    55.1
             *

 90          KK    R4-5
 91          KM        ROUTE FLOW FROM CP4 TO CP5
 92          RK  2307.4    .005    .016            TRAP      44       1     YES
             *

 93          KK    SUB5
 94          KM   SUB-BASIN SUB5
 95          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
 96          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
 97          KM     L =  .44  Kb = .058  Adj. Slope =   24.0
 98          BA    .067
 99          LG    .300    .250   4.800    .360  15.000
100          UC    .846    .744
101          UA       0       5      16      30      65      77      84      90      94      97
102          UA     100
             *

103          KK    DIV5
104          KM        DIVERT FOR IRRIGATED LAWNS SUB5
105          DT      D5     .94
106          DI       0       1
107          DQ       0     .50
             *

108          KK    C4-5
109          KM        COMBINE HYDROGRAPHS SUB4 & SUB5 AT CP5
110          HC       2
             *

111          KK    SUB6
112          KM   SUB-BASIN SUB6
113          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
114          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
115          KM     L =  .26  Kb = .102  Adj. Slope = 2367.0
116          BA    .090
```



```
LINE         ID.......1.......2.......3.......4.......5.......6.......7.......8.......9......10

117          LG    .113    .341   4.700    .250  50.000
118          UC    .142    .057
119          UA       0       3       5       8      12      20      43      75      90      96
120          UA     100
             *

121          KK    R6-7
122          KM        ROUTE FLOW FROM SUB6 TO SUB7
123          RK  2972.0    .013     .07            TRAP       0       3     YES
             *

124          KK    SUB7
125          KM   SUB-BASIN SUB7
126          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
127          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
128          KM     L =  .56  Kb = .052  Adj. Slope =   71.0
129          BA    .153
130          LG    .295    .269   5.400    .280  18.000
131          UC    .546    .346
132          UA       0       5      16      30      65      77      84      90      94      97
133          UA     100
             *

134          KK    DIV7
135          KM        DIVERT FOR IRRIGATED LAWNS SUB7
136          DT      D7    2.30
137          DI       0       1
138          DQ       0    .427
             *
```

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139        KK    C6-7
140        KM        COMBINE HYDROGRAPHS SUB6 & SUB7 AT CP7
141        HC       2
           *

142        KK    R7-8
143        KM        ROUTE FLOW FROM SUB7 TO SUB8
144        RK  2302.1     .001     .016            TRAP      40       1     YES
           *

145        KK    SUB8
146        KM   SUB-BASIN SUB8
147        KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
148        KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
149        KM     L =  .44  Kb = .057  Adj. Slope =   52.0
150        BA    .068
151        LG    .300     .250    4.350     .480  15.000
152        UC    .696     .594
153        UA       0        5       16       30       65       77       84       90       94       97
154        UA     100
           *
1
                                        HEC-1 INPUT                                                          PAGE  5
LINE       ID.......1.......2.......3.......4.......5.......6.......7.......8.......9......10

155        KK    DIV8
156        KM        DIVERT FOR IRRIGATED LAWNS SUB8
157        DT      D8      .99
158        DI       0        1
159        DQ       0       .6
           *

160        KK    C7-8
161        KM        COMBINE HYDROGRAPHS SUB7 & SUB8 AT CP8
162        HC       2
           *

163        KK    R8-9
164        KM        ROUTE FLOW FROM SUB8 TO SUB9
165        RK  1314.7     .010     .016            TRAP      20       1     YES
           *

166        KK    SUB9
167        KM   SUB-BASIN SUB9
168        KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
169        KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
170        KM     L =  .25  Kb = .058  Adj. Slope =   55.0
171        BA    .065
172        LG    .300     .250    4.500     .430  15.000
173        UC    .454     .241
174        UA       0        5       16       30       65       77       84       90       94       97
175        UA     100
           *

176        KK    DIV9
177        KM        DIVERT FOR IRRIGATED LAWNS SUB9
178        DT      D9      .94
179        DI       0        1
180        DQ       0       .6
           *

181        KK    C8-9
182        KM        COMBINE HYDROGRAPHS SUB8 & SUB9   AT CP9
183        HC       2
           *

184        KK    R9-5
185        KM        ROUTE FLOW FROM SUB9 TO  SUB5
186        RK  1784.7     .007     .016            TRAP      40       1     YES
           *

187        KK    C9-5
188        KM        COMBINE HYDROGRAPH SUB9  & SUB5  AT CP5
189        HC       2
           *
           *      3       0
           *
```

```
LINE          ID.......1.......2.......3.......4.......5.......6.......7.......8.......9......10

  190         KK   R5-10
  191         KM        ROUTE FLOW ALONG CHANNEL FROM SUB5 TO  SUB10
  192         RS       1    FLOW      -1
  193         SV       0       1       3      13      50     110     162
  194         SQ       0      75     250     500    1200    2400    4000
              *

  195         KK   SUB10
  196         KM   SUB-BASIN SUB10
  197         KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
  198         KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
  199         KM     L =  .34  Kb = .056  Adj. Slope =   37.0
  200         BA    .093
  201         LG    .299    .250   4.800    .360  15.000
  202         UC    .579    .330
  203         UA       0       5      16      30      65      77      84      90      94      97
  204         UA     100
              *

  205         KK   DIV10
  206         KM        DIVERT FOR IRRIGATED LAWNS SUB10
  207         DT     D10    1.17
  208         DI       0       1
  209         DQ       0    .445
              *

  210         KK   C5-10
  211         KM        COMBINE HYDROGRAPH SUB5  & SUB10 AT CP10
  212         HC       2
              *
              *      3       0
              *

  213         KK  R10-15
  214         KM        ROUTE FLOW ALONG CHANNEL FROM SUB10 TO SUB15
  215         RS       1    FLOW      -1
  216         SV       0       2       5       8      46     156     247
  217         SQ       0      75     250     500    1200    2400    4000
              *

  218         KK   SUB11
  219         KM   SUB-BASIN SUB11
  220         KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
  221         KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
  222         KM     L =  .56  Kb = .106  Adj. Slope = 1740.0
  223         BA    .093
  224         LG    .115    .350   4.550    .270  39.000
  225         UC    .237    .183
  226         UA       0       3       5       8      12      20      43      75      90      96
  227         UA     100
              *
```



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LINE          ID.......1.......2.......3.......4.......5.......6.......7.......8.......9......10

  228         KK  R11-12
  229         KM        ROUTE FLOW FROM SUB11 TO   SUB12
  230         RK    1632    .058     .07            TRAP       0       3     YES
              *

  231         KK   SUB12
  232         KM   SUB-BASIN SUB12
  233         KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
  234         KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
  235         KM     L =  .31  Kb = .064  Adj. Slope =  304.0
  236         BA    .120
  237         LG    .269    .279   5.700    .200   9.000
  238         UC    .246    .102
  239         UA       0       5      16      30      65      77      84      90      94      97
  240         UA     100
              *

  241         KK   DIV12
```

```
242          KM        DIVERT FOR IRRIGATED LAWNS SUB12
243          DT     D12     .31
244          DI       0       1
245          DQ       0    .079
             *

246          KK  C11-12
247          KM        COMBINE HYDROGRAPH SUB11 & SUB12 AT CP12
248          HC       2
             *

249          KK  R12-13
250          KM        ROUTE FLOW FROM SUB12 TO SUB13
251          RK  1362.2    .020    .016            TRAP      60       1     YES      50
             *

252          KK   SUB13
253          KM   SUB-BASIN SUB13
254          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
255          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
256          KM     L =  .26  Kb = .054  Adj. Slope =  107.0
257          BA    .129
258          LG    .300    .230   6.200    .200  15.000
259          UC    .283    .100
260          UA       0       5      16      30      65      77      84      90      94      97
261          UA     100
             *

262          KK   DIV13
263          KM        DIVERT FOR IRRIGATED LAWNS SUB13
264          DT     D13     .98
265          DI       0       1
266          DQ       0      .2
             *
                                        HEC-1 INPUT                                          PAGE  8

LINE         ID.......1.......2.......3.......4.......5.......6.......7.......8.......9......10

267          KK  C12-13
268          KM        COMBINE HYDROGRAPHS SUB12 & SUB13 AT CP13
269          HC       2
             *

270          KK  R13-14
271          KM        ROUTE FL OW FROM SUB13 TO SUB14
272          RK  1314.7    .014    .016            TRAP      60       1     YES
             *

273          KK   SUB14
274          KM   SUB-BASIN SUB14
275          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
276          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
277          KM     L =  .25  Kb = .054  Adj. Slope =   74.0
278          BA    .126
279          LG    .300    .250   4.100    .550  15.000
280          UC    .433    .157
281          UA       0       5      16      30      65      77      84      90      94      97
282          UA     100
             *

283          KK   DIV14
284          KM        DIVERT FOR IRRIGATED LAWNS SUB14
285          DT     D14    1.57
286          DI       0       1
287          DQ       0      .6
             *

288          KK  C13-14
289          KM        COMBINE HYDROGRAPHS SUB13 & SUB14 AT CP14
290          HC       2
             *

291          KK  R14-15
292          KM        ROUTE FLOW FROM SUB 14 TO SUB15
293          RK  1985.3    .011    .016            TRAP      60       1     YES
             *

294          KK   SUB15
```

```
295          KM   SUB-BASIN SUB15
296          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
297          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
298          KM     L =  .38  Kb = .054  Adj. Slope =   56.0
299          BA    .126
300          LG    .297    .250   4.650    .390  16.000
301          UC    .529    .274
302          UA       0       5      16      30      65      77      84      90      94      97
303          UA     100
             *
                                          HEC-1 INPUT                                          PAGE  9

LINE         ID.......1.......2.......3.......4.......5.......6.......7.......8.......9......10


304          KK   DIV15
305          KM        DIVERT FOR IRRIGATED LAWNS SUB15
306          DT     D15    2.05
307          DI       0       1
308          DQ       0    .585
             *

309          KK  C15-10
310          KM        COMBINE SUB14, SUB10 WITH SUB15
311          HC       3
             *      1       2
             *

312          KK   D56ST
313          KM        DIVERT FLOW THAT CROSSES 56TH ST. BRIDGE
314          DT   D56ST
315          DI       0     400     650     790    1040    1139    1334    1484    1689    1900
316          DQ       0       0     240     318     400     489     584     684     789     900
             *
             *      3       0
             *

317          KK  R15-20
318          KM        ROUTE FLOW ALONG CHANNEL FROM SUB15 TO SUB20
319          RS       1    FLOW      -1
320          SV       0      14      18      25      35      72     111
321          SQ       0      75     250     500    1200    2400    4000
             *

322          KK   SUB16
323          KM   SUB-BASIN SUB16
324          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
325          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
326          KM     L =  .65  Kb = .102  Adj. Slope = 2052.0
327          BA    .129
328          LG    .104    .350   4.700    .240  47.000
329          UC    .233    .167
330          UA       0       3       5       8      12      20      43      75      90      96
331          UA     100
             *

332          KK  R16-17
333          KM        ROUTE FLOW FROM SUB16 TO SUB17
334          RK    1668    .058     .07            TRAP       0       3     YES
             *

335          KK   SUB17
336          KM   SUB-BASIN SUB17
337          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
338          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
339          KM     L =  .32  Kb = .058  Adj. Slope =  183.0
340          BA    .073
341          LG    .298    .252   4.350    .400  10.000
342          UC    .329    .193
                                          HEC-1 INPUT                                          PAGE 10

LINE         ID.......1.......2.......3.......4.......5.......6.......7.......8.......9......10

343          UA       0       5      16      30      65      77      84      90      94      97
344          UA     100
             *

345          KK   DIV17
346          KM        DIVERT FOR IRRIGATED LAWNS SUB17
```

```
347          DT     D17     .11
348          DI       0       1
349          DQ       0    .074
             *

350          KK  C16-17
351          KM        COMBINE HYDROGRAPH SUB16 & SUB17 AT CP17
352          HC       2
             *

353          KK  R17-18
354          KM        ROUTE FLOW FROM SUB17 TO SUB18
355          RK  1378.1    .019    .016            TRAP      40       1     YES
             *

356          KK   SUB18
357          KM   SUB-BASIN SUB18
358          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
359          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
360          KM     L =  .26  Kb = .058  Adj. Slope =  102.0
361          BA    .067
362          LG    .300    .250   4.150    .530  15.000
363          UC    .404    .215
364          UA       0       5      16      30      65      77      84      90      94      97
365          UA     100
             *

366          KK   DIV18
367          KM        DIVERT FOR IRRIGATED LAWNS SUB18
368          DT     D18     .81
369          DI       0       1
370          DQ       0      .6
             *

371          KK  C17-18
372          KM        COMBINE  HYDROGRAPH SUB17 & SUB18 AT CP18
373          HC       2
             *

374          KK  R18-19
375          KM        ROUTE FLOW SUB18 TO SUB19
376          RK  1335.8    .014    .016            TRAP      40       1     YES
             *
                                          HEC-1 INPUT                                          PAGE 11

LINE         ID.......1.......2.......3.......4.......5.......6.......7.......8.......9......10

377          KK   SUB19
378          KM   SUB-BASIN SUB19
379          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
380          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
381          KM     L =  .25  Kb = .057  Adj. Slope =   77.0
382          BA    .075
383          LG    .300    .250   3.950    .580  15.000
384          UC    .450    .220
385          UA       0       5      16      30      65      77      84      90      94      97
386          UA     100
             *

387          KK   DIV19
388          KM        DIVERT FOR IRRIGATED LAWNS SUB19
389          DT     D19     .91
390          DI       0       1
391          DQ       0      .6
             *

392          KK  C18-19
393          KM        COMBINE HYDROGRAPH SUB18 & SUB19 AT CP19
394          HC       2
             *

395          KK  R19-20
396          KM        ROUTE FLOW FROM SUB19 TO SUB20
397          RK  1473.1    .010    .016            TRAP      30       1     YES
             *

398          KK   SUB20
399          KM   SUB-BASIN SUB20
```

```
400          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
401          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
402          KM     L =  .28  Kb = .054  Adj. Slope =   54.0
403          BA    .129
404          LG    .300    .250   4.450    .450  15.000
405          UC    .479    .190
406          UA       0       5      16      30      65      77      84      90      94      97
407          UA     100
             *

408          KK   DIV20
409          KM        DIVERT FOR IRRIGATED LAWNS SUB20
410          DT     D20    1.86
411          DI       0       1
412          DQ       0      .6
             *

413          KK  C20-15
414          KM        COMBINE SUB19, SUB15 WITH SUB20
415          HC       3
             *      1       2
             *
             *      3       0
             *
```



```
LINE         ID.......1.......2.......3.......4.......5.......6.......7.......8.......9......10

416          KK  R20-25
417          KM        ROUTE FLOW ALONG CHANNEL FROM SUB20 TO SUB25
418          RS       1    FLOW      -1
419          SV       0      23      27      35      37      84     122
420          SQ       0      75     250     500    1200    2400    4000
             *

421          KK   SUB21
422          KM   SUB-BASIN SUB21
423          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
424          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
425          KM     L =  .56  Kb = .102  Adj. Slope = 2352.0
426          BA    .124
427          LG    .104    .350   4.700    .240  46.000
428          UC    .208    .134
429          UA       0       3       5       8      12      20      43      75      90      96
430          UA     100
             *

431          KK  R21-22
432          KM        ROUTE FLOW FROM SUB21 TO SUB22
433          RK    2735    .026     .07            TRAP       0       3     YES
             *

434          KK   SUB22
435          KM   SUB-BASIN SUB22
436          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
437          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
438          KM     L =  .52  Kb = .060  Adj. Slope =  134.0
439          BA    .112
440          LG    .281    .266   4.000    .480  11.000
441          UC    .571    .410
442          UA       0       5      16      30      65      77      84      90      94      97
443          UA     100
             *

444          KK   DIV22
445          KM        DIVERT FOR IRRIGATED LAWNS SUB22
446          DT     D22     .12
447          DI       0       1
448          DQ       0    .063
             *

449          KK  C21-22
450          KM        COMBINE HYDROGRAPH SUB21 & SUB22 AT CP22
451          HC       2
             *

452          KK  R22-23
453          KM        ROUTE FLOW FROM SUB22 TO SUB23
```

```
454          RK  1240.8    .025    .016            TRAP      20       1     YES
             *
                                          HEC-1 INPUT                                                    PAGE 13

LINE         ID.......1.......2.......3.......4.......5.......6.......7.......8.......9......10


455          KK   SUB23
456          KM   SUB-BASIN SUB23
457          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
458          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
459          KM     L =  .23  Kb = .058  Adj. Slope =  132.0
460          BA    .060
461          LG    .300    .250   3.950    .580  15.000
462          UC    .350    .177
463          UA       0       5      16      30      65      77      84      90      94      97
464          UA     100
             *

465          KK   DIV23
466          KM        DIVERT FOR IRRIGATED LAWNS SUB23
467          DT     D23     .72
468          DI       0       1
469          DQ       0    .593
             *

470          KK  C22-23
471          KM        COMBINE HYDROGRAPH SUB22 & SUB23 AT CP23
472          HC       2
             *

473          KK  R23-24
474          KM        ROUTE FLOW FROM SUB 23 TO SUB24
475          RK  1088.9    .015    .016            TRAP      32       1     YES
             *

476          KK   SUB24
477          KM   SUB-BASIN SUB24
478          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
479          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
480          KM     L =  .28  Kb = .057  Adj. Slope =   78.0
481          BA    .077
482          LG    .300    .250   3.950    .580  15.000
483          UC    .479    .255
484          UA       0       5      16      30      65      77      84      90      94      97
485          UA     100
             *

486          KK   DIV24
487          KM        DIVERT FOR IRRIGATED LAWNS SUB24
488          DT     D24     .93
489          DI       0       1
490          DQ       0      .6
             *

491          KK  C23-24
492          KM        COMBINE HYDROGRAPH SUB23 & SUB24 AT CP24
493          HC       2
             *
                                          HEC-1 INPUT                                                    PAGE 14

LINE         ID.......1.......2.......3.......4.......5.......6.......7.......8.......9......10


494          KK  R24-25
495          KM        ROUTE FLOW FROM SUB24 TO SUB25
496          RK  1346.4    .009    .016            TRAP      40       1     YES
             *

497          KK   SUB25
498          KM   SUB-BASIN SUB25
499          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
500          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
501          KM     L =  .25  Kb = .057  Adj. Slope =   46.0
502          BA    .076
503          LG    .300    .250   3.950    .580  15.000
504          UC    .550    .273
505          UA       0       5      16      30      65      77      84      90      94      97
506          UA     100
```

```
*
KK   DIV25
KM        DIVERT FOR IRRIGATED LAWNS SUB25
DT     D25      .93
DI       0        1
DQ       0       .6
*
KK  C25-20
KM        COMBINE SUB19, SUB 20 WITH SUB25
HC       3
*      1        2
*
*      3        0
*
KK  R25-29
KM        ROUTE FLOW ALONG CHANNEL FROM SUB25 TO SUB29
RS       1    FLOW      -1
SV       0        2        6       13       23       35       36
SQ       0       75      250      500     1200     2400     4000
*
KK   SUB26
KM   SUB-BASIN SUB26
KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
KM     L =  .52  Kb = .067  Adj. Slope =  840.0
BA    .053
LG    .272     .295    4.250     .520   17.000
UC    .304     .312
UA       0        5       16       30       65       77       84       90       94       97
UA     100
*
```



```
LINE          ID.......1.......2.......3.......4.......5.......6.......7.......8.......9......10

KK   DIV26
KM        DIVERT FOR GOLF   COURSE
DT     D26      .31
DI       0        1
DQ       0     .312
*
KK  R26-27
KM        ROUTE FLOW FROM SUB26 TO SUB27
RK  1293.6     .024     .016            TRAP       35        1      YES
*
KK   SUB27
KM   SUB-BASIN SUB27
KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
KM     L =  .25  Kb = .058  Adj. Slope =  122.0
BA    .061
LG    .300     .250    3.950     .580   15.000
UC    .379     .205
UA       0        5       16       30       65       77       84       90       94       97
UA     100
*
KK   DIV27
KM        DIVERT FOR IRRIGATED LAWNS SUB27
DT     D27      .74
DI       0      1.0
DQ       0      .60
*
KK  C26-27
KM        COMBINE HYDROGRAPH SUB 26 & SUB27 AT CP27
HC       2
*
KK  R27-28
KM        ROUTE FLOW FROM SUB 27 TO SUB28
RK  1436.2     .017     .016            TRAP       35        1      YES
```

```
*
KK   SUB28
KM   SUB-BASIN SUB28
KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
KM     L =  .27  Kb = .057  Adj. Slope =   89.0
BA    .078
LG    .300    .250   3.950    .580  15.000
UC    .446    .227
UA       0       5      16      30      65      77      84      90      94      97
UA     100
*
```



```
1
LINE          ID.......1.......2.......3.......4.......5.......6.......7.......8.......9......10

KK   DIV28
KM        DIVERT FOR IRRIGATED LAWNS SUB28
DT     D28     .95
DI       0       1
DQ       0     .60
*

KK  C27-28
KM        COMBINE HYDROGRAPH SUB27 & SUB28 AT CP28
HC       2
*

KK  R28-29
KM        ROUTE FLOW FROM SUB 28 TO SUB29
RK  1161.6    .009    .016            TRAP      35       1     YES
*

KK   SUB29
KM   SUB-BASIN SUB29
KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
KM     L =  .22  Kb = .058  Adj. Slope =   47.0
BA    .058
LG    .299    .250   3.950    .580  15.000
UC    .508    .264
UA       0       5      16      30      65      77      84      90      94      97
UA     100
*

KK   DIV29
KM        DIVERT FOR IRRIGATED LAWNS SUB29
DT     D29     .70
DI       0       1
DQ       0    .587
*

KK  C29-25
KM        COMBINE SUB28, SUB25 WITH SUB29
HC       3
*     1       2
*

KK   DOCCC
KM        DIVERT AZ CANAL FLOW TO OCCC
DT   DOCCC
DI       0     200     400     800    1000    1001    1200    4000
DQ       0     200     400     800    1000    1000    1000    1000
*
*     3       0
*
```



```
LINE          ID.......1.......2.......3.......4.......5.......6.......7.......8.......9......10

KK  R29-33
KM        ROUTE FLOW ALONG CHANNEL FROM SUB29 TO SUB33
RS       1    FLOW      -1
SV       0       2       4       7      18      36      60
SQ       0      75     250     500    1200    2400    4000
*
```

```
608          KK   SUB38
609          KM   SUB-BASIN SUB38
610          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
611          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
612          KM     L = 1.28  Kb = .090  Adj. Slope = 1079.0
613          BA    .252
614          LG    .131    .340   4.550    .280  37.000
615          UC    .408    .366
616          UA       0       3       5       8      12      20      43      75      90      96
617          UA     100
             *

618          KK  D38-39
619          KM        DIVERT 16CFS FROM SUB38 TO SUB39
620          DT  D38-39
621          DI       0       5      10      16      50     100     200     400     600
622          DQ       0       5      10      16      16      16      16      16      16
             *

623          KK  R38-30
624          KM        ROUTE FLOW FROM SUB38 TO   SUB30
625          RK    1200    .035    .016            TRAP      30       1     YES
             *

626          KK   SUB30
627          KM   SUB-BASIN SUB30
628          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
629          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
630          KM     L =  .48  Kb = .067  Adj. Slope =  571.0
631          BA    .064
632          LG    .272    .267   4.000    .460  10.000
633          UC    .313    .271
634          UA       0       5      16      30      65      77      84      90      94      97
635          UA     100
             *

636          KK  C30-38
637          KM        COMBINE SUB38 & SUB30 AT CP30
638          HC       2
             *

639          KK  R30-31
640          KM        ROUTE FLOW FROM SUB30 TO SUB31
641          RK    1304   .0225    .025            TRAP      20       1     YES
             *
                                          HEC-1 INPUT                                          PAGE 18

LINE         ID.......1.......2.......3.......4.......5.......6.......7.......8.......9......10

642          KK   SUB31
643          KM   SUB-BASIN SUB31
644          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
645          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
646          KM     L =  .25  Kb = .058  Adj. Slope =  118.0
647          BA    .061
648          LG    .300    .260   3.670    .690  15.000
649          UC    .433    .238
650          UA       0       5      16      30      65      77      84      90      94      97
651          UA     100
             *

652          KK   DIV31
653          KM        DIVERT FOR IRRIGATED LAWNS SUB31
654          DT     D31     .45
655          DI       0       1
656          DQ       0    .400
             *

657          KK  C30-31
658          KM        COMBINE SUB30 & SUB31 AT CP31
659          HC       2
             *

660          KK  R31-32
661          KM        ROUTE FLOW FROM SUB31 TO SUB32
662          RK    1260    .019    .016       0    TRAP      30       1     YES
             *
```

```
663          KK   SUB32
664          KM   SUB-BASIN SUB32
665          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
666          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
667          KM     L =  .27  Kb = .058  Adj. Slope =   77.0
668          BA    .065
669          LG    .300    .250   3.950    .580  15.000
670          UC    .479    .272
671          UA       0       5      16      30      65      77      84      90      94      97
672          UA     100
             *

673          KK   DIV32
674          KM        DIVERT FOR IRRIGATED LAWNS SUB32
675          DT     D32     .79
676          DI     0.0     1.0
677          DQ       0     .60
             *

678          KK  C31-32
679          KM        COMBINE HYDROGRAPH SUB31 & SUB32 AT CP32
680          HC       2
             *
```



```
LINE         ID.......1.......2.......3.......4.......5.......6.......7.......8.......9......10

681          KK  R32-33
682          KM        ROUTE FLOW FROM SUB32 TO SUB33
683          RK    1447   .0144     .07            TRAP       0       3     YES
             *

684          KK   SUB33
685          KM   SUB-BASIN SUB33
686          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
687          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
688          KM     L =  .22  Kb = .058  Adj. Slope =   65.0
689          BA    .062
690          LG    .277    .250   3.950    .580  22.000
691          UC    .408    .199
692          UA       0       5      16      30      65      77      84      90      94      97
693          UA     100
             *

694          KK   DIV33
695          KM        DIVERT FOR IRRIGATED LAWNS SUB33
696          DT     D33     .62
697          DI       0       1
698          DQ       0     .37
             *

699          KK  C33-29
700          KM        COMBINE SUB32, SUB29 WITH SUB33
701          HC       3
             *      1       2
             *
             *      3       0
             *

702          KK  R33-35
703          KM        ROUTE FLOW ALONG CHANNEL FROM SUB33 TO SUB35
704          RS       1    FLOW      -1
705          SV       0       5      10      22      50      93     142
706          SQ       0      75     250     500    1200    2400    4000
             *

707          KK   SUB34
708          KM   SUB-BASIN SUB34
709          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
710          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
711          KM     L =  .57  Kb = .050  Adj. Slope =   87.0
712          BA    .167
713          LG    .284    .250   3.950    .590  20.000
714          UC    .617    .383
715          UA       0       5      16      30      65      77      84      90      94      97
716          UA     100
             *
```

```
LINE          ID.......1.......2.......3.......4.......5.......6.......7.......8.......9......10

 717          KK   DIV34
 718          KM        DIVERT FOR IRRIGATED LAWNS SUB34
 719          DT     D34    1.53
 720          DI       0       1
 721          DQ       0    .366
              *

 722          KK  R34-35
 723          KM        ROUTE FLOW FROM SUB34 TO SUB35
 724          RK  1531.2    .018    .016            TRAP      40       1     YES
              *

 725          KK   SUB35
 726          KM   SUB-BASIN SUB35
 727          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
 728          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
 729          KM     L =  .29  Kb = .048  Adj. Slope =   51.0
 730          BA    .128
 731          LG    .223    .250   3.950    .600  39.000
 732          UC    .400    .160
 733          UA       0       5      16      30      65      77      84      90      94      97
 734          UA     100
              *

 735          KK   DIV35
 736          KM        DIVERT FOR IRRIGATED LAWNS SUB35
 737          DT     D35     .53
 738          DI     0.0     1.0
 739          DQ     0.0    .095
              *

 740          KK  C35-33
 741          KM        COMBINE SUB34, SUB33 WITH SUB35
 742          HC       3
              *
              *      3       0
              *

 743          KK  R35-36
 744          KM        ROUTE FLOW ALONG CHANNEL FROM SUB35 TO SUB36
 745          RS       1    FLOW      -1
 746          SV       0       4       9      28      67     131     179
 747          SQ       0      75     250     500    1200    2400    4000
              *

 748          KK   SUB40
 749          KM   SUB-BASIN SUB40
 750          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
 751          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
 752          KM     L =  .31  Kb = .090  Adj. Slope = 1822.0
 753          BA    .074
 754          LG    .203    .314   4.000    .420  11.000
 755          UC    .188    .100
 756          UA       0       3       5       8      12      20      43      75      90      96
```



```
LINE          ID.......1.......2.......3.......4.......5.......6.......7.......8.......9......10

 757          UA     100
              *

 758          KK  R40-41
 759          KM        ROUTE FLOW FROM SUB40 TO SUB41
 760          RK    1452   .0221     .05            TRAP       6       2     YES
              *

 761          KK   SUB41
 762          KM   SUB-BASIN SUB41
 763          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
 764          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
 765          KM     L =  .54  Kb = .053  Adj. Slope =  110.0
 766          BA    .156
 767          LG    .281    .252   4.350    .420  16.000
 768          UC    .508    .308
```

```
769          UA       0       5      16      30      65      77      84      90      94      97
770          UA     100
             *

771          KK  C40-41
772          KM        COMBINE HYDROGRAPH SUB40 & SUB41 AT CP41
773          HC       2
             *

774          KK  R41-39
775          KM        ROUTE FLOW FROM SUB41 TO   SUB39
776          RK    2865   .0341     .05            TRAP       4       3     YES
             *

777          KK   SUB37
778          KM   SUB-BASIN SUB37
779          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
780          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
781          KM     L =  .30  Kb = .059  Adj. Slope =  247.0
782          BA    .049
783          LG    .300    .250   3.950    .490   5.000
784          UC    .321    .223
785          UA       0       5      16      30      65      77      84      90      94      97
786          UA     100
             *

787          KK  R37-39
788          KM        ROUTE FLOW FROM SUB37 TO   SUB39
789          RK    3500    .018    .016            TRAP      70       1     YES
             *

790          KK   SUB39
791          KM   SUB-BASIN SUB39
792          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
793          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
794          KM     L =  .84  Kb = .050  Adj. Slope =   79.0
795          BA    .224
796          LG    .233    .259   4.300    .450  29.000
797          UC    .667    .481
```



```
LINE         ID.......1.......2.......3.......4.......5.......6.......7.......8.......9......10

798          UA       0       5      16      30      65      77      84      90      94      97
799          UA     100
             *

800          KK  D39-36
801          KM        DIVERT FLOW OF CAMELBACK RD. OVERTOPPING AND RUNNING TO SUB36
802          DT  D39-36
803          DI       0    99.5     160     200     300     500     700    1000
804          DQ       0       0       0      40     140     340     540     840
             *

805          KK   DCBR1
806          KM        DIVERT 55 CFS FROM WATERSHED STORM DRAIN OUTLETS AT 40TH STREET SYSTEM
807          DT   DCBR1
808          DI       0      20      50      55     100     200     500    1000    2000    3000
809          DQ       0      20      50      55      55      55      55      55      55      55
             *

810          KK   DCBR2
811          KM        DIVERT 60 CFS FOR STORM DRAIN THAT OUTLETS INTO AZ. CANAL IN SUBBASIN 36
812          DT   DCBR2
813          DI       0      20      50      60     150     300     600    1000    2000    3000
814          DQ       0      20      50      60      60      60      60      60      60      60
             *

815          KK  RD3839
816          KM        RECALL DIVERSION FROM SUBBASIN 38
817          DR  D38-39
             *

818          KK  C37-41
819          KM        COMBINE HYDROGRAPHS SUB41, SUB37 & SUB39 AT CP39 AND RECALL DIVERSION
820          HC       4
             *

821          KK  R39-36
```

```
822          KM        ROUTE FLOW FROM SUB39 TO   SUB36
823          RK    1250    .006    .016            TRAP      26       1     YES
             *

824          KK   SUB36
825          KM   SUB-BASIN SUB36
826          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
827          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
828          KM     L =  .28  Kb = .052  Adj. Slope =   14.0
829          BA    .089
830          LG    .232    .250   3.950    .590  41.000
831          UC    .646    .327
832          UA       0       5      16      30      65      77      84      90      94      97
833          UA     100
             *
                                          HEC-1 INPUT                                          PAGE 23

LINE         ID.......1.......2.......3.......4.......5.......6.......7.......8.......9......10

834          KK   DIV36
835          KM        DIVERT FOR IRRIGATED LAWNS SUB36
836          DT     D36     .61
837          DI     0.0     1.0
838          DQ     0.0    .150
             *

839          KK  RDCBR2
840          KM        RECALL DIVERSION FOR STORM DRAIN ALONG CAMELBACK RD.
841          DR   DCBR2
             *

842          KK  RD39366
843          KM        RECALL DIVERSION FROM SUB 39 TO    SUB36
844          DR  D39-36
             *

845          KK  C36-35
846          KM        COMBINE SUB39, SUB35, 2 RECALLED DIVERSIONS AND SUB36
847          HC       5
             *

848          KK   D40ST
849          KM        DIVERT FLOW FOR 40TH ST.
850          DT   D40ST
851          DI       0      10     100     300     500     700     900    1100    1300    1500
852          DQ       0       0      90     290     490     690     890    1090    1290    1490
             *
             *      3       0
             *

853          KK  R36-42
854          KM        ROUTE FLOW FROM SUB36 TO SUB42
855          RS       1    FLOW      -1
856          SV       0       3       6      10      34      60     130
857          SQ       0      75     250     500    1200    2400    4000
             *

858          KK   SUB42
859          KM   SUB-BASIN SUB42
860          KM   6-HOUR RAINFALL, PATTERN NO. 2.20 WAS USED TO FIND TC & R FOR THIS BASIN
861          KM   THIS BASIN USED RAINFALL REDUCTION FACTOR OF  .967
862          KM     L =  .51  Kb = .044  Adj. Slope =   29.0
863          BA    .206
864          LG    .247    .250   5.600    .250  27.000
865          UC    .587    .294
866          UA       0       5      16      30      65      77      84      90      94      97
867          UA     100
             *
                                          HEC-1 INPUT                                          PAGE 24

LINE         ID.......1.......2.......3.......4.......5.......6.......7.......8.......9......10

868          KK   DIV42
869          KM        DIVERT FOR IRRIGATED LAWNS SUB42
870          DT     D42     .75
871          DI       0       1
872          DQ       0    .072
```

```
                 *      1       2
                 *

873              KK  C42-36
874              KM        COMBINE HYDROGRAPH SUB42 WITH SUB36
875              HC       2
                 *
                 *      3       0
                 *
876              ZZ
```

SCHEMATIC DIAGRAM OF STREAM NETWORK

```
INPUT
 LINE     (V) ROUTING          (--->) DIVERSION OR PUMP FLOW

 NO.      (.) CONNECTOR        (<---) RETURN OF DIVERTED OR PUMPED FLOW

  5         SUB1
               V
               V
 22         R1-2
               .
               .
 25            .        SUB2
               .           .
               .           .
 37            .           .------->      D2
 35            .        DIV2
               .           .
               .           .
 40         C1-2............
               V
               V
 43         R2-3
               .
               .
 46            .        SUB3
               .           .
               .           .
 58            .           .------->      D3
 56            .        DIV3
               .           .
               .           .
 61         C2-3............
               V
               V
 64         R3-4
               .
               .
 67            .        SUB4
               .           .
               .           .
 79            .           .------->      D4
 77            .        DIV4
               .           .
               .           .
 82         C3-4............
               .
               .
 87            .------->    DIBW
 85       DIVIBW
               V
               V
 90         R4-5
               .
               .
 93            .        SUB5
               .           .
               .           .
105            .           .------->      D5
103            .        DIV5
               .           .
               .           .
108         C4-5............
               .
               .
111            .        SUB6
               .           V
               .           V
```

```
121          .        R6-7
             .          .
             .          .
124          .          .        SUB7
             .          .          .
             .          .          .
136          .          .          .-------->     D7
134          .          .        DIV7
             .          .          .
             .          .          .
139          .        C6-7............
             .          V
             .          V
142          .        R7-8
             .          .
             .          .
145          .          .        SUB8
             .          .          .
             .          .          .
157          .          .          .-------->     D8
155          .          .        DIV8
             .          .          .
             .          .          .
160          .        C7-8............
             .          V
             .          V
163          .        R8-9
             .          .
             .          .
166          .          .        SUB9
             .          .          .
             .          .          .
178          .          .          .-------->     D9
176          .          .        DIV9
             .          .          .
             .          .          .
181          .        C8-9............
             .          V
             .          V
184          .        R9-5
             .          .
             .          .
187       C9-5............
             V
             V
190       R5-10
             .
             .
195          .       SUB10
             .          .
             .          .
207          .          .-------->     D10
205          .       DIV10
             .          .
             .          .
210       C5-10...........
             V
             V
213       R10-15
             .
             .
218          .       SUB11
             .          V
             .          V
228          .      R11-12
             .          .
             .          .
231          .          .        SUB12
             .          .          .
             .          .          .
243          .          .          .-------->     D12
241          .          .        DIV12
             .          .          .
             .          .          .
246          .      C11-12...........
             .          V
             .          V
249          .      R12-13
             .          .
```

```
252                 SUB13
                      .
                      .
264                   .-------> D13
262                 DIV13
                      .
                      .
267          C12-13............
                 V
                 V
270          R13-14
                 .
                 .
273                 SUB14
                      .
                      .
285                   .-------> D14
283                 DIV14
                      .
                      .
288          C13-14............
                 V
                 V
291          R14-15
                 .
                 .
294                 SUB15
                      .
                      .
306                   .-------> D15
304                 DIV15
                      .
                      .
309     C15-10........................
                 .
                 .
314              .-------> D56ST
312     D56ST
            V
            V
317     R15-20
                 .
                 .
322          SUB16
                 V
                 V
332          R16-17
                 .
                 .
335                 SUB17
                      .
                      .
347                   .-------> D17
345                 DIV17
                      .
                      .
350          C16-17............
                 V
                 V
353          R17-18
                 .
                 .
356                 SUB18
                      .
                      .
368                   .-------> D18
366                 DIV18
                      .
                      .
371          C17-18............
                 V
                 V
374          R18-19
                 .
                 .
377                 SUB19
                      .
                      .
```

```
389                                  .-------->   D19
387                          DIV19
                                     .
                                     .
392                  C18-19............
                         V
                         V
395                  R19-20
                         .
                         .
398                          SUB20
                                     .
                                     .
410                                  .-------->   D20
408                          DIV20
                                     .
                                     .
413          C20-15........................
                 V
                 V
416          R20-25
                 .
                 .
421                  SUB21
                         V
                         V
431                  R21-22
                         .
                         .
434                          SUB22
                                     .
                                     .
446                                  .-------->   D22
444                          DIV22
                                     .
                                     .
449                  C21-22............
                         V
                         V
452                  R22-23
                         .
                         .
455                          SUB23
                                     .
                                     .
467                                  .-------->   D23
465                          DIV23
                                     .
                                     .
470                  C22-23............
                         V
                         V
473                  R23-24
                         .
                         .
476                          SUB24
                                     .
                                     .
488                                  .-------->   D24
486                          DIV24
                                     .
                                     .
491                  C23-24............
                         V
                         V
494                  R24-25
                         .
                         .
497                          SUB25
                                     .
                                     .
509                                  .-------->   D25
507                          DIV25
                                     .
                                     .
512          C25-20........................
                 V
                 V
515          R25-29
```

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                .
                .
520             .       SUB26
                .           .
                .           .
532             .           .-------->     D26
530             .       DIV26
                .           V
                .           V
535             .      R26-27
                .           .
                .           .
538             .           .       SUB27
                .           .           .
                .           .           .
550             .           .           .-------->     D27
548             .           .       DIV27
                .           .           .
                .           .           .
553             .      C26-27............
                .           V
                .           V
556             .      R27-28
                .           .
                .           .
559             .           .       SUB28
                .           .           .
                .           .           .
571             .           .           .-------->     D28
569             .           .       DIV28
                .           .           .
                .           .           .
574             .      C27-28............
                .           V
                .           V
577             .      R28-29
                .           .
                .           .
580             .           .       SUB29
                .           .           .
                .           .           .
592             .           .           .-------->     D29
590             .           .       DIV29
                .           .           .
                .           .           .
595       C29-25........................
                .
                .
600             .-------->  DOCCC
598        DOCCC
               V
               V
603       R29-33
                .
                .
608             .       SUB38
                .           .
                .           .
620             .           .-------->  D38-39
618             .      D38-39
                .           V
                .           V
623             .      R38-30
                .           .
                .           .
626             .           .       SUB30
                .           .           .
                .           .           .
636             .      C30-38............
                .           V
                .           V
639             .      R30-31
                .           .
                .           .
642             .           .       SUB31
                .           .           .
                .           .           .
654             .           .           .-------->     D31
652             .           .       DIV31
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                .          .          .
                .          .          .
657             .      C30-31.........
                .          V
                .          V
660             .      R31-32
                .          .
                .          .
663             .          .      SUB32
                .          .          .
                .          .          .
675             .          .          .-------->     D32
673             .          .      DIV32
                .          .          .
                .          .          .
678             .      C31-32.........
                .          V
                .          V
681             .      R32-33
                .          .
                .          .
684             .          .      SUB33
                .          .          .
                .          .          .
696             .          .          .-------->     D33
694             .          .      DIV33
                .          .          .
                .          .          .
699         C33-29.......................
                V
                V
702         R33-35
                .
                .
707             .      SUB34
                .          .
                .          .
719             .          .-------->     D34
717             .      DIV34
                .          V
                .          V
722             .      R34-35
                .          .
                .          .
725             .          .      SUB35
                .          .          .
                .          .          .
737             .          .          .-------->     D35
735             .          .      DIV35
                .          .          .
                .          .          .
740         C35-33.......................
                V
                V
743         R35-36
                .
                .
748             .      SUB40
                .          V
                .          V
758             .      R40-41
                .          .
                .          .
761             .          .      SUB41
                .          .          .
                .          .          .
771             .      C40-41.........
                .          V
                .          V
774             .      R41-39
                .          .
                .          .
777             .          .      SUB37
                .          .          V
                .          .          V
787             .          .     R37-39
                .          .          .
                .          .          .
790             .          .          .      SUB39
```

```
802                                  .-------> D39-36
800                            D39-36
807                                  .-------> DCBR1
805                             DCBR1
812                                  .-------> DCBR2
810                             DCBR2
817                                            .<------- D38-39
815                                       RD3839
818                       C37-41.................................
                              V
                              V
821                       R39-36
824                            SUB36
836                                  .-------> D36
834                            DIV36
841                                  .<------- DCBR2
839                            RDCBR2
844                                            .<------- D39-36
842                                       RD3936
845                 C36-35.............................................
                  .-------> D40ST
848                D40ST
                      V
                      V
853                 R36-42
858                   SUB42
870                   .-------> D42
868                   DIV42
873                 C42-36............
```

(***) RUNOFF ALSO COMPUTED AT THIS LOCATION

```
*****************************************
*                                       *
*   FLOOD HYDROGRAPH PACKAGE  (HEC-1)   *
*              MAY   1991               *
*           VERSION 4.0.1E              *
*                                       *
*  RUN DATE  09/01/95  TIME  05:44:09   *
*                                       *
*****************************************
```

```
*****************************************
*                                       *
*    U.S. ARMY CORPS OF ENGINEERS       *
*    HYDROLOGIC ENGINEERING CENTER      *
*          609 SECOND STREET            *
*       DAVIS, CALIFORNIA 95616         *
*           (916) 551-1748              *
*                                       *
*****************************************
```

DDM MCUHP1 ARCADIA AREA 100yr 6hr

```
  4 IO          OUTPUT CONTROL VARIABLES
                      IPRNT          5  PRINT CONTROL
                      IPLOT          0  PLOT CONTROL
```

```
                QSCAL          0.  HYDROGRAPH PLOT SCALE

IT          HYDROGRAPH TIME DATA
                 NMIN            5  MINUTES IN COMPUTATION INTERVAL
                IDATE      1     0  STARTING DATE
                ITIME         0000  STARTING TIME
                   NQ          300  NUMBER OF HYDROGRAPH ORDINATES
               NDDATE      2     0  ENDING DATE
               NDTIME         0055  ENDING TIME
               ICENT           19  CENTURY MARK

          COMPUTATION INTERVAL    0.08 HOURS
               TOTAL TIME BASE   24.92 HOURS

     ENGLISH UNITS
          DRAINAGE AREA          SQUARE MILES
          PRECIPITATION DEPTH    INCHES
          LENGTH, ELEVATION      FEET
          FLOW                   CUBIC FEET PER SECOND
          STORAGE VOLUME         ACRE-FEET
          SURFACE AREA           ACRES
          TEMPERATURE            DEGREES FAHRENHEIT

1
                                   RUNOFF SUMMARY
                              FLOW IN CUBIC FEET PER SECOND
                          TIME IN HOURS,  AREA IN SQUARE MILES
```

OPERATION	STATION	PEAK FLOW	TIME OF PEAK	AVERAGE FLOW FOR MAXIMUM PERIOD 6-HOUR	24-HOUR	72-HOUR	BASIN AREA	MAXIMUM STAGE	TIME OF MAX STAGE
HYDROGRAPH AT	SUB1	56.	4.08	9.	2.	2.	0.04		
+ ROUTED TO	R1-2	56.	4.17	9.	2.	2.	0.04		
HYDROGRAPH AT	SUB2	80.	4.33	15.	4.	4.	0.12		
DIVERSION TO	D2	28.	4.33	2.	0.	0.	0.12		
+ HYDROGRAPH AT	DIV2	80.	4.33	13.	3.	3.	0.12		
2 COMBINED AT	C1-2	129.	4.25	22.	5.	5.	0.16		
ROUTED TO	R2-3	127.	4.33	22.	5.	5.	0.16		
+ HYDROGRAPH AT	SUB3	56.	4.25	9.	2.	2.	0.07		
DIVERSION TO	D3	28.	4.25	2.	0.	0.	0.07		
HYDROGRAPH AT	DIV3	56.	4.25	7.	2.	2.	0.07		
+ 2 COMBINED AT	C2-3	182.	4.33	29.	7.	7.	0.22		
ROUTED TO	R3-4	179.	4.33	29.	7.	7.	0.22		
HYDROGRAPH AT	SUB4	65.	4.17	10.	2.	2.	0.06		
+ DIVERSION TO	D4	34.	4.25	2.	1.	0.	0.06		
+ HYDROGRAPH AT	DIV4	64.	4.25	8.	2.	2.	0.06		
2 COMBINED AT	C3-4	239.	4.33	37.	9.	9.	0.29		

DIVERSION TO	DIBW	120.	4.33	20.	5.	5.	0.29
HYDROGRAPH AT	DIVIBW	119.	4.33	17.	4.	4.	0.29
ROUTED TO	R4-5	118.	4.42	17.	4.	4.	0.29
HYDROGRAPH AT	SUB5	39.	4.50	10.	3.	2.	0.07
DIVERSION TO	D5	20.	4.58	2.	0.	0.	0.07
HYDROGRAPH AT	DIV5	38.	4.58	8.	2.	2.	0.07
2 COMBINED AT	C4-5	137.	4.58	25.	6.	6.	0.35
HYDROGRAPH AT	SUB6	146.	4.00	21.	5.	5.	0.09
ROUTED TO	R6-7	142.	4.08	21.	5.	5.	0.09
HYDROGRAPH AT	SUB7	143.	4.25	25.	6.	6.	0.15
DIVERSION TO	D7	59.	4.33	5.	1.	1.	0.15
HYDROGRAPH AT	DIV7	141.	4.33	20.	5.	5.	0.15
2 COMBINED AT	C6-7	240.	4.33	42.	10.	10.	0.24
ROUTED TO	R7-8	235.	4.42	42.	10.	10.	0.24
HYDROGRAPH AT	SUB8	42.	4.42	9.	2.	2.	0.07
DIVERSION TO	D8	25.	4.50	2.	0.	0.	0.07
HYDROGRAPH AT	DIV8	41.	4.50	7.	2.	2.	0.07
2 COMBINED AT	C7-8	275.	4.42	49.	12.	12.	0.31
ROUTED TO	R8-9	266.	4.42	49.	12.	12.	0.31
HYDROGRAPH AT	SUB9	63.	4.17	9.	2.	2.	0.06
DIVERSION TO	D9	30.	4.17	2.	0.	0.	0.06
HYDROGRAPH AT	DIV9	63.	4.17	7.	2.	2.	0.06
2 COMBINED AT	C8-9	315.	4.42	56.	14.	14.	0.38
ROUTED TO	R9-5	305.	4.42	56.	14.	14.	0.38
2 COMBINED AT	C9-5	442.	4.42	81.	20.	20.	0.73
ROUTED TO	R5-10	352.	4.67	81.	20.	20.	0.73

HYDROGRAPH AT	SUB10	83.	4.25	14.	3.	3.	0.09
DIVERSION TO	D10	35.	4.33	2.	1.	1.	0.09
HYDROGRAPH AT	DIV10	82.	4.33	12.	3.	3.	0.09
2 COMBINED AT	C5-10	406.	4.58	92.	23.	22.	0.82
ROUTED TO	R10-15	391.	4.75	92.	23.	22.	0.82
HYDROGRAPH AT	SUB11	126.	4.08	20.	5.	5.	0.09
ROUTED TO	R11-12	124.	4.17	20.	5.	5.	0.09
HYDROGRAPH AT	SUB12	165.	4.00	20.	5.	5.	0.12
DIVERSION TO	D12	12.	4.08	1.	0.	0.	0.12
HYDROGRAPH AT	DIV12	164.	4.08	19.	5.	5.	0.12
2 COMBINED AT	C11-12	284.	4.08	39.	10.	9.	0.21
ROUTED TO	R12-13	279.	4.08	39.	10.	9.	0.21
HYDROGRAPH AT	SUB13	182.	4.08	23.	6.	6.	0.13
DIVERSION TO	D13	32.	4.08	2.	0.	0.	0.13
HYDROGRAPH AT	DIV13	182.	4.08	21.	5.	5.	0.13
2 COMBINED AT	C12-13	462.	4.08	59.	15.	14.	0.34
ROUTED TO	R13-14	452.	4.08	60.	15.	14.	0.34
HYDROGRAPH AT	SUB14	124.	4.08	16.	4.	4.	0.13
DIVERSION TO	D14	52.	4.08	3.	1.	1.	0.13
HYDROGRAPH AT	DIV14	124.	4.08	13.	3.	3.	0.13
2 COMBINED AT	C13-14	576.	4.08	73.	18.	18.	0.47
ROUTED TO	R14-15	566.	4.17	73.	18.	18.	0.47
HYDROGRAPH AT	SUB15	119.	4.25	19.	5.	5.	0.13
DIVERSION TO	D15	62.	4.25	4.	1.	1.	0.13
HYDROGRAPH AT	DIV15	119.	4.25	15.	4.	4.	0.13
3 COMBINED AT	C15-10	821.	4.25	179.	45.	43.	1.42
DIVERSION TO							

	D56ST	328.	4.25	38.	10.	9.	1.42
HYDROGRAPH AT	D56ST	493.	4.25	141.	36.	34.	1.42
ROUTED TO	R15-20	394.	5.08	132.	36.	34.	1.42
HYDROGRAPH AT	SUB16	186.	4.08	30.	7.	7.	0.13
ROUTED TO	R16-17	182.	4.17	30.	7.	7.	0.13
HYDROGRAPH AT	SUB17	78.	4.08	10.	2.	2.	0.07
DIVERSION TO	D17	4.	4.08	0.	0.	0.	0.07
HYDROGRAPH AT	DIV17	78.	4.08	10.	2.	2.	0.07
2 COMBINED AT	C16-17	258.	4.17	39.	10.	10.	0.20
ROUTED TO	R17-18	258.	4.17	39.	10.	10.	0.20
HYDROGRAPH AT	SUB18	63.	4.17	9.	2.	2.	0.07
DIVERSION TO	D18	25.	4.17	2.	0.	0.	0.07
HYDROGRAPH AT	DIV18	63.	4.17	7.	2.	2.	0.07
2 COMBINED AT	C17-18	321.	4.17	47.	12.	11.	0.27
ROUTED TO	R18-19	319.	4.17	47.	12.	11.	0.27
HYDROGRAPH AT	SUB19	67.	4.17	9.	2.	2.	0.08
DIVERSION TO	D19	33.	4.17	2.	0.	0.	0.08
HYDROGRAPH AT	DIV19	67.	4.17	8.	2.	2.	0.08
2 COMBINED AT	C18-19	386.	4.17	54.	14.	13.	0.34
ROUTED TO	R19-20	381.	4.17	54.	14.	13.	0.34
HYDROGRAPH AT	SUB20	130.	4.17	18.	4.	4.	0.13
DIVERSION TO	D20	64.	4.17	4.	1.	1.	0.13
HYDROGRAPH AT	DIV20	130.	4.17	14.	4.	3.	0.13
3 COMBINED AT	C20-15	713.	4.33	196.	53.	51.	1.89
ROUTED TO	R20-25	462.	5.00	169.	53.	51.	1.89
HYDROGRAPH AT	SUB21	187.	4.08	28.	7.	7.	0.12
ROUTED TO	R21-22	184.	4.17	28.	7.	7.	0.12

HYDROGRAPH AT	SUB22	81.	4.25	14.	4.	3.	0.11
DIVERSION TO	D22	4.	4.25	0.	0.	0.	0.11
HYDROGRAPH AT	DIV22	81.	4.25	14.	4.	3.	0.11
2 COMBINED AT	C21-22	258.	4.17	42.	11.	10.	0.24
ROUTED TO	R22-23	255.	4.17	42.	11.	10.	0.24
HYDROGRAPH AT	SUB23	59.	4.08	8.	2.	2.	0.06
DIVERSION TO	D23	25.	4.08	1.	0.	0.	0.06
HYDROGRAPH AT	DIV23	59.	4.08	6.	2.	1.	0.06
2 COMBINED AT	C22-23	312.	4.17	48.	12.	12.	0.30
ROUTED TO	R23-24	309.	4.17	49.	12.	12.	0.30
HYDROGRAPH AT	SUB24	65.	4.17	10.	2.	2.	0.08
DIVERSION TO	D24	30.	4.17	2.	0.	0.	0.08
HYDROGRAPH AT	DIV24	65.	4.17	8.	2.	2.	0.08
2 COMBINED AT	C23-24	374.	4.17	56.	14.	14.	0.37
ROUTED TO	R24-25	370.	4.25	56.	14.	14.	0.37
HYDROGRAPH AT	SUB25	62.	4.25	10.	2.	2.	0.08
DIVERSION TO	D25	32.	4.25	2.	0.	0.	0.08
HYDROGRAPH AT	DIV25	62.	4.25	8.	2.	2.	0.08
3 COMBINED AT	C25-20	630.	4.58	226.	69.	66.	2.34
ROUTED TO	R25-29	571.	4.92	225.	69.	66.	2.34
HYDROGRAPH AT	SUB26	44.	4.17	7.	2.	2.	0.05
DIVERSION TO	D26	9.	4.17	1.	0.	0.	0.05
HYDROGRAPH AT	DIV26	44.	4.17	6.	2.	2.	0.05
ROUTED TO	R26-27	44.	4.17	6.	2.	2.	0.05
HYDROGRAPH AT	SUB27	56.	4.17	8.	2.	2.	0.06
DIVERSION TO	D27	23.	4.17	1.	0.	0.	0.06

HYDROGRAPH AT	DIV27	56.	4.17	6.	2.	1.	0.06
2 COMBINED AT	C26-27	100.	4.17	13.	3.	3.	0.11
ROUTED TO	R27-28	98.	4.17	13.	3.	3.	0.11
HYDROGRAPH AT	SUB28	69.	4.17	10.	2.	2.	0.08
DIVERSION TO	D28	34.	4.17	2.	0.	0.	0.08
HYDROGRAPH AT	DIV28	69.	4.17	8.	2.	2.	0.08
2 COMBINED AT	C27-28	167.	4.17	20.	5.	5.	0.19
ROUTED TO	R28-29	163.	4.25	21.	5.	5.	0.19
HYDROGRAPH AT	SUB29	48.	4.25	7.	2.	2.	0.06
DIVERSION TO	D29	21.	4.25	1.	0.	0.	0.06
HYDROGRAPH AT	DIV29	48.	4.25	6.	1.	1.	0.06
3 COMBINED AT	C29-25	622.	4.83	250.	75.	72.	2.59
DIVERSION TO	DOCCC	622.	0.08	250.	75.	72.	2.59
HYDROGRAPH AT	DOCCC	0.	0.08	0.	0.	0.	2.59
ROUTED TO	R29-33	0.	0.08	0.	0.	0.	2.59
HYDROGRAPH AT	SUB38	267.	4.25	52.	13.	13.	0.25
DIVERSION TO	D38-39	16.	4.25	11.	3.	3.	0.25
HYDROGRAPH AT	D38-39	251.	4.25	40.	10.	10.	0.25
ROUTED TO	R38-30	250.	4.33	40.	10.	10.	0.25
HYDROGRAPH AT	SUB30	58.	4.17	8.	2.	2.	0.06
2 COMBINED AT	C30-38	303.	4.25	48.	12.	12.	0.32
ROUTED TO	R30-31	301.	4.33	48.	12.	12.	0.32
HYDROGRAPH AT	SUB31	49.	4.17	7.	2.	2.	0.06
DIVERSION TO	D31	16.	4.17	1.	0.	0.	0.06
HYDROGRAPH AT	DIV31	49.	4.17	6.	2.	1.	0.06
2 COMBINED AT	C30-31	346.	4.25	55.	14.	13.	0.38
ROUTED TO							

	R31-32	343.	4.33	55.	14.	13.	0.38
HYDROGRAPH AT	SUB32	54.	4.17	8.	2.	2.	0.06
DIVERSION TO	D32	25.	4.17	2.	0.	0.	0.06
HYDROGRAPH AT	DIV32	54.	4.17	7.	2.	2.	0.06
2 COMBINED AT	C31-32	396.	4.25	61.	15.	15.	0.44
ROUTED TO	R32-33	395.	4.33	61.	15.	15.	0.44
HYDROGRAPH AT	SUB33	61.	4.17	9.	2.	2.	0.06
DIVERSION TO	D33	20.	4.17	1.	0.	0.	0.06
HYDROGRAPH AT	DIV33	61.	4.17	8.	2.	2.	0.06
3 COMBINED AT	C33-29	445.	4.33	69.	17.	17.	3.09
ROUTED TO	R33-35	298.	4.67	68.	17.	17.	3.09
HYDROGRAPH AT	SUB34	122.	4.25	23.	6.	6.	0.17
DIVERSION TO	D34	42.	4.33	3.	1.	1.	0.17
HYDROGRAPH AT	DIV34	122.	4.33	20.	5.	5.	0.17
ROUTED TO	R34-35	119.	4.42	20.	5.	5.	0.17
HYDROGRAPH AT	SUB35	150.	4.08	24.	6.	6.	0.13
DIVERSION TO	D35	13.	4.17	1.	0.	0.	0.13
HYDROGRAPH AT	DIV35	146.	4.17	22.	6.	5.	0.13
3 COMBINED AT	C35-33	481.	4.42	109.	28.	27.	3.39
ROUTED TO	R35-36	329.	5.00	109.	28.	27.	3.39
HYDROGRAPH AT	SUB40	91.	4.08	10.	2.	2.	0.07
ROUTED TO	R40-41	89.	4.08	10.	2.	2.	0.07
HYDROGRAPH AT	SUB41	141.	4.25	23.	6.	5.	0.16
2 COMBINED AT	C40-41	223.	4.17	33.	8.	8.	0.23
ROUTED TO	R41-39	219.	4.25	33.	8.	8.	0.23
HYDROGRAPH AT	SUB37	45.	4.08	6.	1.	1.	0.05
ROUTED TO	R37-39	45.	4.25	6.	1.	1.	0.05

HYDROGRAPH AT	SUB39	176.	4.33	38.	10.	9.	0.22
DIVERSION TO	D39-36	16.	4.25	1.	0.	0.	0.22
HYDROGRAPH AT	D39-36	160.	4.25	37.	9.	9.	0.22
DIVERSION TO	DCBR1	55.	4.25	22.	6.	5.	0.22
HYDROGRAPH AT	DCBR1	105.	4.25	15.	4.	4.	0.22
DIVERSION TO	DCBR2	60.	4.25	11.	3.	3.	0.22
HYDROGRAPH AT	DCBR2	45.	4.25	4.	1.	1.	0.22
HYDROGRAPH AT	RD3839	16.	3.33	11.	3.	3.	0.00
4 COMBINED AT	C37-41	325.	4.25	54.	14.	13.	0.50
ROUTED TO	R39-36	323.	4.25	54.	14.	13.	0.50
HYDROGRAPH AT	SUB36	83.	4.25	17.	4.	4.	0.09
DIVERSION TO	D36	12.	4.42	1.	0.	0.	0.09
HYDROGRAPH AT	DIV36	79.	4.42	16.	4.	4.	0.09
HYDROGRAPH AT	RDCBR2	60.	4.08	11.	3.	3.	0.00
HYDROGRAPH AT	RD3936	16.	4.33	1.	0.	0.	0.00
5 COMBINED AT	C36-35	708.	4.42	187.	48.	47.	3.98
DIVERSION TO	D40ST	698.	0.92	177.	45.	43.	3.98
HYDROGRAPH AT	D40ST	10.	0.92	10.	4.	4.	3.98
ROUTED TO	R36-42	10.	5.17	10.	4.	4.	3.98
HYDROGRAPH AT	SUB42	221.	4.25	39.	10.	9.	0.21
DIVERSION TO	D42	16.	4.25	2.	0.	0.	0.21
HYDROGRAPH AT	DIV42	205.	4.25	38.	9.	9.	0.21
2 COMBINED AT	C42-36	215.	4.25	47.	13.	13.	4.19

SUMMARY OF KINEMATIC WAVE - MUSKINGUM-CUNGE ROUTING
(FLOW IS DIRECT RUNOFF WITHOUT BASE FLOW)

ISTAQ	ELEMENT	DT (MIN)	PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	INTERPOLATED TO COMPUTATION INTERVAL DT (MIN)	PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)

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R1-2  MANE        4.36    55.85   252.66     2.18     5.00    55.52   250.00       2.18

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.4276E+01 EXCESS=0.0000E+00 OUTFLOW=0.4301E+01 BASIN STORAGE=0.2195E-05 PERCENT ERROR=  -0.6

R2-3  MANE        0.95   128.83   257.32     1.29     5.00   127.41   260.00       1.29

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.1076E+02 EXCESS=0.0000E+00 OUTFLOW=0.1077E+02 BASIN STORAGE=0.4878E-04 PERCENT ERROR=  -0.1

R3-4  MANE        0.84   181.08   261.42     1.21     5.00   179.43   260.00       1.21

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.1436E+02 EXCESS=0.0000E+00 OUTFLOW=0.1437E+02 BASIN STORAGE=0.9252E-04 PERCENT ERROR=  -0.1

R4-5  MANE        1.89   118.10   264.47     0.54     5.00   117.50   265.00       0.54

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.8250E+01 EXCESS=0.0000E+00 OUTFLOW=0.8274E+01 BASIN STORAGE=0.8960E-04 PERCENT ERROR=  -0.3

R6-7  MANE        3.52   142.74   245.52     2.21     5.00   141.56   245.00       2.21

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.1054E+02 EXCESS=0.0000E+00 OUTFLOW=0.1061E+02 BASIN STORAGE=0.2330E-05 PERCENT ERROR=  -0.7

R7-8  MANE        2.33   237.49   264.42     1.61     5.00   235.49   265.00       1.61

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.2077E+02 EXCESS=0.0000E+00 OUTFLOW=0.2080E+02 BASIN STORAGE=0.3815E-03 PERCENT ERROR=  -0.2

R8-9  MANE        0.59   273.35   266.07     1.47     5.00   265.73   265.00       1.47

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.2438E+02 EXCESS=0.0000E+00 OUTFLOW=0.2438E+02 BASIN STORAGE=0.1233E-03 PERCENT ERROR=   0.0

R9-5  MANE        0.84   313.49   267.17     1.40     5.00   305.37   265.00       1.40

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.2800E+02 EXCESS=0.0000E+00 OUTFLOW=0.2801E+02 BASIN STORAGE=0.4088E-03 PERCENT ERROR=  -0.1

R11-12  MANE      1.23   125.52   247.53     1.97     5.00   124.24   250.00       1.97

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.9756E+01 EXCESS=0.0000E+00 OUTFLOW=0.9765E+01 BASIN STORAGE=0.3149E-07 PERCENT ERROR=  -0.1

R12-13  MANE      0.07   283.59   246.53     1.69     5.00   279.43   245.00       1.69

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.1922E+02 EXCESS=0.0000E+00 OUTFLOW=0.1922E+02 BASIN STORAGE=0.1767E-04 PERCENT ERROR=   0.0

R13-14  MANE      0.49   460.02   246.28     1.62     5.00   451.99   245.00       1.63

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.2959E+02 EXCESS=0.0000E+00 OUTFLOW=0.2962E+02 BASIN STORAGE=0.5235E-04 PERCENT ERROR=  -0.1

R14-15  MANE      0.86   574.69   246.87     1.45     5.00   566.01   250.00       1.45

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.3613E+02 EXCESS=0.0000E+00 OUTFLOW=0.3616E+02 BASIN STORAGE=0.1698E-03 PERCENT ERROR=  -0.1

R16-17  MANE      1.23   185.25   247.57     2.15     5.00   182.23   250.00       2.15

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.1479E+02 EXCESS=0.0000E+00 OUTFLOW=0.1480E+02 BASIN STORAGE=0.2771E-07 PERCENT ERROR=  -0.1

R17-18  MANE      0.59   258.16   250.36     1.82     5.00   258.14   250.00       1.82
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CONTINUITY SUMMARY (AC-FT) - INFLOW=0.1960E+02 EXCESS=0.0000E+00 OUTFLOW=0.1961E+02 BASIN STORAGE=0.9280E-05 PERCENT ERROR= -0.1

R18-19	MANE	0.66	320.16	250.71	1.62	5.00	319.48	250.00	1.62

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.2316E+02 EXCESS=0.0000E+00 OUTFLOW=0.2317E+02 BASIN STORAGE=0.2847E-04 PERCENT ERROR= 0.0

R19-20	MANE	0.61	385.13	251.02	1.47	5.00	380.60	250.00	1.47

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.2700E+02 EXCESS=0.0000E+00 OUTFLOW=0.2701E+02 BASIN STORAGE=0.5081E-04 PERCENT ERROR= -0.1

R21-22	MANE	2.38	183.80	248.39	2.13	5.00	183.59	250.00	2.13

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.1408E+02 EXCESS=0.0000E+00 OUTFLOW=0.1411E+02 BASIN STORAGE=0.6787E-06 PERCENT ERROR= -0.2

R22-23	MANE	0.37	257.92	250.94	1.68	5.00	255.43	250.00	1.68

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.2108E+02 EXCESS=0.0000E+00 OUTFLOW=0.2109E+02 BASIN STORAGE=0.3245E-05 PERCENT ERROR= 0.0

R23-24	MANE	0.46	311.69	250.75	1.53	5.00	309.21	250.00	1.53

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.2415E+02 EXCESS=0.0000E+00 OUTFLOW=0.2415E+02 BASIN STORAGE=0.1223E-04 PERCENT ERROR= 0.0

R24-25	MANE	0.61	373.79	251.44	1.41	5.00	369.54	255.00	1.41

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.2808E+02 EXCESS=0.0000E+00 OUTFLOW=0.2809E+02 BASIN STORAGE=0.5090E-04 PERCENT ERROR= -0.1

R26-27	MANE	0.82	44.02	251.28	1.11	5.00	43.79	250.00	1.11

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.3141E+01 EXCESS=0.0000E+00 OUTFLOW=0.3145E+01 BASIN STORAGE=0.4836E-05 PERCENT ERROR= -0.1

R27-28	MANE	0.83	99.68	251.70	1.03	5.00	98.25	250.00	1.03

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.6233E+01 EXCESS=0.0000E+00 OUTFLOW=0.6241E+01 BASIN STORAGE=0.1730E-04 PERCENT ERROR= -0.1

R28-29	MANE	0.70	166.75	251.71	1.00	5.00	163.21	255.00	1.00

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.1019E+02 EXCESS=0.0000E+00 OUTFLOW=0.1020E+02 BASIN STORAGE=0.3296E-04 PERCENT ERROR= -0.1

R38-30	MANE	0.42	250.60	255.96	1.48	5.00	250.46	260.00	1.48

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.1992E+02 EXCESS=0.0000E+00 OUTFLOW=0.1993E+02 BASIN STORAGE=0.1441E-05 PERCENT ERROR= 0.0

R30-31	MANE	0.53	302.61	256.02	1.43	5.00	300.73	260.00	1.43

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.2402E+02 EXCESS=0.0000E+00 OUTFLOW=0.2402E+02 BASIN STORAGE=0.6377E-05 PERCENT ERROR= 0.0

R31-32	MANE	0.45	345.64	256.01	1.35	5.00	343.36	260.00	1.35

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.2708E+02 EXCESS=0.0000E+00 OUTFLOW=0.2709E+02 BASIN STORAGE=0.1416E-04 PERCENT ERROR= 0.0

R32-33	MANE	1.38	395.93	257.76	1.29	5.00	394.68	260.00	1.29

```
ONTINUITY SUMMARY (AC-FT) - INFLOW=0.3040E+02 EXCESS=0.0000E+00 OUTFLOW=0.3042E+02 BASIN STORAGE=0.7978E-05 PERCENT ERROR=  -0.1

          R34-35  MANE        0.76    121.83    261.37      1.11      5.00    119.38    265.00        1.11

ONTINUITY SUMMARY (AC-FT) - INFLOW=0.9901E+01 EXCESS=0.0000E+00 OUTFLOW=0.9908E+01 BASIN STORAGE=0.1228E-04 PERCENT ERROR=  -0.1

          R40-41  MANE        1.19     91.18    247.07      1.24      5.00     89.48    245.00        1.24

 CONTINUITY SUMMARY (AC-FT) - INFLOW=0.4895E+01 EXCESS=0.0000E+00 OUTFLOW=0.4909E+01 BASIN STORAGE=0.3695E-06 PERCENT ERROR=  -0.3

          R41-39  MANE        1.68    222.49    253.51      1.32      5.00    218.71    255.00        1.32

ONTINUITY SUMMARY (AC-FT) - INFLOW=0.1621E+02 EXCESS=0.0000E+00 OUTFLOW=0.1624E+02 BASIN STORAGE=0.2203E-05 PERCENT ERROR=  -0.2

          R37-39  MANE        3.22     45.14    252.75      1.07      5.00     44.87    255.00        1.07

ONTINUITY SUMMARY (AC-FT) - INFLOW=0.2782E+01 EXCESS=0.0000E+00 OUTFLOW=0.2798E+01 BASIN STORAGE=0.1967E-03 PERCENT ERROR=  -0.6

          R39-36  MANE        0.66    323.93    255.91      1.01      5.00    323.44    255.00        1.01

 CONTINUITY SUMMARY (AC-FT) - INFLOW=0.2703E+02 EXCESS=0.0000E+00 OUTFLOW=0.2704E+02 BASIN STORAGE=0.1159E-03 PERCENT ERROR=   0.0


** NORMAL END OF HEC-1 ***
```

A-5

HEC-2 MODEL

```
*********************************************
*  HEC-2 WATER SURFACE PROFILES             *
*                                           *
*  Version   4.6.2;  May 1991               *
*                                           *
*  RUN DATE    31AUG95    TIME   10:05:11   *
*********************************************
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************************************
*  U.S. ARMY CORPS OF ENGINEERS
*  HYDROLOGIC ENGINEERING CENTER
*  609 SECOND STREET, SUITE D
*  DAVIS, CALIFORNIA 95616-4687
*          (916) 756-1104
************************************
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X     X  XXXXXXX   XXXXX              XXXXX
X     X  X        X     X            X     X
X     X  X        X                        X
XXXXXXX  XXXX     X          XXXXX    XXXXX
X     X  X        X                  X
X     X  X        X     X            X
X     X  XXXXXXX   XXXXX             XXXXXXX
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THIS RUN EXECUTED 31AUG95 10:05:11

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************************************
 HEC-2 WATER SURFACE PROFILES

 Version   4.6.2;  May 1991
************************************
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AZCANAL1.DAT
HEC-2 ANALYSIS OF AZ. CANAL UTILIZING SPLIT FLOW
FOR WATER PONDING NORTH OF CANAL BANK.
EXISTING CONDITIONS
PREPARED BY: HUITT-ZOLLARS INC. 8-31-95

SPLIT FLOW BEING PERFORMED

SF

```
TW      SPILT FLOW AT 56TH ST.
WS     2   99267   99327   99266     3.4
WC     0  1255.2      60  1255.3

TW      SPLIT FL OW STA.991+67 TO 992+66
WS     2   99167   99266   99167     3.4
WC     0  1255.6      99  1255.6

TW      SPLIT FL OW STA.990+80 TO 991+67
WS     2   99080   99167   99080     3.4
WC     0  1255.6      87  1255.6

TW      SPLIT FL OW STA.990+00 TO 990+80
WS     2   99000   99080   99000     3.4
WC     0  1255.6      80  1255.6

TW      SPLIT FLOW STA. 988+15 TO 990+00
WS     2   98815   99000   98815     3.4
WC     0 1254.59     185  1255.6

TW      SPLIT FLOW STA. 985+00 TO 988+15
WS     2   98500   98815   98500     3.4
WC     0 1254.56     315 1254.59
```

```
TW      SPLIT FLOW STA. 980+00 TO 985+00
WS    2   98000   98500   98000     3.4
WC    0  1253.7     500 1254.76

TW      SPLIT FLOW STA. 975+00 TO 980+00
WS    2   97500   98000   97500     3.4
WC    0  1253.9     500 1254.76

TW      SPLIT FLOW STA. 970+00 TO 975+00
WS    2   97000   97500   97000     3.4
WC    0  1253.9     500  1253.9

TW      SPLIT FLOW STA. 965+00 TO 970+00
WS    2   96500   97000   96500     3.4
WC    0  1254.3     500  1253.9

TW      SPLIT FLOW STA. 960+00 TO 965+00
WS    2   96000   96500   96000     3.4
WC    0  1254.3     500  1254.3

TW      SPLIT FLOW STA. 955+00 TO 960+00
WS    2   95500   96000   95500     3.4
WC    0  1254.1     500  1254.3

TW      SPLIT FLOW STA. 950+00 TO 955+00
WS    2   95000   95500   95000     3.4
WC    0  1254.1     500  1254.3

TW      SPLIT FLOW STA. 945+00 TO 950+00
WS    2   94500   95000   94500     3.4
WC    0  1253.4     500  1254.1

TW      SPLIT FLOW STA. 940+00 TO 945+00
WS    2   94000   94500   94000     3.4
WC    0  1253.4     500  1253.4
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T1
T2
T3

J1  ICHECK    INQ       NINV      IDIR      STRT      METRIC    HVINS     Q         WSEL      FQ

                2                           .0006                                   1248.5

J2  NPROF     IPLOT     PRFVS     XSECV     XSECH     FN        ALLDC     IBW       CHNIM     ITRACE

     1                  -1

J3  VARIABLE CODES FOR SUMMARY PRINTOUT

    150

        STATIONS FOR MODIFIED PULS ROUTING

J4                     *************ROUTING REACHES*************

  ** 102500.000 104000.000 **  99408.000 102500.000 **  97000.000  99408.000 **  94500.000  97500.000 **  93574.000  95000.000
  **  92000.000  93574.000 **  89545.000  92000.000 **  86415.000  89545.000 **  84000.000  86415.000 **

J5  LPRNT    NUMSEC                    ********REQUESTED SECTION NUMBERS********

    -10       -10

NC      .02        .8       .018

QT        6        75        250        500       1200       2400       4000

X1    84000        36      65.52     143.71
X3       10                            65.52       1251
GR   1245.9         0    1246.32      13.28    1249.55      33.84    1251.52      39.28    1251.00      65.52
GR   1247.7     72.77     1247.7     135.13    1247.78     137.47    1249.87     143.61    1249.89     143.71
GR   1249.6    153.40    1249.37     158.50    1249.52     171.57    1249.01     188.41    1248.76     190.37
GR   1248.6    194.25    1248.47     203.17    1248.90     207.00    1248.30     216.58    1240.93     228.76
GR   1241.1    301.88    1241.98     399.16    1246.89     408.17    1246.01     434.38    1246.01     436.60
GR   1247.0    444.66    1249.06     459.78    1248.81     473.34    1249.54     499.26    1249.91     508.21
GR   1250.2    518.13    1250.43     528.22    1250.30     549.55    1250.10     579.01     1251.7     600.20
GR   1253.3    700.00

X1    84500        21      63.29     162.86       500        500        500
X3       10                            63.29    1252.78
GR   1246.9         0    1246.54      18.39    1252.20      34.70    1252.78      63.29     1247.9      73.46
GR   1247.9    135.23    1251.86     142.67    1252.15     157.01    1252.79     162.86    1252.3     185.18
GR   1251.6    202.87    1248.51     304.79    1248.16     370.77    1248.24     376.54    1249.1     385.61
GR   1249.7    399.40    1236.36     469.43    1236.89     488.09     1237.0     499.89    1237.6     600.52
GR   1237.0    700.00
```

X1	85000	31	31.46	183.86	500	500	500			
X3	10			31.46	1250.24					
GR	1246.1	0	1247.13	18.88	1250.24	31.46	1248.72	73.12	1248.1	74.57
GR	1248.1	137.24	1251.47	144.06	1251.47	144.13	1251.38	164.74	1251.11	165.57
GR	1252.3	183.86	1252.93	198.24	1254.46	310.56	1253.18	337.65	1252.23	348.50
GR	1252.1	353.03	1252.40	385.83	1251.87	388.89	1251.14	402.80	1251.00	414.79
GR	1251.0	417.40	1251.09	423.50	1251.67	451.93	1253.93	498.70	1254.25	499.70
GR	1254.0	502.03	1253.53	521.94	1253.53	521.94	1253.04	521.94	1253.04	552.23
GR	1253.5	605.72								

X1	85500	36	64.69	156.79	500	500	500			
X3	10			64.69	1250.07					
GR	1245.8	0	1246.09	21.28	1250.09	29.14	1250.07	64.69	1248.2	67.84
GR	1248.2	134.90	1250.81	140.75	1251.31	156.79	1250.74	165.57	1251.77	177.97
GR	1251.3	203.68	1251.76	283.45	1251.44	285.14	1245.19	286.55	1246.81	306.44
GR	1247.8	319.51	1248.12	320.05	1248.23	322.03	1249.36	322.88	1249.30	323.29
GR	1248.6	332.89	1248.42	338.30	1251.62	429.21	1248.49	445.15	1247.62	455.73
GR	1253.1	456.87	1253.15	474.74	1251.92	486.26	1250.57	500.93	1251.75	518.71
GR	1252.6	563.72	1252.25	564.30	1252.48	577.43	1253.03	592.10	1252.69	602.36
GR	1253.6	700.00								

X1	86024	28	64.9	159.98	524	524	524			
X3	10			64.9	1250.03					
GR	1248.7	0	1249.11	16.88	1250.03	64.90	1248.4	65.77	1248.4	129.60
GR	1252.1	140.33	1252.36	159.98	1251.46	172.26	1250.86	172.76	1250.96	187.74
GR	1251.4	196.65	1250.85	201.88	1250.98	210.65	1251.24	217.55	1251.09	225.97
GR	1251.7	226.47	1252.91	234.97	1253.53	250.08	1253.11	341.54	1252.72	443.11
GR	1253.6	503.66	1256.43	536.63	1253.39	543.48	1252.06	623.44	1251.94	645.48
GR	1252.0	648.28	1252.66	672.53	1253.47	700.00				

X1	86415	46	67.27	140.43	391	391	391			
X3	10			67.27	1251.27					
GR	1246.0	0	1247.34	25.58	1251.27	37.09	1252.02	67.27	1248.6	74.66
GR	1248.6	74.66	1246.29	123.43	1250.79	125.95	1250.90	140.43	1251.37	178.12
GR	1252.0	178.76	1251.97	178.76	1251.99	183.65	1252.06	195.02	1251.52	195.64
GR	1251.4	197.79	1250.68	240.35	1251.48	244.22	1251.74	260.49	1251.15	270.52
GR	1250.3	277.30	1250.93	282.56	1251.15	284.55	1251.93	289.49	1252.46	292.13
GR	1252.0	300.09	1252.68	345.32	1253.04	345.70	1254.06	356.13	1254.21	356.13
GR	1254.2	359.15	1254.66	402.35	1255.90	422.27	1254.71	501.21	1254.37	520.62
GR	1253.9	535.82	1254.01	538.35	1253.41	538.86	1253.22	541.27	1252.65	555.41
GR	1252.9	583.11	1253.48	583.72	1253.43	586.62	1252.86	587.35	1252.76	609.48
GR	1253.9	700.00								

X1	87000	33	61.34	138	585	585	585			
X3	10			61.34	1253.4					
GR	1246.7	0	1246.64	24.41	1252.82	40.38	1253.40	61.34	1248.8	72.12
GR	1248.8	130.40	1251.00	138.00	1250.88	144.09	1250.29	157.84	1248.66	159.52
GR	1248.8	164.61	1248.68	200.19	1249.13	202.38	1248.85	211.86	1249.08	217.27
GR	1249.4	233.92	1249.05	244.62	1249.42	252.97	1249.77	270.62	1250.34	273.43

GR	1250.4	300.37	1250.57	315.88	1250.16	350.91	1250.46	413.78	1250.22	452.10
GR	1250.7	467.41	1251.53	476.63	1251.53	479.03	1251.37	482.34	1251.80	506.85
GR	1252.0	597.78	1252.25	600.48	1253.64	700.00				
X1	87500	33	39.19	139.45	500	500	500			
X3	10			39.19	1253.67					
GR	1248.5	0	1248.44	19.18	1253.67	39.19	1253.55	62.66	1248.9	71.71
GR	1248.9	132.17	1252.17	139.45	1252.08	142.96	1251.54	155.95	1251.95	157.46
GR	1251.3	160.54	1250.32	166.92	1250.89	199.62	1251.81	220.22	1251.50	228.45
GR	1252.9	238.64	1251.61	252.93	1252.45	265.47	1252.26	299.45	1252.60	312.27
GR	1251.8	351.52	1251.95	400.40	1252.05	418.53	1251.64	426.06	1251.83	431.17
GR	1252.2	433.67	1252.97	454.47	1254.18	470.13	1253.53	500.20	1252.91	511.41
GR	1253.3	586.52	1253.90	600.33	1254.19	700.00				
X1	88000	30	61.51	137.65	500	500	500			
X3	10			61.51	1253.47					
GR	1247.9	0	1247.74	24.42	1251.12	32.82	1253.28	39.35	1253.47	61.51
GR	1249.0	70.47	1249.0	130.27	1251.26	137.65	1250.35	163.83	1250.08	169.10
GR	1250.6	183.79	1251.01	186.61	1251.03	199.69	1251.43	255.80	1251.35	271.13
GR	1250.7	294.20	1250.15	300.91	1250.30	331.76	1250.70	332.76	1250.83	337.60
GR	1251.6	350.00	1251.98	364.16	1252.28	397.38	1252.04	452.02	1252.46	502.86
GR	1252.3	554.23	1251.63	585.87	1251.22	586.56	1251.78	601.51	1252.66	700.0
X1	88500	26	63.25	154.04	500	500	500			
X3	10			63.25	1252.86					
GR	1247.6	0	1247.45	27.37	1252.65	39.98	1252.86	63.25	1249.1	69.72
GR	1249.1	131.44	1250.66	137.94	1251.14	154.04	1250.08	157.91	1249.42	160.21
GR	1250.0	169.78	1249.94	197.32	1249.89	298.12	1249.98	307.94	1250.05	310.84
GR	1250.1	316.99	1249.86	326.96	1250.92	330.31	1251.11	352.11	1251.19	395.87
GR	1251.8	440.30	1251.93	487.71	1252.35	511.68	1252.65	559.34	1252.81	603.65
GR	1253.7	700.00								
X1	89000	34	45.36	138.71	500	500	500			
X3	10			45.36	1252.46					
GR	1248.1	0	1248.83	32.63	1252.46	45.36	1251.46	64.93	1249.3	71.04
GR	1249.3	132.88	1250.59	138.71	1249.97	165.32	1249.82	177.85	1250.05	188.39
GR	1250.5	199.89	1250.64	231.40	1250.65	303.39	1251.02	310.05	1251.08	315.89
GR	1250.7	316.90	1250.97	338.91	1250.83	350.56	1251.22	351.75	1251.58	359.92
GR	1252.3	404.47	1252.83	450.80	1253.28	496.72	1252.73	497.64	1253.08	503.65
GR	1253.4	510.67	1254.16	535.01	1254.25	538.38	1253.93	558.78	1253.76	562.50
GR	1253.8	583.69	1254.05	584.73	1254.33	602.65	1255.53	700.0		
X1	89545	31	65.33	135.02	455	455	455			
X3	10			65.33	1252.1					
GR	1250.3	0	1250.91	24.54	1252.10	65.33	1252.03	70.97	1249.5	73.76
GR	1249.5	127.35	1251.95	135.02	1251.10	158.37	1250.52	160.32	1250.47	163.59
GR	1250.7	208.61	1251.14	284.82	1250.83	285.62	1251.13	290.60	1251.52	301.13
GR	1251.2	315.36	1253.01	317.04	1252.57	320.27	1252.98	385.13	1252.72	400.20
GR	1252.5	434.09	1253.57	436.75	1253.86	450.31	1254.17	452.71	1254.54	494.05

GR	1254.3	512.44	1254.14	557.50	1254.59	571.23	1254.34	575.64	1255.43	592.84
GR	1256.7	700.00								

X1	90000	33	63.73	167.61	545	545	545			
X3	10			63.73	1253.15					
GR	1247.8	0	1248.20	31.99	1252.99	45.08	1253.15	63.73	1249.6	72.51
GR	1249.6	131.94	1250.37	135.66	1251.79	167.61	1251.91	169.51	1251.76	173.64
GR	1251.8	200.66	1250.95	252.82	1251.21	270.60	1251.82	276.10	1251.42	277.00
GR	1251.8	288.92	1251.34	302.78	1251.29	307.20	1252.20	309.01	1253.00	310.33
GR	1252.2	324.02	1252.18	329.52	1252.59	350.80	1252.50	406.83	1255.56	451.32
GR	1255.2	505.42	1254.80	523.02	1254.86	546.17	1255.19	553.08	1255.42	590.25
GR	1256.5	592.53	1256.20	594.21	1255.82	700.00				

X1	90500	22	53.26	161.31	500	500	500			
X3	10			53.26	1254.17					
GR	1248.2	0	1248.64	32.94	1251.86	40.56	1254.17	53.26	1249.5	73.00
GR	1249.5	73.00	1247.04	134.32	1251.29	139.71	1251.08	154.06	1251.53	161.31
GR	1251.7	201.18	1251.45	252.66	1251.9	299.06	1252.37	307.34	1251.4	314.99
GR	1253.5	401.54	1253.61	429.26	1254.79	448.24	1255.1	491.51	1255.26	553.76
GR	1256.0	599.46	1257.2	700.00						

X1	91000	26	64.02	139.54	500	500	500			
X3	10			64.02	1254.89					
GR	1248.4	0	1248.98	37.65	1254.39	47.35	1254.89	64.02	1249.7	74.36
GR	1249.7	134.03	1251.14	139.54	1251.08	168.26	1251.08	195.07	1251.42	248.99
GR	1251.9	271.27	1252.02	272.62	1251.95	281.22	1252.09	282.91	1252.72	295.14
GR	1252.6	306.49	1252.24	311.40	1252.64	312.30	1252.93	346.18	1253.51	405.03
GR	1255.1	458.28	1255.12	504.19	1255.26	516.96	1255.89	553.43	1256.44	597.43
GR	1258.1	700.00								

X1	91500	29	63.7	170.53	500	500	500			
X3	10			63.7	1254.2					
GR	1248.2	0	1249.50	37.76	1253.79	49.90	1254.20	63.70	1249.8	73.12
GR	1249.8	130.94	1251.02	135.91	1251.31	170.53	1251.26	200.55	1251.13	206.99
GR	1252.6	266.41	1252.17	296.06	1252.06	328.94	1253.06	345.15	1253.24	355.46
GR	1253.4	400.51	1253.69	405.94	1254.44	430.80	1254.51	464.74	1254.51	476.06
GR	1254.1	480.41	1254.75	488.49	1255.48	502.24	1256.72	560.72	1255.93	563.67
GR	1256.7	579.11	1256.89	584.77	1256.48	593.96	1257.80	700.00		

X1	92000	28	63.12	150.53	500	500	500			
X3	10			63.12	1253.93					
GR	1249.3	0	1249.75	18.52	1251.06	40.66	1253.93	63.12	1249.9	72.77
GR	1249.9	129.22	1250.90	132.78	1251.47	136.43	1252.37	150.53	1251.54	151.07
GR	1252.3	161.17	1252.98	202.68	1252.97	252.40	1253.58	303.29	1253.53	320.44
GR	1253.6	324.06	1254.04	324.96	1254.41	342.72	1254.55	396.20	1255.08	472.73
GR	1255.9	476.30	1255.91	483.90	1255.66	489.90	1255.72	495.89	1255.99	504.70
GR	1257.1	538.17	1257.0	592.75	1258.45	700.00				

X1	92500	32	61.34	155.76	500	500	500			
X3	10			61.34	1254.57					
GR	1248.9	0	1250.23	33.31	1254.15	44.16	1254.57	61.34	1250.0	71.28
GR	1250.0	126.74	1251.93	140.81	1252.08	155.76	1252.52	165.02	1252.48	207.52
GR	1253.0	267.89	1252.62	302.90	1252.73	311.42	1253.73	314.37	1254.14	315.38
GR	1254.2	349.15	1254.55	400.67	1255.06	402.29	1256.15	405.88	1255.72	410.35
GR	1255.1	420.99	1255.58	434.14	1255.86	462.23	1255.87	498.79	1256.05	543.15
GR	1255.9	552.26	1255.57	580.73	1256.36	581.81	1256.90	585.82	1257.57	587.90
GR	1257.6	604.11	1258.67	700.0						
X1	93000	34	64.27	135.43	500	500	500			
X3	10			64.27	1255.48					
GR	1249.7	0	1250.75	29.70	1255.26	40.76	1255.48	64.27	1250.2	73.43
GR	1250.2	126.73	1250.40	130.76	1253.39	135.43	1253.02	153.06	1252.61	158.59
GR	1252.9	207.13	1253.1	221.70	1253.63	233.87	1253.64	236.69	1253.14	246.68
GR	1253.7	263.44	1253.45	269.09	1253.08	270.38	1253.56	290.99	1253.00	299.54
GR	1253.8	304.72	1254.88	306.68	1254.42	315.74	1254.49	391.46	1254.96	402.30
GR	1255.5	405.75	1256.01	439.50	1256.53	450.56	1256.86	571.17	1256.76	572.01
GR	1256.9	584.91	1257.25	588.92	1256.46	602.61	1259.21	700.0		
NC	.018	.8	.07							
X1	93574	28	136.8	304.21	426	426	426			
X3	10			65.58	1253.76					
GR	1237.7	0	1238.4	13.55	1253.73	19.43	1253.79	22.72	1252.77	30.16
GR	1253.0	35.56	1253.64	60.01	1253.76	65.58	1254.02	70.02	1250.4	71.70
GR	1250.4	108.28	1253.57	110.98	1253.67	119.72	1254.01	136.80	1253.89	159.39
GR	1253.1	206.04	1253.11	231.59	1253.30	249.02	1253.61	304.21	1254.05	350.76
GR	1254.2	392.24	1254.95	431.19	1254.25	451.42	1253.21	460.32	1255.98	522.09
GR	1256.6	581.88	1256.71	597.16	1258.47	700.0				
X1	94000	23	144.93	330.44	574	574	574			
X3	10			50.61	1255.12					
GR	1250.1	0	1250.6	29.61	1254.16	40.35	1254.63	41.55	1255.12	50.61
GR	1254.9	64.02	1250.5	74.45	1250.5	127.62	1253.43	144.93	1253.09	165.70
GR	1251.1	176.02	1251.07	176.42	1250.07	182.86	1251.53	190.01	1252.1	194.90
GR	1252.1	201.00	1252.2	220.79	1253.9	330.44	1254.0	338.29	1254.8	412.66
GR	1256.5	549.34	1256.5	556.33	1256.8	600				
X1	94500	18	148.08	400.16	500	500	500			
X3	10			41.2	1255.02					
GR	1252.5	0	1254.75	39.35	1255.02	41.20	1254.62	63.07	1250.8	73.67
GR	1250.8	124.40	1253.14	130.65	1254.2	148.08	1253.0	169.54	1251.7	178.31
GR	1251.7	182.56	1252.7	193.74	1252.5	194.78	1254.1	303.45	1255.1	400.16
GR	1256.3	503.07	1257.4	607.32	1258.9	700.00				

X1	95000	18	146.49	401.96	500	500	500			
X3	10			43.9	1256.7					
GR	1251.5	0	1251.9	33.43	1256.7	43.90	1256.5	63.35	1251.1	72.85
GR	1251.0	126.08	1255.2	135.58	1255.4	146.49	1255.0	149.04	1254.0	155.48
GR	1253.9	183.88	1254.0	190.48	1254.3	237.30	1254.3	304.10	1255.3	401.96
GR	1257.6	501.44	1257.4	600.27	1259.1	700.00				
X1	95500	22	139.99	455.42	500	500	500			
X3	10			61.65	1256.3					
GR	1251.0	0	1251.33	33.12	1256.30	61.65	1251.3	72.12	1251.3	123.61
GR	1254.3	131.74	1254.43	139.99	1254.01	143.12	1252.2	157.30	1253.8	164.42
GR	1252.9	168.05	1252.9	178.14	1254.3	237.30	1253.8	245.15	1254.45	329.41
GR	1254.5	346.02	1254.3	434.65	1254.6	445.33	1256.3	454.37	1256.5	455.42
GR	1255.9	504.42	1257.8	700.00						
X1	96000	26	130.88	323.74	500	500	500			
X3	10			59.84	1256.18					
GR	1250.7	0	1251.02	30.65	1255.68	42.88	1256.18	59.84	1251.5	70.81
GR	1251.5	123.28	1254.20	130.88	1253.65	152.87	1253.6	160.19	1253.5	189.67
GR	1253.9	320.01	1254.3	322.37	1254.6	323.50	1254.6	323.74	1254.4	325.35
GR	1254.7	357.45	1255.1	357.71	1255.1	367.59	1255.0	385.30	1254.8	402.57
GR	1255.4	425.41	1254.9	458.94	1255.2	474.94	1256.3	499.35	1257.8	613.71
GR	1258.2	700.00								
X1	96500	32	133.32	318.41	500	500	500			
X3	10			42.13	1257.6					
GR	1251.4	0	1251.97	28.65	1257.6	42.13	1256.9	62.38	1251.6	73.38
GR	1251.6	127.30	1253.8	133.32	1253.3	163.78	1252.7	188.81	1253.1	203.5
GR	1252.7	231.51	1252.6	256.49	1252.9	269.06	1253.2	276.42	1253.4	279.82
GR	1253.2	282.04	1253.6	312.53	1254.6	318.41	1254.9	320.44	1254.8	321.31
GR	1254.7	324.02	1254.6	326.84	1254.6	329.03	1254.7	370.16	1255.1	384.90
GR	1255.2	410.81	1256.8	550.77	1257.0	558.70	1257.4	597.30	1257.7	654.20
GR	1257.5	660.38	1258.3	700.00						
X1	97000	34	144.47	315.26	500	500	500			
X3	10			47.97	1257.8					
GR	1251.2	0	1251.8	29.79	1257.8	47.97	1257.1	62.06	1251.8	72.33
GR	1251.8	127.27	1253.42	132.62	1254.01	144.47	1252.8	194.9	1253.0	212.73
GR	1253.3	248.36	1253.7	262.48	1253.9	279.30	1254.2	281.09	1253.8	282.07
GR	1254.0	311.60	1254.4	312.80	1254.9	315.26	1255.0	315.37	1254.5	318.62
GR	1254.7	344.52	1254.7	354.10	1254.5	359.93	1255.8	443.00	1257.0	471.31
GR	1257.0	489.17	1256.5	511.97	1257.5	572.84	1257.1	583.48	1257.0	596.99
GR	1257.5	604.80	1258.1	607.15	1257.7	628.54	1258.1	700.00		

X1	97500	22	136.38	299.19	500	500	500			
X3	10			45.94	1258					
GR	1252.3	0	1252.55	29.9	1258.0	45.94	1255.1	67.10	1252.2	74.76
GR	1252.2	128.40	1254.9	136.38	1253.78	158.39	1253.57	167.9	1253.5	197.2
GR	1254.9	282.51	1255.1	299.19	1254.9	313.82	1255.2	314.86	1254.8	327.16
GR	1256.1	512.32	1255.9	540.28	1257.2	548.05	1256.8	549.35	1257.7	626.55
GR	1257.3	632.82	1258.2	700.00						
X1	98000	17	135.6	404.34	500	500	500			
X3	10			46.48	1257.9					
GR	1251.9	0	1252.3	34.07	1257.9	46.48	1256.3	66.48	1252.6	76.34
GR	1252.6	127.92	1254.56	135.6	1254.0	145.94	1253.4	155.77	1253.7	171.62
GR	1253.7	190.29	1253.1	207.93	1253.4	235.51	1253.4	302.01	1255.0	404.34
GR	1257.1	538.99	1258.9	700.00						
X1	98500	19	135.4	400.14	350	330	340			
X3	10			45.9	1257.3					
GR	1252.2	0	1252.1	32.31	1257.3	45.9	1256.8	64.9	1249.49	75.19
GR	1249.5	127.0	1254.76	135.4	1253.2	153.6	1253.81	170.54	1253.5	177.30
GR	1253.2	193.30	1253.6	226.25	1253.5	270.46	1253.1	274.77	1253.1	297.38
GR	1255.2	400.14	1255.4	506.69	1257.0	607.11	1258.4	700.00		
X1	98815	17	150.02	294.58	265	245	255			
X3	10			43.58	1257.4					
GR	1252.4	0	1252.9	32.46	1257.4	43.58	1256.4	64.03	1253.0	74.10
GR	1253.0	126.1	1254.59	150.02	1254.2	156.98	1254.3	162.91	1254.0	175.88
GR	1254.5	181.27	1254.8	202.13	1254.8	294.58	1255.7	401.67	1256.7	500.48
GR	1257.1	598.69	1258.8	700.00						
X1	99000	14	141.7	277.53	185	175	180			
X3	10			42.06	1257.38					
GR	1253.5	0	1253.1	30.91	1257.38	42.06	1256.76	62.98	1253.1	73.75
GR	1253.1	122.3	1254.3	141.7	1254.2	159.3	1254.39	187.4	1254.8	277.53
GR	1256.5	400.45	1257.0	499.15	1258.0	606.40	1260.2	700.00		
X1	99080	14	130.35	397.28	81	75	78			
X3	10			43.81	1258.14					
GR	1254.2	0	1253.9	32.77	1258.14	43.81	1256.49	64.26	1254.1	70.33
GR	1253.1	74.65	1253.1	123.56	1254.71	130.35	1254.51	152.24	1254.9	181.44
GR	1256.7	397.28	1257.2	501.75	1258.0	600.33	1259.1	700.00		
X1	99167	16	135.7	247.3	87	87	87			
X3	10			44.25	1257.57					
GR	1254.8	0	1253.95	34.59	1257.57	44.25	1257.1	64.9	1253.2	75.14
GR	1253.2	124.9	1255.6	135.7	1255.2	160.5	1256.0	194.5	1256.6	247.30
GR	1256.2	283.01	1256.1	330.28	1255.8	342.91	1256.9	492.26	1258.0	603.07
GR	1259.1	700.00								

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          11200.  .        .  I CLER.   M   .        .        .        .        .        .        .
          11250.  .        .  I CLER.  M    .        .        .        .        .        .        .
          11300.  .        . I  CLER.  M    .        .        .        .        .        .        .
          11350.  .        . I  CLE R  M    .        .        .        .        .        .        .
          11400.  .        .I   CLE R  M    .        .        .        .        .        .        .
          11450.  .        .I  CL E R M     .        .        .        .        .        .        .
95500.00  11500.  .        .I  CL E R M     .        .        .        .        .        .        .
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          11950.  C        .  I LRE .  M    .        .        .        .        .        .        .
96000.00  12000.  C        .  I LRE .  M    .        .        .        .        .        .        .
          12050.  C        .  I LRE .  M    .        .        .        .        .        .        .
          12100.  C        .  I LRE .  M    .        .        .        .        .        .        .
          12150.  C        .  I LRE .  M    .        .        .        .        .        .        .
          12200.  C        .  IL RE .  M    .        .        .        .        .        .        .
          12250.  C        .  IL RE .  M    .        .        .        .        .        .        .
          12300.  C        . I L RE .  M    .        .        .        .        .        .        .
          12350.  C        . I L RE .  M    .        .        .        .        .        .        .
          12400.  C        . I L RE .  M    .        .        .        .        .        .        .
          12450.  C        . I L RE .  M    .        .        .        .        .        .        .
96500.00  12500.  C        . I L RE .  M    .        .        .        .        .        .        .
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          12700.  C        .I   L RE .  M   .        .        .        .        .        .        .
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98000.00  14000.  C        .I     LE .   M  .        .        .        .        .        .        .
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          14200.  C        .  I   LE .   M  .        .        .        .        .        .        .
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          14300.  C        .  I   LE .  M   .        .        .        .        .        .        .
98500.00  14350.  C        .   I  LE .  M   .        .        .        .        .        .        .
          14400.  C        .  I   LE .  M   .        .        .        .        .        .        .
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          14500.  C        .  I   LE .   M  .        .        .        .        .        .        .
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98815.00  14600.  C        . I    LE .   M  .        .        .        .        .        .        .
          14650.  C        .  I  LRE .    M .        .        .        .        .        .        .
          14700.  C        .  I  LRE .     M .       .        .        .        .        .        .
          14750.  C        .  I  LRE .     M .       .        .        .        .        .        .
99000.00  14800.  C        .   I LRE .      M .      .        .        .        .        .        .
          14850.  C        .   I  LER.    M  .       .        .        .        .        .        .
99080.00  14900.  C        .   I  LE .R   M  .       .        .        .        .        .        .
99167.00  14950.  .        .       IE.R   M  .       .        .        .        .        .        .
          15000.  C        .       IE.R   M  .       .        .        .        .        .        .
99266.00  15050.  C        .       IE.R   M  .       .        .        .        .        .        .
99267.00  15100.  .        .     MICE.R      .       .        .        .        .        .        .
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 99327.00 15150.  C          .     I LE.R        .         .         .         .         .         .         .         .
 99328.00 15200.  .          .        I E  LM    .         .         .         .         .         .         .         .
 99408.00 15250.  C          .        I RE LM    .         .         .         .         .         .         .         .
 99500.00 15300.  .          .        .IRWE  M  L          .         .         .         .         .         .         .
          15350.  C          .        . IRE   M . L        .         .         .         .         .         .         .
          15400.  C          .        .  IWE  M .   L      .         .         .         .         .         .         .
          15450.  C          .        .  IRWE  M.     L    .         .         .         .         .         .         .
 99717.00 15500.  C          .        .   I E   M        L.         .         .         .         .         .         .
          15550.  C          .        .   IRWE  M         .L        .         .         .         .         .         .
          15600.  C          .        .  I  WE  M         . L       .         .         .         .         .         .
          15650.  C          .        .  I   E  M         .   L     .         .         .         .         .         .
          15700.  C          .        .  I   WE .M        .     L   .         .         .         .         .         .
          15750.  C          .        . I    WER.M        .      L  .         .         .         .         .         .
          15800.  C          .        . I    WE RM        .        L.         .         .         .         .         .
          15850.  C          .        .I      WE.R        .         .L        .         .         .         .         .
          15900.  C          .        .I      WE.MR       .         . L       .         .         .         .         .
          15950.  C          .        .I      WE.M R      .         .   L     .         .         .         .         .
100251.00 16000.  .          .        .I     CWE.M R      .         .    L    .         .         .         .         .
          16050.  C          .        .I      W ERM       .       L .         .         .         .         .         .
          16100.  C          .        .I      RWE  M      .L        .         .         .         .         .         .
          16150.  C          .        .I    R  WE   ML    .         .         .         .         .         .         .
          16200.  C          .        .I  R   LWE   M     .         .         .         .         .         .         .
100500.00 16250.  C          .        .I       WE    M    .         .         .         .         .         .         .
          16300.  C          .        . I       WE    M   .         .         .         .         .         .         .
          16350.  C          .        .  I      .WE   M   .         .         .         .         .         .         .
          16400.  C          .        .   I     . E   M   .         .         .         .         .         .         .
          16450.  C          .        .    I    .   E   M .         .         .         .         .         .         .
          16500.  C          .        .     I   .    E  M .         .         .         .         .         .         .
          16550.  C          .        .      I  .     WE M.         .         .         .         .         .         .
          16600.  C          .        .       I .      WE M         .         .         .         .         .         .
          16650.  C          .        .        I.       WEM         .         .         .         .         .         .
100951.00 16700.  C          .        .         I        WEM        .         .         .         .         .         .
101000.00 16750.  C          .        .         . I      WE    R    .  M L    .         .         .         .         .
101048.00 16800.  C          .        .         . I      W.E   R    .  ML     .         .         .         .         .
          16850.  C          .        .         . I       WE   R    .   L     .         .         .         .         .
          16900.  C          .        .         . I       WE   R    .   L     .         .         .         .         .
          16950.  C          .        .         . I       WE   R    .   L     .         .         .         .         .
          17000.  C          .        .         .  I      W E  R    .   ML    .         .         .         .         .
          17050.  C          .        .         .  I      .WE  R    .   ML    .         .         .         .         .
          17100.  C          .        .         .  I      .WE  R    .   ML    .         .         .         .         .
          17150.  C          .        .         .  I      .WE  R    .    L    .         .         .         .         .
          17200.  C          .        .         .   I     .WE  R    .    L    .         .         .         .         .
101500.00 17250.  C          .        .         .   I     . WE R    .    ML   .         .         .         .         .
          17300.  C          .        .         .   I     . WE R    .    L    .         .         .         .         .
          17350.  C          .        .         .   I     . WE R    .    L    .         .         .         .         .
          17400.  C          .        .         .   I     . WE R    .    L    .         .         .         .         .
          17450.  C          .        .         .   I     . WE  R   .   LM    .         .         .         .         .
          17500.  C          .        .         .   I     .  E  R   .   LM    .         .         .         .         .
          17550.  C          .        .         .   I     .  E  R   .   LM    .         .         .         .         .
          17600.  C          .        .         .    I    .  WE R   .   LM    .         .         .         .         .
          17650.  C          .        .         .    I    .  WE R   .  L M    .         .         .         .         .
          17700.  C          .        .         .    I    .  WE  R  .  L M    .         .         .         .         .
102000.00 17750.  C          .        .         .    I    .  WE  R  .  L M    .         .         .         .         .
          17800.  C          .        .         .    I    .   E  R  .  L M    .         .         .         .         .
          17850.  C          .        .         .    I    .   E  R  .  L M    .         .         .         .         .
          17900.  C          .        .         .    I    .   WE R  . L  M    .         .         .         .         .
          17950.  C          .        .         .     I   .   WE R  . L  M    .         .         .         .         .
          18000.  C          .        .         .     I   .   WE R  . L  M    .         .         .         .         .
          18050.  C          .        .         .     I   .   WE R  . L  M    .         .         .         .         .
          18100.  C          .        .         .     I   .   WE R  . L  M    .         .         .         .         .
          18150.  C          .        .         .     I   .    E R  . L  M    .         .         .         .         .
          18200.  C          .        .         .     I   .   WER  . L  M    .         .         .         .         .
102500.00 18250.  C          .        .         .      I  .   WER  .L   M    .         .         .         .         .
          18300.  C          .        .         .      I  .   WE   . L  M    .         .         .         .         .
          18350.  C          .        .         .      I  .   WE   . L  M    .         .         .         .         .
          18400.  C          .        .         .      I  .    E   . L  M    .         .         .         .         .
          18450.  C          .        .         .      I  .    E   . L  M    .         .         .         .         .
          18500.  C          .        .         .      I  .    WE  .  L M    .         .         .         .         .
          18550.  C          .        .         .      I  .    WE  .  LM     .         .         .         .         .
          18600.  C          .        .         .      I  .   RWE  .  LM     .         .         .         .         .
          18650.  C          .        .         .      I  .   R E  .   L     .         .         .         .         .
          18700.  C          .        .         .      I  .   R E  .   L     .         .         .         .         .
103000.00 18750.  C          .        .         .      I  .   R E  .   L     .         .         .         .         .
          18800.  C          .        .         .      I  .   R WE .   L     .         .         .         .         .
          18850.  C          .        .         .       I .   R WE .   L     .         .         .         .         .
          18900.  C          .        .         .       I .   R WE .  ML     .         .         .         .         .
          18950.  C          .        .         .       I .   R WE .  ML     .         .         .         .         .
          19000.  C          .        .         .       I .    R E .  ML     .         .         .         .         .
          19050.  C          .        .         .        I.    R E .  ML     .         .         .         .         .
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          19100.  C        .        .        .        I.      R E .  ML     .        .        .        .        .
          19150.  C        .        .        .        I.      R E .  M L    .        .        .        .        .
103500.00 19200.  C        .        .        .        I.      R WE. M  L    .        .        .        .        .
          19250.  C        .        .        .        I.      R WE.  M L    .        .        .        .        .
          19300.  C        .        .        .        I.      R WE.  ML     .        .        .        .        .
          19350.  C        .        .        .        I.      R WE.  ML     .        .        .        .        .
          19400.  C        .        .        .        I.      R  E.  ML     .        .        .        .        .
          19450.  C        .        .        .        I.      R  E.  ML     .        .        .        .        .
          19500.  C        .        .        .        I.      R  E.  ML     .        .        .        .        .
          19550.  C        .        .        .        I.      R  E.  ML     .        .        .        .        .
          19600.  C        .        .        .        I.      R  WE  ML     .        .        .        .        .
          19650.  C        .        .        .        I.      R  WE  ML     .        .        .        .        .
104000.00 19700.  C        .        .        .        I.      R  WE  ML     .        .        .        .        .
          19750.  C        .        .        .        I.      R  WE   L     .        .        .        .        .
          19800.  C        .        .        .        I.      R  WE   L     .        .        .        .        .
          19850.  C        .        .        .         I       R  E   L     .        .        .        .        .
          19900.  C        .        .        .         I       R  E   ML     .        .        .        .        .
          19950.  C        .        .        .         I       R  E   ML     .        .        .        .        .
          20000.  C        .        .        .         I       R  E   ML     .        .        .        .        .
          20050.  C        .        .        .         I       R  E   ML     .        .        .        .        .
          20100.  C        .        .        .         I       R  E    L     .        .        .        .        .
          20150.  C        .        .        .         I       R  E    L     .        .        .        .        .
104500.00 20200.  C        .        .        .         I        R E    ML    .        .        .        .        .
          20250.  C        .        .        .         I        R WE   M L   .        .        .        .        .
          20300.  C        .        .        .         I       R  WE  M L    .        .        .        .        .
          20350.  C        .        .        .         I       R  WE M  L    .        .        .        .        .
          20400.  C        .        .        .         I       R  WE M  L    .        .        .        .        .
          20450.  C        .        .        .         I       R  WE M  L    .        .        .        .        .
104818.00 20500.  C        .        .        .         I       R  .EM   L    .        .        .        .        .
          20550.  C        .        .        .         I       R  .EM   L    .        .        .        .        .
          20600.  C        .        .        .         I       R  .EM    L   .        .        .        .        .
          20650.  C        .        .        .         I       R  .EM    L   .        .        .        .        .
105000.00 20700.  C        .        .        .         I        R .E     L   .        .        .        .        .
          20750.  C        .        .        .         I        R .EM    L   .        .        .        .        .
          20800.  C        .        .        .        .I         R.EM   L    .        .        .        .        .
          20850.  C        .        .        .        .I          RWEM  L    .        .        .        .        .
          20900.  C        .        .        .        .I          RWEM L     .        .        .        .        .
          20950.  C        .        .        .        . I         .WE ML     .        .        .        .        .
105294.00 21000.  C        .        .        .        . I         .WE ML     .        .        .        .        .
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T1
T2
T3

J1	ICHECK	INQ	NINV	IDIR	STRT	METRIC	HVINS	Q	WSEL	FQ
		4			.06				1248.75	
J2	NPROF	IPLOT	PRFVS	XSECV	XSECH	FN	ALLDC	IBW	CHNIM	ITRACE
	3									

PROFILE FOR STREAM

PLOTTED POINTS (BY PRIORITY) E-ENERGY,W-WATER SURFACE,I-INVERT,C-CRITICAL W.S.,L-LEFT BANK,R-RIGHT BANK,M-LOWER END STA

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ELEVATION  1246.     1251.     1256.     1261.     1266.     1271.     1276.     1281.     1286.     1291.
   SECNO   CUMDIS

84000.00      0.  .  I WER L.   M     .         .         .         .         .         .         .         .
             50.  C  I W ER LM       .         .         .         .         .         .         .         .
            100.  C  I  WER L        .         .         .         .         .         .         .         .
            150.  C  IM WE RL        .         .         .         .         .         .         .         .
            200.  CM I  WE  RL       .         .         .         .         .         .         .         .
            250.  C  I  WE  RL       .         .         .         .         .         .         .         .
            300.  C  I   E  .RL      .         .         .         .         .         .         .         .
            350.  C  I   E  .RL      .         .         .         .         .         .         .         .
            400.  C  I   WE . L      .         .         .         .         .         .         .         .
            450.  C  I   WE . RL     .         .         .         .         .         .         .         .
84500.00    500.  C  I    E .  L     .         .         .         .         .         .         .         .
            550.  C  I    E . LR     .         .         .         .         .         .         .         .
            600.  C  I    E . LR     .         .         .         .         .         .         .         .
            650.  C  I    E .L R     .         .         .         .         .         .         .         .
            700.  C  I    E .L R     .         .         .         .         .         .         .         .
            750.  C  I    E L  R     .         .         .         .         .         .         .         .
            800.  CM I    E L R      .         .         .         .         .         .         .         .
            850.  C  I M  EL. R      .         .         .         .         .         .         .         .
            900.  C   I   EL. R      .         .         .         .         .         .         .         .
            950.  C   I   E .MR      .         .         .         .         .         .         .         .
85000.00   1000.  C   I   E . R M    .         .         .         .         .         .         .         .
           1050.  C   I   WE. R M    .         .         .         .         .         .         .         .
           1100.  C   I   WE. R M    .         .         .         .         .         .         .         .
           1150.  C   I   WE.R  M    .         .         .         .         .         .         .         .
           1200.  C   I   WE.R  M    .         .         .         .         .         .         .         .
           1250.  C   I   WE.R   M   .         .         .         .         .         .         .         .
           1300.  C   I   WE.R   M   .         .         .         .         .         .         .         .
           1350.  C   I   LE.R   M   .         .         .         .         .         .         .         .
           1400.  C   I   LER    M   .         .         .         .         .         .         .         .
           1450.  C   I   LER    M   .         .         .         .         .         .         .         .
85500.00   1500.  .   I C LER    M   .         .         .         .         .         .         .         .
           1550.  C   I   LER    M   .         .         .         .         .         .         .         .
           1600.  C   I   LER    M   .         .         .         .         .         .         .         .
           1650.  C   I   LE.R   M   .         .         .         .         .         .         .         .
           1700.  C   I   LE.R   M   .         .         .         .         .         .         .         .
           1750.  C   I   LE.R  M    .         .         .         .         .         .         .         .
           1800.  C   I   LE.R  M    .         .         .         .         .         .         .         .
           1850.  C   I   LE.R  M    .         .         .         .         .         .         .         .
           1900.  C   I  L E. R M    .         .         .         .         .         .         .         .
           1950.  C   I  L E. R M    .         .         .         .         .         .         .         .
           2000.  C   I  L E. R M    .         .         .         .         .         .         .         .
86024.00   2050.  C   I  L E. R M    .         .         .         .         .         .         .         .
           2100.  C   I   LE. R M    .         .         .         .         .         .         .         .
           2150.  C  I    LE.R   M   .         .         .         .         .         .         .         .
           2200.  C  I     E.R   M   .         .         .         .         .         .         .         .
           2250.  C I      ELR   M   .         .         .         .         .         .         .         .
           2300.  C I      EL    M   .         .         .         .         .         .         .         .
           2350.  CI       ERL   M   .         .         .         .         .         .         .         .
           2400.  I        ERL   M   .         .         .         .         .         .         .         .
86415.00   2450.  I    C   WEL   M   .         .         .         .         .         .         .         .
           2500.  I        WE L  M   .         .         .         .         .         .         .         .
           2550.  CI       WE L  M   .         .         .         .         .         .         .         .
           2600.  CI       WE L  M   .         .         .         .         .         .         .         .
           2650.  C I      WE L  M   .         .         .         .         .         .         .         .
           2700.  C I      WE  L M   .         .         .         .         .         .         .         .
           2750.  C  I     WE  L M   .         .         .         .         .         .         .         .
           2800.  C  I     RE  L M   .         .         .         .         .         .         .         .
           2850.  C  I     RE  L M   .         .         .         .         .         .         .         .
           2900.  C   I    RE   LM   .         .         .         .         .         .         .         .
           2950.  C   I    RE   LM   .         .         .         .         .         .         .         .
87000.00   3000.  C    I   RE   LM   .         .         .         .         .         .         .         .
           3050.  C    I    E   LM   .         .         .         .         .         .         .         .
           3100.  C    I    E   LM   .         .         .         .         .         .         .         .
           3150.  C    I    E   LM   .         .         .         .         .         .         .         .
           3200.  C    I    E   LM   .         .         .         .         .         .         .         .
           3250.  C    I    ER  LM   .         .         .         .         .         .         .         .
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	11200.	C	.	I	WER.	M	.	.	.	.	.	.	.	.
	11250.	C	.	I	WER.	M	.	.	.	.	.	.	.	.
	11300.	C	.	I	LER.	M	.	.	.	.	.	.	.	.
	11350.	C	.	I	LE R	M	.	.	.	.	.	.	.	.
	11400.	C	.	I	LE R	M	.	.	.	.	.	.	.	.
	11450.	C	.	I	L E R	M	.	.	.	.	.	.	.	.
95500.00	11500.	C	.	I	L E R	M	.	.	.	.	.	.	.	.
	11550.	C	.	I	L E R	M	.	.	.	.	.	.	.	.
	11600.	C	.	I	L E R	M	.	.	.	.	.	.	.	.
	11650.	C	.	I	L ER.	M	.	.	.	.	.	.	.	.
	11700.	C	.	I	L ER.	M	.	.	.	.	.	.	.	.
	11750.	C	.	I	L ER.	M	.	.	.	.	.	.	.	.
	11800.	C	.	I	L E .	M	.	.	.	.	.	.	.	.
	11850.	C	.	I	L E .	M	.	.	.	.	.	.	.	.
	11900.	C	.	I	LRE .	M	.	.	.	.	.	.	.	.
	11950.	C	.	I	LRE .	M	.	.	.	.	.	.	.	.
96000.00	12000.	C	.	I	LRE .	M	.	.	.	.	.	.	.	.
	12050.	C	.	I	LRE .	M	.	.	.	.	.	.	.	.
	12100.	C	.	I	LRE .	M	.	.	.	.	.	.	.	.
	12150.	C	.	I	LRE .	M	.	.	.	.	.	.	.	.
	12200.	C	.	IL	RE .	M	.	.	.	.	.	.	.	.
	12250.	C	.	IL	RE .	M	.	.	.	.	.	.	.	.
	12300.	C	.	I	L RE .	M	.	.	.	.	.	.	.	.
	12350.	C	.	I	L RE .	M	.	.	.	.	.	.	.	.
	12400.	C	.	I	L RE .	M	.	.	.	.	.	.	.	.
	12450.	C	.	I	L RE .	M	.	.	.	.	.	.	.	.
96500.00	12500.	.	.	I	C RE .	M	.	.	.	.	.	.	.	.
	12550.	C	.	I	L RE .	M	.	.	.	.	.	.	.	.
	12600.	C	.	I	L RE .	M	.	.	.	.	.	.	.	.
	12650.	C	.	I	L RE .	M	.	.	.	.	.	.	.	.
	12700.	C	.	I	L RE .	M	.	.	.	.	.	.	.	.
	12750.	C	.	I	L RE .	M	.	.	.	.	.	.	.	.
	12800.	C	.	I	L RE .	M	.	.	.	.	.	.	.	.
	12850.	C	.	I	L RE .	M	.	.	.	.	.	.	.	.
	12900.	C	.	I	L RE .	M	.	.	.	.	.	.	.	.
	12950.	C	.	I	L RE .	M	.	.	.	.	.	.	.	.
97000.00	13000.	C	.	I	L RE .	M	.	.	.	.	.	.	.	.
	13050.	C	.	I	LRE .	M	.	.	.	.	.	.	.	.
	13100.	C	.	I	LRE .	M	.	.	.	.	.	.	.	.
	13150.	C	.	I	LRE .	M	.	.	.	.	.	.	.	.
	13200.	C	.	I	LRE .	M	.	.	.	.	.	.	.	.
	13250.	C	.	I	LRE .	M	.	.	.	.	.	.	.	.
	13300.	C	.	I	LE .	M	.	.	.	.	.	.	.	.
	13350.	C	.	I	LE .	M	.	.	.	.	.	.	.	.
	13400.	C	.	I	LE .	M	.	.	.	.	.	.	.	.
	13450.	C	.	I	LE .	M	.	.	.	.	.	.	.	.
97500.00	13500.	C	.	I	LE .	M	.	.	.	.	.	.	.	.
	13550.	C	.	I	LE .	M	.	.	.	.	.	.	.	.
	13600.	C	.	I	LE .	M	.	.	.	.	.	.	.	.
	13650.	C	.	I	LE .	M	.	.	.	.	.	.	.	.
	13700.	C	.	I	LE .	M	.	.	.	.	.	.	.	.
	13750.	C	.	I	LE .	M	.	.	.	.	.	.	.	.
	13800.	C	.	I	LE .	M	.	.	.	.	.	.	.	.
	13850.	C	.	I	LE .	M	.	.	.	.	.	.	.	.
	13900.	C	.	I	LE .	M	.	.	.	.	.	.	.	.
	13950.	C	.	I	LE .	M	.	.	.	.	.	.	.	.
98000.00	14000.	C	.	I	LE .	M	.	.	.	.	.	.	.	.
	14050.	C	.	I	LE .	M	.	.	.	.	.	.	.	.
	14100.	C	.	I	LE .	M	.	.	.	.	.	.	.	.
	14150.	C	.	I	LE .	M	.	.	.	.	.	.	.	.
	14200.	C	.	I	LWE.	M	.	.	.	.	.	.	.	.
	14250.	C	.	I	LWE.	M	.	.	.	.	.	.	.	.
	14300.	C	.	I	LWE.	M	.	.	.	.	.	.	.	.
98500.00	14350.	C	.	I	LWE.	M	.	.	.	.	.	.	.	.
	14400.	C	.	I	LWE.	M	.	.	.	.	.	.	.	.
	14450.	C	.	I	LWE.	M	.	.	.	.	.	.	.	.
	14500.	C	.	I	LWE.	M	.	.	.	.	.	.	.	.
	14550.	C	.	I	LWE.	M	.	.	.	.	.	.	.	.
98815.00	14600.	C	.	I	LWE.	M	.	.	.	.	.	.	.	.
	14650.	C	.	I	LRWE.	M	.	.	.	.	.	.	.	.
	14700.	C	.	I	LRWE.	M	.	.	.	.	.	.	.	.
	14750.	C	.	I	LRWE.	M	.	.	.	.	.	.	.	.
99000.00	14800.	C	.	I	LRWE.	M	.	.	.	.	.	.	.	.
	14850.	C	.	I	LWE.	M	.	.	.	.	.	.	.	.
99080.00	14900.	C	.	I	LWE.R	M	.	.	.	.	.	.	.	.
99167.00	14950.	.	.		IE.R	M	.	.	.	.	.	.	.	.
	15000.	C	.		IE.R	M	.	.	.	.	.	.	.	.
99266.00	15050.	C	.		IE.R	M	.	.	.	.	.	.	.	.
99267.00	15100.	.	.		MIWE.R		.	.	.	.	.	.	.	.

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 99327.00 15150.  C          .     MILE.R        .         .         .         .         .         .         .         .
 99328.00 15200.  .          .         I RE LM   .         .         .         .         .         .         .         .
 99408.00 15250.  C          .         I RWELM   .         .         .         .         .         .         .         .
 99500.00 15300.  .          .         .IR WE M  L         .         .         .         .         .         .         .
          15350.  C          .         . IRWE  M . L       .         .         .         .         .         .         .
          15400.  C          .         .  I WE M .   L     .         .         .         .         .         .         .
          15450.  C          .         .  IR WE M.     L   .         .         .         .         .         .         .
 99717.00 15500.  C          .         .   I  E  M        L.         .         .         .         .         .         .
          15550.  C          .         .   IR WE M         .L        .         .         .         .         .         .
          15600.  C          .         .  I  RW EM         . L       .         .         .         .         .         .
          15650.  C          .         .  I   RWEM         .   L     .         .         .         .         .         .
          15700.  C          .         .  I    W EM        .     L   .         .         .         .         .         .
          15750.  C          .         . I     WREM        .      L  .         .         .         .         .         .
          15800.  C          .         . I      WRE        .        L.         .         .         .         .         .
          15850.  C          .         .I       W.E        .         .L        .         .         .         .         .
          15900.  C          .         .I       W.ME       .         . L       .         .         .         .         .
          15950.  C          .         .I        WMER      .         .   L     .         .         .         .         .
100251.00 16000.  .          .         .I        WM E      .         .    L    .         .         .         .         .
          16050.  C          .         .I        WRME      .       L .         .         .         .         .         .
          16100.  C          .         .I      R .W E     .L         .         .         .         .         .         .
          16150.  C          .         .I    R   .W EML    .         .         .         .         .         .         .
          16200.  C          .         .I  R   L .W  E     .         .         .         .         .         .         .
100500.00 16250.  C          .         .I        . W EM    .         .         .         .         .         .         .
          16300.  C          .         . I       .  W EM   .         .         .         .         .         .         .
          16350.  C          .         .  I      .   W E   .         .         .         .         .         .         .
          16400.  C          .         .   I     .    WE   .         .         .         .         .         .         .
          16450.  C          .         .    I    .     WME.         .         .         .         .         .         .
          16500.  C          .         .     I   .      W E         .         .         .         .         .         .
          16550.  C          .         .      I  .       W.E        .         .         .         .         .         .
          16600.  C          .         .       I .        MWE       .         .         .         .         .         .
          16650.  C          .         .        I.        M WE      .         .         .         .         .         .
100951.00 16700.  C          .         .         I        .M WE     .         .         .         .         .         .
101000.00 16750.  C          .         .         . I       .  W E    .  M L    .         .         .         .         .
101048.00 16800.  C          .         .         . I       .  W E    .  ML     .         .         .         .         .
          16850.  C          .         .         . I       .  W E    .   L     .         .         .         .         .
          16900.  C          .         .         . I       .   WE    .   L     .         .         .         .         .
          16950.  C          .         .         . I       .   WE    .   L     .         .         .         .         .
          17000.  C          .         .         .  I      .   WE    .   ML    .         .         .         .         .
          17050.  C          .         .         .  I      .   WRE   .   ML    .         .         .         .         .
          17100.  C          .         .         .  I      .   WRE   .   ML    .         .         .         .         .
          17150.  C          .         .         .  I      .    WE   .    L    .         .         .         .         .
          17200.  C          .         .         .   I     .    WE   .    L    .         .         .         .         .
101500.00 17250.  C          .         .         .   I     .    WE   .    ML   .         .         .         .         .
          17300.  C          .         .         .   I     .    WE   .    L    .         .         .         .         .
          17350.  C          .         .         .   I     .    W E  .    L    .         .         .         .         .
          17400.  C          .         .         .   I     .    RWE  .    L    .         .         .         .         .
          17450.  C          .         .         .   I     .     WE  .   LM    .         .         .         .         .
          17500.  C          .         .         .   I     .     WE  .   LM    .         .         .         .         .
          17550.  C          .         .         .   I     .     WE  .   LM    .         .         .         .         .
          17600.  C          .         .         .    I    .     WE  .   LM    .         .         .         .         .
          17650.  C          .         .         .    I    .     RE  .  L M    .         .         .         .         .
          17700.  C          .         .         .    I    .      E  .  L M    .         .         .         .         .
102000.00 17750.  C          .         .         .    I    .      WE .  L M    .         .         .         .         .
          17800.  C          .         .         .    I    .      WE .  L M    .         .         .         .         .
          17850.  C          .         .         .    I    .      WE .  L M    .         .         .         .         .
          17900.  C          .         .         .    I    .      WE . L  M    .         .         .         .         .
          17950.  C          .         .         .     I   .      WE . L  M    .         .         .         .         .
          18000.  C          .         .         .     I   .      WE . L  M    .         .         .         .         .
          18050.  C          .         .         .     I   .      RWE. L  M    .         .         .         .         .
          18100.  C          .         .         .     I   .      RWE. L  M    .         .         .         .         .
          18150.  C          .         .         .     I   .      RWE. L  M    .         .         .         .         .
          18200.  C          .         .         .     I   .      RWE. L  M    .         .         .         .         .
102500.00 18250.  .          .         .         .      I  .     CRWE.L   M    .         .         .         .         .
          18300.  C          .         .         .      I  .     R WE. L  M    .         .         .         .         .
          18350.  C          .         .         .      I  .     R  WE L  M    .         .         .         .         .
          18400.  C          .         .         .      I  .     R  WE L  M    .         .         .         .         .
          18450.  C          .         .         .      I  .     R  WE L  M    .         .         .         .         .
          18500.  C          .         .         .      I  .     R  WE  L M    .         .         .         .         .
          18550.  C          .         .         .      I  .     R  WE  LM     .         .         .         .         .
          18600.  C          .         .         .      I  .    R    E  LM     .         .         .         .         .
          18650.  C          .         .         .      I  .    R    E   L     .         .         .         .         .
          18700.  C          .         .         .      I  .    R    WE  L     .         .         .         .         .
103000.00 18750.  C          .         .         .      I  .    R    WE  L     .         .         .         .         .
          18800.  C          .         .         .      I  .    R    WE  L     .         .         .         .         .
          18850.  C          .         .         .       I .    R    WE  L     .         .         .         .         .
          18900.  C          .         .         .       I .    R    WE ML     .         .         .         .         .
          18950.  C          .         .         .       I .    R    .E ML     .         .         .         .         .
          19000.  C          .         .         .       I .     R   .E ML     .         .         .         .         .
          19050.  C          .         .         .        I.     R   .E ML     .         .         .         .         .
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          7250.  C     I  R  E   L  .  M     .     .     .     .     .     .     .     .
          7300.  C     I  R  E  L   .  M     .     .     .     .     .     .     .     .
          7350.  C     I  R  E  L   .  M     .     .     .     .     .     .     .     .
          7400.  C     I  R  E  L   .  M     .     .     .     .     .     .     .     .
          7450.  C     I  R  E  L   .  M     .     .     .     .     .     .     .     .
91500.00  7500.  C     I  R  E  L   .  M     .     .     .     .     .     .     .     .
          7550.  C     I  R  E  L   .  M     .     .     .     .     .     .     .     .
          7600.  C     I  R  E  L   .  M     .     .     .     .     .     .     .     .
          7650.  C     I  .R E  L   .  M     .     .     .     .     .     .     .     .
          7700.  C     I  .R E  L   .   M    .     .     .     .     .     .     .     .
          7750.  C     I  .R E  L   .   M    .     .     .     .     .     .     .     .
          7800.  C     I  .R E L    .   M    .     .     .     .     .     .     .     .
          7850.  C     I  . RE L    .   M    .     .     .     .     .     .     .     .
          7900.  C     I  . RE L    .   M    .     .     .     .     .     .     .     .
          7950.  C     I  . RE L    .   M    .     .     .     .     .     .     .     .
92000.00  8000.  C     I  . RE L    .   M    .     .     .     .     .     .     .     .
          8050.  C     I  . RE L    .   M    .     .     .     .     .     .     .     .
          8100.  C     I  . RE  L   .   M    .     .     .     .     .     .     .     .
          8150.  C     I  . RE  L   .   M    .     .     .     .     .     .     .     .
          8200.  C     I  . RE  L   .   M    .     .     .     .     .     .     .     .
          8250.  C     I  . RE  L   .    M   .     .     .     .     .     .     .     .
          8300.  C     I  . RE  L   .    M   .     .     .     .     .     .     .     .
          8350.  C     I  . RE  L   .    M   .     .     .     .     .     .     .     .
          8400.  C     I  . RE  L   .    M   .     .     .     .     .     .     .     .
          8450.  C     I  . RE  L   .    M   .     .     .     .     .     .     .     .
92500.00  8500.  C     I  . RE   L  .    M   .     .     .     .     .     .     .     .
          8550.  C     I  . RE   L  .    M   .     .     .     .     .     .     .     .
          8600.  C     I  . RE   L  .    M   .     .     .     .     .     .     .     .
          8650.  C      I . RE   L  .    M   .     .     .     .     .     .     .     .
          8700.  C      I .  WE  L  .    M   .     .     .     .     .     .     .     .
          8750.  C      I .  WE  L  .    M   .     .     .     .     .     .     .     .
          8800.  C      I .  WE   L .    M   .     .     .     .     .     .     .     .
          8850.  C      I .  WE   L .     M  .     .     .     .     .     .     .     .
          8900.  C      I .  WE   L .     M  .     .     .     .     .     .     .     .
          8950.  C      I .  WE   L .     M  .     .     .     .     .     .     .     .
93000.00  9000.  C      I .  WE   L .     M  .     .     .     .     .     .     .     .
          9050.  C       I.   E   L .     M  .     .     .     .     .     .     .     .
          9100.  C       I.   E   L .    M   .     .     .     .     .     .     .     .
          9150.  C        I   E  L  .    M   .     .     .     .     .     .     .     .
          9200.  C        .I  WE L  .    M   .     .     .     .     .     .     .     .
          9250.  C        .I  RE L  .    M   .     .     .     .     .     .     .     .
          9300.  C        . I  EL   .    M   .     .     .     .     .     .     .     .
          9350.  C        .  I EL   .    M   .     .     .     .     .     .     .     .
          9400.  C        .  I WE   .   M    .     .     .     .     .     .     .     .
93574.00  9450.  .        .   IWE   .   M    .     .     .     .     .     .     .     .
          9500.  .        .  I WE   .   M    .     .     .     .     .     .     .     .
          9550.  .        .  I WE   .   M    .     .     .     .     .     .     .     .
          9600.  .        . I  CE   .  M     .     .     .     .     .     .     .     .
          9650.  .        . I  CE   .  M     .     .     .     .     .     .     .     .
          9700.  .        .I   CE   .  M     .     .     .     .     .     .     .     .
          9750.  .        I   CLE   .  M     .     .     .     .     .     .     .     .
          9800.  .        I   CLE   . M      .     .     .     .     .     .     .     .
          9850.  .       I.   CLE   . M      .     .     .     .     .     .     .     .
          9900.  .       I.   CLE   . M      .     .     .     .     .     .     .     .
          9950.  .      I .   CRE   .M       .     .     .     .     .     .     .     .
94000.00 10000.  .      I .   CRE   .M       .     .     .     .     .     .     .     .
         10050.  C      I .   LRE   .M       .     .     .     .     .     .     .     .
         10100.  C      I .    LE   . M      .     .     .     .     .     .     .     .
         10150.  C      I .    LE   . M      .     .     .     .     .     .     .     .
         10200.  C      I .    LE   .  M     .     .     .     .     .     .     .     .
         10250.  C      I .    LE   .  M     .     .     .     .     .     .     .     .
         10300.  C      I .    LER  .   M    .     .     .     .     .     .     .     .
         10350.  C       I.    LER  .   M    .     .     .     .     .     .     .     .
         10400.  C       I.     ER  .   M    .     .     .     .     .     .     .     .
         10450.  C       I.     ER  .    M   .     .     .     .     .     .     .     .
94500.00 10500.  C       I.     E R .    M   .     .     .     .     .     .     .     .
         10550.  C        I     E R .    M   .     .     .     .     .     .     .     .
         10600.  C        I     E R .    M   .     .     .     .     .     .     .     .
         10650.  C        .I    ELR .    M   .     .     .     .     .     .     .     .
         10700.  C        . I   WER .    M   .     .     .     .     .     .     .     .
         10750.  C        . I   WER .    M   .     .     .     .     .     .     .     .
         10800.  C        .  I   ER .    M   .     .     .     .     .     .     .     .
         10850.  C        .  I   ER .    M   .     .     .     .     .     .     .     .
         10900.  C        .   I  EL .     M  .     .     .     .     .     .     .     .
         10950.  C        .    I WE .     M  .     .     .     .     .     .     .     .
95000.00 11000.  .        .    I WE .     M  .     .     .     .     .     .     .     .
         11050.  C        .    I WE .    M   .     .     .     .     .     .     .     .
         11100.  C        .    I WER.    M   .     .     .     .     .     .     .     .
         11150.  C        .   I  WER.    M   .     .     .     .     .     .     .     .
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          3300.  C    I    ER   L    .         .         .         .         .         .         .         .         .
          3350.  C    I    ER   L    .         .         .         .         .         .         .         .         .
          3400.  C    I    ER   LM   .         .         .         .         .         .         .         .         .
          3450.  C    I    E R  LM   .         .         .         .         .         .         .         .         .
87500.00  3500.  C    I    E R  LM   .         .         .         .         .         .         .         .         .
          3550.  C    I    WER  L    .         .         .         .         .         .         .         .         .
          3600.  C    I    WE   L    .         .         .         .         .         .         .         .         .
          3650.  C    I    WE   L    .         .         .         .         .         .         .         .         .
          3700.  C    I    WE   L    .         .         .         .         .         .         .         .         .
          3750.  C    I    WE  ML    .         .         .         .         .         .         .         .         .
          3800.  C    I    WE  ML    .         .         .         .         .         .         .         .         .
          3850.  C    I    RE  L     .         .         .         .         .         .         .         .         .
          3900.  C    I    RE ML     .         .         .         .         .         .         .         .         .
          3950.  C    I    RE ML     .         .         .         .         .         .         .         .         .
88000.00  4000.  C    I    RE ML     .         .         .         .         .         .         .         .         .
          4050.  C    I    RE ML     .         .         .         .         .         .         .         .         .
          4100.  C    I    RE ML     .         .         .         .         .         .         .         .         .
          4150.  C    I    RE ML     .         .         .         .         .         .         .         .         .
          4200.  C    I    RE  L     .         .         .         .         .         .         .         .         .
          4250.  C     I   RE  L     .         .         .         .         .         .         .         .         .
          4300.  C     I   RE  L     .         .         .         .         .         .         .         .         .
          4350.  C     I   RE  L     .         .         .         .         .         .         .         .         .
          4400.  C     I   RE LM     .         .         .         .         .         .         .         .         .
          4450.  C     I   RE L M    .         .         .         .         .         .         .         .         .
88500.00  4500.  C     I   RE L M    .         .         .         .         .         .         .         .         .
          4550.  C     I   RE L M    .         .         .         .         .         .         .         .         .
          4600.  C     I  R.E L  M   .         .         .         .         .         .         .         .         .
          4650.  C     I  R.E L  M   .         .         .         .         .         .         .         .         .
          4700.  C     I  R.E L  M   .         .         .         .         .         .         .         .         .
          4750.  C     I  R.E L   M  .         .         .         .         .         .         .         .         .
          4800.  C     I  R.E L   M  .         .         .         .         .         .         .         .         .
          4850.  C     I  R.E L   M  .         .         .         .         .         .         .         .         .
          4900.  C     I  R.EL     M .         .         .         .         .         .         .         .         .
          4950.  C     I  R.WE     M .         .         .         .         .         .         .         .         .
89000.00  5000.  C     I  R.WE     M .         .         .         .         .         .         .         .         .
          5050.  C     I  R.WE      M.         .         .         .         .         .         .         .         .
          5100.  C     I  R.WE      M.         .         .         .         .         .         .         .         .
          5150.  C     I  R.WE      M.         .         .         .         .         .         .         .         .
          5200.  C     I   RWE       M         .         .         .         .         .         .         .         .
          5250.  C     I   RWE       M         .         .         .         .         .         .         .         .
          5300.  C     I   R E       M         .         .         .         .         .         .         .         .
          5350.  C     I   .RE       M         .         .         .         .         .         .         .         .
          5400.  C     I   .RE       .M        .         .         .         .         .         .         .         .
          5450.  C     I   .RE       .M        .         .         .         .         .         .         .         .
89545.00  5500.  C     I   .RE       .M        .         .         .         .         .         .         .         .
          5550.  C     I   .RE       .M        .         .         .         .         .         .         .         .
          5600.  C     I   .RE       M         .         .         .         .         .         .         .         .
          5650.  C     I   .RE       M         .         .         .         .         .         .         .         .
          5700.  C     I   .RE       M         .         .         .         .         .         .         .         .
          5750.  C      I  .REL      M         .         .         .         .         .         .         .         .
          5800.  C      I  .REL      M         .         .         .         .         .         .         .         .
          5850.  C      I  .REL      M         .         .         .         .         .         .         .         .
          5900.  C      I  .REL      M         .         .         .         .         .         .         .         .
          5950.  C      I  .REL     M.         .         .         .         .         .         .         .         .
90000.00  6000.  C      I  .RE L    M.         .         .         .         .         .         .         .         .
          6050.  C     I   .RE L    M.         .         .         .         .         .         .         .         .
          6100.  C     I   .RE L     M         .         .         .         .         .         .         .         .
          6150.  C    I    .RE L     M         .         .         .         .         .         .         .         .
          6200.  C    I    .RE  L    M         .         .         .         .         .         .         .         .
          6250.  C   I     .RE  L    M         .         .         .         .         .         .         .         .
          6300.  C   I     .RE  L    .M        .         .         .         .         .         .         .         .
          6350.  C  I      .RE  L    .M        .         .         .         .         .         .         .         .
          6400.  C  I      .RE  L    .M        .         .         .         .         .         .         .         .
          6450.  C I       .RE   L   . M       .         .         .         .         .         .         .         .
90500.00  6500.  C I       R E   L   . M       .         .         .         .         .         .         .         .
          6550.  C I       R E   L   . M       .         .         .         .         .         .         .         .
          6600.  C  I      R E   L   . M       .         .         .         .         .         .         .         .
          6650.  C  I      R E   L   . M       .         .         .         .         .         .         .         .
          6700.  C   I     R E   L   .  M       .         .         .         .         .         .         .         .
          6750.  C   I     R WE  L   .  M       .         .         .         .         .         .         .         .
          6800.  C    I    R WE   L  .  M       .         .         .         .         .         .         .         .
          6850.  C    I    R WE   L  .  M       .         .         .         .         .         .         .         .
          6900.  C     I   R WE   L  .  M       .         .         .         .         .         .         .         .
          6950.  C     I   R WE   L  .  M       .         .         .         .         .         .         .         .
91000.00  7000.  C      I  R WE   L  .   M      .         .         .         .         .         .         .         .
          7050.  C      I  R WE   L  .   M      .         .         .         .         .         .         .         .
          7100.  C      I  R WE   L  .  M       .         .         .         .         .         .         .         .
          7150.  C      I  R WE   L  .  M       .         .         .         .         .         .         .         .
          7200.  C      I  R WE   L  .  M       .         .         .         .         .         .         .         .
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          19100.  C     .     .     .     I.    R   .WEML   .     .     .     .     .
          19150.  C     .     .     .     I.    R   .WEM L  .     .     .     .     .
103500.00 19200.  C     .     .     .     I.    R   .WE  L  .     .     .     .     .
          19250.  C     .     .     .     I.    R   .WEM L  .     .     .     .     .
          19300.  C     .     .     .     I.    R   .WEML   .     .     .     .     .
          19350.  C     .     .     .     I.    R   . EML   .     .     .     .     .
          19400.  C     .     .     .     I.    R   . EML   .     .     .     .     .
          19450.  C     .     .     .     I.    R   . WEL   .     .     .     .     .
          19500.  C     .     .     .     I.    R   . WEL   .     .     .     .     .
          19550.  C     .     .     .     I.    R   . WEL   .     .     .     .     .
          19600.  C     .     .     .     I.    R   . WEL   .     .     .     .     .
          19650.  C     .     .     .     I.    R   . WEL   .     .     .     .     .
104000.00 19700.  C     .     .     .     I.    R   . WEL   .     .     .     .     .
          19750.  C     .     .     .     I.    R   .  EL   .     .     .     .     .
          19800.  C     .     .     .     I.    R   .  EL   .     .     .     .     .
          19850.  C     .     .     .      I     R  .  EL   .     .     .     .     .
          19900.  C     .     .     .      I     R  .  EML  .     .     .     .     .
          19950.  C     .     .     .      I     R  .  EML  .     .     .     .     .
          20000.  C     .     .     .      I     R  .  WEL  .     .     .     .     .
          20050.  C     .     .     .      I     R  .  WEL  .     .     .     .     .
          20100.  C     .     .     .      I     R  .  WEL  .     .     .     .     .
          20150.  C     .     .     .      I     R  .  WEL  .     .     .     .     .
104500.00 20200.  C     .     .     .      I      R .  WEML .     .     .     .     .
          20250.  C     .     .     .      I      R .   E L .     .     .     .     .
          20300.  C     .     .     .      I     R  .   E L .     .     .     .     .
          20350.  C     .     .     .      I     R  .  ME L  .     .     .     .     .
          20400.  C     .     .     .      I     R  .  ME L  .     .     .     .     .
          20450.  C     .     .     .      I     R  .  ME L  .     .     .     .     .
104818.00 20500.  C     .     .     .      I     R  . M E L  .     .     .     .     .
          20550.  C     .     .     .      I     R  . M E L  .     .     .     .     .
          20600.  C     .     .     .      I     R  . M E  L .     .     .     .     .
          20650.  C     .     .     .      I     R  . M E  L .     .     .     .     .
105000.00 20700.  C     .     .     .      I      R .M  WE L  .     .     .     .     .
          20750.  C     .     .     .      I      R . M WE L  .     .     .     .     .
          20800.  C     .     .     .     .I       R. M WEL  .     .     .     .     .
          20850.  C     .     .     .     .I        R  MWEL  .     .     .     .     .
          20900.  C     .     .     .     .I        R  M E   .     .     .     .     .
          20950.  C     .     .     .     . I       .R  ME   .     .     .     .     .
105294.00 21000.  C     .     .     .     . I       . R ME   .     .     .     .     .
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T1
T2
T3

J1	ICHECK	INQ	NINV	IDIR	STRT	METRIC	HVINS	Q	WSEL	FQ
		5			.06				1249.89	
J2	NPROF	IPLOT	PRFVS	XSECV	XSECH	FN	ALLDC	IBW	CHNIM	ITRACE
	4									

PROFILE FOR STREAM

PLOTTED POINTS (BY PRIORITY) E-ENERGY,W-WATER SURFACE,I-INVERT,C-CRITICAL W.S.,L-LEFT BANK,R-RIGHT BANK,M-LOWER END STA

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ELEVATION  1246.     1251.     1256.     1261.     1266.     1271.     1276.     1281.     1286.     1291.
   SECNO   CUMDIS

84000.00      0.  .  I   WEL.   M    .         .         .         .         .         .         .         .
             50.  .  I   WE LM       .         .         .         .         .         .         .         .
            100.  .  I   WE L        .         .         .         .         .         .         .         .
            150.  .  IM  WERL        .         .         .         .         .         .         .         .
            200.  .M I   WE RL       .         .         .         .         .         .         .         .
            250.  M  I   W ERL       .         .         .         .         .         .         .         .
            300.  M  I   W E.RL      .         .         .         .         .         .         .         .
            350.  M  I    WE.RL      .         .         .         .         .         .         .         .
            400.  M  I    WE. L      .         .         .         .         .         .         .         .
            450.  M  I    W E RL     .         .         .         .         .         .         .         .
84500.00    500.  M  I    W E  L     .         .         .         .         .         .         .         .
            550.  M  I    W E LR     .         .         .         .         .         .         .         .
            600.  M  I    W E LR     .         .         .         .         .         .         .         .
            650.  M  I    CWEL R     .         .         .         .         .         .         .         .
            700.  M  I    CWEL R     .         .         .         .         .         .         .         .
            750.  M  I    CWE  R     .         .         .         .         .         .         .         .
            800.  .M I    CWE R      .         .         .         .         .         .         .         .
            850.  .  I M  CLWER      .         .         .         .         .         .         .         .
            900.  .   I   CLWER      .         .         .         .         .         .         .         .
            950.  .   I   C WER      .         .         .         .         .         .         .         .
85000.00   1000.  .   I   C .ER M    .         .         .         .         .         .         .         .
           1050.  .   I   C .ER M    .         .         .         .         .         .         .         .
           1100.  .   I   C .ER M    .         .         .         .         .         .         .         .
           1150.  .   I   C .E  M    .         .         .         .         .         .         .         .
           1200.  .   I   C .E  M    .         .         .         .         .         .         .         .
           1250.  .   I   C .E   M   .         .         .         .         .         .         .         .
           1300.  .   I   C .E   M   .         .         .         .         .         .         .         .
           1350.  .   I   C .E   M   .         .         .         .         .         .         .         .
           1400.  .   I   C RE   M   .         .         .         .         .         .         .         .
           1450.  .   I   C RE   M   .         .         .         .         .         .         .         .
85500.00   1500.  .   I   C RE   M   .         .         .         .         .         .         .         .
           1550.  C   I   L RE   M   .         .         .         .         .         .         .         .
           1600.  C   I   L RE   M   .         .         .         .         .         .         .         .
           1650.  C   I   L .E   M   .         .         .         .         .         .         .         .
           1700.  C   I   L .WE  M   .         .         .         .         .         .         .         .
           1750.  C   I   L .WE M    .         .         .         .         .         .         .         .
           1800.  C   I   L .WE M    .         .         .         .         .         .         .         .
           1850.  C   I   L .WE M    .         .         .         .         .         .         .         .
           1900.  C   I  L  .WE M    .         .         .         .         .         .         .         .
           1950.  C   I  L  .WE M    .         .         .         .         .         .         .         .
           2000.  C   I  L  .WE M    .         .         .         .         .         .         .         .
86024.00   2050.  C   I  L  .WE M    .         .         .         .         .         .         .         .
           2100.  C   I   L .WE M    .         .         .         .         .         .         .         .
           2150.  C  I    L .WE  M   .         .         .         .         .         .         .         .
           2200.  C  I     L.WE  M   .         .         .         .         .         .         .         .
           2250.  C I       LRE  M   .         .         .         .         .         .         .         .
           2300.  C I       L E  M   .         .         .         .         .         .         .         .
           2350.  CI        RLE  M   .         .         .         .         .         .         .         .
           2400.  I         RLE  M   .         .         .         .         .         .         .         .
86415.00   2450.  I        CR.LE  M   .         .         .         .         .         .         .         .
           2500.  I         R. E  M   .         .         .         .         .         .         .         .
           2550.  CI        R. E  M   .         .         .         .         .         .         .         .
           2600.  CI        R. E  M   .         .         .         .         .         .         .         .
           2650.  C I       R. E  M   .         .         .         .         .         .         .         .
           2700.  C I       R. EL M   .         .         .         .         .         .         .         .
           2750.  C  I      R. EL M   .         .         .         .         .         .         .         .
           2800.  C  I      R. WE M   .         .         .         .         .         .         .         .
           2850.  C  I      R. WE M   .         .         .         .         .         .         .         .
           2900.  C   I     R. WELM   .         .         .         .         .         .         .         .
           2950.  C   I     R. WELM   .         .         .         .         .         .         .         .
87000.00   3000.  C    I   R. WELM   .         .         .         .         .         .         .         .
           3050.  C    I    R WELM   .         .         .         .         .         .         .         .
           3100.  C    I    R WELM   .         .         .         .         .         .         .         .
           3150.  C    I    R WELM   .         .         .         .         .         .         .         .
           3200.  C    I    R WELM   .         .         .         .         .         .         .         .
           3250.  C    I    .RWELM   .         .         .         .         .         .         .         .
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          3300.  C    I    .R E L    .         .         .         .         .         .         .         .         .
          3350.  C    I    .R E L    .         .         .         .         .         .         .         .         .
          3400.  C    I    .R E LM   .         .         .         .         .         .         .         .         .
          3450.  C    I    . RE LM   .         .         .         .         .         .         .         .         .
87500.00  3500.  C    I    . RE LM   .         .         .         .         .         .         .         .         .
          3550.  C    I    . RE L    .         .         .         .         .         .         .         .         .
          3600.  C    I    .R WEL    .         .         .         .         .         .         .         .         .
          3650.  C    I    .R WEL    .         .         .         .         .         .         .         .         .
          3700.  C    I    .R WEL    .         .         .         .         .         .         .         .         .
          3750.  C    I    .R WEL    .         .         .         .         .         .         .         .         .
          3800.  C    I    .R WEL    .         .         .         .         .         .         .         .         .
          3850.  C    I    R  WE     .         .         .         .         .         .         .         .         .
          3900.  C    I    R  WE     .         .         .         .         .         .         .         .         .
          3950.  C    I    R  WE     .         .         .         .         .         .         .         .         .
88000.00  4000.  C    I    R  WE     .         .         .         .         .         .         .         .         .
          4050.  C    I    R  WE     .         .         .         .         .         .         .         .         .
          4100.  C    I    R  ME     .         .         .         .         .         .         .         .         .
          4150.  C    I    R  ME     .         .         .         .         .         .         .         .         .
          4200.  C    I    R   E     .         .         .         .         .         .         .         .         .
          4250.  C     I   R   E     .         .         .         .         .         .         .         .         .
          4300.  C     I   R   E     .         .         .         .         .         .         .         .         .
          4350.  C     I   R   E     .         .         .         .         .         .         .         .         .
          4400.  C     I   R  LE     .         .         .         .         .         .         .         .         .
          4450.  C     I   R  LEM    .         .         .         .         .         .         .         .         .
88500.00  4500.  C     I   R  LEM    .         .         .         .         .         .         .         .         .
          4550.  C     I   R  LEM    .         .         .         .         .         .         .         .         .
          4600.  C     I  R.  LE M   .         .         .         .         .         .         .         .         .
          4650.  C     I  R.  LE M   .         .         .         .         .         .         .         .         .
          4700.  C     I  R.  LE M   .         .         .         .         .         .         .         .         .
          4750.  C     I  R.  LE  M  .         .         .         .         .         .         .         .         .
          4800.  C     I  R.  LWE M  .         .         .         .         .         .         .         .         .
          4850.  C     I  R.  LWE M  .         .         .         .         .         .         .         .         .
          4900.  C     I  R. L WE  M .         .         .         .         .         .         .         .         .
          4950.  C     I  R. L WE  M .         .         .         .         .         .         .         .         .
89000.00  5000.  C     I  R. L WE  M .         .         .         .         .         .         .         .         .
          5050.  C     I  R. L WE   M.         .         .         .         .         .         .         .         .
          5100.  C     I  R. L WE   M.         .         .         .         .         .         .         .         .
          5150.  C     I  R. L WE   M.         .         .         .         .         .         .         .         .
          5200.  C     I   R L WE    M         .         .         .         .         .         .         .         .
          5250.  C     I   R L WE    M         .         .         .         .         .         .         .         .
          5300.  C     I   R L WE    M         .         .         .         .         .         .         .         .
          5350.  C     I   .RL  E    M         .         .         .         .         .         .         .         .
          5400.  C     I   .RL  E    .M        .         .         .         .         .         .         .         .
          5450.  C     I   .RL  E    .M        .         .         .         .         .         .         .         .
89545.00  5500.  C     I   .RL  E    .M        .         .         .         .         .         .         .         .
          5550.  C     I   .RL  E    .M        .         .         .         .         .         .         .         .
          5600.  C     I   .RL  E    M         .         .         .         .         .         .         .         .
          5650.  C     I   .RL  E    M         .         .         .         .         .         .         .         .
          5700.  C     I   .RL  E    M         .         .         .         .         .         .         .         .
          5750.  C      I  .R L E    M         .         .         .         .         .         .         .         .
          5800.  C      I  .R L E    M         .         .         .         .         .         .         .         .
          5850.  C      I  .R L E    M         .         .         .         .         .         .         .         .
          5900.  C      I  .R L E    M         .         .         .         .         .         .         .         .
          5950.  C      I  .R L E   M.         .         .         .         .         .         .         .         .
90000.00  6000.  C      I  .R  LE   M.         .         .         .         .         .         .         .         .
          6050.  C     I   .R  LE   M.         .         .         .         .         .         .         .         .
          6100.  C     I   .R  LE    M         .         .         .         .         .         .         .         .
          6150.  C    I    .R  LE    M         .         .         .         .         .         .         .         .
          6200.  C    I    .R   E    M         .         .         .         .         .         .         .         .
          6250.  C   I     .R   E    M         .         .         .         .         .         .         .         .
          6300.  C   I     .R   E    .M        .         .         .         .         .         .         .         .
          6350.  C  I      .R   E    .M        .         .         .         .         .         .         .         .
          6400.  C  I      .R   E    .M        .         .         .         .         .         .         .         .
          6450.  C I       .R   EL   . M       .         .         .         .         .         .         .         .
90500.00  6500.  C I       R    EL   . M       .         .         .         .         .         .         .         .
          6550.  C I       R    WE   . M       .         .         .         .         .         .         .         .
          6600.  C  I      R    WE   . M       .         .         .         .         .         .         .         .
          6650.  C  I      R    WE   . M       .         .         .         .         .         .         .         .
          6700.  C   I     R    WE   .  M      .         .         .         .         .         .         .         .
          6750.  C   I     R    WE   .  M      .         .         .         .         .         .         .         .
          6800.  C    I    R    WEL  .  M      .         .         .         .         .         .         .         .
          6850.  C    I    R    WEL  .  M      .         .         .         .         .         .         .         .
          6900.  C     I   R    WEL  .  M      .         .         .         .         .         .         .         .
          6950.  C     I   R    WEL  .  M      .         .         .         .         .         .         .         .
91000.00  7000.  C      I  R    WEL  .   M     .         .         .         .         .         .         .         .
          7050.  C      I  R    WEL  .   M     .         .         .         .         .         .         .         .
          7100.  C      I  R    WEL  .  M      .         .         .         .         .         .         .         .
          7150.  C      I  R    WEL  .  M      .         .         .         .         .         .         .         .
          7200.  C      I  R    WEL  .  M      .         .         .         .         .         .         .         .
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X1    99266      16     135.7    247.3      99      99      99
X3       10                     44.25 1257.57
GR    1254.8       0   1253.95    34.59 1257.57   44.25  1257.1    64.9  1253.2   75.14
GR    1253.2   124.9    1255.6    135.7  1255.2   160.5  1256.0   194.5  1256.6  247.30
GR    1256.2  283.01    1256.1   330.28  1255.8  342.91  1256.9  492.26  1258.0  603.07
GR    1259.1  700.00
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FLOW CROSSING 56TH ST. BRIDGE

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NC      .016    .016     .016
X1    99267      12       65      312       1       1       1
X3       10
GR    1254.5       0   1255.2       65  1255.2      80  1254.7     140  1254.6     162
GR    1254.8     195     1255      215  1255.9     245  1256.0   259.5  1256.6     312
GR    1257.7     500     1258      600

X1    99327      12      150      397      60      60      60
X3       10
GR    1254.5       0   1255.3      150  1255.3     165  1254.7     225  1254.6     245
GR    1254.9     280   1255.4      300    1256     320  1256.0     345  1256.6     397
GR    1257.7     500     1258      600

X1    99328      21   151.01    312.4       1       1       1
X3       10                     35.79  1259.5
GR    1255.3       0   1255.9    26.98  1259.5   35.79 1259.36   56.63  1253.3   70.27
GR    1253.3   121.6   1254.3    128.9  1256.6  134.76  1257.7  139.23  1258.1  140.75
GR    1258.9  151.01   1258.6   181.64  1257.2  187.95  1256.3  192.38 1256.69  256.65
GR    1256.8  277.13  1257.19    312.4  1257.5  397.83  1258.2  500.87  1258.1  596.17
GR    1259.2  700.00

NC      .018      .8     .025
X1    99408      21   151.01    312.4      80      82      81
X3       10                     35.79  1259.5
GR    1255.3       0   1255.9    26.98  1259.5   35.79 1259.36   56.63  1253.3   70.27
GR    1253.3   121.6   1254.3    128.9  1256.6  134.76  1257.7  139.23  1258.1  140.75
GR    1258.9  151.01   1258.6   181.64  1257.2  187.95  1256.3  192.38 1256.69  256.65
GR    1256.8  277.13  1257.19    312.4  1257.5  397.83  1258.2  500.87  1258.1  596.17
GR    1259.2  700.00

X1    99500      19   150.95   300.56      92      90      91
X3       10                     26.68  1260.17
GR    1255.4       0  1256.07    16.27  1260.17   26.68  1259.6   51.27  1253.4   68.28
GR    1253.4   119.8  1256.49    129.9  1258.0  133.27  1260.1  136.92  1260.9  138.48
GR    1261.1  150.95   1260.6   192.21  1257.0  200.84 1257.32  250.49  1257.5  300.56
GR    1256.7  401.39   1258.7   493.57  1259.0  607.79  1259.7  700.00
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X1	99717	18	210.69	314.55	220	215	217			
X3	10			48.97	1262.4					
GR	1260.6	0	1262.7	4.31	1262.0	18.18	1262.4	48.97	1253.4	67.52
GR	1253.4	117.5	1263.4	138.6	1264.8	168.66	1265.3	176.41	1265.8	210.69
GR	1266.1	221.95	1263.7	227.39	1258.3	238.97	1258.48	314.55	1258.5	401.80
GR	1260.0	503.01	1259.0	601.42	1261.2	700.00				
NC	.025	.8	.019							
X1	100251	25	169.81	219.05	510	400	470			
X3	10			64.7	1274.29					
GR	1263.0	0	1262.8	24.0	1273.78	45.34	1274.29	64.70	1271.2	70.3
GR	1271.2	132.1	1274.1	138.3	1273.7	169.81	1269.6	177.13	1267.9	181.78
GR	1266.1	185.60	1265.2	187.33	1264.8	188.14	1263.1	192.22	1263.2	194.65
GR	1260.0	199.07	1256.9	203.62	1256.6	208.48	1259.5	213.39	1261.1	216.24
GR	1262.9	219.05	1262.5	376.39	1261.1	507.33	1261.8	599.93	1262.0	700.00
NC				.3	.5					
NH	3	.05	175.99	.019	187.99	.8	700			
X1	100500	18	175.99	187.99	249	249	249			
X3	10			35.5	1273.15			1263	1263	
GR	1261.7	0	1262.6	14.5	1273.15	35.5	1273.09	63.76	1271.2	69.48
GR	1271.2	132.6	1273.7	139.3	1273.2	157.27	1270.2	163.09	1257	175.99
GR	1257.0	187.99	1258.9	191.27	1260.5	193.68	1263.1	197.61	1262.7	307.57
GR	1263.4	501.16	1263.4	597.87	1263.8	700.00				
SC	1.013	.4	3	450	6	12	451	8.1	1262.1	1261.44
NH	3	.05	171.4	.013	183.4	.8	567.43			
X1	100951	15	171.4	183.4	471	431	451			
X2			2		1268.2					
X3	10							1268.2	1268.2	
BT	-4	154.7	1274		171.4	1268.6		183.4	1268.6	
BT		199.66	1268.6							
GR	1266.7	0	1273.4	25.9	1273.7	63.6	1271.3	70.1	1271.3	133.5
GR	1273.7	141.7	1274.0	154.7	1261.2	171.4	1261.2	183.4	1268.6	199.66
GR	1268.6	208.6	1268.7	250.46	1269.0	300.23	1270.9	382.35	1272.6	567.43
NC	.025	.8	.019							
X1	101000	21	140.8	195.9	48	50	49			
X3	10			65.4	1273.5					
GR	1266.5	0	1269.5	18.5	1272.8	32.27	1273.5	65.4	1271.3	70.14
GR	1271.3	130.9	1273.58	140.8	1270.4	160.0	1262.2	172.1	1262.17	177.5
GR	1268.4	184.6	1269.0	195.9	1269.2	299.94	1269.7	316.90	1269.8	337.53
GR	1270.2	338.73	1271.4	344.88	1271.2	346.48	1271.1	399.04	1271.3	497.42
GR	1272.8	570.19								

X1	101048	21	159.37	188.96	48	48	48			
X3	10			35.8	1274.1					
GR	1266.4	0	1266.6	10.6	1274.1	35.8	1273.1	64.6	1271.3	68.3
GR	1271.3	130.8	1273.95	138.6	1273.2	159.37	1269.0	166.15	1266.8	169.66
GR	1265.5	171.15	1262.9	174.33	1262.3	175.08	1262.2	180.49	1267.6	187.47
GR	1268.4	188.36	1268.9	188.96	1269.5	196.41	1269.4	299.80	1270.9	400.42
GR	1273.0	582.89								
X1	101500	23	154.7	184.32	452	452	452			
X3	10			48.74	1274.2					
GR	1268.8	0	1269.5	35.2	1274.2	48.74	1273.2	63.4	1271.4	66.9
GR	1271.4	130.5	1274.28	136.3	1274.1	154.7	1263.49	170.0	1263.2	176.9
GR	1264.0	177.71	1265.1	179.31	1268.7	184.32	1269.7	200.77	1270.2	241.46
GR	1269.8	263.19	1269.9	271.18	1270.3	281.27	1270.6	300.86	1271.6	400.43
GR	1272.8	500.69	1273.5	604.11	1273.7	697.31				
X1	102000	25	154.8	190.72	500	500	500			
X3	10			64.22	1273.5					
GR	1268.5	0	1268.9	37.64	1269.9	44.7	1273.0	52.3	1273.5	64.22
GR	1271.6	68.5	1271.6	130.48	1273.7	137.5	1272.7	154.8	1267.8	162.9
GR	1265.4	165.2	1263.7	166.9	1263.9	172.7	1269.6	188.9	1269.66	190.72
GR	1269.6	220.4	1270.1	251.17	1269.7	254.06	1270.1	280.54	1270.5	362.21
GR	1271.1	430.24	1271.4	434.16	1271.5	436.74	1271.5	488.31	1273.9	700.00
NC	.02	.8	.025							
X1	102500	18	155.0	182.86	500	500	500			
X3	10			63.8	1273.3					
GR	1267.7	0	1268.1	42.0	1273.3	51.9	1273.3	63.8	1271.7	67.6
GR	1271.7	130.0	1272.96	135.4	1272.0	155.0	1264.7	166.4	1264.6	170.4
GR	1265.2	171.70	1265.8	172.99	1268.1	176.84	1269.6	182.86	1270.0	298.75
GR	1271.7	516.33	1272.8	604.91	1273.9	700.00				
X1	103000	20	156.4	184.79	500	500	500			
X3	10			52	1273.8					
GR	1267.5	0	1267.26	40.5	1273.8	52.0	1273.58	62.9	1271.9	69.01
GR	1271.9	128.7	1274.0	135.0	1273.3	156.4	1265.1	169.0	1264.9	175.5
GR	1266.9	179.29	1268.8	182.14	1268.7	184.79	1269.1	191.87	1269.4	200.38
GR	1270.2	300.35	1270.7	402.41	1271.6	503.13	1272.0	598.89	1273.2	700.00
X1	103500	16	155.1	180.79	500	470	480			
X3	10			52	1274					
GR	1268.2	0	1267.2	33.1	1274.0	52.0	1273.68	62.5	1271.9	67.7
GR	1271.9	130.2	1274.1	136.4	1273.6	155.1	1266.8	166.4	1266.0	173.8
GR	1269.5	180.79	1269.8	191.2	1269.8	206.63	1270.9	298.68	1271.9	499.91
GR	1272.5	607.91								

X1	104000	17	156.6	178.6	500	475	480			
X3	10			52	1274.3					
GR	1269.2	0	1268.78	42.1	1274.3	52.0	1273.86	63.6	1272.0	67.6
GR	1272.0	132.8	1274.3	138.7	1273.3	156.6	1266.2	165.9	1266.0	173.9
GR	1269.4	178.6	1270.0	209.69	1271.1	307.75	1270.7	402.81	1272.1	502.79
GR	1272.9	599.96	1273.0	700.00						
X1	104500	19	165.2	189.73	500	500	500			
X3	10			49.91	1274.86					
GR	1268.8	0	1269.1	36.5	1274.86	49.91	1274.19	63.15	1272.1	68.65
GR	1272.1	132.13	1274.16	139.34	1274.05	165.2	1266.18	174.59	1267.85	185.39
GR	1270.1	189.73	1270.7	339.19	1271.3	344.50	1271.8	347.33	1271.2	349.45
GR	1271.9	474.61	1272.3	481.03	1273.0	598.96	1273.7	700.00		
X1	104818	21	138.97	193.58	318	318	318			
X3	10			48.02	1274.36					
GR	1269.7	0	1269.62	39.2	1274.36	48.02	1274.08	61.06	1274.08	61.07
GR	1272.2	66.25	1272.2	132.32	1274.15	138.97	1273.3	168.68	1270.7	172.23
GR	1266.1	178.66	1266.1	185.46	1267.3	187.91	1269.9	193.58	1271.1	225.22
GR	1271.1	360.39	1270.8	370.29	1271.1	376.14	1271.4	471.12	1272.6	577.86
GR	1272.3	700.00								
X1	105000	28	169.95	197.31	182	182	182			
X3	10			48.47	1274.78					
GR	1271.8	0	1270.63	40.48	1274.78	48.47	1272.2	67.54	1272.2	132.99
GR	1275.0	169.95	1268.3	181.83	1266.17	187.57	1270.05	197.31	1269.54	206.79
GR	1269.7	211.21	1270.4	235.26	1270.53	250.99	1270.1	302.52	1270.93	357.13
GR	1270.7	364.47	1270.6	372.33	1270.94	373.09	1271.07	378.01	1271.69	380.27
GR	1271.3	382.49	1271.15	384.06	1271.0	393.47	1271.16	454.46	1271.11	497.63
GR	1272.5	524.55	1272.0	559.41	1272.0	600				
X1	105294	19	150.95	185.32	294	294	294			
X3	10			44.93	1274.95					
GR	1273.3	0	1272.69	30.25	1274.95	44.93	1274.55	58.59	1272.2	63.09
GR	1272.2	140.03	1273.24	145.34	1273.56	150.95	1273.2	160.05	1267.42	174.63
GR	1271.0	182.82	1272.1	185.32	1271.7	205.26	1270.8	227.20	1270.7	299.75
GR	1271.3	373.35	1272.2	501.43	1271.9	598.86	1273.5	700.00		

T1
T2
T3

J1	ICHECK	INQ	NINV	IDIR	STRT	METRIC	HVINS	Q	WSEL	FQ
		3			.06				1248.5	
J2	NPROF	IPLOT	PRFVS	XSECV	XSECH	FN	ALLDC	IBW	CHNIM	ITRACE
	2									

PROFILE FOR STREAM

PLOTTED POINTS (BY PRIORITY) E-ENERGY,W-WATER SURFACE,I-INVERT,C-CRITICAL W.S.,L-LEFT BANK,R-RIGHT BANK,M-LOWER END STA

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ELEVATION  1246.     1251.     1256.     1261.     1266.     1271.     1276.     1281.     1286.     1291.
   SECNO   CUMDIS
84000.00     0.  .  IWE R L.   M     .         .         .         .         .         .         .         .
            50.  C  I E  R LM        .         .         .         .         .         .         .         .
           100.  C  I E - R L        .         .         .         .         .         .         .         .
           150.  C  IMWE  RL         .         .         .         .         .         .         .         .
           200.  CM I WE   RL        .         .         .         .         .         .         .         .
           250.  C  I WE   RL        .         .         .         .         .         .         .         .
           300.  C  I WE   .RL       .         .         .         .         .         .         .         .
           350.  C  I  E   .RL       .         .         .         .         .         .         .         .
           400.  C  I  E   . L       .         .         .         .         .         .         .         .
           450.  C  I  E   . RL      .         .         .         .         .         .         .         .
84500.00   500.  C  I  E   .  L      .         .         .         .         .         .         .         .
           550.  C  I  E   . LR      .         .         .         .         .         .         .         .
           600.  C  I  WE  . LR      .         .         .         .         .         .         .         .
           650.  C  I  WE  .L R      .         .         .         .         .         .         .         .
           700.  C  I  WE  .L R      .         .         .         .         .         .         .         .
           750.  C  I   E  L  R      .         .         .         .         .         .         .         .
           800.  CM I   E  L R       .         .         .         .         .         .         .         .
           850.  C  I M E L. R       .         .         .         .         .         .         .         .
           900.  C   I  EML. R       .         .         .         .         .         .         .         .
           950.  C   I  EL .MR       .         .         .         .         .         .         .         .
85000.00  1000.  C   I  EL . R M     .         .         .         .         .         .         .         .
          1050.  C   I  EL . R M     .         .         .         .         .         .         .         .
          1100.  C   I  EL . R M     .         .         .         .         .         .         .         .
          1150.  C   I  EL .R  M     .         .         .         .         .         .         .         .
          1200.  C   I  EL .R  M     .         .         .         .         .         .         .         .
          1250.  C   I  EL .R   M    .         .         .         .         .         .         .         .
          1300.  C   I  EL .R   M    .         .         .         .         .         .         .         .
          1350.  C   I  EL .R   M    .         .         .         .         .         .         .         .
          1400.  C   I  EL R    M    .         .         .         .         .         .         .         .
          1450.  C   I  EL R    M    .         .         .         .         .         .         .         .
85500.00  1500.  C   I  EL R    M    .         .         .         .         .         .         .         .
          1550.  C   I  EL R    M    .         .         .         .         .         .         .         .
          1600.  C   I  EL R    M    .         .         .         .         .         .         .         .
          1650.  C   I  EL .R   M    .         .         .         .         .         .         .         .
          1700.  C   I  WE .R   M    .         .         .         .         .         .         .         .
          1750.  C   I  WE .R  M     .         .         .         .         .         .         .         .
          1800.  C   I  WE .R  M     .         .         .         .         .         .         .         .
          1850.  C   I  WE .R  M     .         .         .         .         .         .         .         .
          1900.  C   I  WE . R M     .         .         .         .         .         .         .         .
          1950.  C   I  LE . R M     .         .         .         .         .         .         .         .
          2000.  C   I  LE . R M     .         .         .         .         .         .         .         .
86024.00  2050.  C   I  LE . R M     .         .         .         .         .         .         .         .
          2100.  C   I   E . R M     .         .         .         .         .         .         .         .
          2150.  C  I    E .R   M    .         .         .         .         .         .         .         .
          2200.  C  I    EL.R   M    .         .         .         .         .         .         .         .
          2250.  C I     E LR   M    .         .         .         .         .         .         .         .
          2300.  C I     E L    M    .         .         .         .         .         .         .         .
          2350.  CI      E RL   M    .         .         .         .         .         .         .         .
          2400.  I       E RL   M    .         .         .         .         .         .         .         .
86415.00  2450.  I   C   ER.L   M    .         .         .         .         .         .         .         .
          2500.  I       ER. L  M    .         .         .         .         .         .         .         .
          2550.  CI      ER. L  M    .         .         .         .         .         .         .         .
          2600.  CI      ER. L  M    .         .         .         .         .         .         .         .
          2650.  C I     ER. L  M    .         .         .         .         .         .         .         .
          2700.  C I     ER.  L M    .         .         .         .         .         .         .         .
          2750.  C  I    ER.  L M    .         .         .         .         .         .         .         .
          2800.  C  I    ER.  L M    .         .         .         .         .         .         .         .
          2850.  C  I    ER.  L M    .         .         .         .         .         .         .         .
          2900.  C   I   ER.   LM    .         .         .         .         .         .         .         .
          2950.  C   I   ER.   LM    .         .         .         .         .         .         .         .
87000.00  3000.  C    I  ER.   LM    .         .         .         .         .         .         .         .
          3050.  C    I  E R   LM    .         .         .         .         .         .         .         .
          3100.  C    I  E R   LM    .         .         .         .         .         .         .         .
          3150.  C    I  E R   LM    .         .         .         .         .         .         .         .
          3200.  C    I  E R   LM    .         .         .         .         .         .         .         .
          3250.  C    I  E .R  LM    .         .         .         .         .         .         .         .
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          3300.  C    I  WE.R   L    .         .         .         .         .         .         .         .         .
          3350.  C    I  WE.R   L    .         .         .         .         .         .         .         .         .
          3400.  C    I  WE.R   LM   .         .         .         .         .         .         .         .         .
          3450.  C    I   E. R  LM   .         .         .         .         .         .         .         .         .
 87500.00 3500.  C    I   E. R  LM   .         .         .         .         .         .         .         .         .
          3550.  C    I   E. R  L    .         .         .         .         .         .         .         .         .
          3600.  C    I   E.R   L    .         .         .         .         .         .         .         .         .
          3650.  C    I   E.R   L    .         .         .         .         .         .         .         .         .
          3700.  C    I   E.R   L    .         .         .         .         .         .         .         .         .
          3750.  C    I   E.R  ML    .         .         .         .         .         .         .         .         .
          3800.  C    I   E.R  ML    .         .         .         .         .         .         .         .         .
          3850.  C    I   ER   L     .         .         .         .         .         .         .         .         .
          3900.  C    I   ER  ML     .         .         .         .         .         .         .         .         .
          3950.  C    I   ER  ML     .         .         .         .         .         .         .         .         .
 88000.00 4000.  C    I   ER  ML     .         .         .         .         .         .         .         .         .
          4050.  C    I   ER  ML     .         .         .         .         .         .         .         .         .
          4100.  C    I   ER  ML     .         .         .         .         .         .         .         .         .
          4150.  C    I   ER  ML     .         .         .         .         .         .         .         .         .
          4200.  C    I   ER   L     .         .         .         .         .         .         .         .         .
          4250.  C     I  ER   L     .         .         .         .         .         .         .         .         .
          4300.  C     I  ER   L     .         .         .         .         .         .         .         .         .
          4350.  C     I  ER   L     .         .         .         .         .         .         .         .         .
          4400.  C     I  ER  LM     .         .         .         .         .         .         .         .         .
          4450.  C     I  ER  L M    .         .         .         .         .         .         .         .         .
 88500.00 4500.  C     I  ER  L M    .         .         .         .         .         .         .         .         .
          4550.  C     I  WE  L M    .         .         .         .         .         .         .         .         .
          4600.  C     I  WE  L  M   .         .         .         .         .         .         .         .         .
          4650.  C     I  WE  L  M   .         .         .         .         .         .         .         .         .
          4700.  C     I  WE  L  M   .         .         .         .         .         .         .         .         .
          4750.  C     I  RE  L   M  .         .         .         .         .         .         .         .         .
          4800.  C     I  RE  L   M  .         .         .         .         .         .         .         .         .
          4850.  C     I  RE  L   M  .         .         .         .         .         .         .         .         .
          4900.  C     I  RE L     M .         .         .         .         .         .         .         .         .
          4950.  C     I  RE L     M .         .         .         .         .         .         .         .         .
 89000.00 5000.  C     I  RE L     M .         .         .         .         .         .         .         .         .
          5050.  C     I  RE L      M.         .         .         .         .         .         .         .         .
          5100.  C     I  RE L      M.         .         .         .         .         .         .         .         .
          5150.  C     I  RE L      M.         .         .         .         .         .         .         .         .
          5200.  C     I   E L       M         .         .         .         .         .         .         .         .
          5250.  C     I   E L       M         .         .         .         .         .         .         .         .
          5300.  C     I   E L       M         .         .         .         .         .         .         .         .
          5350.  C     I   ERL       M         .         .         .         .         .         .         .         .
          5400.  C     I   ERL       .M        .         .         .         .         .         .         .         .
          5450.  C     I   ERL       .M        .         .         .         .         .         .         .         .
 89545.00 5500.  C     I   ERL       .M        .         .         .         .         .         .         .         .
          5550.  C     I   ERL       .M        .         .         .         .         .         .         .         .
          5600.  C     I   ERL       M         .         .         .         .         .         .         .         .
          5650.  C     I   ERL       M         .         .         .         .         .         .         .         .
          5700.  C     I   ERL       M         .         .         .         .         .         .         .         .
          5750.  C      I  ER L      M         .         .         .         .         .         .         .         .
          5800.  C      I  ER L      M         .         .         .         .         .         .         .         .
          5850.  C      I  ER L      M         .         .         .         .         .         .         .         .
          5900.  C      I  ER L      M         .         .         .         .         .         .         .         .
          5950.  C      I  ER L     M.         .         .         .         .         .         .         .         .
 90000.00 6000.  C      I  WE  L    M.         .         .         .         .         .         .         .         .
          6050.  C     I   WE  L    M.         .         .         .         .         .         .         .         .
          6100.  C     I   WE  L     M         .         .         .         .         .         .         .         .
          6150.  C    I    WE  L     M         .         .         .         .         .         .         .         .
          6200.  C    I    WE   L    M         .         .         .         .         .         .         .         .
          6250.  C   I     WE   L    M         .         .         .         .         .         .         .         .
          6300.  C   I     .E   L    .M        .         .         .         .         .         .         .         .
          6350.  C  I      .E   L    .M        .         .         .         .         .         .         .         .
          6400.  C  I      .E   L    .M        .         .         .         .         .         .         .         .
          6450.  C I       .E    L   . M       .         .         .         .         .         .         .         .
 90500.00 6500.  C I       RE    L   . M       .         .         .         .         .         .         .         .
          6550.  C I       RE    L   . M       .         .         .         .         .         .         .         .
          6600.  C  I      RE    L   . M       .         .         .         .         .         .         .         .
          6650.  C  I      RE    L   . M       .         .         .         .         .         .         .         .
          6700.  C   I     RE    L   .  M      .         .         .         .         .         .         .         .
          6750.  C   I     RE    L   .  M      .         .         .         .         .         .         .         .
          6800.  C    I    RE     L  .  M      .         .         .         .         .         .         .         .
          6850.  C    I    RE     L  .  M      .         .         .         .         .         .         .         .
          6900.  C     I   RE     L  .  M      .         .         .         .         .         .         .         .
          6950.  C     I   RE     L  .  M      .         .         .         .         .         .         .         .
 91000.00 7000.  C      I  RE     L  .   M     .         .         .         .         .         .         .         .
          7050.  C      I  RE     L  .   M     .         .         .         .         .         .         .         .
          7100.  C      I  RE     L  .  M      .         .         .         .         .         .         .         .
          7150.  C      I  RE     L  .  M      .         .         .         .         .         .         .         .
          7200.  C      I  RE     L  .  M      .         .         .         .         .         .         .         .
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          7250.  C     I  RE     L  .  M     .     .     .     .     .     .     .     .
          7300.  C     I  RE    L   .  M     .     .     .     .     .     .     .     .
          7350.  C     I  RE    L   .  M     .     .     .     .     .     .     .     .
          7400.  C     I  RE    L   .  M     .     .     .     .     .     .     .     .
          7450.  C     I  RE    L   .  M     .     .     .     .     .     .     .     .
91500.00  7500.  C     I  RE    L   .  M     .     .     .     .     .     .     .     .
          7550.  C     I  RE    L   .  M     .     .     .     .     .     .     .     .
          7600.  C     I  RE    L   .  M     .     .     .     .     .     .     .     .
          7650.  C     I  .E    L   .  M     .     .     .     .     .     .     .     .
          7700.  C     I  .E    L   .   M    .     .     .     .     .     .     .     .
          7750.  C     I  .E    L   .   M    .     .     .     .     .     .     .     .
          7800.  C     I  .E   L    .   M    .     .     .     .     .     .     .     .
          7850.  C     I  .ER  L    .   M    .     .     .     .     .     .     .     .
          7900.  C     I  .ER  L    .   M    .     .     .     .     .     .     .     .
          7950.  C     I  .ER  L    .   M    .     .     .     .     .     .     .     .
92000.00  8000.  C     I  .ER  L    .   M    .     .     .     .     .     .     .     .
          8050.  C     I  .ER  L    .   M    .     .     .     .     .     .     .     .
          8100.  C     I  .ER   L   .   M    .     .     .     .     .     .     .     .
          8150.  C     I  .ER   L   .   M    .     .     .     .     .     .     .     .
          8200.  C     I  .ER   L   .   M    .     .     .     .     .     .     .     .
          8250.  C     I  .ER   L   .    M   .     .     .     .     .     .     .     .
          8300.  C     I  .ER   L   .    M   .     .     .     .     .     .     .     .
          8350.  C     I  .ER   L   .    M   .     .     .     .     .     .     .     .
          8400.  C     I  .WE   L   .    M   .     .     .     .     .     .     .     .
          8450.  C     I  .WE   L   .    M   .     .     .     .     .     .     .     .
92500.00  8500.  C     I  .WE    L  .    M   .     .     .     .     .     .     .     .
          8550.  C     I  . E    L  .    M   .     .     .     .     .     .     .     .
          8600.  C     I  . E    L  .    M   .     .     .     .     .     .     .     .
          8650.  C      I . E    L  .    M   .     .     .     .     .     .     .     .
          8700.  C      I . ER   L  .    M   .     .     .     .     .     .     .     .
          8750.  C      I . ER   L  .    M   .     .     .     .     .     .     .     .
          8800.  C      I . ER    L .    M   .     .     .     .     .     .     .     .
          8850.  C      I . ER    L .     M  .     .     .     .     .     .     .     .
          8900.  C      I . E R   L .     M  .     .     .     .     .     .     .     .
          8950.  C      I . E R   L .     M  .     .     .     .     .     .     .     .
93000.00  9000.  C      I . E R   L .     M  .     .     .     .     .     .     .     .
          9050.  C       I. E R   L .     M  .     .     .     .     .     .     .     .
          9100.  C       I.  ER   L .    M   .     .     .     .     .     .     .     .
          9150.  C        I  ER  L  .    M   .     .     .     .     .     .     .     .
          9200.  C        .I WE  L  .    M   .     .     .     .     .     .     .     .
          9250.  C        .I  E  L  .    M   .     .     .     .     .     .     .     .
          9300.  C        . I ERL   .    M   .     .     .     .     .     .     .     .
          9350.  C        .  IWEL   .    M   .     .     .     .     .     .     .     .
          9400.  C        .  I EL   .   M    .     .     .     .     .     .     .     .
93574.00  9450.  .        .   IWE   .   M    .     .     .     .     .     .     .     .
          9500.  .        .  I WE   .   M    .     .     .     .     .     .     .     .
          9550.  .        .  I WE   .   M    .     .     .     .     .     .     .     .
          9600.  .        . I CWE   .  M     .     .     .     .     .     .     .     .
          9650.  .        . I CWE   .  M     .     .     .     .     .     .     .     .
          9700.  .        .I  CWE   .  M     .     .     .     .     .     .     .     .
          9750.  .        I   CWE   .  M     .     .     .     .     .     .     .     .
          9800.  .        I   CWE   . M      .     .     .     .     .     .     .     .
          9850.  .       I.  C WE   . M      .     .     .     .     .     .     .     .
          9900.  .       I.  C WE   . M      .     .     .     .     .     .     .     .
          9950.  .      I .  CLRE   .M       .     .     .     .     .     .     .     .
94000.00 10000.  .      I .  CLRE   .M       .     .     .     .     .     .     .     .
         10050.  C      I .   LRE   .M       .     .     .     .     .     .     .     .
         10100.  C      I .    LE   . M      .     .     .     .     .     .     .     .
         10150.  C       I.    LE   . M      .     .     .     .     .     .     .     .
         10200.  C       I.    LE   .  M     .     .     .     .     .     .     .     .
         10250.  C       I.    LE   .  M     .     .     .     .     .     .     .     .
         10300.  C        I    LER  .   M    .     .     .     .     .     .     .     .
         10350.  C        I    LER  .   M    .     .     .     .     .     .     .     .
         10400.  C        I     ER  .   M    .     .     .     .     .     .     .     .
         10450.  C        I     ER  .    M   .     .     .     .     .     .     .     .
94500.00 10500.  C        .I    E R .    M   .     .     .     .     .     .     .     .
         10550.  C        .I    E R .    M   .     .     .     .     .     .     .     .
         10600.  C        . I   E R .    M   .     .     .     .     .     .     .     .
         10650.  C        . I   ELR .    M   .     .     .     .     .     .     .     .
         10700.  C        .  I   ER .    M   .     .     .     .     .     .     .     .
         10750.  C        .  I   ER .    M   .     .     .     .     .     .     .     .
         10800.  C        .  I   ER .    M   .     .     .     .     .     .     .     .
         10850.  C        .   I  ER .    M   .     .     .     .     .     .     .     .
         10900.  C        .   I   E .     M  .     .     .     .     .     .     .     .
         10950.  C        .    I  E .     M  .     .     .     .     .     .     .     .
95000.00 11000.  .        .    I CE .     M  .     .     .     .     .     .     .     .
         11050.  .        .    IC E .    M   .     .     .     .     .     .     .     .
         11100.  .        .    IC ER.    M   .     .     .     .     .     .     .     .
         11150.  .        .   I C ER.    M   .     .     .     .     .     .     .     .
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          7250.  C     I  R    WEL  .  M     .         .         .         .         .         .         .
          7300.  C     I  R     E   .  M     .         .         .         .         .         .         .
          7350.  C     I  R     E   .  M     .         .         .         .         .         .         .
          7400.  C     I  R     E   .  M     .         .         .         .         .         .         .
          7450.  C     I  R     E   .  M     .         .         .         .         .         .         .
91500.00  7500.  C     I  R     E   .  M     .         .         .         .         .         .         .
          7550.  C     I  R     E   .  M     .         .         .         .         .         .         .
          7600.  C     I  R     E   .  M     .         .         .         .         .         .         .
          7650.  C     I  .R    E   .  M     .         .         .         .         .         .         .
          7700.  C     I  .R    E   .   M    .         .         .         .         .         .         .
          7750.  C     I  .R    E   .   M    .         .         .         .         .         .         .
          7800.  C     I  .R   LE   .   M    .         .         .         .         .         .         .
          7850.  C     I  . R  LE   .   M    .         .         .         .         .         .         .
          7900.  C     I  . R  LE   .   M    .         .         .         .         .         .         .
          7950.  C     I  . R  LE   .   M    .         .         .         .         .         .         .
92000.00  8000.  C     I  . R  LE   .   M    .         .         .         .         .         .         .
          8050.  C     I  . R  LE   .   M    .         .         .         .         .         .         .
          8100.  C     I  . R   E   .   M    .         .         .         .         .         .         .
          8150.  C     I  . R   E   .   M    .         .         .         .         .         .         .
          8200.  C     I  . R   E   .   M    .         .         .         .         .         .         .
          8250.  C     I  . R   E   .    M   .         .         .         .         .         .         .
          8300.  C     I  . R   E   .    M   .         .         .         .         .         .         .
          8350.  C     I  . R   WE  .    M   .         .         .         .         .         .         .
          8400.  C     I  . R   WE  .    M   .         .         .         .         .         .         .
          8450.  C     I  . R   WE  .    M   .         .         .         .         .         .         .
92500.00  8500.  C     I  . R   WE  .    M   .         .         .         .         .         .         .
          8550.  C     I  . R   WE  .    M   .         .         .         .         .         .         .
          8600.  C     I  . R   WE  .    M   .         .         .         .         .         .         .
          8650.  C      I . R   WE  .    M   .         .         .         .         .         .         .
          8700.  C      I .  R  WE  .    M   .         .         .         .         .         .         .
          8750.  C      I .  R  WE  .    M   .         .         .         .         .         .         .
          8800.  C      I .  R  WEL .    M   .         .         .         .         .         .         .
          8850.  C      I .  R  WEL .     M  .         .         .         .         .         .         .
          8900.  C      I .   R WEL .     M  .         .         .         .         .         .         .
          8950.  C      I .   R WEL .     M  .         .         .         .         .         .         .
93000.00  9000.  C      I .   R WEL .     M  .         .         .         .         .         .         .
          9050.  C       I.   R WEL .     M  .         .         .         .         .         .         .
          9100.  C       I.   R  EL .    M   .         .         .         .         .         .         .
          9150.  C        I   R  E  .    M   .         .         .         .         .         .         .
          9200.  C        .I  R  E  .    M   .         .         .         .         .         .         .
          9250.  C        .I  R  E  .    M   .         .         .         .         .         .         .
          9300.  C        . I  RLE  .    M   .         .         .         .         .         .         .
          9350.  C        .  I RLE  .    M   .         .         .         .         .         .         .
          9400.  C        .  I RLE  .   M    .         .         .         .         .         .         .
93574.00  9450.  C        .   IL E  .   M    .         .         .         .         .         .         .
          9500.  C        .  I L E  .   M    .         .         .         .         .         .         .
          9550.  C        .  I L E  .   M    .         .         .         .         .         .         .
          9600.  C        . I  L E  .  M     .         .         .         .         .         .         .
          9650.  C        . I  L WE .  M     .         .         .         .         .         .         .
          9700.  C        .I   L WE .  M     .         .         .         .         .         .         .
          9750.  C        I    L WE .  M     .         .         .         .         .         .         .
          9800.  C        I    L WE . M      .         .         .         .         .         .         .
          9850.  C       I.    L WE . M      .         .         .         .         .         .         .
          9900.  C       I.    L WE . M      .         .         .         .         .         .         .
          9950.  C      I .   LR WE .M       .         .         .         .         .         .         .
94000.00 10000.  .      I .   CR  E .M       .         .         .         .         .         .         .
         10050.  C      I .   LR  E .M       .         .         .         .         .         .         .
         10100.  C      I .    LR E . M      .         .         .         .         .         .         .
         10150.  C      I .    LR E . M      .         .         .         .         .         .         .
         10200.  C      I .    LR E .  M     .         .         .         .         .         .         .
         10250.  C      I .    LR E .  M     .         .         .         .         .         .         .
         10300.  C      I .    L RE .   M    .         .         .         .         .         .         .
         10350.  C       I.    L RE .   M    .         .         .         .         .         .         .
         10400.  C       I.     LRE .   M    .         .         .         .         .         .         .
         10450.  C       I.     LRE .    M   .         .         .         .         .         .         .
94500.00 10500.  C       I.     L E .    M   .         .         .         .         .         .         .
         10550.  C        I     L E .    M   .         .         .         .         .         .         .
         10600.  C        I     L E .    M   .         .         .         .         .         .         .
         10650.  C        .I     LE .    M   .         .         .         .         .         .         .
         10700.  C        . I    LE .    M   .         .         .         .         .         .         .
         10750.  C        . I    LE .    M   .         .         .         .         .         .         .
         10800.  C        .  I   LWE.    M   .         .         .         .         .         .         .
         10850.  C        .  I   LWE.    M   .         .         .         .         .         .         .
         10900.  C        .   I   WE.     M  .         .         .         .         .         .         .
         10950.  C        .    I  WE.     M  .         .         .         .         .         .         .
95000.00 11000.  .        .    I  WE.     M  .         .         .         .         .         .         .
         11050.  C        .    I  WE.    M   .         .         .         .         .         .         .
         11100.  C        .    I  WE.    M   .         .         .         .         .         .         .
         11150.  C        .   I   WE.    M   .         .         .         .         .         .         .
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          11200.  C        .   I  L E.    M    .         .         .         .         .         .         .
          11250.  C        .   I  L E.   M     .         .         .         .         .         .         .
          11300.  C        .  I   L E.   M     .         .         .         .         .         .         .
          11350.  C        .  I   L ER   M     .         .         .         .         .         .         .
          11400.  C        . I    L ER   M     .         .         .         .         .         .         .
          11450.  C        . I   L  WE  M      .         .         .         .         .         .         .
95500.00  11500.  C        . I   L  WE  M      .         .         .         .         .         .         .
          11550.  C        . I   L  WE  M      .         .         .         .         .         .         .
          11600.  C        .I    L  WE  M      .         .         .         .         .         .         .
          11650.  C        .I    L  WE  M      .         .         .         .         .         .         .
          11700.  C        .I    L  WE  M      .         .         .         .         .         .         .
          11750.  C        I     L  WE  M      .         .         .         .         .         .         .
          11800.  C        I     L R E  M      .         .         .         .         .         .         .
          11850.  C        I     L R E   M     .         .         .         .         .         .         .
          11900.  C       I.     LR  E   M     .         .         .         .         .         .         .
          11950.  C       I.     LR  E   M     .         .         .         .         .         .         .
96000.00  12000.  C       I.     LR  E   M     .         .         .         .         .         .         .
          12050.  C       I.     LR  E   M     .         .         .         .         .         .         .
          12100.  C       I.     LR  E   M     .         .         .         .         .         .         .
          12150.  C       I.     LR  E   M     .         .         .         .         .         .         .
          12200.  C       I.    L R  E   M     .         .         .         .         .         .         .
          12250.  C        I    L R  E   M     .         .         .         .         .         .         .
          12300.  C        I    L R  E   M     .         .         .         .         .         .         .
          12350.  C        I    L R  E   M     .         .         .         .         .         .         .
          12400.  C        I    L R  E   M     .         .         .         .         .         .         .
          12450.  C        I    L R  E   M     .         .         .         .         .         .         .
96500.00  12500.  C        I    L R  E   M     .         .         .         .         .         .         .
          12550.  C        I    L R  E   M     .         .         .         .         .         .         .
          12600.  C        I    L R  E   M     .         .         .         .         .         .         .
          12650.  C        I    L R  E   M     .         .         .         .         .         .         .
          12700.  C        I    L R  E   M     .         .         .         .         .         .         .
          12750.  C        I    L R  E   M     .         .         .         .         .         .         .
          12800.  C        I    L R  E   M     .         .         .         .         .         .         .
          12850.  C        I    L R  E   M     .         .         .         .         .         .         .
          12900.  C        I    L R  E   M     .         .         .         .         .         .         .
          12950.  C        I    L R  E   M     .         .         .         .         .         .         .
97000.00  13000.  C        I    L R  E   M     .         .         .         .         .         .         .
          13050.  C        I     LR  E   M     .         .         .         .         .         .         .
          13100.  C        I     LR  E   M     .         .         .         .         .         .         .
          13150.  C        I     LR  E   M     .         .         .         .         .         .         .
          13200.  C        .I    LR  E   M     .         .         .         .         .         .         .
          13250.  C        .I    LR  E   M     .         .         .         .         .         .         .
          13300.  C        .I     L  E   M     .         .         .         .         .         .         .
          13350.  C        .I     L  E   M     .         .         .         .         .         .         .
          13400.  C        .I     LR E   M     .         .         .         .         .         .         .
          13450.  C        . I    LR E   M     .         .         .         .         .         .         .
97500.00  13500.  C        . I    LR E   M     .         .         .         .         .         .         .
          13550.  C        . I    LR E   M     .         .         .         .         .         .         .
          13600.  C        . I    LR WE  M     .         .         .         .         .         .         .
          13650.  C        . I    LR WE  M     .         .         .         .         .         .         .
          13700.  C        . I    LR WE  M     .         .         .         .         .         .         .
          13750.  C        . I    LR WE   M    .         .         .         .         .         .         .
          13800.  C        .I     L  WE   M    .         .         .         .         .         .         .
          13850.  C        .I     L  WE   M    .         .         .         .         .         .         .
          13900.  C        .I     L  WE   M    .         .         .         .         .         .         .
          13950.  C        .I     L  .E   M    .         .         .         .         .         .         .
98000.00  14000.  C        .I     L  .E   M    .         .         .         .         .         .         .
          14050.  C        . I    L  .E   M    .         .         .         .         .         .         .
          14100.  C        . I    LR .E   M    .         .         .         .         .         .         .
          14150.  C        . I    LR .E   M    .         .         .         .         .         .         .
          14200.  C        .  I   LR .E   M    .         .         .         .         .         .         .
          14250.  C        .  I   LR .E  M     .         .         .         .         .         .         .
          14300.  C        .  I   LR .E  M     .         .         .         .         .         .         .
98500.00  14350.  C        .   I  LR .E  M     .         .         .         .         .         .         .
          14400.  C        .  I   LR .E  M     .         .         .         .         .         .         .
          14450.  C        .  I   LR .E   M    .         .         .         .         .         .         .
          14500.  C        .  I   L  .E   M    .         .         .         .         .         .         .
          14550.  C        .  I   L  .E   M    .         .         .         .         .         .         .
98815.00  14600.  C        . I    L  WE   M    .         .         .         .         .         .         .
          14650.  C        .  I  LR  .E    M   .         .         .         .         .         .         .
          14700.  C        .  I  LR  .E     M  .         .         .         .         .         .         .
          14750.  C        .  I  LR  .E     M  .         .         .         .         .         .         .
99000.00  14800.  C        .   I LR  .E      M .         .         .         .         .         .         .
          14850.  C        .   I  L RWE    M   .         .         .         .         .         .         .
99080.00  14900.  C        .   I  L  WE    M   .         .         .         .         .         .         .
99167.00  14950.  C        .   I    LWE    M   .         .         .         .         .         .         .
          15000.  C        .   I    LWE    M   .         .         .         .         .         .         .
99266.00  15050.  C        .   I    L.WE   M   .         .         .         .         .         .         .
99267.00  15100.  C        .     I L .WE       .         .         .         .         .         .         .
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 99327.00 15150.  C          .     I L .WE       .         .         .         .         .         .         .         .
 99328.00 15200.  .          .        I RWELM    .         .         .         .         .         .         .         .
 99408.00 15250.  .          .        I R WEM    .         .         .         .         .         .         .         .
 99500.00 15300.  .          .        .IR  W E  L          .         .         .         .         .         .         .
          15350.  .          .        . IR  WEM . L        .         .         .         .         .         .         .
          15400.  .          .        .  I  CWE .   L      .         .         .         .         .         .         .
          15450.  .          .        .  IR  W E.     L    .         .         .         .         .         .         .
 99717.00 15500.  .          .        .   I   W E        L.         .         .         .         .         .         .
          15550.  .          .        .   IR   WME        .L        .         .         .         .         .         .
          15600.  .          .        .  I  R  CWE        . L       .         .         .         .         .         .
          15650.  .          .        .  I   R  W E       .   L     .         .         .         .         .         .
          15700.  .          .        .  I    R .W E      .     L   .         .         .         .         .         .
          15750.  .          .        . I      R.CW E     .      L  .         .         .         .         .         .
          15800.  .          .        . I       RMW  E    .        L.         .         .         .         .         .
          15850.  .          .        .I        .R W E    .         .L        .         .         .         .         .
          15900.  .          .        .I        .MR W E   .         . L       .         .         .         .         .
          15950.  .          .        .I        .M RW  E  .         .   L     .         .         .         .         .
100251.00 16000.  .          .        .I        .M R W E  .         .    L    .         .         .         .         .
          16050.  .          .        .I        .RM  W  E .       L .         .         .         .         .         .
          16100.  .          .        .I      R .  M W   E.L        .         .         .         .         .         .
          16150.  .          .        .I    R   .   MW   E.         .         .         .         .         .         .
          16200.  .          .        .I  R   L .   M W   E         .         .         .         .         .         .
100500.00 16250.  .          .        .I        .    MW   E         .         .         .         .         .         .
          16300.  C          .        . I       .     MW  .E       .         .         .         .         .         .
          16350.  C          .        .  I      .     M W . E      .         .         .         .         .         .
          16400.  C          .        .   I     .      M W.   E    .         .         .         .         .         .
          16450.  C          .        .    I    .       M .W   E   .         .         .         .         .         .
          16500.  C          .        .     I   .       M . W   E  .         .         .         .         .         .
          16550.  C          .        .      I  .        M.  W   E .         .         .         .         .         .
          16600.  C          .        .       I .         M   W   E .         .         .         .         .         .
          16650.  C          .        .        I.         M    W  E.         .         .         .         .         .
100951.00 16700.  C          .        .         I         .M    W  E         .         .         .         .         .
101000.00 16750.  C          .        .         . I       .   R   W.E M L     .         .         .         .         .
101048.00 16800.  .          .        .         . I       .   RC  W.E ML      .         .         .         .         .
          16850.  .          .        .         . I       .   RC  W.E  L      .         .         .         .         .
          16900.  .          .        .         . I       .   RC  W. E L      .         .         .         .         .
          16950.  .          .        .         . I       .   RC   W E L      .         .         .         .         .
          17000.  .          .        .         .  I      .   RC   W E ML     .         .         .         .         .
          17050.  .          .        .         .  I      .   R C  W E ML     .         .         .         .         .
          17100.  .          .        .         .  I      .   R C  W E ML     .         .         .         .         .
          17150.  .          .        .         .  I      .   R C  W E  L     .         .         .         .         .
          17200.  .          .        .         .   I     .   R C  .W E L     .         .         .         .         .
101500.00 17250.  .          .        .         .   I     .   R C  .W E ML    .         .         .         .         .
          17300.  C          .        .         .   I     .   R    .W E L     .         .         .         .         .
          17350.  C          .        .         .   I     .   R    .W E L     .         .         .         .         .
          17400.  C          .        .         .   I     .   R    .W E L     .         .         .         .         .
          17450.  C          .        .         .   I     .    R   . WELM     .         .         .         .         .
          17500.  C          .        .         .   I     .    R   . WELM     .         .         .         .         .
          17550.  C          .        .         .   I     .    R   . WELM     .         .         .         .         .
          17600.  C          .        .         .    I    .    R   . WELM     .         .         .         .         .
          17650.  C          .        .         .    I    .    R   .  WEM     .         .         .         .         .
          17700.  C          .        .         .    I    .     R  .  WEM     .         .         .         .         .
102000.00 17750.  C          .        .         .    I    .     R  .  WEM     .         .         .         .         .
          17800.  C          .        .         .    I    .     R  .  WEM     .         .         .         .         .
          17850.  C          .        .         .    I    .     R  .  WEM     .         .         .         .         .
          17900.  C          .        .         .    I    .     R  . LWEM     .         .         .         .         .
          17950.  C          .        .         .     I   .     R  . LWEM     .         .         .         .         .
          18000.  C          .        .         .     I   .     R  . LWEM     .         .         .         .         .
          18050.  C          .        .         .     I   .     R  . L EM     .         .         .         .         .
          18100.  C          .        .         .     I   .     R  . L EM     .         .         .         .         .
          18150.  C          .        .         .     I   .     R  . L EM     .         .         .         .         .
          18200.  C          .        .         .     I   .     R  . L EM     .         .         .         .         .
102500.00 18250.  C          .        .         .      I  .     R  .L  EM     .         .         .         .         .
          18300.  C          .        .         .      I  .    R   . L EM     .         .         .         .         .
          18350.  C          .        .         .      I  .    R   . L WE     .         .         .         .         .
          18400.  C          .        .         .      I  .    R   . L WE     .         .         .         .         .
          18450.  C          .        .         .      I  .    R   . L WE     .         .         .         .         .
          18500.  C          .        .         .      I  .    R   .  LWE     .         .         .         .         .
          18550.  C          .        .         .      I  .    R   .  LWE     .         .         .         .         .
          18600.  C          .        .         .      I  .   R    .  LWE     .         .         .         .         .
          18650.  C          .        .         .      I  .   R    .   WE     .         .         .         .         .
          18700.  C          .        .         .      I  .   R    .   LE     .         .         .         .         .
103000.00 18750.  C          .        .         .      I  .   R    .   LE     .         .         .         .         .
          18800.  C          .        .         .      I  .   R    .   LE     .         .         .         .         .
          18850.  C          .        .         .       I .   R    .   LE     .         .         .         .         .
          18900.  C          .        .         .       I .   R    .  MLE     .         .         .         .         .
          18950.  C          .        .         .       I .   R    .  MLE     .         .         .         .         .
          19000.  C          .        .         .       I .    R   .  MLE     .         .         .         .         .
          19050.  C          .        .         .        I.    R   .  MLWE    .         .         .         .         .
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           19100.  C     .     .     .     I.    R   .  MLWE  .     .     .     .     .
           19150.  C     .     .     .     I.    R   .  M WE  .     .     .     .     .
103500.00  19200.  C     .     .     .     I.    R   . M  WE  .     .     .     .     .
           19250.  C     .     .     .     I.    R   .  M WE  .     .     .     .     .
           19300.  C     .     .     .     I.    R   .  MLWE  .     .     .     .     .
           19350.  C     .     .     .     I.    R   .  ML E  .     .     .     .     .
           19400.  C     .     .     .     I.    R   .  ML E  .     .     .     .     .
           19450.  C     .     .     .     I.    R   .  ML E  .     .     .     .     .
           19500.  C     .     .     .     I.    R   .  ML E  .     .     .     .     .
           19550.  C     .     .     .     I.    R   .  ML E  .     .     .     .     .
           19600.  C     .     .     .     I.    R   .  ML E  .     .     .     .     .
           19650.  C     .     .     .     I.    R   .  ML E  .     .     .     .     .
104000.00  19700.  C     .     .     .     I.    R   .  ML E  .     .     .     .     .
           19750.  C     .     .     .     I.    R   .   L E  .     .     .     .     .
           19800.  C     .     .     .     I.    R   .   L WE .     .     .     .     .
           19850.  C     .     .     .      I     R  .   L WE .     .     .     .     .
           19900.  C     .     .     .      I     R  .   MLWE .     .     .     .     .
           19950.  C     .     .     .      I     R  .   MLWE .     .     .     .     .
           20000.  C     .     .     .      I     R  .   MLWE .     .     .     .     .
           20050.  C     .     .     .      I     R  .   MLWE .     .     .     .     .
           20100.  C     .     .     .      I     R  .    LWE .     .     .     .     .
           20150.  C     .     .     .      I     R  .    L E .     .     .     .     .
104500.00  20200.  C     .     .     .      I      R .    MLE .     .     .     .     .
           20250.  C     .     .     .      I      R .   M LE .     .     .     .     .
           20300.  C     .     .     .      I     R  .   M LE .     .     .     .     .
           20350.  C     .     .     .      I     R  .  M  LE .     .     .     .     .
           20400.  C     .     .     .      I     R  .  M  LE .     .     .     .     .
           20450.  C     .     .     .      I     R  .  M  LE .     .     .     .     .
104818.00  20500.  C     .     .     .      I     R  . M   LE .     .     .     .     .
           20550.  C     .     .     .      I     R  . M   LE .     .     .     .     .
           20600.  C     .     .     .      I     R  . M    WE .     .     .     .     .
           20650.  C     .     .     .      I     R  . M    WE .     .     .     .     .
105000.00  20700.  C     .     .     .      I      R .M     WE .     .     .     .     .
           20750.  C     .     .     .      I      R . M    WE .     .     .     .     .
           20800.  C     .     .     .     .I       R. M   LWE .     .     .     .     .
           20850.  C     .     .     .     .I        R  M  L E .     .     .     .     .
           20900.  C     .     .     .     .I        R  M L  E .     .     .     .     .
           20950.  C     .     .     .     . I       .R  ML  E .     .     .     .     .
105294.00  21000.  C     .     .     .     . I       . R ML  E .     .     .     .     .
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T1
T2
T3

J1	ICHECK	INQ	NINV	IDIR	STRT	METRIC	HVINS	Q	WSEL	FQ
		6			.06				1249.96	

J2	NPROF	IPLOT	PRFVS	XSECV	XSECH	FN	ALLDC	IBW	CHNIM	ITRACE
	5									

PROFILE FOR STREAM

PLOTTED POINTS (BY PRIORITY) E-ENERGY,W-WATER SURFACE,I-INVERT,C-CRITICAL W.S.,L-LEFT BANK,R-RIGHT BANK,M-LOWER END STA

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ELEVATION  1246.     1251.     1256.     1261.     1266.     1271.     1276.     1281.     1286.     1291.
   SECNO   CUMDIS

84000.00      0.  .  I   W E.   M     .         .         .         .         .         .         .         .
             50.  .  I    WELM       .         .         .         .         .         .         .         .
            100.  .  I    W E        .         .         .         .         .         .         .         .
            150.  .  IM   WRE        .         .         .         .         .         .         .         .
            200.  .M I    W RE       .         .         .         .         .         .         .         .
            250.  M  I     WRE       .         .         .         .         .         .         .         .
            300.  M  I     W.RE      .         .         .         .         .         .         .         .
            350.  M  I     W.RE      .         .         .         .         .         .         .         .
            400.  M  I      W E      .         .         .         .         .         .         .         .
            450.  M  I      W RE     .         .         .         .         .         .         .         .
84500.00    500.  M  I      W  E     .         .         .         .         .         .         .         .
            550.  M  I      W LE     .         .         .         .         .         .         .         .
            600.  M  I      CWLE     .         .         .         .         .         .         .         .
            650.  M  I      CW RE    .         .         .         .         .         .         .         .
            700.  M  I      CLWRE    .         .         .         .         .         .         .         .
            750.  M  I      C WRE    .         .         .         .         .         .         .         .
            800.  .M I      C W E    .         .         .         .         .         .         .         .
            850.  .  I M   LC RWE    .         .         .         .         .         .         .         .
            900.  .   I_  MLC RWE    .         .         .         .         .         .         .         .
            950.  .   I   L CMRWE    .         .         .         .         .         .         .         .
85000.00   1000.  .   I   L C R E    .         .         .         .         .         .         .         .
           1050.  .   I   L C R E    .         .         .         .         .         .         .         .
           1100.  .   I   L C R E    .         .         .         .         .         .         .         .
           1150.  .   I   L CR  E    .         .         .         .         .         .         .         .
           1200.  .   I   L CR  E    .         .         .         .         .         .         .         .
           1250.  .   I   L CR  EM   .         .         .         .         .         .         .         .
           1300.  .   I   L CR  EM   .         .         .         .         .         .         .         .
           1350.  .   I   L CR  EM   .         .         .         .         .         .         .         .
           1400.  .   I   L C   EM   .         .         .         .         .         .         .         .
           1450.  .   I   L C   EM   .         .         .         .         .         .         .         .
85500.00   1500.  .   I   L C   WE   .         .         .         .         .         .         .         .
           1550.  C   I   L R   WE   .         .         .         .         .         .         .         .
           1600.  C   I   L R   WE   .         .         .         .         .         .         .         .
           1650.  C   I   L .R  WE   .         .         .         .         .         .         .         .
           1700.  C   I   L .R  WE   .         .         .         .         .         .         .         .
           1750.  C   I   L .R  WE   .         .         .         .         .         .         .         .
           1800.  C   I   L .R  WE   .         .         .         .         .         .         .         .
           1850.  C   I   L .R  WE   .         .         .         .         .         .         .         .
           1900.  C   I  L  . R WE   .         .         .         .         .         .         .         .
           1950.  C   I  L  . R WE   .         .         .         .         .         .         .         .
           2000.  C   I  L  . R WE   .         .         .         .         .         .         .         .
86024.00   2050.  C   I  L  . R WE   .         .         .         .         .         .         .         .
           2100.  C   I   L . R WE   .         .         .         .         .         .         .         .
           2150.  C  I    L .R  WE   .         .         .         .         .         .         .         .
           2200.  C  I     L.R  WE   .         .         .         .         .         .         .         .
           2250.  C I       LR  WE   .         .         .         .         .         .         .         .
           2300.  C I       L   WE   .         .         .         .         .         .         .         .
           2350.  CI        RL  WE   .         .         .         .         .         .         .         .
           2400.  I         RL  WE   .         .         .         .         .         .         .         .
86415.00   2450.  I        R.C  WE   .         .         .         .         .         .         .         .
           2500.  I        R. L  E   .         .         .         .         .         .         .         .
           2550.  I        R. L  E   .         .         .         .         .         .         .         .
           2600.  I        R. L  E   .         .         .         .         .         .         .         .
           2650.  I        R. L  E   .         .         .         .         .         .         .         .
           2700.  I        R.  L WE  .         .         .         .         .         .         .         .
           2750.  I        R.  L WE  .         .         .         .         .         .         .         .
           2800.  I        R.  L WE  .         .         .         .         .         .         .         .
           2850.  I        R.  L WE  .         .         .         .         .         .         .         .
           2900.  CI       R.   LWE  .         .         .         .         .         .         .         .
           2950.  CI       R.   LWE  .         .         .         .         .         .         .         .
87000.00   3000.  CI       R.   LWE  .         .         .         .         .         .         .         .
           3050.  CI        R   LWE  .         .         .         .         .         .         .         .
           3100.  CI        R   LWE  .         .         .         .         .         .         .         .
           3150.  C I       R   LWE  .         .         .         .         .         .         .         .
           3200.  C I       R   LWE  .         .         .         .         .         .         .         .
           3250.  C I       .R  LWE  .         .         .         .         .         .         .         .
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          3300.  C  I      .R   W E  .          .          .          .          .          .          .          .
          3350.  C  I      .R   LWE  .          .          .          .          .          .          .          .
          3400.  C   I     .R   LWE  .          .          .          .          .          .          .          .
          3450.  C   I     . R  LWE  .          .          .          .          .          .          .          .
87500.00  3500.  C   I     . R  LWE  .          .          .          .          .          .          .          .
          3550.  C   I     . R  LWE  .          .          .          .          .          .          .          .
          3600.  C   I     .R   LWE  .          .          .          .          .          .          .          .
          3650.  C   I     .R   LWE  .          .          .          .          .          .          .          .
          3700.  C   I     .R   LWE  .          .          .          .          .          .          .          .
          3750.  C   I     .R  MLWE  .          .          .          .          .          .          .          .
          3800.  C  I      .R  MLWE  .          .          .          .          .          .          .          .
          3850.  C  I      R   L WE  .          .          .          .          .          .          .          .
          3900.  C  I      R  ML WE  .          .          .          .          .          .          .          .
          3950.  C  I      R  ML  E  .          .          .          .          .          .          .          .
88000.00  4000.  C  I      R  ML  E  .          .          .          .          .          .          .          .
          4050.  C  I      R  ML  E  .          .          .          .          .          .          .          .
          4100.  C  I      R  ML  WE .          .          .          .          .          .          .          .
          4150.  C  I      R  ML  WE .          .          .          .          .          .          .          .
          4200.  C  I      R   L  WE .          .          .          .          .          .          .          .
          4250.  C  I      R   L  WE .          .          .          .          .          .          .          .
          4300.  C  I      R   L  WE .          .          .          .          .          .          .          .
          4350.  C I       R   L  WE .          .          .          .          .          .          .          .
          4400.  C I       R  LM  WE .          .          .          .          .          .          .          .
          4450.  C I       R  L M WE .          .          .          .          .          .          .          .
88500.00  4500.  C I       R  L M WE .          .          .          .          .          .          .          .
          4550.  C I       R  L M WE .          .          .          .          .          .          .          .
          4600.  C  I     R.  L  MWE .          .          .          .          .          .          .          .
          4650.  C  I     R.  L  MWE .          .          .          .          .          .          .          .
          4700.  C  I     R.  L  MWE .          .          .          .          .          .          .          .
          4750.  C  I     R.  L   WE .          .          .          .          .          .          .          .
          4800.  C  I     R.  L   ME .          .          .          .          .          .          .          .
          4850.  C  I     R.  L   ME .          .          .          .          .          .          .          .
          4900.  C  I     R. L     E .          .          .          .          .          .          .          .
          4950.  C  I     R. L     E .          .          .          .          .          .          .          .
89000.00  5000.  C   I    R. L     E .          .          .          .          .          .          .          .
          5050.  C   I    R. L     EM.          .          .          .          .          .          .          .
          5100.  C   I    R. L     EM.          .          .          .          .          .          .          .
          5150.  C    I   R. L     EM.          .          .          .          .          .          .          .
          5200.  C    I    R L     E M          .          .          .          .          .          .          .
          5250.  C    I    R L     E M          .          .          .          .          .          .          .
          5300.  C    I    R L     E M          .          .          .          .          .          .          .
          5350.  C     I   .RL     E M          .          .          .          .          .          .          .
          5400.  C     I   .RL     E .M         .          .          .          .          .          .          .
          5450.  C     I   .RL     E .M         .          .          .          .          .          .          .
89545.00  5500.  C     I   .RL     E .M         .          .          .          .          .          .          .
          5550.  C     I   .RL     E .M         .          .          .          .          .          .          .
          5600.  C     I   .RL     E M          .          .          .          .          .          .          .
          5650.  C    I    .RL     E M          .          .          .          .          .          .          .
          5700.  C    I    .RL     E M          .          .          .          .          .          .          .
          5750.  C    I    .R L    WEM          .          .          .          .          .          .          .
          5800.  C    I    .R L    WEM          .          .          .          .          .          .          .
          5850.  C   I     .R L    WEM          .          .          .          .          .          .          .
          5900.  C   I     .R L    WEM          .          .          .          .          .          .          .
          5950.  C   I     .R L    WE.          .          .          .          .          .          .          .
90000.00  6000.  C  I      .R  L   WE.          .          .          .          .          .          .          .
          6050.  C  I      .R  L   WE.          .          .          .          .          .          .          .
          6100.  C  I      .R  L   WEM          .          .          .          .          .          .          .
          6150.  C  I      .R  L   WEM          .          .          .          .          .          .          .
          6200.  C I       .R   L  WEM          .          .          .          .          .          .          .
          6250.  C I       .R   L  WEM          .          .          .          .          .          .          .
          6300.  C I       .R   L  WE.M         .          .          .          .          .          .          .
          6350.  C I       .R   L  WE.M         .          .          .          .          .          .          .
          6400.  C I       .R   L   E.M         .          .          .          .          .          .          .
          6450.  C I       .R    L  E. M        .          .          .          .          .          .          .
90500.00  6500.  C I       R     L  E. M        .          .          .          .          .          .          .
          6550.  C I       R     L  E. M        .          .          .          .          .          .          .
          6600.  C I       R     L WE. M        .          .          .          .          .          .          .
          6650.  C I       R     L WE. M        .          .          .          .          .          .          .
          6700.  C  I      R     L WE.  M       .          .          .          .          .          .          .
          6750.  C  I      R     L WE.  M       .          .          .          .          .          .          .
          6800.  C  I      R      LWE.  M       .          .          .          .          .          .          .
          6850.  C  I      R      LWE.  M       .          .          .          .          .          .          .
          6900.  C   I     R      LWE.  M       .          .          .          .          .          .          .
          6950.  C   I     R      LWE.  M       .          .          .          .          .          .          .
91000.00  7000.  C   I     R      LWE.   M       .          .          .          .          .          .          .
          7050.  C   I     R      LWE.   M       .          .          .          .          .          .          .
          7100.  C   I     R      LWE.  M        .          .          .          .          .          .          .
          7150.  C   I     R      LWE.  M        .          .          .          .          .          .          .
          7200.  C   I     R      L E.  M        .          .          .          .          .          .          .
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          7250.  C  I     R      L E.  M      .         .         .         .         .         .         .         .
          7300.  C  I     R     L  E.  M      .         .         .         .         .         .         .         .
          7350.  C  I     R     L  E.  M      .         .         .         .         .         .         .         .
          7400.  C  I     R     L  E.  M      .         .         .         .         .         .         .         .
          7450.  C  I     R     L  E.  M      .         .         .         .         .         .         .         .
91500.00  7500.  C  I     R     L  WE  M      .         .         .         .         .         .         .         .
          7550.  C  I     R     L  WE  M      .         .         .         .         .         .         .         .
          7600.  C  I     R     L  WE  M      .         .         .         .         .         .         .         .
          7650.  C  I     .R    L  WE  M      .         .         .         .         .         .         .         .
          7700.  C   I    .R    L  WE   M     .         .         .         .         .         .         .         .
          7750.  C   I    .R    L  WE   M     .         .         .         .         .         .         .         .
          7800.  C   I    .R   L   WE   M     .         .         .         .         .         .         .         .
          7850.  C   I    . R  L   WE   M     .         .         .         .         .         .         .         .
          7900.  C    I   . R  L   WE   M     .         .         .         .         .         .         .         .
          7950.  C    I   . R  L   WE   M     .         .         .         .         .         .         .         .
92000.00  8000.  C    I   . R  L   WE   M     .         .         .         .         .         .         .         .
          8050.  C    I   . R  L   WE   M     .         .         .         .         .         .         .         .
          8100.  C    I   . R   L  WE   M     .         .         .         .         .         .         .         .
          8150.  C    I   . R   L  WE   M     .         .         .         .         .         .         .         .
          8200.  C    I   . R   L  WE   M     .         .         .         .         .         .         .         .
          8250.  C    I   . R   L  WE    M    .         .         .         .         .         .         .         .
          8300.  C    I   . R   L  WE    M    .         .         .         .         .         .         .         .
          8350.  C   I    . R   L  WE    M    .         .         .         .         .         .         .         .
          8400.  C   I    . R   L  WE    M    .         .         .         .         .         .         .         .
          8450.  C   I    . R   L   E    M    .         .         .         .         .         .         .         .
92500.00  8500.  C   I    . R    L  E    M    .         .         .         .         .         .         .         .
          8550.  C   I    . R    L  E    M    .         .         .         .         .         .         .         .
          8600.  C    I   . R    L  E    M    .         .         .         .         .         .         .         .
          8650.  C    I   . R    L WE    M    .         .         .         .         .         .         .         .
          8700.  C    I   .  R   L WE    M    .         .         .         .         .         .         .         .
          8750.  C    I   .  R   L WE    M    .         .         .         .         .         .         .         .
          8800.  C    I   .  R    LWE    M    .         .         .         .         .         .         .         .
          8850.  C    I   .  R    LWE     M   .         .         .         .         .         .         .         .
          8900.  C    I   .   R   LWE     M   .         .         .         .         .         .         .         .
          8950.  C     I  .   R   LWE     M   .         .         .         .         .         .         .         .
93000.00  9000.  C     I  .   R   LWE     M   .         .         .         .         .         .         .         .
          9050.  C      I .   R   LWE     M   .         .         .         .         .         .         .         .
          9100.  C      I .   R   LWE    M    .         .         .         .         .         .         .         .
          9150.  C       I.   R  L WE    M    .         .         .         .         .         .         .         .
          9200.  C        I   R  LW E    M    .         .         .         .         .         .         .         .
          9250.  C        .I  R  LWE.    M    .         .         .         .         .         .         .         .
          9300.  C        . I  RL WE.    M    .         .         .         .         .         .         .         .
          9350.  C        . I  RLW E.    M    .         .         .         .         .         .         .         .
          9400.  C        .  I RLW E.   M     .         .         .         .         .         .         .         .
93574.00  9450.  .        .   IL W E.   M     .         .         .         .         .         .         .         .
          9500.  .        .  I L W E.   M     .         .         .         .         .         .         .         .
          9550.  .        .  I L W E.   M     .         .         .         .         .         .         .         .
          9600.  .        . I  L CWE.  M      .         .         .         .         .         .         .         .
          9650.  .        . I  LC WE.  M      .         .         .         .         .         .         .         .
          9700.  .        .I   LC WE.  M      .         .         .         .         .         .         .         .
          9750.  .        I    LC WE.  M      .         .         .         .         .         .         .         .
          9800.  .        I    LC WE. M       .         .         .         .         .         .         .         .
          9850.  .       I.    LC WE. M       .         .         .         .         .         .         .         .
          9900.  .       I.    LC  E. M       .         .         .         .         .         .         .         .
          9950.  .      I .   LRC  E.M        .         .         .         .         .         .         .         .
94000.00 10000.  .      I .   LC   WEM        .         .         .         .         .         .         .         .
         10050.  C      I .   LR   WEM        .         .         .         .         .         .         .         .
         10100.  C      I .    LR  WE M       .         .         .         .         .         .         .         .
         10150.  C      I .    LR  WE M       .         .         .         .         .         .         .         .
         10200.  C      I .    LR  WE  M      .         .         .         .         .         .         .         .
         10250.  C      I .    LR  WE  M      .         .         .         .         .         .         .         .
         10300.  C      I .    L R WE   M     .         .         .         .         .         .         .         .
         10350.  C       I.    L R WE   M     .         .         .         .         .         .         .         .
         10400.  C       I.     LR WE   M     .         .         .         .         .         .         .         .
         10450.  C       I.     LR WE    M    .         .         .         .         .         .         .         .
94500.00 10500.  C       I.     L R E    M    .         .         .         .         .         .         .         .
         10550.  C       I.     L R E    M    .         .         .         .         .         .         .         .
         10600.  C       I.     L R E    M    .         .         .         .         .         .         .         .
         10650.  C       I.      LR E    M    .         .         .         .         .         .         .         .
         10700.  C       I.      LR E    M    .         .         .         .         .         .         .         .
         10750.  C       I.      LR E    M    .         .         .         .         .         .         .         .
         10800.  C       I.      LR E    M    .         .         .         .         .         .         .         .
         10850.  C       I.      LR E    M    .         .         .         .         .         .         .         .
         10900.  C       I.       L E     M   .         .         .         .         .         .         .         .
         10950.  C       I.       L WE    M   .         .         .         .         .         .         .         .
95000.00 11000.  C       I.       L WE    M   .         .         .         .         .         .         .         .
         11050.  C       I.       L WE   M    .         .         .         .         .         .         .         .
         11100.  C       I.       LRWE   M    .         .         .         .         .         .         .         .
         11150.  C       I.       LRWE   M    .         .         .         .         .         .         .         .
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          11200.  C        I.      L RWE   M    .         .         .         .         .         .         .         .
          11250.  C        I.      L RWE  M     .         .         .         .         .         .         .         .
          11300.  C        I.      L RWE  M     .         .         .         .         .         .         .         .
          11350.  C        I.      L  WE  M     .         .         .         .         .         .         .         .
          11400.  C        I.      L  WE  M     .         .         .         .         .         .         .         .
          11450.  C        I.     L   RE M      .         .         .         .         .         .         .         .
95500.00  11500.  C        I.     L   RE M      .         .         .         .         .         .         .         .
          11550.  C        I.     L   RE M      .         .         .         .         .         .         .         .
          11600.  C        I.     L   RE M      .         .         .         .         .         .         .         .
          11650.  C        I.     L  R.E M      .         .         .         .         .         .         .         .
          11700.  C        I.     L  R.E M      .         .         .         .         .         .         .         .
          11750.  C        I.     L  R.E M      .         .         .         .         .         .         .         .
          11800.  C        I.     L R .E M      .         .         .         .         .         .         .         .
          11850.  C        I.     L R .E  M     .         .         .         .         .         .         .         .
          11900.  C        I.     LR  .WE M     .         .         .         .         .         .         .         .
          11950.  C        I.     LR  .WE M     .         .         .         .         .         .         .         .
96000.00  12000.  C        I.     LR  .WE M     .         .         .         .         .         .         .         .
          12050.  C        I.     LR  .WE M     .         .         .         .         .         .         .         .
          12100.  C        I.     LR  .WE M     .         .         .         .         .         .         .         .
          12150.  C        I.     LR  .WE M     .         .         .         .         .         .         .         .
          12200.  C        I.    L R  .WE M     .         .         .         .         .         .         .         .
          12250.  C         I    L R  .WE M     .         .         .         .         .         .         .         .
          12300.  C         I    L R  .WE M     .         .         .         .         .         .         .         .
          12350.  C         I    L R  .WE M     .         .         .         .         .         .         .         .
          12400.  C         I    L R  .WE M     .         .         .         .         .         .         .         .
          12450.  C         I    L R  . E M     .         .         .         .         .         .         .         .
96500.00  12500.  C         I    L R  . E M     .         .         .         .         .         .         .         .
          12550.  C         I    L R  . E M     .         .         .         .         .         .         .         .
          12600.  C         I    L R  . E M     .         .         .         .         .         .         .         .
          12650.  C         I    L R  . E M     .         .         .         .         .         .         .         .
          12700.  C         I    L R  . E M     .         .         .         .         .         .         .         .
          12750.  C         I    L R  . E M     .         .         .         .         .         .         .         .
          12800.  C         I    L R  . E M     .         .         .         .         .         .         .         .
          12850.  C         I    L R  . E M     .         .         .         .         .         .         .         .
          12900.  C         I    L R  . E M     .         .         .         .         .         .         .         .
          12950.  C         I    L R  . E M     .         .         .         .         .         .         .         .
97000.00  13000.  C         I    L R  . E M     .         .         .         .         .         .         .         .
          13050.  C         I     LR  . E M     .         .         .         .         .         .         .         .
          13100.  C         I     LR  . E M     .         .         .         .         .         .         .         .
          13150.  C         I     LR  . E M     .         .         .         .         .         .         .         .
          13200.  C        .I     LR  . WEM     .         .         .         .         .         .         .         .
          13250.  C        .I     LR  . WEM     .         .         .         .         .         .         .         .
          13300.  C        .I      L  . WEM     .         .         .         .         .         .         .         .
          13350.  C        .I      L  . WEM     .         .         .         .         .         .         .         .
          13400.  C        .I      LR . WEM     .         .         .         .         .         .         .         .
          13450.  C        . I     LR . WEM     .         .         .         .         .         .         .         .
97500.00  13500.  C        . I     LR . WEM     .         .         .         .         .         .         .         .
          13550.  C        . I     LR . WEM     .         .         .         .         .         .         .         .
          13600.  C        . I     LR . WEM     .         .         .         .         .         .         .         .
          13650.  C        . I     LR . WEM     .         .         .         .         .         .         .         .
          13700.  C        . I     LR . WEM     .         .         .         .         .         .         .         .
          13750.  C        . I     LR .  E M    .         .         .         .         .         .         .         .
          13800.  C        .I      L  .  E M    .         .         .         .         .         .         .         .
          13850.  C        .I      L  .  E M    .         .         .         .         .         .         .         .
          13900.  C        .I      L  .  E M    .         .         .         .         .         .         .         .
          13950.  C        .I      L  .  E M    .         .         .         .         .         .         .         .
98000.00  14000.  C        .I      L  .  E M    .         .         .         .         .         .         .         .
          14050.  C        .I      L  .  E M    .         .         .         .         .         .         .         .
          14100.  C         I      LR .  E M    .         .         .         .         .         .         .         .
          14150.  C        I.      LR .  E M    .         .         .         .         .         .         .         .
          14200.  C       I .      LR .  E M    .         .         .         .         .         .         .         .
          14250.  C       I .      LR .  EM     .         .         .         .         .         .         .         .
          14300.  C      I  .      LR .  EM     .         .         .         .         .         .         .         .
98500.00  14350.  C     I   .      LR .  EM     .         .         .         .         .         .         .         .
          14400.  C       I .      LR .  EM     .         .         .         .         .         .         .         .
          14450.  C        I.      LR .  E M    .         .         .         .         .         .         .         .
          14500.  C         I      L  .  E M    .         .         .         .         .         .         .         .
          14550.  C        .I      L  .  E M    .         .         .         .         .         .         .         .
98815.00  14600.  C        . I     L  .  E M    .         .         .         .         .         .         .         .
          14650.  C        .  I  LR  .  E  M     .         .         .         .         .         .         .         .
          14700.  C        .  I  LR  .  WE  M    .         .         .         .         .         .         .         .
          14750.  C        .  I  LR  .  WE  M    .         .         .         .         .         .         .         .
99000.00  14800.  C        .   I LR  .  WE   M   .         .         .         .         .         .         .         .
          14850.  C        .   I  L R.  WE M     .         .         .         .         .         .         .         .
99080.00  14900.  C        .   I  L  .R WE M     .         .         .         .         .         .         .         .
99167.00  14950.  .        .       IL.RW E M     .         .         .         .         .         .         .         .
          15000.  .        .       IL.RW E M     .         .         .         .         .         .         .         .
99266.00  15050.  .        .       IL.RCWE M     .         .         .         .         .         .         .         .
99267.00  15100.  C        .     I L .R  E       .         .         .         .         .         .         .         .
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 99327.00 15150.  C          .     I L .R  E     .         .         .         .         .         .         .         .
 99328.00 15200.  .          .        I R  WE    .         .         .         .         .         .         .         .
 99408.00 15250.  .          .        I R  WE    .         .         .         .         .         .         .         .
 99500.00 15300.  .          .        .IR    W EL         .         .         .         .         .         .         .
          15350.  .          .        . IR    W E L       .         .         .         .         .         .         .
          15400.  .          .        .  I    W .E  L     .         .         .         .         .         .         .
          15450.  .          .        .  IR    W. E   L   .         .         .         .         .         .         .
 99717.00 15500.  .          .        .   I     W  E     L.         .         .         .         .         .         .
          15550.  .          .        .   IR    MW  E     .L        .         .         .         .         .         .
          15600.  .          .        .  I  R   M W  E    . L       .         .         .         .         .         .
          15650.  .          .        .  I   R  M  W  E   .   L     .         .         .         .         .         .
          15700.  .          .        .  I    R .M W   E  .     L   .         .         .         .         .         .
          15750.  .          .        . I      R.M  W   E .      L .         .         .         .         .         .
          15800.  .          .        . I       RM   W   E.        L.         .         .         .         .         .
          15850.  .          .        .I        .R    W   E         .L        .         .         .         .         .
          15900.  .          .        .I        .MR    W  .E        . L       .         .         .         .         .
          15950.  .          .        .I        .M R    W . E       .   L     .         .         .         .         .
100251.00 16000.  .          .        .I        .M R    W . E       .    L    .         .         .         .         .
          16050.  .          .        .I        .RM      W.  E    L .         .         .         .         .         .
          16100.  .          .        .I      R .  M     W.L  E     .         .         .         .         .         .
          16150.  .          .        .I    R   .  ML    W    E     .         .         .         .         .         .
          16200.  .          .        .I  R   L .  M     .W    E    .         .         .         .         .         .
100500.00 16250.  .          .        .I        .   M    .W     E  .         .         .         .         .         .
          16300.  .          .        . I       .    M   .  W    E .         .         .         .         .         .
          16350.  .          .        .  I      .    M   .   W    E          .         .         .         .         .
          16400.  .          .        .   I     .     M  .    W    .E        .         .         .         .         .
          16450.  .          .        .    I    .      M .     W   . E       .         .         .         .         .
          16500.  .          .        .     I   .      M .       W . E       .         .         .         .         .
          16550.  .          .        .      I  .       M.        W.   E     .         .         .         .         .
          16600.  .          .        .       I .        M         W     E   .         .         .         .         .
          16650.  .          .        .        I.        M         .W     E  .         .         .         .         .
100951.00 16700.  .          .        .         I        .M        .  W    E .         .         .         .         .
101000.00 16750.  C          .        .          . I      .    R   .  M L   WE         .         .         .         .
101048.00 16800.  C          .        .          . I      .    R   .  ML    WE         .         .         .         .
          16850.  C          .        .          . I      .    R   .   L    WE         .         .         .         .
          16900.  C          .        .          . I      .    R   .   L    WE         .         .         .         .
          16950.  C          .        .          . I      .    R   .   L    WE         .         .         .         .
          17000.  C          .        .          .  I     .    R   .   ML   WE         .         .         .         .
          17050.  C          .        .          .  I     .    R   .   ML   WE         .         .         .         .
          17100.  C          .        .          .  I     .    R   .   ML   WE         .         .         .         .
          17150.  C          .        .          .  I     .    R   .    L   WE         .         .         .         .
          17200.  C          .        .          .   I    .    R   .    L   WE         .         .         .         .
101500.00 17250.  C          .        .          .   I    .    R   .    ML  WE         .         .         .         .
          17300.  C          .        .          .   I    .    R   .    L   WE         .         .         .         .
          17350.  C          .        .          .   I    .    R   .    L   WE         .         .         .         .
          17400.  C          .        .          .   I    .    R   .    L   WE         .         .         .         .
          17450.  C          .        .          .   I    .     R  .   LM    E         .         .         .         .
          17500.  C          .        .          .   I    .     R  .   LM    E         .         .         .         .
          17550.  C          .        .          .   I    .     R  .   LM    E         .         .         .         .
          17600.  C          .        .          .    I   .     R  .   LM    E         .         .         .         .
          17650.  C          .        .          .    I   .     R  .  L M    E         .         .         .         .
          17700.  C          .        .          .    I   .      R .  L M    E         .         .         .         .
102000.00 17750.  C          .        .          .    I   .      R .  L M    E         .         .         .         .
          17800.  C          .        .          .    I   .      R .  L M    E         .         .         .         .
          17850.  C          .        .          .    I   .      R .  L M    E         .         .         .         .
          17900.  C          .        .          .    I   .      R . L  M    E         .         .         .         .
          17950.  C          .        .          .     I  .      R . L  M    E         .         .         .         .
          18000.  C          .        .          .     I  .      R . L  M    E         .         .         .         .
          18050.  C          .        .          .     I  .      R . L  M    E         .         .         .         .
          18100.  C          .        .          .     I  .      R . L  M    E         .         .         .         .
          18150.  C          .        .          .     I  .      R . L  M    E         .         .         .         .
          18200.  C          .        .          .     I  .      R . L  M    E         .         .         .         .
102500.00 18250.  C          .        .          .      I .      R .L   M    E         .         .         .         .
          18300.  C          .        .          .      I .     R  . L  M    E         .         .         .         .
          18350.  C          .        .          .      I .     R  . L  M    E         .         .         .         .
          18400.  C          .        .          .      I .     R  . L  M    E         .         .         .         .
          18450.  C          .        .          .      I .     R  . L  M    E         .         .         .         .
          18500.  C          .        .          .      I .     R  .  L M    E         .         .         .         .
          18550.  C          .        .          .      I .     R  .  LM     E         .         .         .         .
          18600.  C          .        .          .      I .    R   .  LM     E         .         .         .         .
          18650.  C          .        .          .      I .    R   .   L     E         .         .         .         .
          18700.  C          .        .          .      I .    R   .   L     E         .         .         .         .
103000.00 18750.  C          .        .          .      I .    R   .   L     E         .         .         .         .
          18800.  C          .        .          .      I .    R   .   L     E         .         .         .         .
          18850.  C          .        .          .       I .   R   .   L     E         .         .         .         .
          18900.  C          .        .          .       I .   R   .  ML     E         .         .         .         .
          18950.  C          .        .          .       I .   R   .  ML     WE        .         .         .         .
          19000.  C          .        .          .       I .    R  .  ML     WE        .         .         .         .
          19050.  C          .        .          .        I.    R  .  ML     WE        .         .         .         .
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           19100.  C     .     .     .     I.    R   .  ML    WE    .     .     .     .
           19150.  C     .     .     .     I.    R   .  M L   WE    .     .     .     .
103500.00  19200.  C     .     .     .     I.    R   . M  L   WE    .     .     .     .
           19250.  C     .     .     .     I.    R   .  M L   WE    .     .     .     .
           19300.  C     .     .     .     I.    R   .  ML    WE    .     .     .     .
           19350.  C     .     .     .     I.    R   .  ML    WE    .     .     .     .
           19400.  C     .     .     .     I.    R   .  ML    WE    .     .     .     .
           19450.  C     .     .     .     I.    R   .  ML    .E    .     .     .     .
           19500.  C     .     .     .     I.    R   .  ML    .E    .     .     .     .
           19550.  C     .     .     .     I.    R   .  ML    .E    .     .     .     .
           19600.  C     .     .     .     I.    R   .  ML    .E    .     .     .     .
           19650.  C     .     .     .     I.    R   .  ML    .E    .     .     .     .
104000.00  19700.  C     .     .     .     I.    R   .  ML    .E    .     .     .     .
           19750.  C     .     .     .     I.    R   .   L    .E    .     .     .     .
           19800.  C     .     .     .     I.    R   .   L    .E    .     .     .     .
           19850.  C     .     .     .      I     R  .   L    .E    .     .     .     .
           19900.  C     .     .     .      I     R  .   ML   .E    .     .     .     .
           19950.  C     .     .     .      I     R  .   ML   .E    .     .     .     .
           20000.  C     .     .     .      I     R  .   ML   .E    .     .     .     .
           20050.  C     .     .     .      I     R  .   ML   .E    .     .     .     .
           20100.  C     .     .     .      I     R  .    L   .E    .     .     .     .
           20150.  C     .     .     .      I     R  .    L   .E    .     .     .     .
104500.00  20200.  C     .     .     .      I      R .    ML  .E    .     .     .     .
           20250.  C     .     .     .      I      R .   M L  .E    .     .     .     .
           20300.  C     .     .     .      I     R  .   M L  .E    .     .     .     .
           20350.  C     .     .     .      I     R  .  M  L  .E    .     .     .     .
           20400.  C     .     .     .      I     R  .  M  L  .E    .     .     .     .
           20450.  C     .     .     .      I     R  .  M  L  .E    .     .     .     .
104818.00  20500.  C     .     .     .      I     R  . M   L  .E    .     .     .     .
           20550.  C     .     .     .      I     R  . M   L  .E    .     .     .     .
           20600.  C     .     .     .      I     R  . M    L .E    .     .     .     .
           20650.  C     .     .     .      I     R  . M    L .E    .     .     .     .
105000.00  20700.  C     .     .     .      I      R .M     L .E    .     .     .     .
           20750.  C     .     .     .      I      R . M    L .E    .     .     .     .
           20800.  C     .     .     .     .I       R. M   L  .E    .     .     .     .
           20850.  C     .     .     .     .I        R  M  L  .E    .     .     .     .
           20900.  C     .     .     .     .I        R  M L   .E    .     .     .     .
           20950.  C     .     .     .     . I       .R  ML   .WE   .     .     .     .
105294.00  21000.  C     .     .     .     . I       . R ML   .WE   .     .     .     .
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T1
T2
T3

J1	ICHECK	INQ	NINV	IDIR	STRT	METRIC	HVINS	Q	WSEL	FQ
		7			.06				1250.5	
J2	NPROF	IPLOT	PRFVS	XSECV	XSECH	FN	ALLDC	IBW	CHNIM	ITRACE
	6									

PROFILE FOR STREAM

PLOTTED POINTS (BY PRIORITY) E-ENERGY,W-WATER SURFACE,I-INVERT,C-CRITICAL W.S.,L-LEFT BANK,R-RIGHT BANK,M-LOWER END STA

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ELEVATION  1245.     1250.     1255.     1260.     1265.     1270.     1275.     1280.     1285.     1290.
   SECNO   CUMDIS

84000.00     0.  .    I   W. L E M   .         .         .         .         .         .         .         .
            50.  .    I    W LME     .         .         .         .         .         .         .         .
           100.  .    I    MWL  E    .         .         .         .         .         .         .         .
           150.  .    IM   .W L E    .         .         .         .         .         .         .         .
           200.  .  M I    . WL E    .         .         .         .         .         .         .         .
           250.  M    I    . CW E    .         .         .         .         .         .         .         .
           300.  M    I    .  WL E   .         .         .         .         .         .         .         .
           350.  M    I    .  CW E   .         .         .         .         .         .         .         .
           400.  M    I    .   CWE   .         .         .         .         .         .         .         .
           450.  M    I    .    WE   .         .         .         .         .         .         .         .
84500.00   500.  M    I    .    CWE  .         .         .         .         .         .         .         .
           550.  M    I    .    CWE  .         .         .         .         .         .         .         .
           600.  M    I    .   LCWE  .         .         .         .         .         .         .         .
           650.  M   I     .   LCWE  .         .         .         .         .         .         .         .
           700.  M   I     .  L CWE  .         .         .         .         .         .         .         .
           750.  M   I     .  L CWE  .         .         .         .         .         .         .         .
           800.  .  I      . L CRWE  .         .         .         .         .         .         .         .
           850.  .  I   M  . L CRWE  .         .         .         .         .         .         .         .
           900.  .  I      ML  C WE  .         .         .         .         .         .         .         .
           950.  . I       .L MC WE  .         .         .         .         .         .         .         .
85000.00  1000.  . I       L   C WE  .         .         .         .         .         .         .         .
          1050.  C I       L   R  WE .         .         .         .         .         .         .         .
          1100.  CI        L   R  WE .         .         .         .         .         .         .         .
          1150.  CI        L   R  WE .         .         .         .         .         .         .         .
          1200.  CI        L  R   WE .         .         .         .         .         .         .         .
          1250.  CI        L  R   WE .         .         .         .         .         .         .         .
          1300.  CI        L  R   WE .         .         .         .         .         .         .         .
          1350.  CI        L  R   WE .         .         .         .         .         .         .         .
          1400.  I         L  R   WE .         .         .         .         .         .         .         .
          1450.  I         L R    WE .         .         .         .         .         .         .         .
85500.00  1500.  I         L R    WE .         .         .         .         .         .         .         .
          1550.  CI        L R    WE .         .         .         .         .         .         .         .
          1600.  CI        L  R   WE .         .         .         .         .         .         .         .
          1650.  C I       L  R   WE .         .         .         .         .         .         .         .
          1700.  C I       L  R   WE .         .         .         .         .         .         .         .
          1750.  C  I      L  R   MWE.         .         .         .         .         .         .         .
          1800.  C   I     L  R   MWE.         .         .         .         .         .         .         .
          1850.  C   I     L   R  MWE.         .         .         .         .         .         .         .
          1900.  C    I    L   R  MWE.         .         .         .         .         .         .         .
          1950.  C     I   L   R  MWE.         .         .         .         .         .         .         .
          2000.  C     I   L   R  MWE.         .         .         .         .         .         .         .
86024.00  2050.  C     I   L   R  MWE.         .         .         .         .         .         .         .
          2100.  C     I   L   R  MWE.         .         .         .         .         .         .         .
          2150.  C    I    .L  R  W E.         .         .         .         .         .         .         .
          2200.  C    I    .L R   W E.         .         .         .         .         .         .         .
          2250.  C   I     . LR   W E.         .         .         .         .         .         .         .
          2300.  C   I     . L   WM E.         .         .         .         .         .         .         .
          2350.  C  I      . RL  WM E.         .         .         .         .         .         .         .
          2400.  C  I      . RL  WM E.         .         .         .         .         .         .         .
86415.00  2450.  . I       .R  L WM E.         .         .         .         .         .         .         .
          2500.  C  I      .R  L WM E.         .         .         .         .         .         .         .
          2550.  C  I      .R  L WM E.         .         .         .         .         .         .         .
          2600.  C  I      .R  L WM E.         .         .         .         .         .         .         .
          2650.  C   I     .R   L W E.         .         .         .         .         .         .         .
          2700.  C   I     . R  L W E.         .         .         .         .         .         .         .
          2750.  C    I    . R  L W  E         .         .         .         .         .         .         .
          2800.  C    I    . R  L W  E         .         .         .         .         .         .         .
          2850.  C     I   . R   LMW E         .         .         .         .         .         .         .
          2900.  C     I   . R   LMW E         .         .         .         .         .         .         .
          2950.  C     I   . R   LMW E         .         .         .         .         .         .         .
87000.00  3000.  C      I  . R   LM W.E        .         .         .         .         .         .         .
          3050.  C      I  . R   LM W.E        .         .         .         .         .         .         .
          3100.  C      I  . R    L W.E        .         .         .         .         .         .         .
          3150.  C      I  . R    L W.E        .         .         .         .         .         .         .
          3200.  C      I  .  R   L W.E        .         .         .         .         .         .         .
          3250.  C      I  .  R   L W.E        .         .         .         .         .         .         .
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          3300.  C      I  .  R   LMW.E        .         .         .         .         .         .         .         .
          3350.  C      I  .  R   LM WE        .         .         .         .         .         .         .         .
          3400.  C      I  .  R   LM WE        .         .         .         .         .         .         .         .
          3450.  C      I  .   R  LM W E       .         .         .         .         .         .         .         .
87500.00  3500.  C      I  .   R  LM W E       .         .         .         .         .         .         .         .
          3550.  C     I   .   R  LM W E       .         .         .         .         .         .         .         .
          3600.  C     I   .   R  L  W E       .         .         .         .         .         .         .         .
          3650.  C     I   .  R   L  W E       .         .         .         .         .         .         .         .
          3700.  C     I   .  R   L  .WE       .         .         .         .         .         .         .         .
          3750.  C     I   .  R  ML  .WE       .         .         .         .         .         .         .         .
          3800.  C     I   .  R  ML  .WE       .         .         .         .         .         .         .         .
          3850.  C     I   .  R  ML  .WE       .         .         .         .         .         .         .         .
          3900.  C    I    .  R  ML  .WE       .         .         .         .         .         .         .         .
          3950.  C    I    . R  M L  .WE       .         .         .         .         .         .         .         .
88000.00  4000.  C    I    . R  M L  .WE       .         .         .         .         .         .         .         .
          4050.  C    I    . R  ML   .WE       .         .         .         .         .         .         .         .
          4100.  C    I    . R  ML   .W E      .         .         .         .         .         .         .         .
          4150.  C    I    . R   L   . WE      .         .         .         .         .         .         .         .
          4200.  C    I    . R   L   . WE      .         .         .         .         .         .         .         .
          4250.  C    I    . R   L   . WE      .         .         .         .         .         .         .         .
          4300.  C    I    . R   L   . WE      .         .         .         .         .         .         .         .
          4350.  C    I    . R   L   . WE      .         .         .         .         .         .         .         .
          4400.  C    I    . R   LM  . WE      .         .         .         .         .         .         .         .
          4450.  C    I    . R  L M  . WE      .         .         .         .         .         .         .         .
88500.00  4500.  C    I    . R  L M  . WE      .         .         .         .         .         .         .         .
          4550.  C    I    . R  L M  . WE      .         .         .         .         .         .         .         .
          4600.  C    I    . R  L  M . WE      .         .         .         .         .         .         .         .
          4650.  C    I    . R  L  M . WE      .         .         .         .         .         .         .         .
          4700.  C    I    .R   L  M . WE      .         .         .         .         .         .         .         .
          4750.  C    I    .R   L   M. WE      .         .         .         .         .         .         .         .
          4800.  C    I    .R   L   M. WE      .         .         .         .         .         .         .         .
          4850.  C    I    .R   L    M WE      .         .         .         .         .         .         .         .
          4900.  C     I   .R   L    M WE      .         .         .         .         .         .         .         .
          4950.  C     I   .R   L    M WE      .         .         .         .         .         .         .         .
89000.00  5000.  C     I   .R   L    .MWE      .         .         .         .         .         .         .         .
          5050.  C     I   .R  L     .MWE      .         .         .         .         .         .         .         .
          5100.  C     I   .R  L     .MWE      .         .         .         .         .         .         .         .
          5150.  C      I  . R L     .M E      .         .         .         .         .         .         .         .
          5200.  C      I  . R L     . ME      .         .         .         .         .         .         .         .
          5250.  C      I  . R L     . ME      .         .         .         .         .         .         .         .
          5300.  C       I . RL      . ME      .         .         .         .         .         .         .         .
          5350.  C       I . RL      . ME      .         .         .         .         .         .         .         .
          5400.  C       I . RL      .  E      .         .         .         .         .         .         .         .
          5450.  C        I. RL      .  WE     .         .         .         .         .         .         .         .
89545.00  5500.  C        I.  L      .  WE     .         .         .         .         .         .         .         .
          5550.  C       I . RL      .  WE     .         .         .         .         .         .         .         .
          5600.  C       I . RL      .  WE     .         .         .         .         .         .         .         .
          5650.  C       I . RL      .  WE     .         .         .         .         .         .         .         .
          5700.  C      I  . R L     . MWE     .         .         .         .         .         .         .         .
          5750.  C      I  . R L     . MWE     .         .         .         .         .         .         .         .
          5800.  C      I  . R L     . MWE     .         .         .         .         .         .         .         .
          5850.  C     I   . R L     . MWE     .         .         .         .         .         .         .         .
          5900.  C     I   . R L     . MWE     .         .         .         .         .         .         .         .
          5950.  C     I   . R  L    . MWE     .         .         .         .         .         .         .         .
90000.00  6000.  C    I    . R  L    .M WE     .         .         .         .         .         .         .         .
          6050.  C    I    . R  L    . MWE     .         .         .         .         .         .         .         .
          6100.  C    I    . R  L    . MWE     .         .         .         .         .         .         .         .
          6150.  C    I    . R   L   . MWE     .         .         .         .         .         .         .         .
          6200.  C    I    . R   L   . MWE     .         .         .         .         .         .         .         .
          6250.  C   I     . R   L   .  WE     .         .         .         .         .         .         .         .
          6300.  C   I     . R   L   .  WE     .         .         .         .         .         .         .         .
          6350.  C   I     . R   L   .  WE     .         .         .         .         .         .         .         .
          6400.  C   I     . R    L  .  WE     .         .         .         .         .         .         .         .
          6450.  C   I     . R    L  .   E     .         .         .         .         .         .         .         .
90500.00  6500.  C   I     . R    L  .   E     .         .         .         .         .         .         .         .
          6550.  C   I     . R    L  .  WE     .         .         .         .         .         .         .         .
          6600.  C   I     . R    L  .  WE     .         .         .         .         .         .         .         .
          6650.  C    I    . R    L  .  WEM    .         .         .         .         .         .         .         .
          6700.  C    I    . R     L.  WEM     .         .         .         .         .         .         .         .
          6750.  C    I    . R     L.  WEM     .         .         .         .         .         .         .         .
          6800.  C    I    . R     L.  WEM     .         .         .         .         .         .         .         .
          6850.  C     I   . R     L.  WEM     .         .         .         .         .         .         .         .
          6900.  C     I   . R     L.  WEM     .         .         .         .         .         .         .         .
          6950.  C     I   . R     L.  WE M    .         .         .         .         .         .         .         .
91000.00  7000.  C     I   . R     L.  WE M    .         .         .         .         .         .         .         .
          7050.  C     I   . R     L.  WE M    .         .         .         .         .         .         .         .
          7100.  C     I   . R     L.  W EM    .         .         .         .         .         .         .         .
          7150.  C     I   . R     L.  W EM    .         .         .         .         .         .         .         .
          7200.  C     I   . R     L.   WEM    .         .         .         .         .         .         .         .
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          7250.  C    I   . R      L.   WEM  .         .         .         .         .         .         .
          7300.  C    I   . R      L.   WE   .         .         .         .         .         .         .
          7350.  C    I   . R     L .   WE   .         .         .         .         .         .         .
          7400.  C    I   . R     L .   WE   .         .         .         .         .         .         .
          7450.  C    I   . R     L .   WE   .         .         .         .         .         .         .
91500.00  7500.  C    I   . R     L .   WE   .         .         .         .         .         .         .
          7550.  C    I   . R     L .   WE   .         .         .         .         .         .         .
          7600.  C    I   .  R    L .   WE   .         .         .         .         .         .         .
          7650.  C     I  .  R    L .   WEM  .         .         .         .         .         .         .
          7700.  C     I  .  R    L .   WEM  .         .         .         .         .         .         .
          7750.  C     I  .  R    L .   WEM  .         .         .         .         .         .         .
          7800.  C     I  .   R   L .   WEM  .         .         .         .         .         .         .
          7850.  C      I .   R   L .   WEM  .         .         .         .         .         .         .
          7900.  C      I .   R   L .   WEM  .         .         .         .         .         .         .
          7950.  C      I .   R   L .   WEM  .         .         .         .         .         .         .
92000.00  8000.  C      I .   R  L  .   WE M .         .         .         .         .         .         .
          8050.  C      I .   R   L .   WE M .         .         .         .         .         .         .
          8100.  C      I .   R   L .   WE M .         .         .         .         .         .         .
          8150.  C      I .   R   L .   WE M .         .         .         .         .         .         .
          8200.  C      I .   R   L .   WE M .         .         .         .         .         .         .
          8250.  C      I .   R   L .   WE M .         .         .         .         .         .         .
          8300.  C      I .   R   L .    E M .         .         .         .         .         .         .
          8350.  C      I .   R   L .    E M .         .         .         .         .         .         .
          8400.  C      I .   R    L.    E M .         .         .         .         .         .         .
          8450.  C      I .   R    L.    E M .         .         .         .         .         .         .
92500.00  8500.  C     I  .   R    L.    E M .         .         .         .         .         .         .
          8550.  C      I .   R    L.    E M .         .         .         .         .         .         .
          8600.  C      I .   R    L.    WEM .         .         .         .         .         .         .
          8650.  C      I .    R   L.    WEM .         .         .         .         .         .         .
          8700.  C      I .    R   L.    WEM .         .         .         .         .         .         .
          8750.  C      I .    R    L    WE M .         .         .         .         .         .         .
          8800.  C      I .    R    L   W E M .         .         .         .         .         .         .
          8850.  C       I.     R   L   W E M .         .         .         .         .         .         .
          8900.  C       I.     R   L   W E M .         .         .         .         .         .         .
          8950.  C       I.     R   L   W E M .         .         .         .         .         .         .
93000.00  9000.  C       I.     R   .L  W E M .         .         .         .         .         .         .
          9050.  C        I     R   L   W E M .         .         .         .         .         .         .
          9100.  C        .I     R  L  W E  M .         .         .         .         .         .         .
          9150.  C        .I     R  L  W E  M .         .         .         .         .         .         .
          9200.  C        . I    R L.  WE  M  .         .         .         .         .         .         .
          9250.  C        .  I   R L. W E  M  .         .         .         .         .         .         .
          9300.  C        .   I  R L. W E  M  .         .         .         .         .         .         .
          9350.  C        .    I RL .W E   M  .         .         .         .         .         .         .
          9400.  C        .    I RL .W E   M  .         .         .         .         .         .         .
93574.00  9450.  .        .     IRL .W E   M  .         .         .         .         .         .         .
          9500.  .        .    I RL W  E  M   .         .         .         .         .         .         .
          9550.  .        .    I L  W  E  M   .         .         .         .         .         .         .
          9600.  .        .   I  L  W  E  M   .         .         .         .         .         .         .
          9650.  .        .   I  L  W  E M    .         .         .         .         .         .         .
          9700.  .        .  I   L  W  E M    .         .         .         .         .         .         .
          9750.  .        .  I   L  W  E M    .         .         .         .         .         .         .
          9800.  .        . I    L  W E  M    .         .         .         .         .         .         .
          9850.  .        . I    L  W E M     .         .         .         .         .         .         .
          9900.  .        .I     L  W E M     .         .         .         .         .         .         .
          9950.  .        .I     L W. E M     .         .         .         .         .         .         .
94000.00 10000.  .        I     LR W. EM      .         .         .         .         .         .         .
         10050.  C        I      LR W E M     .         .         .         .         .         .         .
         10100.  C        I      LR W  EM     .         .         .         .         .         .         .
         10150.  C        I      LR W  EM     .         .         .         .         .         .         .
         10200.  C        I      LR .W E M    .         .         .         .         .         .         .
         10250.  C        I      L R.W E M    .         .         .         .         .         .         .
         10300.  C        .I     L R.W E  M   .         .         .         .         .         .         .
         10350.  C        .I      LR. WE  M   .         .         .         .         .         .         .
         10400.  C        .I      LR. WE   M  .         .         .         .         .         .         .
         10450.  C        .I      L R WE   M  .         .         .         .         .         .         .
94500.00 10500.  C        .I      L R  WE  M  .         .         .         .         .         .         .
         10550.  C        .I      L R  WE  M  .         .         .         .         .         .         .
         10600.  C        .I       LR  WE   M .         .         .         .         .         .         .
         10650.  C        .I       LR  WE   M .         .         .         .         .         .         .
         10700.  C        .I       LR  WE   M .         .         .         .         .         .         .
         10750.  C        .I       LR  WE   M .         .         .         .         .         .         .
         10800.  C        .I       LR  WE   M .         .         .         .         .         .         .
         10850.  C        . I       L  WE   M .         .         .         .         .         .         .
         10900.  C        . I       L  W E  M .         .         .         .         .         .         .
         10950.  C        . I       L  W E  M .         .         .         .         .         .         .
95000.00 11000.  .        . I       L CW E  M .         .         .         .         .         .         .
         11050.  C        . I       L  W E  M .         .         .         .         .         .         .
         11100.  C        . I       LR W E M  .         .         .         .         .         .         .
         11150.  C        . I       LR W E M  .         .         .         .         .         .         .
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          11200.  C        . I       LR W E M  .        .        .        .        .        .        .
          11250.  C        . I      L.R  WE M  .        .        .        .        .        .        .
          11300.  C        . I      L. R WEM   .        .        .        .        .        .        .
          11350.  C        . I      L. R WEM   .        .        .        .        .        .        .
          11400.  C        . I      L. R WEM   .        .        .        .        .        .        .
          11450.  C        . I      L. R  E    .        .        .        .        .        .        .
95500.00  11500.  C        . I     L .  R WE   .        .        .        .        .        .        .
          11550.  C        . I     L . R  WE   .        .        .        .        .        .        .
          11600.  C        . I     L . R  WE   .        .        .        .        .        .        .
          11650.  C        .I      L .R   WE   .        .        .        .        .        .        .
          11700.  C        .I      L .R   WE   .        .        .        .        .        .        .
          11750.  C        .I      L .R   WE   .        .        .        .        .        .        .
          11800.  C        .I      L R    WE   .        .        .        .        .        .        .
          11850.  C        .I      L R    WE   .        .        .        .        .        .        .
          11900.  C        .I      L R    WE   .        .        .        .        .        .        .
          11950.  C        .I      LR.    WE   .        .        .        .        .        .        .
96000.00  12000.  C        .I      LR.    WE   .        .        .        .        .        .        .
          12050.  C        .I      LR.    WE   .        .        .        .        .        .        .
          12100.  C        .I      LR.    WE   .        .        .        .        .        .        .
          12150.  C        .I      LR.     E   .        .        .        .        .        .        .
          12200.  C        . I     LR.     E   .        .        .        .        .        .        .
          12250.  C        . I     LR.     E   .        .        .        .        .        .        .
          12300.  C        . I     LR.     E   .        .        .        .        .        .        .
          12350.  C        . I    L R.     E   .        .        .        .        .        .        .
          12400.  C        . I    L R.     E   .        .        .        .        .        .        .
          12450.  C        . I    L R.     WE  .        .        .        .        .        .        .
96500.00  12500.  C        . I    L R.     WE  .        .        .        .        .        .        .
          12550.  C        . I    L R.     WE  .        .        .        .        .        .        .
          12600.  C        . I    L R.     WE  .        .        .        .        .        .        .
          12650.  C        . I    L R.     WE  .        .        .        .        .        .        .
          12700.  C        . I    L R.     WE  .        .        .        .        .        .        .
          12750.  C        . I    L R.     WE  .        .        .        .        .        .        .
          12800.  C        . I    L R.     WE  .        .        .        .        .        .        .
          12850.  C        . I     LR.     WE  .        .        .        .        .        .        .
          12900.  C        . I     LR.     WE  .        .        .        .        .        .        .
          12950.  C        . I     LR.     WE  .        .        .        .        .        .        .
97000.00  13000.  C        . I     LR.     WE  .        .        .        .        .        .        .
          13050.  C        . I     LR.     WE  .        .        .        .        .        .        .
          13100.  C        . I     L R     WE  .        .        .        .        .        .        .
          13150.  C        .  I    L R     WE  .        .        .        .        .        .        .
          13200.  C        .  I    L R     ME  .        .        .        .        .        .        .
          13250.  C        .  I     LR     ME  .        .        .        .        .        .        .
          13300.  C        .  I     LR     ME  .        .        .        .        .        .        .
          13350.  C        .  I     LR     ME  .        .        .        .        .        .        .
          13400.  C        .   I    LR     ME  .        .        .        .        .        .        .
          13450.  C        .   I    LR     MWE .        .        .        .        .        .        .
97500.00  13500.  C        .   I    LR     MWE .        .        .        .        .        .        .
          13550.  C        .   I    LR     MWE .        .        .        .        .        .        .
          13600.  C        .   I    LR     MWE .        .        .        .        .        .        .
          13650.  C        .   I    LR     MWE .        .        .        .        .        .        .
          13700.  C        .   I    LR      WE .        .        .        .        .        .        .
          13750.  C        .   I    LR      WE .        .        .        .        .        .        .
          13800.  C        .   I    LR      WE .        .        .        .        .        .        .
          13850.  C        .   I    LR      WE .        .        .        .        .        .        .
          13900.  C        .   I    LR      WE .        .        .        .        .        .        .
          13950.  C        .  I     LR      ME .        .        .        .        .        .        .
98000.00  14000.  C        .  I     LR      ME .        .        .        .        .        .        .
          14050.  C        .  I     LR      ME .        .        .        .        .        .        .
          14100.  C        . I      LR      ME .        .        .        .        .        .        .
          14150.  C        .I       LR      ME .        .        .        .        .        .        .
          14200.  C        .I       LR      ME .        .        .        .        .        .        .
          14250.  C        I        LR      ME .        .        .        .        .        .        .
          14300.  C       I.        LR      ME .        .        .        .        .        .        .
98500.00  14350.  C       I.        LR     M E .        .        .        .        .        .        .
          14400.  C        I        LR      ME .        .        .        .        .        .        .
          14450.  C        .I       LR      ME .        .        .        .        .        .        .
          14500.  C        . I      LR      ME .        .        .        .        .        .        .
          14550.  C        .  I     L.      ME .        .        .        .        .        .        .
98815.00  14600.  C        .   I    L.      ME .        .        .        .        .        .        .
          14650.  C        .    I   L.       E .        .        .        .        .        .        .
          14700.  C        .    I  LR.       EM.        .        .        .        .        .        .
          14750.  C        .     I LR.       E M        .        .        .        .        .        .
99000.00  14800.  C        .     I LR.       E M        .        .        .        .        .        .
          14850.  C        .     I  L. R     WE.        .        .        .        .        .        .
99080.00  14900.  C        .     I  L.  R    WE.        .        .        .        .        .        .
99167.00  14950.  C        .     I   .L R   WME.        .        .        .        .        .        .
          15000.  C        .     I   .L R   WME.        .        .        .        .        .        .
99266.00  15050.  C        .     I   .L R    WE.        .        .        .        .        .        .
99267.00  15100.  C        .        IL  R     E.        .        .        .        .        .        .
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 99327.00 15150.  C         .         IL  R     E.         .         .         .         .         .         .         .
 99328.00 15200.  .         .         . I R  CME.         .         .         .         .         .         .         .
 99408.00 15250.  C         .         . I R  WME.         .         .         .         .         .         .         .
 99500.00 15300.  .         .         .   IR   M. WE      .         .         .         .         .         .         .
          15350.  .         .         .   IR    M  WE     .         .         .         .         .         .         .
          15400.  .         .         .    IR   M  W EL   .         .         .         .         .         .         .
          15450.  .         .         .    IR   .M  W E L .         .         .         .         .         .         .
 99717.00 15500.  .         .         .     IR  . M W   E .L         .         .         .         .         .         .
          15550.  .         .         .     I R . M  W   E.  L       .         .         .         .         .         .
          15600.  .         .         .    I  R . M   W   E    L     .         .         .         .         .         .
          15650.  .         .         .    I   R.  M   W  . E   L    .         .         .         .         .         .
          15700.  .         .         .    I    R  M    W .  E    L .         .         .         .         .         .
          15750.  .         .         .   I     .R M     W.   E     L         .         .         .         .         .
          15800.  .         .         .   I     . RM      W    E    .L        .         .         .         .         .
          15850.  .         .         .   I     .  R      .W    E   .  L      .         .         .         .         .
          15900.  .         .         .  I      .  MR     . W    E  .    L    .         .         .         .         .
          15950.  .         .         .  I      .   MR    .  W    E.     L   .         .         .         .         .
100251.00 16000.  .         .         .  I      .   MR    .   W   E.      L  .         .         .         .         .
          16050.  .         .         .  I      .  RM     .    W   LE        .         .         .         .         .
          16100.  .         .         .  I      .R   M    .   L W   . E      .         .         .         .         .
          16150.  .         .         .  I    R .     ML  .      W  .  E     .         .         .         .         .
          16200.  .         .         .  I  R   L      M  .      W .    E    .         .         .         .         .
100500.00 16250.  .         .         .   I     .      M  .       W .    E   .         .         .         .         .
          16300.  .         .         .    I    .       M .         W      E  .         .         .         .         .
          16350.  .         .         .    I    .        M.         .W      E .         .         .         .         .
          16400.  .         .         .     I   .        M.         . W     E.         .         .         .         .
          16450.  .         .         .      I  .         M         .   W    E         .         .         .         .
          16500.  .         .         .       I .         M         .    W   .E        .         .         .         .
          16550.  .         .         .        I.         .M        .     W   . E      .         .         .         .
          16600.  .         .         .         I         . M       .      W  .  E     .         .         .         .
          16650.  .         .         .         .I        . M       .        W.   E    .         .         .         .
100951.00 16700.  .         .         .         . I       .  M      .         W   E    .         .         .         .
101000.00 16750.  C         .         .         .   I     .       R .    M L  .     WE .         .         .         .
101048.00 16800.  C         .         .         .   I     .     R  .     L   .     WE .         .         .         .
          16850.  C         .         .         .   I     .     R  .     L   .     WE .         .         .         .
          16900.  C         .         .         .   I     .     R  .     L   .     WE .         .         .         .
          16950.  C         .         .         .    I    .     R  .     ML  .     WE .         .         .         .
          17000.  C         .         .         .    I    .     R  .     ML  .     WE .         .         .         .
          17050.  C         .         .         .    I    .     R  .     ML  .     WE .         .         .         .
          17100.  C         .         .         .    I    .     R  .      L  .     WE .         .         .         .
          17150.  C         .         .         .     I   .     R  .      L  .     WE .         .         .         .
          17200.  C         .         .         .     I   .     R  .      ML .     WE .         .         .         .
101500.00 17250.  C         .         .         .     I   .     R  .      ML .      E .         .         .         .
          17300.  C         .         .         .     I   .     R  .      ML .      E .         .         .         .
          17350.  C         .         .         .     I   .     R  .      L  .      E .         .         .         .
          17400.  C         .         .         .     I   .      R .      L  .      E .         .         .         .
          17450.  C         .         .         .     I   .      R .      L  .      E .         .         .         .
          17500.  C         .         .         .      I  .      R .     LM  .      E .         .         .         .
          17550.  C         .         .         .      I  .      R .     LM  .      E .         .         .         .
          17600.  C         .         .         .      I  .      R .     LM  .      E .         .         .         .
          17650.  C         .         .         .      I  .       R.     LM  .      E .         .         .         .
          17700.  C         .         .         .      I  .       R.    L M  .      E .         .         .         .
102000.00 17750.  C         .         .         .      I  .       R.    L M  .      E .         .         .         .
          17800.  C         .         .         .      I  .       R.    L M  .      E .         .         .         .
          17850.  C         .         .         .      I  .       R.    L M  .      E .         .         .         .
          17900.  C         .         .         .       I .       R.    L M  .      E .         .         .         .
          17950.  C         .         .         .       I .       R.   L  M  .      E .         .         .         .
          18000.  C         .         .         .       I .       R.   L  M  .      E .         .         .         .
          18050.  C         .         .         .       I .       R.   L  M  .      E .         .         .         .
          18100.  C         .         .         .       I .       R.   L  M  .      E .         .         .         .
          18150.  C         .         .         .       I .       R.   L  M  .      E .         .         .         .
          18200.  C         .         .         .        I.       R.   L  M  .      E .         .         .         .
102500.00 18250.  C         .         .         .        I.       R.   L  M  .      E .         .         .         .
          18300.  C         .         .         .        I.       R.   L  M  .      E .         .         .         .
          18350.  C         .         .         .        I.      R .   L  M  .      E .         .         .         .
          18400.  C         .         .         .        I.      R .   L  M  .      E .         .         .         .
          18450.  C         .         .         .        I.      R .    L M  .      E .         .         .         .
          18500.  C         .         .         .        I.      R .    L M  .      E .         .         .         .
          18550.  C         .         .         .        I.      R .    L M  .      E .         .         .         .
          18600.  C         .         .         .        I.      R .    LM   .      E .         .         .         .
          18650.  C         .         .         .        I.     R  .     L   .      E .         .         .         .
          18700.  C         .         .         .        I.     R  .     L   .      E .         .         .         .
103000.00 18750.  C         .         .         .        I.     R  .     L   .      E .         .         .         .
          18800.  C         .         .         .         I     R  .     L   .      E .         .         .         .
          18850.  C         .         .         .         I     R  .     L   .      E .         .         .         .
          18900.  C         .         .         .         I      R .     L   .      E .         .         .         .
          18950.  C         .         .         .         I      R .    ML   .      E .         .         .         .
          19000.  C         .         .         .        .I      R .    M L  .      E .         .         .         .
          19050.  C         .         .         .        .I      R .    M L  .      E .         .         .         .
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          19100.  C        .        .        .       .I     R .    M L  .     E  .        .        .        .
          19150.  C        .        .        .       .I     R .    M L  .     E  .        .        .        .
103500.00 19200.  C        .        .        .       . I     R.    M L  .     WE .        .        .        .
          19250.  C        .        .        .       . I     R.    M L  .     WE .        .        .        .
          19300.  C        .        .        .       . I     R.    M L  .     WE .        .        .        .
          19350.  C        .        .        .       . I     R.    M L  .     WE .        .        .        .
          19400.  C        .        .        .       . I     R.    M L  .     WE .        .        .        .
          19450.  C        .        .        .       . I     R.    M L  .     WE .        .        .        .
          19500.  C        .        .        .       . I    R .    ML   .     WE .        .        .        .
          19550.  C        .        .        .       . I    R .    ML   .     WE .        .        .        .
          19600.  C        .        .        .       . I    R .    ML   .     WE .        .        .        .
          19650.  C        .        .        .       . I    R .     L   .     WE .        .        .        .
104000.00 19700.  C        .        .        .       . I    R .     L   .     WE .        .        .        .
          19750.  C        .        .        .       . I     R.     L   .     WE .        .        .        .
          19800.  C        .        .        .       . I     R.     ML  .     WE .        .        .        .
          19850.  C        .        .        .       . I     R.     ML  .     WE .        .        .        .
          19900.  C        .        .        .       . I     R.     ML  .     WE .        .        .        .
          19950.  C        .        .        .       . I     R.     ML  .     WE .        .        .        .
          20000.  C        .        .        .       . I     R.     ML  .      E .        .        .        .
          20050.  C        .        .        .       . I     R.      L  .      E .        .        .        .
          20100.  C        .        .        .       . I      R      L  .      E .        .        .        .
          20150.  C        .        .        .       . I      R      ML .      E .        .        .        .
104500.00 20200.  C        .        .        .       . I      R      ML .      E .        .        .        .
          20250.  C        .        .        .       . I      R      ML .      E .        .        .        .
          20300.  C        .        .        .       . I      R     M L .      E .        .        .        .
          20350.  C        .        .        .       . I      R     M L .      E .        .        .        .
          20400.  C        .        .        .       . I      R    M  L .      E .        .        .        .
          20450.  C        .        .        .       . I      R    M  L .      E .        .        .        .
104818.00 20500.  C        .        .        .       . I     R.   M   L .      E .        .        .        .
          20550.  C        .        .        .       . I      R   M   L .      E .        .        .        .
          20600.  C        .        .        .       . I      R   M    L.      E .        .        .        .
          20650.  C        .        .        .       . I      R   M    L.      E .        .        .        .
105000.00 20700.  C        .        .        .       . I      R   M     L      E .        .        .        .
          20750.  C        .        .        .       . I      R   M    L.      E .        .        .        .
          20800.  C        .        .        .       .  I     .R   M   L.      E .        .        .        .
          20850.  C        .        .        .       .  I     . R  M  L .      E .        .        .        .
          20900.  C        .        .        .       .   I    .  R  M L .      E .        .        .        .
          20950.  C        .        .        .       .   I    .  R  ML  .      E .        .        .        .
105294.00 21000.  C        .        .        .       .   I    .   R  L  .      E .        .        .        .
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THIS RUN EXECUTED 31AUG95 10:14:07

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HEC-2 WATER SURFACE PROFILES

Version 4.6.2; May 1991
****

OTE- ASTERISK (*) AT LEFT OF CROSS-SECTION NUMBER INDICATES MESSAGE IN SUMMARY OF ERRORS LIST

SUMMARY PRINTOUT TABLE 150

	SECNO	XLCH	ELTRD	ELLC	ELMIN	Q	CWSEL	CRIWS	EG	10*KS	VCH	AREA	.01K
	84000.000	.00	.00	.00	1247.70	75.00	1248.42	.00	1248.46	5.98	1.58	47.43	30.68
*	84000.000	.00	.00	.00	1247.70	250.00	1248.47	1248.47	1248.84	52.67	4.91	50.94	34.45
	84000.000	.00	.00	.00	1247.70	500.00	1248.91	1248.91	1249.49	45.48	6.11	81.81	74.14
	84000.000	.00	.00	.00	1247.70	1200.00	1249.90	1249.90	1250.12	13.13	4.77	1976.74	331.20
	84000.000	.00	.00	.00	1247.70	2400.00	1249.93	1249.93	1250.79	50.97	9.48	1988.09	336.17
*	84000.000	.00	.00	.00	1247.70	4000.00	1249.89	1249.89	1252.32	147.78	15.96	1971.80	329.04
	84500.000	500.00	.00	.00	1247.90	75.00	1248.69	.00	1248.72	4.77	1.51	49.81	34.34
	84500.000	500.00	.00	.00	1247.90	250.00	1249.41	.00	1249.51	5.97	2.56	97.77	102.36
*	84500.000	500.00	.00	.00	1247.90	500.00	1250.04	.00	1250.24	7.32	3.53	141.61	184.74
*	84500.000	500.00	.00	.00	1247.90	1200.00	1250.12	1250.11	1251.16	37.95	8.19	146.44	194.79
	84500.000	500.00	.00	.00	1247.90	2400.00	1251.36	1251.36	1252.95	33.60	10.12	237.15	414.03
	84500.000	500.00	.00	.00	1247.90	4000.00	1253.13	1252.81	1253.49	9.12	6.16	5574.52	1324.46
	85000.000	500.00	.00	.00	1248.10	75.00	1248.92	.00	1248.95	4.37	1.41	53.01	35.87
	85000.000	500.00	.00	.00	1248.10	250.00	1249.71	.00	1249.78	4.76	2.09	119.36	114.57
	85000.000	500.00	.00	.00	1248.10	500.00	1250.42	.00	1250.53	4.64	2.57	199.14	232.23
	85000.000	500.00	.00	.00	1248.10	1200.00	1251.58	1250.21	1251.75	5.59	3.40	369.20	507.39
*	85000.000	500.00	.00	.00	1248.10	2400.00	1253.15	1251.12	1253.37	3.73	3.80	849.95	1242.15
	85000.000	500.00	.00	.00	1246.10	4000.00	1253.41	1252.07	1253.92	8.20	5.89	963.27	1397.19
	85500.000	500.00	.00	.00	1248.20	75.00	1249.09	.00	1249.12	2.65	1.22	61.47	46.10
	85500.000	500.00	.00	.00	1248.20	250.00	1249.91	.00	1249.97	3.32	2.07	120.62	137.15
	85500.000	500.00	.00	.00	1248.20	500.00	1250.62	1249.39	1250.73	3.57	2.69	208.99	264.77
	85500.000	500.00	.00	.00	1248.20	1200.00	1251.83	1250.47	1251.97	3.80	3.33	930.76	615.50
	85500.000	500.00	.00	.00	1248.20	2400.00	1253.33	1251.32	1253.54	3.36	4.10	1775.02	1309.79
	85500.000	500.00	.00	.00	1245.19	4000.00	1253.81	.00	1254.29	6.46	6.08	2102.17	1573.74
	86024.000	524.00	.00	.00	1248.40	75.00	1249.25	.00	1249.28	3.51	1.36	55.32	40.04
	86024.000	524.00	.00	.00	1248.40	250.00	1250.08	.00	1250.16	3.90	2.22	115.99	126.65
	86024.000	524.00	.00	.00	1248.40	500.00	1250.81	.00	1250.91	3.54	2.67	215.92	265.66
	86024.000	524.00	.00	.00	1248.40	1200.00	1252.00	.00	1252.18	3.94	3.61	379.54	604.86
	86024.000	524.00	.00	.00	1248.40	2400.00	1253.50	.00	1253.74	4.06	4.21	1015.19	1191.45
	86024.000	524.00	.00	.00	1248.40	4000.00	1254.15	.00	1254.63	6.63	5.94	1451.56	1553.50

	SECNO	XLCH	ELTRD	ELLC	ELMIN	Q	CWSEL	CRIWS	EG	10*KS	VCH	AREA	.01K
*	86415.000	391.00	.00	.00	1246.29	75.00	1249.30	1247.53	1249.31	.45	.80	94.02	112.37
	86415.000	391.00	.00	.00	1246.29	250.00	1250.20	1248.29	1250.25	1.37	1.77	141.27	213.33
	86415.000	391.00	.00	.00	1246.29	500.00	1250.93	1248.89	1251.05	3.27	2.73	188.45	276.66
	86415.000	391.00	.00	.00	1246.29	1200.00	1252.08	1250.05	1252.35	5.12	4.28	431.97	530.56
	86415.000	391.00	.00	.00	1246.29	2400.00	1253.53	1251.61	1253.91	5.11	5.35	989.94	1061.43
*	86415.000	391.00	.00	.00	1246.29	4000.00	1252.97	1252.97	1254.51	22.98	10.50	738.79	834.45
	87000.000	585.00	.00	.00	1248.80	75.00	1249.30	.00	1249.39	24.07	2.51	29.90	15.29
*	87000.000	585.00	.00	.00	1248.80	250.00	1250.29	.00	1250.40	6.84	2.68	93.29	95.62
	87000.000	585.00	.00	.00	1248.80	500.00	1251.14	.00	1251.29	5.33	3.14	550.08	216.66
	87000.000	585.00	.00	.00	1248.80	1200.00	1252.38	.00	1252.69	6.64	4.64	1127.58	465.58
	87000.000	585.00	.00	.00	1246.64	2400.00	1253.71	.00	1254.29	8.28	6.39	1939.55	833.94
	87000.000	585.00	.00	.00	1248.80	4000.00	1254.44	.00	1255.49	12.80	8.77	2446.69	1118.09
*	87500.000	500.00	.00	.00	1248.90	75.00	1249.75	.00	1249.78	3.76	1.41	53.22	38.69
	87500.000	500.00	.00	.00	1248.90	250.00	1250.58	.00	1250.67	4.35	2.33	107.35	119.89
	87500.000	500.00	.00	.00	1248.90	500.00	1251.39	.00	1251.53	4.60	3.06	163.42	233.05
	87500.000	500.00	.00	.00	1248.90	1200.00	1252.69	.00	1253.01	6.13	4.59	514.08	484.81

87500.000	500.00	.00	.00	1248.44	2400.00	1254.19	.00	1254.71	8.68	5.92	1273.41	814.67
87500.000	500.00	.00	.00	1248.44	4000.00	1255.27	.00	1256.04	9.62	7.34	2025.87	1289.59
88000.000	500.00	.00	.00	1249.00	75.00	1249.92	.00	1249.95	2.98	1.31	57.28	43.46
88000.000	500.00	.00	.00	1249.00	250.00	1250.79	.00	1250.86	3.55	2.17	115.24	132.77
88000.000	500.00	.00	.00	1249.00	500.00	1251.62	.00	1251.74	3.72	2.84	334.26	259.15
88000.000	500.00	.00	.00	1249.00	1200.00	1253.01	.00	1253.28	4.63	4.19	1024.86	557.50
88000.000	500.00	.00	.00	1247.74	2400.00	1254.63	.00	1255.02	4.69	5.34	2130.72	1108.15
88000.000	500.00	.00	.00	1247.74	4000.00	1255.81	.00	1256.40	5.67	6.72	2959.49	1679.57
88500.000	500.00	.00	.00	1249.10	75.00	1250.06	.00	1250.08	2.43	1.21	61.90	48.12
88500.000	500.00	.00	.00	1249.10	250.00	1250.97	.00	1251.03	3.18	1.96	127.24	140.14
88500.000	500.00	.00	.00	1249.10	500.00	1251.82	.00	1251.90	2.87	2.40	592.46	294.96
88500.000	500.00	.00	.00	1249.10	1200.00	1253.30	.00	1253.46	2.97	3.36	1341.65	696.59
88500.000	500.00	.00	.00	1247.45	2400.00	1254.97	.00	1255.20	2.65	4.09	2520.49	1473.66
88500.000	500.00	.00	.00	1247.45	4000.00	1256.27	.00	1256.61	3.18	5.17	3418.05	2242.65
89000.000	500.00	.00	.00	1249.30	75.00	1250.19	.00	1250.22	3.06	1.29	58.04	42.85
89000.000	500.00	.00	.00	1249.30	250.00	1251.12	.00	1251.18	2.87	1.99	247.23	147.45
89000.000	500.00	.00	.00	1249.30	500.00	1251.96	.00	1252.06	3.36	2.59	497.56	272.65
89000.000	500.00	.00	.00	1249.30	1200.00	1253.45	.00	1253.61	3.19	3.37	1135.97	672.13
89000.000	500.00	.00	.00	1248.10	2400.00	1255.10	.00	1255.34	2.92	4.18	2112.02	1404.08
89000.000	500.00	.00	.00	1248.10	4000.00	1256.40	.00	1256.78	3.50	5.32	3015.68	2139.21
89545.000	455.00	.00	.00	1249.50	75.00	1250.35	.00	1250.39	4.85	1.59	47.18	34.07
89545.000	455.00	.00	.00	1249.50	250.00	1251.25	.00	1251.35	4.78	2.49	100.41	114.38
89545.000	455.00	.00	.00	1249.50	500.00	1252.09	.00	1252.25	5.32	3.19	357.25	216.77
89545.000	455.00	.00	.00	1249.50	1200.00	1253.58	.00	1253.77	3.88	3.83	926.56	609.39
89545.000	455.00	.00	.00	1249.50	2400.00	1255.21	.00	1255.48	3.50	4.65	1778.24	1282.66
89545.000	455.00	.00	.00	1249.50	4000.00	1256.53	.00	1256.95	4.08	5.82	2610.79	1979.15

SECNO	XLCH	ELTRD	ELLC	ELMIN	Q	CWSEL	CRIWS	EG	10*KS	VCH	AREA	.01K
90000.000	545.00	.00	.00	1249.60	75.00	1250.56	.00	1250.58	2.71	1.23	60.75	45.60
90000.000	545.00	.00	.00	1249.60	250.00	1251.50	.00	1251.55	2.93	1.82	137.21	146.08
90000.000	545.00	.00	.00	1249.60	500.00	1252.37	.00	1252.44	2.54	2.21	351.56	313.80
90000.000	545.00	.00	.00	1249.60	1200.00	1253.80	.00	1253.94	2.54	3.07	881.40	752.66
90000.000	545.00	.00	.00	1247.80	2400.00	1255.44	.00	1255.64	2.36	3.80	1631.18	1562.49
90000.000	545.00	.00	.00	1247.80	4000.00	1256.83	.00	1257.13	2.65	4.71	2534.60	2456.81
* 90500.000	500.00	.00	.00	1247.04	75.00	1250.60	.00	1250.60	.13	.49	153.30	209.70
* 90500.000	500.00	.00	.00	1247.04	250.00	1251.58	.00	1251.60	.54	1.07	236.95	340.77
90500.000	500.00	.00	.00	1247.04	500.00	1252.47	.00	1252.51	.78	1.55	467.97	567.56
90500.000	500.00	.00	.00	1247.04	1200.00	1253.93	.00	1254.03	1.30	2.51	959.83	1050.67
90500.000	500.00	.00	.00	1247.04	2400.00	1255.56	.00	1255.74	1.67	3.48	1729.76	1859.36
90500.000	500.00	.00	.00	1247.04	4000.00	1256.96	.00	1257.24	2.09	4.48	2596.89	2767.16
91000.000	500.00	.00	.00	1249.70	75.00	1250.59	.00	1250.62	3.32	1.35	55.49	41.15
91000.000	500.00	.00	.00	1249.70	250.00	1251.59	.00	1251.65	2.83	2.03	169.42	148.65
* 91000.000	500.00	.00	.00	1249.70	500.00	1252.46	.00	1252.58	3.01	2.69	350.64	288.31
* 91000.000	500.00	.00	.00	1249.70	1200.00	1253.88	.00	1254.14	4.08	4.09	773.99	593.83
91000.000	500.00	.00	.00	1248.40	2400.00	1255.40	.00	1255.87	5.29	5.69	1394.00	1043.95
91000.000	500.00	.00	.00	1248.40	4000.00	1256.73	.00	1257.41	5.92	7.00	2156.02	1644.39
91500.000	500.00	.00	.00	1249.80	75.00	1250.75	.00	1250.77	2.87	1.30	57.54	44.24
91500.000	500.00	.00	.00	1249.80	250.00	1251.75	.00	1251.80	2.81	1.74	168.81	149.01
91500.000	500.00	.00	.00	1249.80	500.00	1252.63	.00	1252.70	2.24	2.12	357.18	334.38
91500.000	500.00	.00	.00	1249.80	1200.00	1254.15	.00	1254.29	2.35	3.00	833.49	783.37
* 91500.000	500.00	.00	.00	1248.20	2400.00	1255.83	.00	1256.04	2.28	3.80	1649.49	1590.25
* 91500.000	500.00	.00	.00	1248.20	4000.00	1257.29	.00	1257.59	2.48	4.65	2506.13	2538.21
92000.000	500.00	.00	.00	1249.90	75.00	1250.89	.00	1250.91	2.63	1.28	58.62	46.29
92000.000	500.00	.00	.00	1249.90	250.00	1251.88	.00	1251.94	2.91	1.98	126.07	146.45
92000.000	500.00	.00	.00	1249.90	500.00	1252.73	.00	1252.84	3.20	2.56	209.51	279.72
92000.000	500.00	.00	.00	1249.90	1200.00	1254.23	.00	1254.43	3.43	3.64	560.77	648.14
92000.000	500.00	.00	.00	1249.30	2400.00	1255.89	.00	1256.17	3.19	4.49	1289.95	1343.63
92000.000	500.00	.00	.00	1249.30	4000.00	1257.34	.00	1257.74	3.43	5.46	2065.76	2158.56
92500.000	500.00	.00	.00	1250.00	75.00	1251.01	.00	1251.04	2.47	1.24	60.70	47.74
92500.000	500.00	.00	.00	1250.00	250.00	1252.03	.00	1252.08	2.87	1.89	132.21	147.60
92500.000	500.00	.00	.00	1250.00	500.00	1252.90	.00	1252.98	2.74	2.38	247.88	302.27
92500.000	500.00	.00	.00	1250.00	1200.00	1254.41	.00	1254.59	2.97	3.39	637.96	696.65
92500.000	500.00	.00	.00	1248.90	2400.00	1256.05	.00	1256.33	3.00	4.35	1342.25	1385.63

92500.000	500.00	.00	.00	1248.90	4000.00	1257.52	.00	1257.90	3.22	5.29	2197.90	2230.42
93000.000	500.00	.00	.00	1250.20	75.00	1251.15	.00	1251.17	3.05	1.36	55.32	42.96
93000.000	500.00	.00	.00	1250.20	250.00	1252.16	.00	1252.23	2.96	2.12	117.81	145.28
93000.000	500.00	.00	.00	1250.20	500.00	1253.01	.00	1253.14	3.51	2.89	173.08	266.86
93000.000	500.00	.00	.00	1250.20	1200.00	1254.48	.00	1254.77	4.64	4.35	504.94	557.10
93000.000	500.00	.00	.00	1249.70	2400.00	1255.98	.00	1256.53	6.12	6.10	1047.24	969.96
93000.000	500.00	.00	.00	1249.70	4000.00	1257.37	.00	1258.12	6.59	7.38	1781.62	1557.95

SECNO	XLCH	ELTRD	ELLC	ELMIN	Q	CWSEL	CRIWS	EG	10*KS	VCH	AREA	.01K
93574.000	426.00	.00	.00	1253.10	75.00	1253.53	1253.53	1253.65	1153.87	2.82	26.64	2.21
93574.000	426.00	.00	.00	1253.10	250.00	1253.82	1253.82	1254.05	919.43	3.83	72.90	8.24
93574.000	426.00	.00	.00	1253.10	500.00	1254.01	1254.01	1254.14	3.06	.25	276.26	285.86
93574.000	426.00	.00	.00	1253.10	1200.00	1254.77	.00	1254.99	5.74	.61	605.01	500.99
* 93574.000	426.00	.00	.00	1253.10	2400.00	1254.81	1254.81	1255.64	21.50	1.21	627.81	517.56
93574.000	426.00	.00	.00	1253.10	4000.00	1255.49	1255.49	1256.62	25.79	1.73	965.93	787.64
* 94000.000	574.00	.00	.00	1250.07	75.00	1251.68	1251.68	1252.09	807.63	5.14	14.58	2.64
* 94000.000	574.00	.00	.00	1250.07	250.00	1254.09	1252.57	1254.10	.24	.13	505.46	506.40
94000.000	574.00	.00	.00	1250.07	500.00	1254.18	1253.04	1254.22	.87	.26	532.06	535.33
94000.000	574.00	.00	.00	1250.07	1200.00	1255.06	1253.44	1255.17	2.02	.54	823.01	845.21
94000.000	574.00	.00	.00	1250.07	2400.00	1255.85	1254.01	1256.08	3.91	.90	1186.33	1213.27
* 94000.000	574.00	.00	.00	1250.07	4000.00	1254.81	1254.81	1256.31	28.36	1.87	733.84	751.11
94500.000	500.00	.00	.00	1251.70	75.00	1253.90	.00	1253.91	11.40	.65	116.25	22.22
94500.000	500.00	.00	.00	1251.70	250.00	1254.10	.00	1254.15	69.20	1.71	146.42	30.05
94500.000	500.00	.00	.00	1250.80	500.00	1254.21	.00	1254.28	1.54	.26	378.36	402.39
94500.000	500.00	.00	.00	1250.80	1200.00	1255.14	.00	1255.30	3.08	.47	664.58	683.48
94500.000	500.00	.00	.00	1250.80	2400.00	1256.04	.00	1256.29	4.57	.80	1067.94	1122.85
94500.000	500.00	.00	.00	1250.80	4000.00	1256.53	.00	1257.00	8.15	1.21	1304.92	1401.00
* 95000.000	500.00	.00	.00	1253.90	75.00	1254.77	.00	1254.78	29.72	.74	101.62	13.76
* 95000.000	500.00	.00	.00	1253.90	250.00	1255.40	1254.60	1255.41	23.65	1.01	247.64	51.40
95000.000	500.00	.00	.00	1253.90	500.00	1254.84	1254.84	1255.13	877.01	4.29	116.66	16.88
95000.000	500.00	.00	.00	1253.90	1200.00	1255.29	1255.29	1255.75	800.67	5.46	219.91	42.41
95000.000	500.00	.00	.00	1251.00	2400.00	1256.05	.00	1256.58	8.06	.83	751.36	845.39
95000.000	500.00	.00	.00	1251.00	4000.00	1256.44	1256.17	1257.55	15.88	1.35	896.89	1003.83
95500.000	500.00	.00	.00	1252.20	75.00	1254.78	.00	1254.78	.03	.03	447.56	417.96
95500.000	500.00	.00	.00	1252.20	250.00	1255.43	1253.96	1255.44	.16	.11	697.70	631.31
* 95500.000	500.00	.00	.00	1252.20	500.00	1255.24	.00	1255.28	.79	.22	622.67	562.33
* 95500.000	500.00	.00	.00	1252.20	1200.00	1256.00	.00	1256.11	1.96	.47	918.45	856.66
95500.000	500.00	.00	.00	1251.00	2400.00	1256.63	.00	1256.87	4.34	.83	1230.81	1152.37
95500.000	500.00	.00	.00	1251.00	4000.00	1257.66	.00	1257.96	4.98	1.11	1879.82	1792.47
96000.000	500.00	.00	.00	1253.50	75.00	1254.78	.00	1254.78	.04	.04	414.53	392.14
96000.000	500.00	.00	.00	1253.50	250.00	1255.44	.00	1255.45	.19	.13	651.23	579.65
96000.000	500.00	.00	.00	1253.50	500.00	1255.28	.00	1255.32	.89	.27	585.05	530.10
96000.000	500.00	.00	.00	1250.70	1200.00	1256.09	.00	1256.21	2.26	.57	924.24	798.12
96000.000	500.00	.00	.00	1250.70	2400.00	1256.83	.00	1257.10	4.56	.97	1305.48	1124.48
96000.000	500.00	.00	.00	1250.70	4000.00	1257.86	.00	1258.23	5.58	1.29	1898.62	1692.78
96500.000	500.00	.00	.00	1252.60	75.00	1254.79	.00	1254.79	.03	.05	510.85	426.79
96500.000	500.00	.00	.00	1252.60	250.00	1255.45	.00	1255.46	.16	.15	731.33	627.43
96500.000	500.00	.00	.00	1252.60	500.00	1255.33	1253.68	1255.36	.72	.31	687.11	587.93
96500.000	500.00	.00	.00	1251.40	1200.00	1256.22	.00	1256.31	1.77	.60	1041.05	902.65
96500.000	500.00	.00	.00	1251.40	2400.00	1257.06	.00	1257.30	3.65	1.01	1440.27	1255.38
96500.000	500.00	.00	.00	1251.40	4000.00	1258.14	.00	1258.49	4.86	1.37	2103.33	1813.67

SECNO	XLCH	ELTRD	ELLC	ELMIN	Q	CWSEL	CRIWS	EG	10*KS	VCH	AREA	.01K
97000.000	500.00	.00	.00	1252.80	75.00	1254.79	.00	1254.79	.04	.05	422.83	374.02
97000.000	500.00	.00	.00	1251.20	250.00	1255.46	.00	1255.47	.19	.15	656.70	573.49
97000.000	500.00	.00	.00	1252.80	500.00	1255.36	.00	1255.40	.85	.30	623.02	542.75
97000.000	500.00	.00	.00	1251.20	1200.00	1256.31	.00	1256.41	1.86	.58	977.16	879.90
97000.000	500.00	.00	.00	1251.20	2400.00	1257.25	.00	1257.48	3.47	.96	1393.60	1288.08
97000.000	500.00	.00	.00	1251.20	4000.00	1258.39	.00	1258.72	4.42	1.29	2094.99	1901.59

*	97500.000	500.00	.00	.00	1253.50	75.00	1254.79	.00	1254.80	14.82	.70	107.77	19.49
	97500.000	500.00	.00	.00	1252.20	250.00	1255.47	.00	1255.48	.37	.16	463.86	408.83
	97500.000	500.00	.00	.00	1253.50	500.00	1255.39	.00	1255.46	1.65	.31	437.13	388.91
	97500.000	500.00	.00	.00	1252.20	1200.00	1256.37	.00	1256.52	3.09	.63	851.85	682.87
	97500.000	500.00	.00	.00	1252.20	2400.00	1257.37	.00	1257.68	5.00	1.04	1363.29	1073.04
	97500.000	500.00	.00	.00	1252.20	4000.00	1258.55	.00	1258.97	5.85	1.38	2125.06	1653.38
	98000.000	500.00	.00	.00	1253.10	75.00	1254.81	.00	1254.81	.10	.07	412.21	237.76
	98000.000	500.00	.00	.00	1251.90	250.00	1255.49	.00	1255.50	.35	.18	646.20	420.72
	98000.000	500.00	.00	.00	1253.10	500.00	1255.49	.00	1255.53	1.39	.36	650.96	424.70
	98000.000	500.00	.00	.00	1251.90	1200.00	1256.57	.00	1256.65	2.19	.63	1083.60	810.72
	98000.000	500.00	.00	.00	1251.90	2400.00	1257.73	.00	1257.88	3.14	.94	1652.78	1355.44
	98000.000	500.00	.00	.00	1251.90	4000.00	1259.00	.00	1259.19	3.45	1.19	2471.49	2152.17
*	98500.000	340.00	.00	.00	1253.10	75.00	1254.81	.00	1254.81	.01	.02	608.91	823.89
*	98500.000	340.00	.00	.00	1253.10	250.00	1255.50	.00	1255.50	.05	.07	851.55	1077.16
	98500.000	340.00	.00	.00	1253.10	500.00	1255.53	.00	1255.55	.21	.14	865.08	1089.71
	98500.000	340.00	.00	.00	1253.10	1200.00	1256.63	.00	1256.69	.56	.32	1397.72	1600.97
*	98500.000	340.00	.00	.00	1249.49	2400.00	1257.83	.00	1257.94	1.09	.57	2099.91	2294.54
*	98500.000	340.00	.00	.00	1249.49	4000.00	1259.10	.00	1259.27	1.50	.80	2987.52	3268.39
	98815.000	255.00	.00	.00	1254.00	75.00	1254.81	.00	1254.81	.28	.03	145.26	140.54
	98815.000	255.00	.00	.00	1252.40	250.00	1255.48	.00	1255.51	.84	.17	325.46	273.40
*	98815.000	255.00	.00	.00	1252.40	500.00	1255.46	.00	1255.56	3.48	.34	318.55	268.19
*	98815.000	255.00	.00	.00	1252.40	1200.00	1256.53	.00	1256.72	4.44	.68	709.40	569.44
	98815.000	255.00	.00	.00	1252.40	2400.00	1257.71	.00	1257.99	5.37	1.03	1340.62	1036.05
	98815.000	255.00	.00	.00	1252.40	4000.00	1258.99	.00	1259.33	5.07	1.27	2210.85	1775.94
	99000.000	180.00	.00	.00	1254.20	75.00	1254.81	.00	1254.82	.36	.06	153.34	125.05
	99000.000	180.00	.00	.00	1253.10	250.00	1255.50	.00	1255.52	.98	.21	314.74	251.96
	99000.000	180.00	.00	.00	1253.10	500.00	1255.53	.00	1255.63	3.71	.42	324.10	259.74
	99000.000	180.00	.00	.00	1253.10	1200.00	1256.60	.00	1256.80	4.85	.77	653.21	544.68
	99000.000	180.00	.00	.00	1253.10	2400.00	1257.79	.00	1258.10	5.96	1.15	1218.31	983.16
	99000.000	180.00	.00	.00	1253.10	4000.00	1259.06	.00	1259.43	5.76	1.40	2009.42	1666.36
	99080.000	78.00	.00	.00	1254.51	75.00	1254.81	.00	1254.82	.47	.05	103.91	109.55
	99080.000	78.00	.00	.00	1253.10	250.00	1255.49	.00	1255.53	1.48	.17	202.51	205.70
	99080.000	78.00	.00	.00	1253.10	500.00	1255.48	.00	1255.66	6.02	.33	200.38	203.79
	99080.000	78.00	.00	.00	1253.10	1200.00	1256.49	.00	1256.85	8.31	.62	449.37	416.31
	99080.000	78.00	.00	.00	1253.10	2400.00	1257.69	.00	1258.15	8.52	1.02	945.74	822.27
	99080.000	78.00	.00	.00	1253.10	4000.00	1259.06	.00	1259.48	6.97	1.29	1792.30	1515.29

	SECNO	XLCH	ELTRD	ELLC	ELMIN	Q	CWSEL	CRIWS	EG	10*KS	VCH	AREA	.01K
	99167.000	87.00	.00	.00	1255.20	75.00	1255.60	1255.60	1255.61	.15	.03	148.79	196.64
*	99167.000	87.00	.00	.00	1255.20	250.00	1255.61	1255.61	1255.66	1.61	.09	148.99	196.92
*	99167.000	87.00	.00	.00	1255.20	500.00	1255.61	1255.61	1255.80	6.45	.19	148.92	196.83
	99167.000	87.00	.00	.00	1253.20	1200.00	1256.40	.00	1256.94	12.63	.55	253.78	337.61
	99167.000	87.00	.00	.00	1255.20	2400.00	1257.06	1257.06	1258.31	23.81	1.15	557.58	491.82
	99167.000	87.00	.00	.00	1253.20	4000.00	1258.77	.00	1259.56	12.48	1.52	1543.46	1132.44
	99266.000	99.00	.00	.00	1255.20	75.00	1255.61	.00	1255.61	.15	.03	148.97	196.90
	99266.000	99.00	.00	.00	1255.20	250.00	1255.62	.00	1255.67	1.56	.10	151.13	199.91
	99266.000	99.00	.00	.00	1255.20	500.00	1255.68	.00	1255.86	5.67	.21	158.35	209.97
	99266.000	99.00	.00	.00	1253.20	1200.00	1256.59	.00	1257.05	10.11	.54	286.44	377.49
*	99266.000	99.00	.00	.00	1255.20	2400.00	1257.85	1257.04	1258.46	10.68	1.09	960.65	734.44
	99266.000	99.00	.00	.00	1253.20	4000.00	1259.00	.00	1259.67	10.23	1.45	1704.21	1250.73
	99267.000	1.00	.00	.00	1254.60	30.89	1255.61	.00	1255.61	.06	.18	167.97	124.23
*	99267.000	1.00	.00	.00	1254.60	196.10	1255.65	1255.20	1255.67	2.17	1.10	175.37	133.09
*	99267.000	1.00	.00	.00	1254.60	469.97	1255.39	1255.39	1255.65	47.83	4.01	115.41	67.95
	99267.000	1.00	.00	.00	1254.50	722.46	1257.03	.00	1257.05	.83	1.22	584.28	791.29
	99267.000	1.00	.00	.00	1254.50	1250.25	1258.45	.00	1258.46	.28	1.06	1313.00	2343.33
*	99267.000	1.00	.00	.00	1254.50	2137.90	1259.66	.00	1259.67	.23	1.18	2038.76	4498.15
	99327.000	60.00	.00	.00	1254.50	75.00	1255.61	.00	1255.61	.26	.35	206.71	147.33
	99327.000	60.00	.00	.00	1254.50	250.00	1255.66	.00	1255.68	2.22	1.08	224.00	167.75
	99327.000	60.00	.00	.00	1254.60	500.00	1255.67	.00	1255.75	8.68	2.14	225.59	169.66
	99327.000	60.00	.00	.00	1254.50	1200.00	1257.02	.00	1257.06	1.44	1.54	728.35	1001.44
	99327.000	60.00	.00	.00	1254.50	2400.00	1258.42	.00	1258.47	.76	1.70	1462.67	2744.32
	99327.000	60.00	.00	.00	1254.50	4000.00	1259.62	.00	1259.68	.64	1.94	2183.01	5011.78
*	99328.000	1.00	.00	.00	1256.30	75.00	1256.84	1256.84	1256.98	57.25	2.98	25.20	9.91

*	99328.000	1.00	.00	.00	1256.30	250.00	1257.18	1257.18	1257.44	48.99	4.08	61.33	35.72
	99328.000	1.00	.00	.00	1256.30	500.00	1257.54	1257.54	1257.83	28.90	4.45	122.74	93.01
	99328.000	1.00	.00	.00	1256.30	1200.00	1258.02	1258.02	1258.45	25.88	5.65	246.16	235.90
	99328.000	1.00	.00	.00	1256.30	2400.00	1258.60	1258.60	1259.05	19.59	6.20	481.62	542.29
*	99328.000	1.00	.00	.00	1256.30	4000.00	1259.50	1258.90	1259.68	2.27	2.49	1411.74	2656.66
	99408.000	81.00	.00	.00	1256.30	75.00	1257.15	.00	1257.18	13.21	1.31	57.05	20.64
	99408.000	81.00	.00	.00	1256.30	250.00	1257.58	.00	1257.66	17.33	2.26	129.97	60.06
	99408.000	81.00	.00	.00	1256.30	500.00	1257.88	.00	1258.05	25.42	3.33	205.50	99.18
*	99408.000	81.00	.00	.00	1256.30	1200.00	1258.11	1258.10	1258.79	81.92	6.68	269.49	132.59
	99408.000	81.00	.00	.00	1256.30	2400.00	1258.91	1258.91	1259.20	3.99	1.74	1026.45	1201.35
	99408.000	81.00	.00	.00	1256.30	4000.00	1258.92	.00	1259.71	10.89	2.90	1038.24	1212.11
*	99500.000	91.00	.00	.00	1257.00	75.00	1257.50	1257.50	1257.63	201.03	3.05	77.47	5.29
*	99500.000	91.00	.00	.00	1257.00	250.00	1257.81	1257.81	1258.09	129.31	4.39	153.56	21.99
	99500.000	91.00	.00	.00	1257.00	500.00	1258.14	1258.14	1258.57	106.38	5.46	238.47	48.48
	99500.000	91.00	.00	.00	1257.00	1200.00	1258.84	1258.84	1259.59	83.47	7.17	441.79	131.35
*	99500.000	91.00	.00	.00	1257.00	2400.00	1259.74	1259.74	1260.89	70.91	8.90	843.90	285.01
*	99500.000	91.00	.00	.00	1257.00	4000.00	1261.18	1261.18	1261.47	3.07	2.07	2215.81	2282.65

	SECNO	XLCH	ELTRD	ELLC	ELMIN	Q	CWSEL	CRIWS	EG	10*KS	VCH	AREA	.01K
*	99717.000	217.00	.00	.00	1258.30	75.00	1258.88	.00	1258.93	28.44	1.96	76.13	14.06
*	99717.000	217.00	.00	.00	1258.30	250.00	1259.31	.00	1259.48	38.18	3.43	170.24	40.46
	99717.000	217.00	.00	.00	1258.30	500.00	1259.69	.00	1260.03	46.14	4.75	288.56	73.61
	99717.000	217.00	.00	.00	1258.30	1200.00	1260.38	1260.28	1261.15	62.62	7.28	563.27	151.65
	99717.000	217.00	.00	.00	1258.30	2400.00	1261.31	1261.31	1262.63	66.43	9.60	983.63	294.47
*	99717.000	217.00	.00	.00	1258.30	4000.00	1262.40	1262.40	1264.21	61.78	11.31	1494.11	508.89
*	100251.000	470.00	.00	.00	1256.60	75.00	1259.43	1258.36	1259.57	7.96	3.07	24.45	26.59
	100251.000	470.00	.00	.00	1256.60	250.00	1260.31	1259.86	1260.99	27.57	6.64	37.63	47.61
*	100251.000	470.00	.00	.00	1256.60	500.00	1261.18	1261.18	1262.57	44.27	9.47	52.80	75.15
*	100251.000	470.00	.00	.00	1256.60	1200.00	1263.54	1263.54	1265.03	34.34	10.27	822.98	204.77
	100251.000	470.00	.00	.00	1256.60	2400.00	1265.36	1265.36	1267.38	34.71	12.46	1756.13	407.37
	100251.000	470.00	.00	.00	1256.60	4000.00	1267.05	1267.05	1269.74	36.96	14.71	2623.48	657.99
*	100500.000	249.00	.00	.00	1257.00	75.00	1259.61	.00	1259.70	2.62	2.40	31.28	46.34
*	100500.000	249.00	.00	.00	1257.00	250.00	1260.95	.00	1261.39	7.24	5.27	47.48	92.90
	100500.000	249.00	.00	.00	1257.00	500.00	1262.20	.00	1263.20	11.66	8.01	62.38	146.43
	100500.000	249.00	.00	.00	1257.00	1200.00	1264.18	1264.18	1266.44	18.93	12.66	644.97	275.83
*	100500.000	249.00	.00	.00	1257.00	2400.00	1267.01	1267.01	1269.94	18.31	15.55	2151.92	560.80
*	100500.000	249.00	.00	.00	1257.00	4000.00	1269.39	1269.39	1273.35	20.52	18.97	3427.14	882.98
*	100951.000	451.00	1268.60	.00	1261.20	75.00	1263.83	.00	1263.91	1.20	2.38	31.51	68.56
*	100951.000	451.00	1268.60	.00	1261.20	250.00	1265.81	.00	1266.13	2.03	4.51	55.38	175.47
*	100951.000	451.00	1268.60	.00	1261.20	500.00	1267.89	.00	1268.49	2.35	6.23	80.30	326.00
*	100951.000	451.00	1268.60	.00	1261.20	1200.00	1269.67	.00	1271.36	5.21	10.85	346.76	525.74
*	100951.000	451.00	1268.60	.00	1261.20	2400.00	1272.59	1272.59	1275.27	6.23	14.45	1261.31	961.40
*	100951.000	451.00	1268.60	.00	1261.20	4000.00	1275.24	1275.24	1277.79	5.58	15.72	2702.19	1692.73
*	101000.000	49.00	.00	.00	1262.17	75.00	1263.77	1263.77	1264.39	57.26	6.35	11.81	9.91
*	101000.000	49.00	.00	.00	1262.17	250.00	1265.56	.00	1266.44	36.68	7.53	33.19	41.28
*	101000.000	49.00	.00	.00	1262.17	500.00	1267.85	.00	1268.59	17.79	6.88	72.64	118.54
*	101000.000	49.00	.00	.00	1262.17	1200.00	1270.95	.00	1271.68	12.90	6.91	416.01	334.06
*	101000.000	49.00	.00	.00	1262.17	2400.00	1275.92	.00	1276.05	1.41	3.40	2900.20	2022.70
*	101000.000	49.00	.00	.00	1262.17	4000.00	1278.39	.00	1278.53	1.12	3.66	4310.29	3780.31
*	101048.000	48.00	.00	.00	1262.20	75.00	1264.33	.00	1264.65	21.23	4.47	16.77	16.28
	101048.000	48.00	.00	.00	1262.20	250.00	1265.94	.00	1266.64	26.29	6.70	37.33	48.76
	101048.000	48.00	.00	.00	1262.20	500.00	1267.92	.00	1268.69	18.65	7.01	71.36	115.78
	101048.000	48.00	.00	.00	1262.20	1200.00	1270.83	1269.26	1271.94	15.91	8.50	363.18	300.84
	101048.000	48.00	.00	.00	1262.20	2400.00	1275.90	.00	1276.08	1.99	4.42	2806.08	1703.18
	101048.000	48.00	.00	.00	1262.20	4000.00	1278.38	.00	1278.55	1.52	4.51	4250.28	3244.42
	101500.000	452.00	.00	.00	1263.20	75.00	1265.29	.00	1265.55	18.22	4.10	18.30	17.57
	101500.000	452.00	.00	.00	1263.20	250.00	1267.16	.00	1267.62	15.76	5.42	46.09	62.97
	101500.000	452.00	.00	.00	1263.20	500.00	1268.85	.00	1269.46	14.17	6.28	79.81	132.81
	101500.000	452.00	.00	.00	1263.20	1200.00	1271.64	1269.80	1272.62	12.95	8.03	398.63	333.51
	101500.000	452.00	.00	.00	1263.20	2400.00	1275.99	.00	1276.19	2.27	4.63	2833.94	1593.86
	101500.000	452.00	.00	.00	1263.20	4000.00	1278.44	.00	1278.63	1.69	4.68	4544.36	3076.67

SECNO	XLCH	ELTRD	ELLC	ELMIN	Q	CWSEL	CRIWS	EG	10*KS	VCH	AREA	.01K
102000.000	500.00	.00	.00	1263.70	75.00	1266.09	.00	1266.26	10.58	3.27	22.95	23.06
102000.000	500.00	.00	.00	1263.70	250.00	1267.99	.00	1268.28	9.97	4.38	57.13	79.18
102000.000	500.00	.00	.00	1263.70	500.00	1269.72	.00	1270.10	9.21	4.91	105.27	164.75
102000.000	500.00	.00	.00	1263.70	1200.00	1272.84	.00	1273.18	4.57	4.99	1065.95	561.54
102000.000	500.00	.00	.00	1263.70	2400.00	1276.15	.00	1276.30	1.56	3.95	3282.77	1923.98
102000.000	500.00	.00	.00	1263.70	4000.00	1278.56	.00	1278.71	1.27	4.17	4969.96	3550.56
102500.000	500.00	.00	.00	1264.60	75.00	1266.89	.00	1267.16	31.52	4.15	18.08	13.36
102500.000	500.00	.00	.00	1264.60	250.00	1268.71	.00	1269.18	31.10	5.49	45.51	44.83
* 102500.000	500.00	.00	.00	1264.60	500.00	1270.34	1269.19	1270.89	23.85	5.99	152.53	102.38
102500.000	500.00	.00	.00	1264.60	1200.00	1273.20	.00	1273.49	8.02	5.03	1271.16	423.72
102500.000	500.00	.00	.00	1264.60	2400.00	1276.29	.00	1276.39	1.78	3.15	3408.69	1800.28
102500.000	500.00	.00	.00	1264.60	4000.00	1278.66	.00	1278.79	1.31	3.17	5070.42	3499.15
* 103000.000	500.00	.00	.00	1264.90	75.00	1267.79	.00	1267.88	7.29	2.39	31.41	27.77
103000.000	500.00	.00	.00	1264.90	250.00	1269.82	.00	1270.01	8.61	3.47	94.07	85.18
103000.000	500.00	.00	.00	1264.90	500.00	1271.37	.00	1271.66	8.97	4.38	422.22	166.98
103000.000	500.00	.00	.00	1264.90	1200.00	1273.62	.00	1273.86	6.38	4.59	1587.25	474.95
103000.000	500.00	.00	.00	1264.90	2400.00	1276.38	.00	1276.50	2.09	3.38	3505.63	1659.27
103000.000	500.00	.00	.00	1264.90	4000.00	1278.73	.00	1278.86	1.48	3.33	5150.01	3288.38
103500.000	480.00	.00	.00	1266.00	75.00	1268.31	.00	1268.50	23.06	3.52	21.28	15.62
103500.000	480.00	.00	.00	1266.00	250.00	1270.30	.00	1270.60	15.29	4.37	82.06	63.93
103500.000	480.00	.00	.00	1266.00	500.00	1271.85	.00	1272.26	14.44	5.30	371.23	131.56
103500.000	480.00	.00	.00	1266.00	1200.00	1273.96	.00	1274.19	7.02	4.59	1431.10	452.98
103500.000	480.00	.00	.00	1266.00	2400.00	1276.48	.00	1276.61	2.50	3.52	2961.46	1518.53
103500.000	480.00	.00	.00	1266.00	4000.00	1278.80	.00	1278.95	1.72	3.46	4365.99	3052.15
* 104000.000	480.00	.00	.00	1266.00	75.00	1268.95	.00	1269.03	5.81	2.22	33.84	31.12
104000.000	480.00	.00	.00	1266.00	250.00	1270.94	.00	1271.14	7.78	3.58	156.15	89.63
104000.000	480.00	.00	.00	1266.00	500.00	1272.54	.00	1272.83	8.71	4.53	662.96	169.39
104000.000	480.00	.00	.00	1266.00	1200.00	1274.31	.00	1274.49	5.25	4.22	1753.89	523.80
104000.000	480.00	.00	.00	1266.00	2400.00	1276.61	.00	1276.74	2.50	3.58	3361.27	1517.87
104000.000	480.00	.00	.00	1266.00	4000.00	1278.88	.00	1279.03	1.75	3.50	4955.93	3023.33
104500.000	500.00	.00	.00	1266.18	75.00	1269.28	.00	1269.36	7.55	2.33	32.17	27.30
104500.000	500.00	.00	.00	1266.18	250.00	1271.35	.00	1271.52	7.04	3.33	219.27	94.22
104500.000	500.00	.00	.00	1266.18	500.00	1273.00	.00	1273.24	7.06	4.09	747.59	188.15
104500.000	500.00	.00	.00	1266.18	1200.00	1274.59	.00	1274.75	4.55	3.85	1749.77	562.31
104500.000	500.00	.00	.00	1266.18	2400.00	1276.73	.00	1276.86	2.55	3.53	3236.73	1502.07
104500.000	500.00	.00	.00	1266.18	4000.00	1278.98	.00	1279.12	1.75	3.43	4807.20	3023.93
104818.000	318.00	.00	.00	1266.10	75.00	1269.48	.00	1269.53	3.24	1.75	42.94	41.70
104818.000	318.00	.00	.00	1266.10	250.00	1271.58	.00	1271.70	4.31	2.82	229.73	120.43
104818.000	318.00	.00	.00	1266.10	500.00	1273.26	.00	1273.44	4.70	3.53	969.71	230.59
104818.000	318.00	.00	.00	1266.10	1200.00	1274.81	.00	1274.90	3.87	2.65	2045.30	610.38
104818.000	318.00	.00	.00	1266.10	2400.00	1276.85	.00	1276.95	2.18	2.68	3469.99	1627.24
104818.000	318.00	.00	.00	1266.10	4000.00	1279.06	.00	1279.18	1.57	2.84	5015.51	3192.99

1

SECNO	XLCH	ELTRD	ELLC	ELMIN	Q	CWSEL	CRIWS	EG	10*KS	VCH	AREA	.01K
105000.000	182.00	.00	.00	1266.17	75.00	1269.55	.00	1269.65	9.88	2.59	29.00	23.87
105000.000	182.00	.00	.00	1266.17	250.00	1271.66	.00	1271.82	7.34	3.34	371.39	92.25
105000.000	182.00	.00	.00	1266.17	500.00	1273.35	.00	1273.54	6.46	3.84	1051.99	196.75
* 105000.000	182.00	.00	.00	1266.17	1200.00	1274.72	.00	1275.24	14.76	6.54	1635.78	312.32
105000.000	182.00	.00	.00	1266.17	2400.00	1276.88	.00	1276.99	2.15	3.10	3161.51	1637.37
105000.000	182.00	.00	.00	1266.17	4000.00	1279.08	.00	1279.21	1.55	3.13	4480.45	3216.38
* 105294.000	294.00	.00	.00	1267.42	75.00	1269.98	.00	1270.33	50.93	4.75	15.80	10.51
* 105294.000	294.00	.00	.00	1267.42	250.00	1271.92	.00	1272.33	28.19	5.14	48.66	47.08
105294.000	294.00	.00	.00	1267.42	500.00	1273.68	.00	1273.73	4.06	2.24	1212.34	248.07
105294.000	294.00	.00	.00	1267.42	1200.00	1275.44	.00	1275.51	2.30	2.36	2378.46	791.30
105294.000	294.00	.00	.00	1267.42	2400.00	1276.95	.00	1277.06	2.40	2.92	3434.79	1549.82
105294.000	294.00	.00	.00	1267.42	4000.00	1279.12	.00	1279.26	1.74	3.06	4955.10	3032.64

SUMMARY PRINTOUT TABLE 150

	SECNO	Q	CWSEL	DIFWSP	DIFWSX	DIFKWS	TOPWID	XLCH
	84000.000	75.00	1248.42	.00	.00	-.08	68.14	.00
*	84000.000	250.00	1248.47	.05	.00	-.03	68.41	.00
*	84000.000	500.00	1248.91	.44	.00	.16	70.69	.00
*	84000.000	1200.00	1249.90	.99	.00	.01	440.13	.00
*	84000.000	2400.00	1249.93	.03	.00	-.03	441.00	.00
*	84000.000	4000.00	1249.89	-.04	.00	-.61	439.83	.00
	84500.000	75.00	1248.69	.00	.27	.00	64.89	500.00
*	84500.000	250.00	1249.41	.72	.94	.00	67.75	500.00
*	84500.000	500.00	1250.04	.64	1.13	.00	70.27	500.00
*	84500.000	1200.00	1250.12	.08	.22	.00	70.54	500.00
*	84500.000	2400.00	1251.36	1.24	1.43	.00	75.47	500.00
*	84500.000	4000.00	1253.13	1.78	3.24	.00	700.00	500.00
	85000.000	75.00	1248.92	.00	.23	.00	71.12	500.00
	85000.000	250.00	1249.71	.79	.30	.00	94.67	500.00
	85000.000	500.00	1250.42	.72	.38	.00	141.94	500.00
*	85000.000	1200.00	1251.58	1.15	1.46	.00	172.74	500.00
*	85000.000	2400.00	1253.15	1.58	1.80	.00	402.49	500.00
	85000.000	4000.00	1253.41	.26	.28	.00	462.88	500.00
	85500.000	75.00	1249.09	.00	.18	.00	70.57	500.00
	85500.000	250.00	1249.91	.81	.20	.00	73.78	500.00
	85500.000	500.00	1250.62	.72	.20	.00	140.33	500.00
	85500.000	1200.00	1251.83	1.21	.25	.00	492.24	500.00
	85500.000	2400.00	1253.33	1.50	.17	.00	670.53	500.00
	85500.000	4000.00	1253.81	.48	.39	.00	700.00	500.00
	86024.000	75.00	1249.25	.00	.15	.00	66.74	524.00
	86024.000	250.00	1250.08	.84	.18	.00	134.49	524.00
	86024.000	500.00	1250.81	.73	.19	.00	136.62	524.00
	86024.000	1200.00	1252.00	1.19	.18	.00	140.05	524.00
	86024.000	2400.00	1253.50	1.49	.17	.00	645.05	524.00
	86024.000	4000.00	1254.15	.66	.34	.00	668.36	524.00
*	86415.000	75.00	1249.30	.00	.06	.00	51.99	391.00
*	86415.000	250.00	1250.20	.89	.11	.00	54.41	391.00
	86415.000	500.00	1250.93	.73	.12	.00	99.63	391.00
	86415.000	1200.00	1252.08	1.15	.08	.00	297.03	391.00
	86415.000	2400.00	1253.53	1.45	.03	.00	482.50	391.00
*	86415.000	4000.00	1252.97	-.55	-1.18	.00	420.62	391.00

	SECNO	Q	CWSEL	DIFWSP	DIFWSX	DIFKWS	TOPWID	XLCH
*	87000.000	75.00	1249.30	.00	-.01	.00	61.18	585.00
*	87000.000	250.00	1250.29	.99	.09	.00	66.92	585.00
	87000.000	500.00	1251.14	.85	.21	.00	405.69	585.00
	87000.000	1200.00	1252.38	1.24	.30	.00	545.98	585.00
	87000.000	2400.00	1253.71	1.33	.18	.00	700.00	585.00
	87000.000	4000.00	1254.44	.73	1.46	.00	700.00	585.00
*	87500.000	75.00	1249.75	.00	.45	.00	64.03	500.00
	87500.000	250.00	1250.58	.83	.30	.00	67.46	500.00
	87500.000	500.00	1251.39	.81	.25	.00	70.85	500.00
	87500.000	1200.00	1252.69	1.30	.31	.00	378.53	500.00
	87500.000	2400.00	1254.19	1.51	.48	.00	700.00	500.00
	87500.000	4000.00	1255.27	1.08	.84	.00	700.00	500.00
	88000.000	75.00	1249.92	.00	.17	.00	64.65	500.00
	88000.000	250.00	1250.79	.87	.21	.00	69.21	500.00
	88000.000	500.00	1251.62	.83	.23	.00	296.71	500.00
	88000.000	1200.00	1253.01	1.40	.33	.00	637.55	500.00
	88000.000	2400.00	1254.63	1.62	.44	.00	700.00	500.00
	88000.000	4000.00	1255.81	1.18	.54	.00	700.00	500.00
	88500.000	75.00	1250.06	.00	.14	.00	67.37	500.00
	88500.000	250.00	1250.97	.91	.18	.00	81.89	500.00
	88500.000	500.00	1251.82	.85	.20	.00	381.76	500.00
	88500.000	1200.00	1253.30	1.48	.28	.00	655.26	500.00
	88500.000	2400.00	1254.97	1.68	.35	.00	700.00	500.00
	88500.000	4000.00	1256.27	1.29	.46	.00	700.00	500.00
	89000.000	75.00	1250.19	.00	.13	.00	68.39	500.00
	89000.000	250.00	1251.12	.93	.15	.00	285.56	500.00
	89000.000	500.00	1251.96	.84	.14	.00	327.87	500.00
	89000.000	1200.00	1253.45	1.49	.16	.00	512.17	500.00
	89000.000	2400.00	1255.10	1.65	.12	.00	665.35	500.00
	89000.000	4000.00	1256.40	1.30	.13	.00	700.00	500.00
	89545.000	75.00	1250.35	.00	.16	.00	57.20	455.00
	89545.000	250.00	1251.25	.90	.13	.00	61.01	455.00
	89545.000	500.00	1252.09	.84	.14	.00	250.41	455.00
	89545.000	1200.00	1253.58	1.48	.13	.00	437.11	455.00
	89545.000	2400.00	1255.21	1.63	.11	.00	589.38	455.00
	89545.000	4000.00	1256.53	1.32	.13	.00	685.61	455.00
	90000.000	75.00	1250.56	.00	.21	.00	69.80	545.00
	90000.000	250.00	1251.50	.94	.25	.00	93.23	545.00
*	90000.000	500.00	1252.37	.87	.27	.00	261.87	545.00
	90000.000	1200.00	1253.80	1.44	.22	.00	425.76	545.00
	90000.000	2400.00	1255.44	1.64	.23	.00	570.17	545.00
	90000.000	4000.00	1256.83	1.39	.30	.00	700.00	545.00

	SECNO	Q	CWSEL	DIFWSP	DIFWSX	DIFKWS	TOPWID	XLCH
*	90500.000	75.00	1250.60	.00	.04	.00	70.47	500.00
*	90500.000	250.00	1251.58	.99	.09	.00	159.57	500.00
*	90500.000	500.00	1252.47	.89	.10	.00	298.52	500.00
	90500.000	1200.00	1253.93	1.46	.13	.00	380.09	500.00
	90500.000	2400.00	1255.56	1.62	.12	.00	572.75	500.00
	90500.000	4000.00	1256.96	1.40	.13	.00	679.84	500.00
*	91000.000	75.00	1250.59	.00	-.01	.00	64.86	500.00
*	91000.000	250.00	1251.59	1.00	.01	.00	186.33	500.00
*	91000.000	500.00	1252.46	.87	-.01	.00	224.90	500.00
*	91000.000	1200.00	1253.88	1.42	-.05	.00	351.55	500.00
*	91000.000	2400.00	1255.40	1.51	-.16	.00	524.96	500.00
*	91000.000	4000.00	1256.73	1.34	-.23	.00	615.80	500.00
	91500.000	75.00	1250.75	.00	.16	.00	63.71	500.00
	91500.000	250.00	1251.75	1.00	.16	.00	163.05	500.00
	91500.000	500.00	1252.63	.89	.17	.00	271.21	500.00
	91500.000	1200.00	1254.15	1.52	.27	.00	358.44	500.00
*	91500.000	2400.00	1255.83	1.68	.44	.00	519.17	500.00
*	91500.000	4000.00	1257.29	1.46	.56	.00	660.09	500.00
	92000.000	75.00	1250.89	.00	.14	.00	62.33	500.00
	92000.000	250.00	1251.88	.99	.13	.00	74.94	500.00
	92000.000	500.00	1252.73	.86	.10	.00	121.73	500.00
	92000.000	1200.00	1254.23	1.49	.08	.00	334.22	500.00
	92000.000	2400.00	1255.89	1.66	.06	.00	493.39	500.00
	92000.000	4000.00	1257.34	1.45	.04	.00	617.68	500.00
	92500.000	75.00	1251.01	.00	.13	.00	65.00	500.00
	92500.000	250.00	1252.03	1.01	.15	.00	83.51	500.00
	92500.000	500.00	1252.90	.87	.16	.00	225.12	500.00
	92500.000	1200.00	1254.41	1.51	.18	.00	318.45	500.00
	92500.000	2400.00	1256.05	1.64	.16	.00	580.24	500.00
	92500.000	4000.00	1257.52	1.46	.18	.00	587.77	500.00
	93000.000	75.00	1251.15	.00	.13	.00	60.15	500.00
	93000.000	250.00	1252.16	1.01	.13	.00	63.48	500.00
	93000.000	500.00	1253.01	.85	.11	.00	66.29	500.00
	93000.000	1200.00	1254.48	1.47	.07	.00	311.68	500.00
	93000.000	2400.00	1255.98	1.50	-.08	.00	437.48	500.00
*	93000.000	4000.00	1257.37	1.39	-.15	.00	634.80	500.00
*	93574.000	75.00	1253.53	.00	2.38	.00	109.21	426.00
*	93574.000	250.00	1253.82	.29	1.66	.00	182.14	426.00
*	93574.000	500.00	1254.01	.19	1.00	.00	371.51	426.00
	93574.000	1200.00	1254.77	.76	.29	.00	480.09	426.00
*	93574.000	2400.00	1254.81	.04	-1.17	.00	484.96	426.00
*	93574.000	4000.00	1255.49	.67	-1.88	.00	511.07	426.00

	SECNO	Q	CWSEL	DIFWSP	DIFWSX	DIFKWS	TOPWID	XLCH
*	94000.000	75.00	1251.68	.00	-1.85	.00	18.24	574.00
*	94000.000	250.00	1254.09	2.42	.27	.00	280.76	574.00
*	94000.000	500.00	1254.18	.09	.17	.00	289.65	574.00
*	94000.000	1200.00	1255.06	.88	.29	.00	379.37	574.00
*	94000.000	2400.00	1255.85	.79	1.04	.00	496.93	574.00
*	94000.000	4000.00	1254.81	-1.04	-.67	.00	349.63	574.00
*	94500.000	75.00	1253.90	.00	2.23	.00	135.88	500.00
*	94500.000	250.00	1254.10	.20	.01	.00	153.82	500.00
	94500.000	500.00	1254.21	.11	.03	.00	250.73	500.00
	94500.000	1200.00	1255.14	.93	.08	.00	403.89	500.00
	94500.000	2400.00	1256.04	.90	.19	.00	481.98	500.00
*	94500.000	4000.00	1256.53	.49	1.72	.00	524.44	500.00
*	95000.000	75.00	1254.77	.00	.87	.00	199.46	500.00
*	95000.000	250.00	1255.40	.63	1.30	.00	259.73	500.00
*	95000.000	500.00	1254.84	-.56	.63	.00	207.17	500.00
*	95000.000	1200.00	1255.29	.45	.15	.00	253.87	500.00
	95000.000	2400.00	1256.05	.76	.00	.00	370.43	500.00
	95000.000	4000.00	1256.44	.39	-.09	.00	387.72	500.00
*	95500.000	75.00	1254.78	.00	.01	.00	381.47	500.00
*	95500.000	250.00	1255.43	.65	.03	.00	386.30	500.00
*	95500.000	500.00	1255.24	-.19	.40	.00	384.86	500.00
*	95500.000	1200.00	1256.00	.76	.71	.00	390.51	500.00
	95500.000	2400.00	1256.63	.63	.58	.00	579.02	500.00
*	95500.000	4000.00	1257.66	1.03	1.22	.00	684.74	500.00
	96000.000	75.00	1254.78	.00	.00	.00	294.39	500.00
	96000.000	250.00	1255.44	.66	.01	.00	418.62	500.00
	96000.000	500.00	1255.28	-.16	.04	.00	401.69	500.00
	96000.000	1200.00	1256.09	.81	.08	.00	434.33	500.00
	96000.000	2400.00	1256.83	.75	.20	.00	539.95	500.00
	96000.000	4000.00	1257.86	1.02	.20	.00	625.93	500.00
	96500.000	75.00	1254.79	.00	.00	.00	304.53	500.00
	96500.000	250.00	1255.45	.67	.01	.00	367.33	500.00
	96500.000	500.00	1255.33	-.12	.05	.00	356.39	500.00
	96500.000	1200.00	1256.22	.89	.13	.00	436.35	500.00
	96500.000	2400.00	1257.06	.84	.23	.00	507.45	500.00
	96500.000	4000.00	1258.14	1.08	.29	.00	692.53	500.00
	97000.000	75.00	1254.79	.00	.00	.00	248.16	500.00
	97000.000	250.00	1255.46	.67	.01	.00	355.97	500.00
	97000.000	500.00	1255.36	-.10	.04	.00	349.68	500.00
	97000.000	1200.00	1256.31	.94	.09	.00	391.37	500.00
	97000.000	2400.00	1257.25	.94	.18	.00	520.03	500.00
	97000.000	4000.00	1258.39	1.14	.24	.00	700.00	500.00

	SECNO	Q	CWSEL	DIFWSP	DIFWSX	DIFKWS	TOPWID	XLCH
*	97500.000	75.00	1254.79	.00	.00	.00	137.07	500.00
	97500.000	250.00	1255.47	.68	.01	.00	357.69	500.00
	97500.000	500.00	1255.39	-.07	.03	.00	346.32	500.00
	97500.000	1200.00	1256.37	.97	.06	.00	485.20	500.00
	97500.000	2400.00	1257.37	1.00	.12	.00	555.01	500.00
	97500.000	4000.00	1258.55	1.18	.16	.00	700.00	500.00
*	98000.000	75.00	1254.81	.00	.02	.00	321.73	500.00
	98000.000	250.00	1255.49	.68	.02	.00	367.07	500.00
	98000.000	500.00	1255.49	.01	.10	.00	367.93	500.00
	98000.000	1200.00	1256.57	1.08	.20	.00	442.13	500.00
	98000.000	2400.00	1257.73	1.16	.36	.00	546.99	500.00
	98000.000	4000.00	1259.00	1.27	.45	.00	700.00	500.00
*	98500.000	75.00	1254.81	.00	.00	.00	313.97	340.00
*	98500.000	250.00	1255.50	.68	.01	.00	446.07	340.00
*	98500.000	500.00	1255.53	.03	.03	.00	448.01	340.00
*	98500.000	1200.00	1256.63	1.10	.06	.00	518.72	340.00
*	98500.000	2400.00	1257.83	1.20	.10	.00	661.54	340.00
*	98500.000	4000.00	1259.10	1.28	.10	.00	700.00	340.00
*	98815.000	75.00	1254.81	.00	.00	.00	227.00	255.00
*	98815.000	250.00	1255.48	.67	-.02	.00	309.01	255.00
*	98815.000	500.00	1255.46	-.02	-.06	.00	306.27	255.00
*	98815.000	1200.00	1256.53	1.07	-.10	.00	422.32	255.00
*	98815.000	2400.00	1257.71	1.17	-.12	.00	634.77	255.00
*	98815.000	4000.00	1258.99	1.29	-.11	.00	700.00	255.00
	99000.000	75.00	1254.81	.00	.00	.00	209.81	180.00
	99000.000	250.00	1255.50	.68	.01	.00	261.36	180.00
	99000.000	500.00	1255.53	.03	.06	.00	264.04	180.00
	99000.000	1200.00	1256.60	1.08	.07	.00	359.20	180.00
	99000.000	2400.00	1257.79	1.19	.08	.00	583.97	180.00
	99000.000	4000.00	1259.06	1.27	.07	.00	651.50	180.00
	99080.000	75.00	1254.81	.00	.00	.00	106.55	78.00
	99080.000	250.00	1255.49	.67	-.01	.00	186.16	78.00
	99080.000	500.00	1255.48	.00	-.04	.00	184.76	78.00
	99080.000	1200.00	1256.49	1.01	-.11	.00	308.46	78.00
	99080.000	2400.00	1257.69	1.19	-.10	.00	512.69	78.00
	99080.000	4000.00	1259.06	1.38	.00	.00	696.36	78.00
*	99167.000	75.00	1255.60	.00	.79	.00	108.86	87.00
*	99167.000	250.00	1255.61	.00	.12	.00	108.94	87.00
*	99167.000	500.00	1255.61	.00	.12	.00	108.91	87.00
	99167.000	1200.00	1256.40	.79	-.10	.00	163.22	87.00
*	99167.000	2400.00	1257.06	.66	-.63	.00	442.99	87.00
	99167.000	4000.00	1258.77	1.71	-.30	.00	670.87	87.00

	SECNO	Q	CWSEL	DIFWSP	DIFWSX	DIFKWS	TOPWID	XLCH
	99266.000	75.00	1255.61	.00	.00	.00	108.94	99.00
	99266.000	250.00	1255.62	.02	.02	.00	109.83	99.00
	99266.000	500.00	1255.68	.06	.08	.00	112.75	99.00
	99266.000	1200.00	1256.59	.91	.19	.00	180.45	99.00
*	99266.000	2400.00	1257.85	1.26	.79	.00	587.38	99.00
	99266.000	4000.00	1259.00	1.15	.23	.00	691.66	99.00
*	99267.000	30.89	1255.61	.00	.00	.00	235.51	1.00
*	99267.000	196.10	1255.65	.04	.03	.00	236.56	1.00
*	99267.000	469.97	1255.39	-.26	-.29	.00	227.95	1.00
*	99267.000	722.46	1257.03	1.64	.44	.00	386.07	1.00
*	99267.000	1250.25	1258.45	1.42	.60	.00	600.00	1.00
*	99267.000	2137.90	1259.66	1.21	.66	.00	600.00	1.00
	99327.000	75.00	1255.61	.00	.00	.00	306.97	60.00
	99327.000	250.00	1255.66	.06	.01	.00	308.84	60.00
*	99327.000	500.00	1255.67	.01	.28	.00	309.01	60.00
	99327.000	1200.00	1257.02	1.35	-.01	.00	436.65	60.00
	99327.000	2400.00	1258.42	1.40	-.03	.00	600.00	60.00
	99327.000	4000.00	1259.62	1.20	-.03	.00	600.00	60.00
*	99328.000	75.00	1256.84	.00	1.23	.00	91.32	1.00
*	99328.000	250.00	1257.18	.34	1.52	.00	123.42	1.00
*	99328.000	500.00	1257.54	.36	1.87	.00	216.97	1.00
*	99328.000	1200.00	1258.02	.49	1.01	.00	290.74	1.00
*	99328.000	2400.00	1258.60	.58	.18	.00	461.71	1.00
*	99328.000	4000.00	1259.50	.90	-.12	.00	700.00	1.00
*	99408.000	75.00	1257.15	.00	.31	.00	120.07	81.00
*	99408.000	250.00	1257.58	.43	.40	.00	221.97	81.00
	99408.000	500.00	1257.88	.30	.34	.00	268.68	81.00
*	99408.000	1200.00	1258.11	.23	.08	.00	305.48	81.00
*	99408.000	2400.00	1258.91	.80	.31	.00	614.61	81.00
*	99408.000	4000.00	1258.92	.02	-.58	.00	616.46	81.00
*	99500.000	75.00	1257.50	.00	.35	.00	238.76	91.00
*	99500.000	250.00	1257.81	.31	.23	.00	253.75	91.00
*	99500.000	500.00	1258.14	.32	.26	.00	269.48	91.00
*	99500.000	1200.00	1258.84	.70	.73	.00	348.76	91.00
*	99500.000	2400.00	1259.74	.90	.83	.00	505.72	91.00
*	99500.000	4000.00	1261.18	1.44	2.26	.00	700.00	91.00
*	99717.000	75.00	1258.88	.00	1.37	.00	189.65	217.00
*	99717.000	250.00	1259.31	.43	1.49	.00	263.28	217.00
*	99717.000	500.00	1259.69	.39	1.56	.00	345.95	217.00
	99717.000	1200.00	1260.38	.69	1.54	.00	428.71	217.00
*	99717.000	2400.00	1261.31	.93	1.58	.00	467.49	217.00
*	99717.000	4000.00	1262.40	1.09	1.22	.00	469.83	217.00

SECNO	Q	CWSEL	DIFWSP	DIFWSX	DIFKWS	TOPWID	XLCH
* 100251.000	75.00	1259.43	.00	.55	.00	13.35	470.00
100251.000	250.00	1260.31	.88	1.00	.00	16.21	470.00
* 100251.000	500.00	1261.18	.87	1.49	.00	18.93	470.00
* 100251.000	1200.00	1263.54	2.36	3.16	.00	508.83	470.00
* 100251.000	2400.00	1265.36	1.83	4.05	.00	512.98	470.00
* 100251.000	4000.00	1267.05	1.69	4.65	.00	516.41	470.00
* 100500.000	75.00	1259.61	.00	.18	.00	12.00	249.00
* 100500.000	250.00	1260.95	1.35	.65	.00	12.00	249.00
* 100500.000	500.00	1262.20	1.25	1.02	.00	12.00	249.00
* 100500.000	1200.00	1264.18	1.98	.64	.00	531.02	249.00
* 100500.000	2400.00	1267.01	2.83	1.64	.00	533.79	249.00
* 100500.000	4000.00	1269.39	2.38	2.34	.00	536.12	249.00
* 100951.000	75.00	1263.83	.00	4.22	.00	12.00	451.00
* 100951.000	250.00	1265.81	1.99	4.86	.00	12.00	451.00
* 100951.000	500.00	1267.89	2.08	5.69	.00	12.00	451.00
* 100951.000	1200.00	1269.67	1.78	5.50	.00	180.57	451.00
* 100951.000	2400.00	1272.59	2.92	5.59	.00	504.35	451.00
* 100951.000	4000.00	1275.24	2.64	5.84	.00	567.43	451.00
* 101000.000	75.00	1263.77	.00	-.06	.00	9.53	49.00
* 101000.000	250.00	1265.56	1.79	-.26	.00	14.24	49.00
* 101000.000	500.00	1267.85	2.29	-.04	.00	20.22	49.00
* 101000.000	1200.00	1270.95	3.10	1.28	.00	185.93	49.00
* 101000.000	2400.00	1275.92	4.97	3.33	.00	570.19	49.00
* 101000.000	4000.00	1278.39	2.47	3.15	.00	570.19	49.00
* 101048.000	75.00	1264.33	.00	.57	.00	10.67	48.00
101048.000	250.00	1265.94	1.61	.39	.00	14.71	48.00
101048.000	500.00	1267.92	1.98	.07	.00	19.97	48.00
101048.000	1200.00	1270.83	2.91	-.12	.00	232.80	48.00
101048.000	2400.00	1275.90	5.07	-.02	.00	582.89	48.00
101048.000	4000.00	1278.38	2.48	-.01	.00	582.89	48.00
101500.000	75.00	1265.29	.00	.95	.00	12.16	452.00
101500.000	250.00	1267.16	1.87	1.22	.00	17.48	452.00
101500.000	500.00	1268.85	1.69	.93	.00	24.53	452.00
101500.000	1200.00	1271.64	2.79	.81	.00	245.65	452.00
101500.000	2400.00	1275.99	4.35	.09	.00	697.31	452.00
101500.000	4000.00	1278.44	2.46	.07	.00	697.31	452.00
102000.000	75.00	1266.09	.00	.80	.00	14.39	500.00
102000.000	250.00	1267.99	1.89	.83	.00	21.73	500.00
102000.000	500.00	1269.72	1.74	.87	.00	70.53	500.00
* 102000.000	1200.00	1272.84	3.12	1.20	.00	523.11	500.00
102000.000	2400.00	1276.15	3.31	.16	.00	700.00	500.00
102000.000	4000.00	1278.56	2.41	.12	.00	700.00	500.00

SECNO	Q	CWSEL	DIFWSP	DIFWSX	DIFKWS	TOPWID	XLCH
* 102500.000	75.00	1266.89	.00	.80	.00	11.83	500.00
* 102500.000	250.00	1268.71	1.82	.73	.00	19.18	500.00
* 102500.000	500.00	1270.34	1.62	.61	.00	184.40	500.00
102500.000	1200.00	1273.20	2.86	.36	.00	575.32	500.00
102500.000	2400.00	1276.29	3.09	.14	.00	700.00	500.00
102500.000	4000.00	1278.66	2.38	.10	.00	700.00	500.00
* 103000.000	75.00	1267.79	.00	.90	.00	15.75	500.00
* 103000.000	250.00	1269.82	2.03	1.11	.00	91.02	500.00
* 103000.000	500.00	1271.37	1.55	1.04	.00	318.53	500.00
103000.000	1200.00	1273.62	2.25	.42	.00	626.40	500.00
103000.000	2400.00	1276.38	2.76	.09	.00	700.00	500.00
103000.000	4000.00	1278.73	2.35	.07	.00	700.00	500.00
* 103500.000	75.00	1268.31	.00	.52	.00	14.50	480.00
103500.000	250.00	1270.30	2.00	.49	.00	88.14	480.00
103500.000	500.00	1271.85	1.54	.47	.00	330.39	480.00
103500.000	1200.00	1273.96	2.11	.34	.00	548.72	480.00
103500.000	2400.00	1276.48	2.53	.10	.00	607.91	480.00
103500.000	4000.00	1278.80	2.32	.07	.00	607.91	480.00
* 104000.000	75.00	1268.95	.00	.65	.00	15.69	480.00
* 104000.000	250.00	1270.94	1.99	.64	.00	209.23	480.00
104000.000	500.00	1272.54	1.60	.69	.00	397.80	480.00
104000.000	1200.00	1274.31	1.77	.35	.00	700.00	480.00
104000.000	2400.00	1276.61	2.30	.12	.00	700.00	480.00
104000.000	4000.00	1278.88	2.28	.09	.00	700.00	480.00
104500.000	75.00	1269.28	.00	.33	.00	17.26	500.00
104500.000	250.00	1271.35	2.07	.41	.00	203.99	500.00
104500.000	500.00	1273.00	1.65	.46	.00	433.41	500.00
104500.000	1200.00	1274.59	1.58	.28	.00	644.75	500.00
104500.000	2400.00	1276.73	2.15	.13	.00	700.00	500.00
104500.000	4000.00	1278.98	2.24	.09	.00	700.00	500.00
* 104818.000	75.00	1269.48	.00	.20	.00	18.72	318.00
104818.000	250.00	1271.58	2.10	.23	.00	316.35	318.00
104818.000	500.00	1273.26	1.68	.26	.00	531.27	318.00
104818.000	1200.00	1274.81	1.55	.22	.00	700.00	318.00
104818.000	2400.00	1276.85	2.04	.11	.00	700.00	318.00
104818.000	4000.00	1279.06	2.21	.08	.00	700.00	318.00
* 105000.000	75.00	1269.55	.00	.07	.00	16.44	182.00
105000.000	250.00	1271.66	2.12	.08	.00	332.05	182.00
105000.000	500.00	1273.35	1.69	.09	.00	427.13	182.00
* 105000.000	1200.00	1274.72	1.36	-.09	.00	429.55	182.00
105000.000	2400.00	1276.88	2.17	.04	.00	600.00	182.00
105000.000	4000.00	1279.08	2.20	.03	.00	600.00	182.00

SECNO	Q	CWSEL	DIFWSP	DIFWSX	DIFKWS	TOPWID	XLCH
* 105294.000	75.00	1269.98	.00	.44	.00	12.33	294.00
* 105294.000	250.00	1271.92	1.93	.25	.00	21.62	294.00
105294.000	500.00	1273.68	1.76	.32	.00	639.72	294.00
* 105294.000	1200.00	1275.44	1.76	.72	.00	700.00	294.00
105294.000	2400.00	1276.95	1.51	.06	.00	700.00	294.00
105294.000	4000.00	1279.12	2.18	.04	.00	700.00	294.00

A-6

CANAL OFFSET LINE AND CROSS SECTIONS

SHEET 1
ARCADIA AREA DRAINAGE STUDY - F.C.D. 94-21
CANAL OFFSET LINE STATIONS DATE: 9-8-95

FILE NAME: MAP-INDX.DGN 09-6-95

FILE NAME: MAP XSEC.DGN 09.06.95

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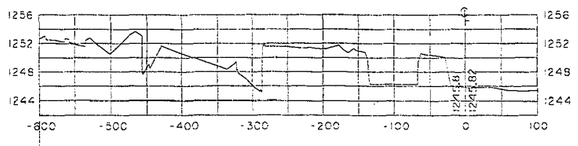

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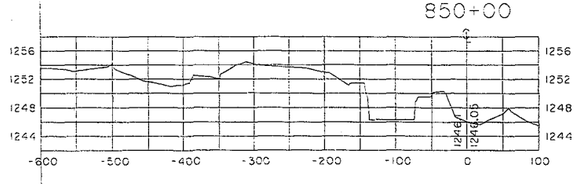

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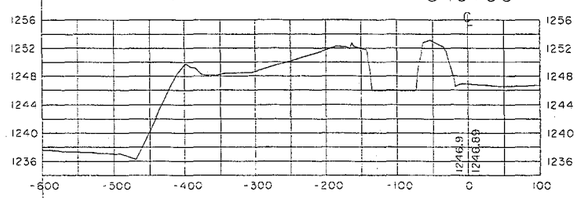

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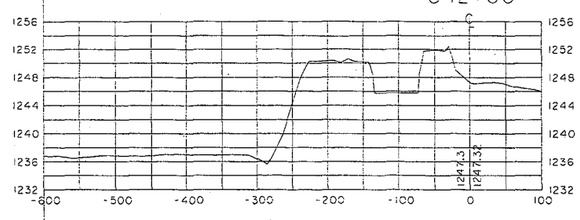

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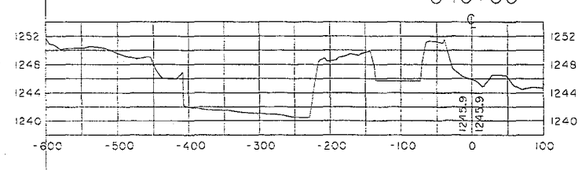

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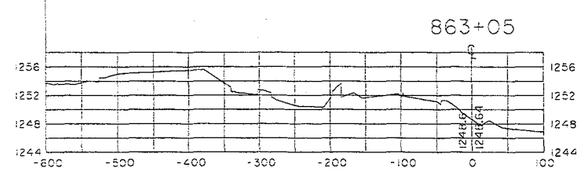

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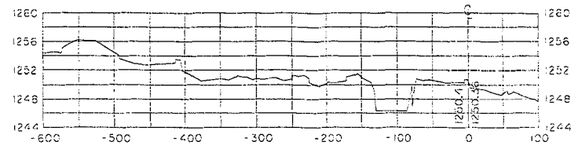

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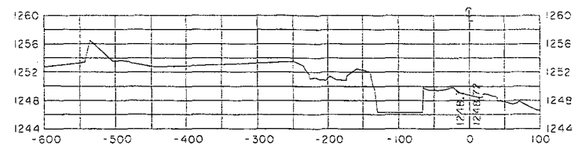

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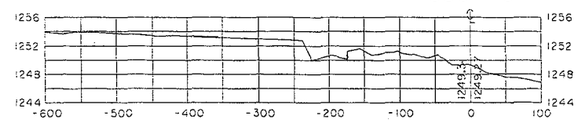

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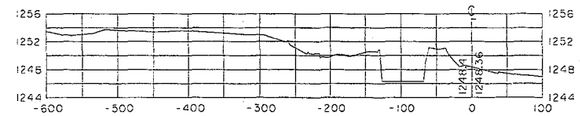
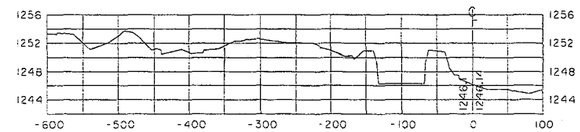


856+72



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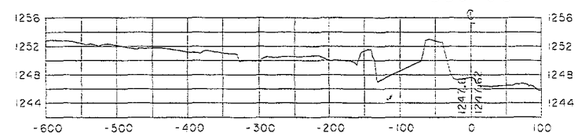
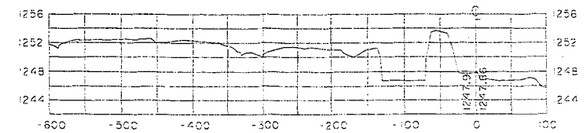
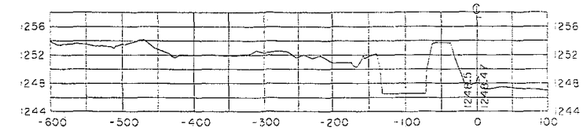


880+00



875+00



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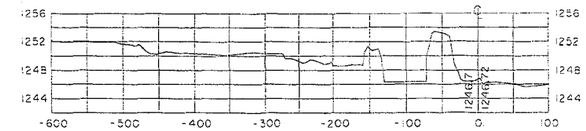

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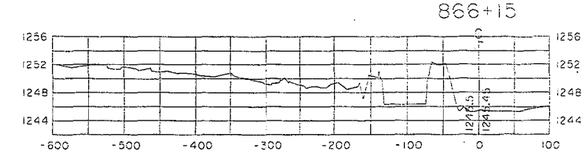
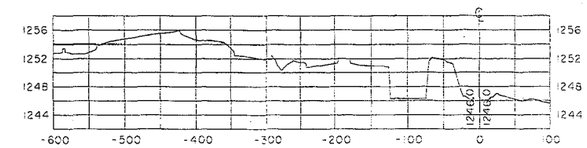
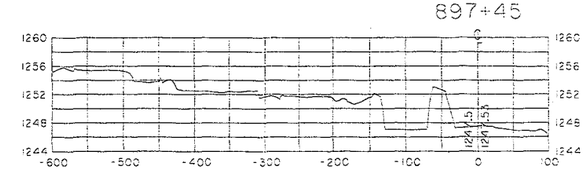


864+15



897+45

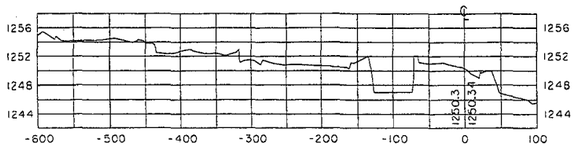


NOTE:
ARIZONA CANAL CHANNEL BOTTOM ELEVATIONS AS SHOWN ON THESE CROSS SECTIONS REFLECT THE WATER SURFACE ELEVATIONS ON THE DATE OF THE AERIAL PHOTOGRAPHY USED TO CREATE THE CROSS SECTIONS AND WERE NOT USED IN THE HEC-2 MODELS INCLUDED WITHIN THIS REPORT. THE CANAL BOTTOM ELEVATIONS USED IN THE HEC-2 MODELS WERE RAISED PER INFORMATION RECEIVED FROM SRP TO REFLECT MAXIMUM OPERATING CONDITIONS.

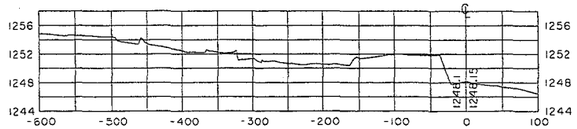
DATE: 9-8-95
ARCADIA AREA DRAINAGE STUDY - F.C.D. 94-21
CANAL OFFSET LINE CROSS SECTIONS 2

FILE NAME: MAP-XSEC.DGN 09-06-95

895+45



894+51



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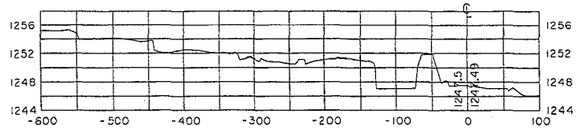

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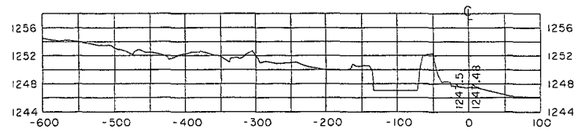

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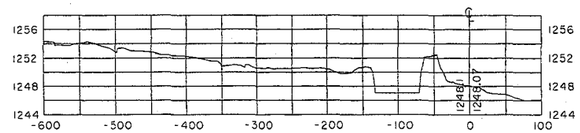
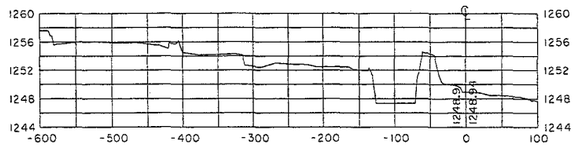
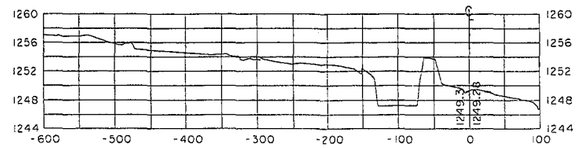


925+00



920+00



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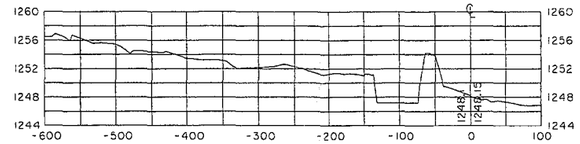

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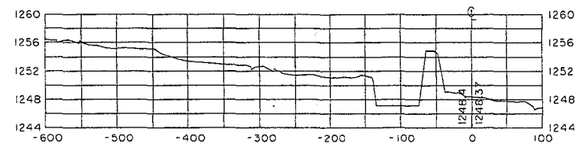
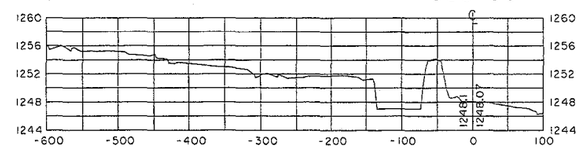


905+00



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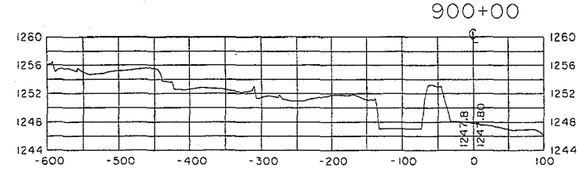
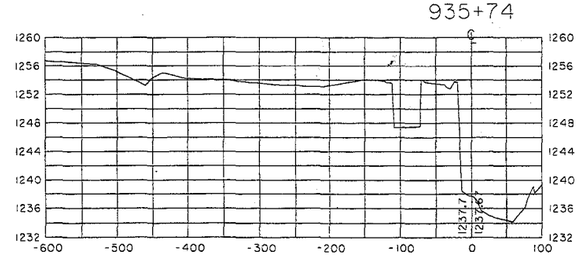


935+74



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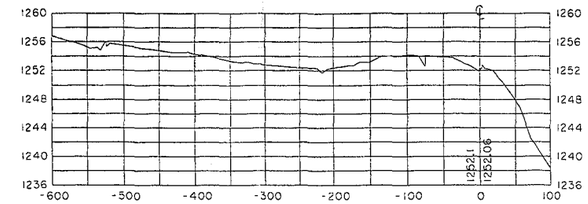

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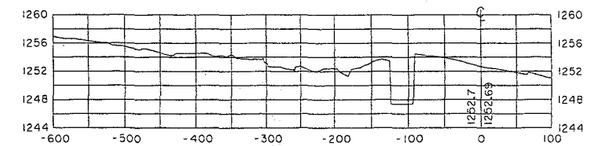
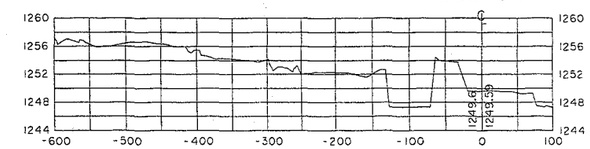


933+34



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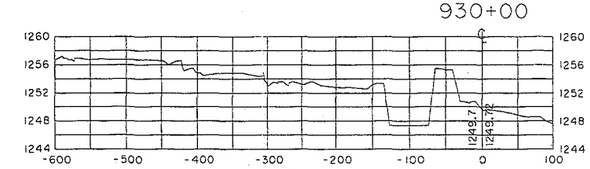

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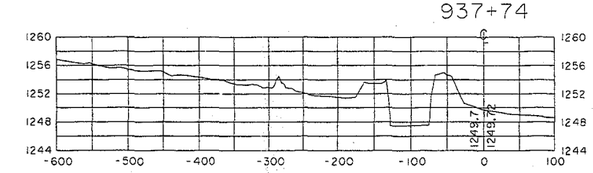


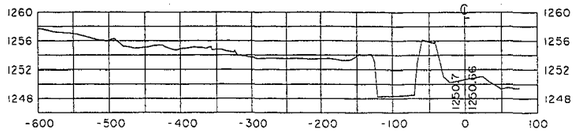
NOTE:
ARIZONA CANAL CHANNEL BOTTOM ELEVATIONS AS SHOWN ON THESE CROSS SECTIONS REFLECT THE WATER SURFACE ELEVATIONS ON THE DATE OF THE AERIAL PHOTOGRAPHY USED TO CREATE THE CROSS SECTIONS AND WERE NOT USED IN THE HEC-2 MODELS INCLUDED WITHIN THIS REPORT. THE CANAL BOTTOM ELEVATIONS USEED IN THE HEC-2 MODELS WERE RAISED PER INFORMATION RECEIVED FROM SRP TO REFLECT MAXIMUM OPERATING CONDITIONS.

DATE: 9-8-95

ARCADIA AREA DRAINAGE STUDY - F.C.D. 94-21
CANAL OFFSET LINE CROSS SECTIONS 3

FILE NAME: MAP-XSEC.DGN 09-06-95

960+00



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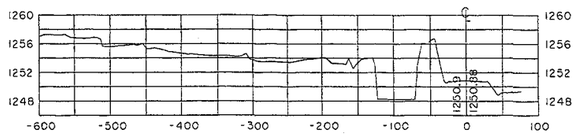
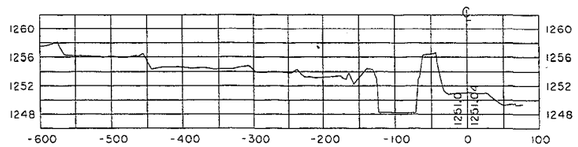


955+00



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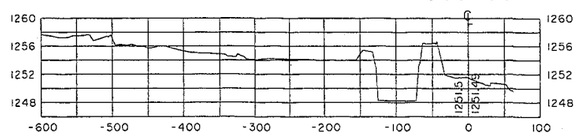
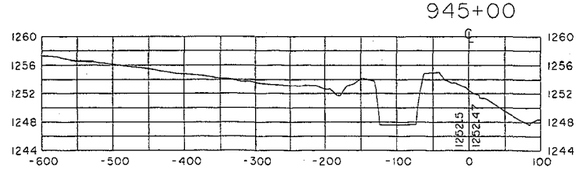


945+00



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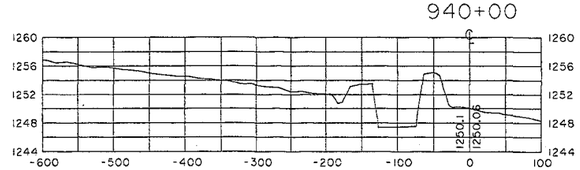

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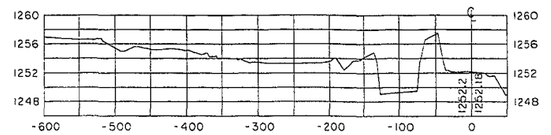

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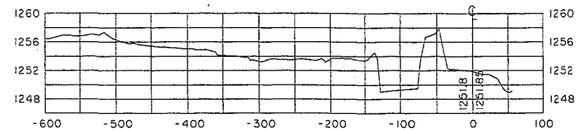

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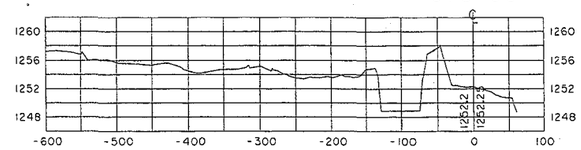

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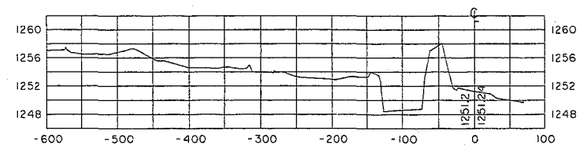

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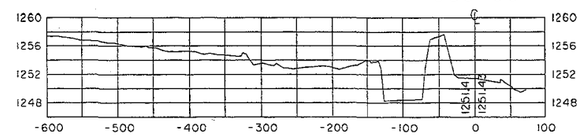

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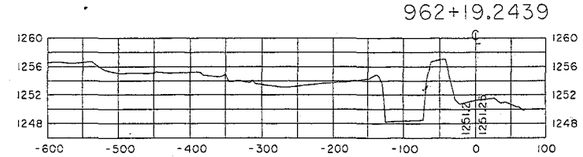

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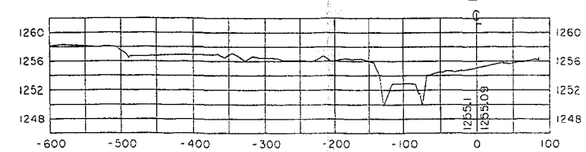

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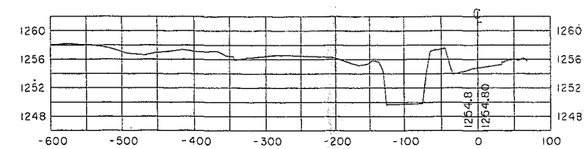

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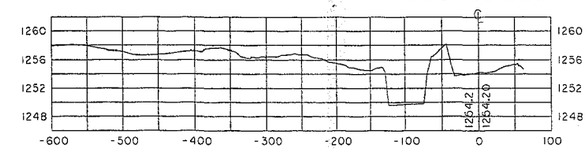
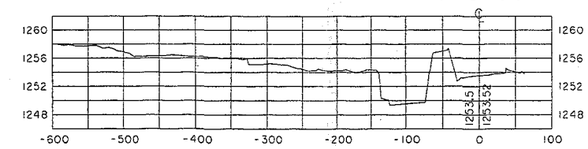
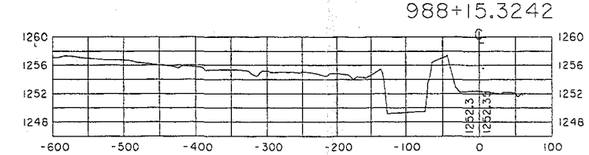


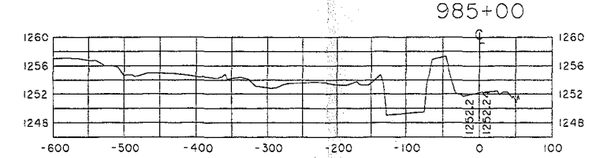
990+00



988+15.3242



985+00



NOTE:
ARIZONA CANAL CHANNEL BOTTOM ELEVATIONS AS SHOWN ON THESE CROSS SECTIONS REFLECT THE WATER SURFACE ELEVATIONS ON THE DATE OF THE AERIAL PHOTOGRAPHY USED TO CREATE THE CROSS SECTIONS AND WERE NOT USED IN THE HEC-2 MODELS INCLUDED WITHIN THIS REPORT. THE CANAL BOTTOM ELEVATIONS USEED IN THE HEC-2 MODELS WERE RAISED PER INFORMATION RECEIVED FROM SRP TO REFLECT MAXIMUM OPERATING CONDITIONS.

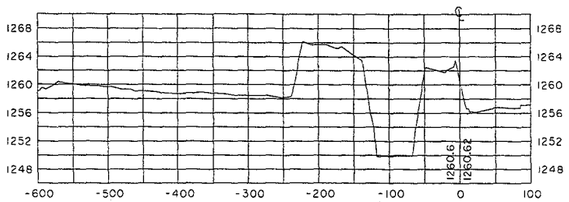
DATE: 9-8-95

ARCADIA AREA DRAINAGE STUDY - F.C.D. 94-21
CANAL OFFSET LINE CROSS SECTIONS 4

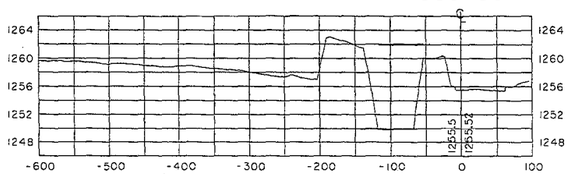
FILE NAME: MAP-XSEC.DGN 09-06-95

NOTE:
ARIZONA CANAL CHANNEL BOTTOM ELEVATIONS AS SHOWN ON THESE CROSS SECTIONS REFLECT THE WATER SURFACE ELEVATIONS ON THE DATE OF THE AERIAL PHOTOGRAPHY USED TO CREATE THE CROSS SECTIONS AND WERE NOT USED IN THE HEC-2 MODELS INCLUDED WITHIN THIS REPORT. THE CANAL BOTTOM ELEVATIONS USEED IN THE HEC-2 MODELS WERE RAISED PER INFORMATION RECEIVED FROM SRP TO REFLECT MAXIMUM OPERATING CONDITIONS.

997+17.3208



995+30



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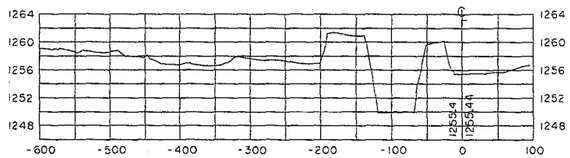

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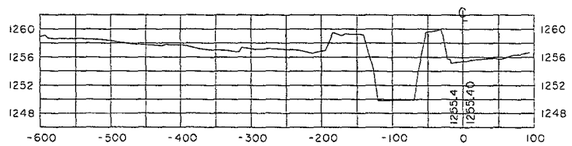

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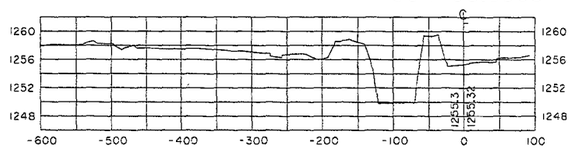

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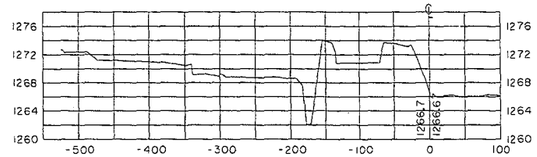

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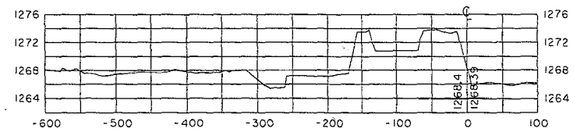

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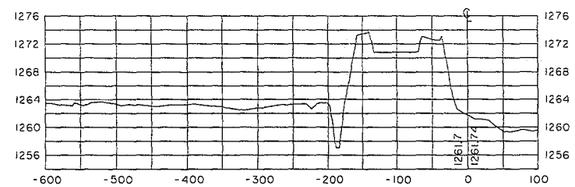

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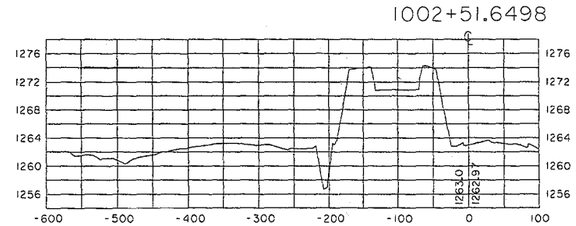

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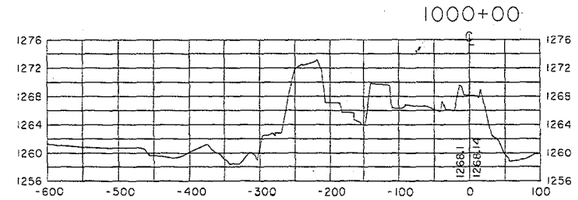
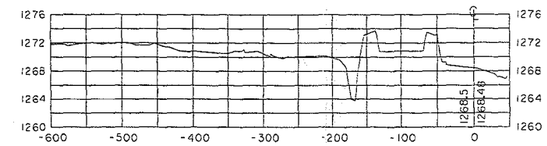
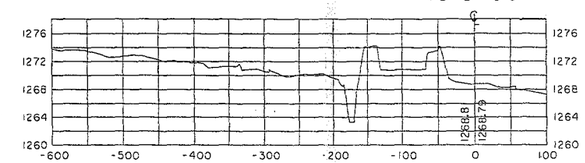


1020+00



1015+00



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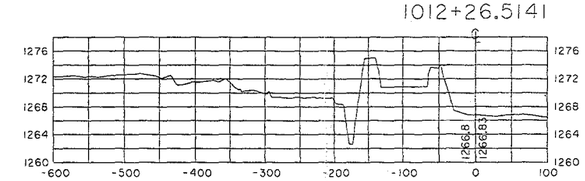

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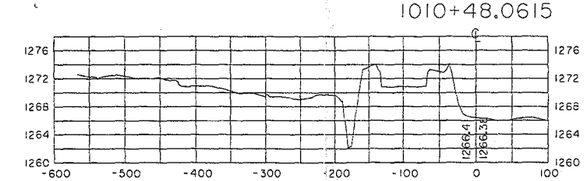

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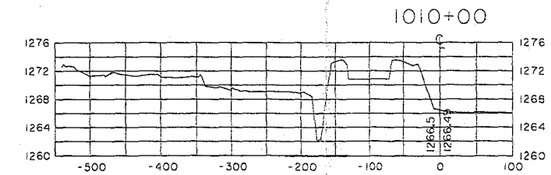
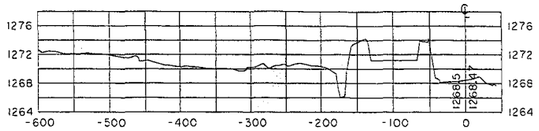


DATE: 9-8-95
ARCADIA AREA DRAINAGE STUDY - F.C.D. 94-21
CANAL OFFSET LINE CROSS SECTIONS 5

FILE NAME: MAP-XSEC.DGN 09-06-95

NOTE:
ARIZONA CANAL CHANNEL BOTTOM ELEVATIONS AS SHOWN ON THESE CROSS SECTIONS REFLECT THE WATER SURFACE ELEVATIONS ON THE DATE OF THE AERIAL PHOTOGRAPHY USED TO CREATE THE CROSS SECTIONS AND WERE NOT USED IN THE HEC-2 MODELS INCLUDED WITHIN THIS REPORT. THE CANAL BOTTOM ELEVATIONS USEED IN THE HEC-2 MODELS WERE RAISED PER INFORMATION RECEIVED FROM SRP TO REFLECT MAXIMUM OPERATING CONDITIONS.

1040+50.0113



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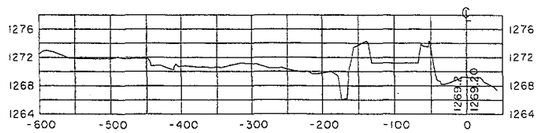
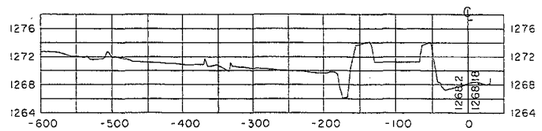
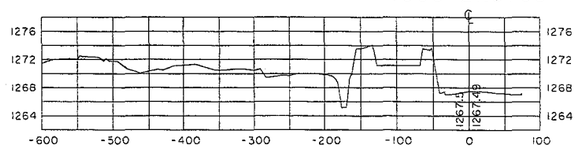


1035+00



1030+21.3753



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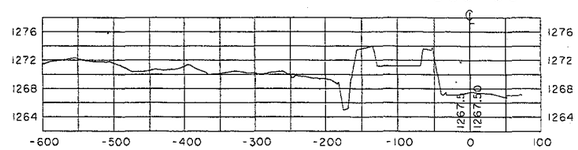
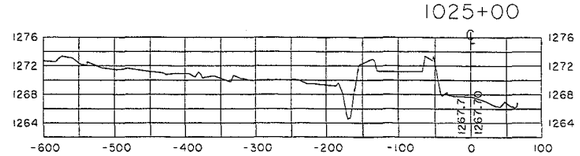
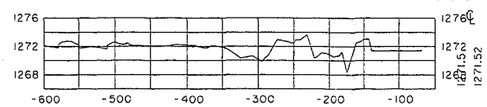


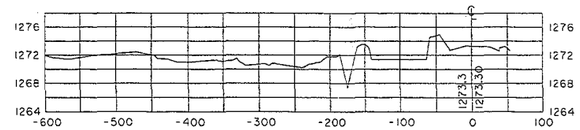
1025+00



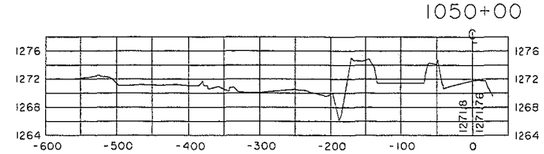
1055+00



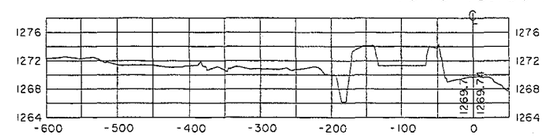
1052+94.8501



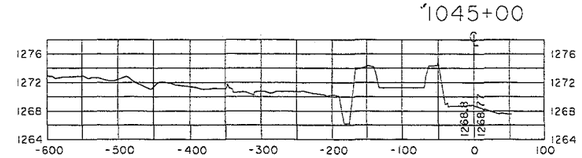
1050+00



1048+18.1804



1045+00



DATE: 9-8-95
ARCADIA AREA DRAINAGE STUDY - F.C.D. 94-21
CANAL OFFSET LINE CROSS SECTIONS 6