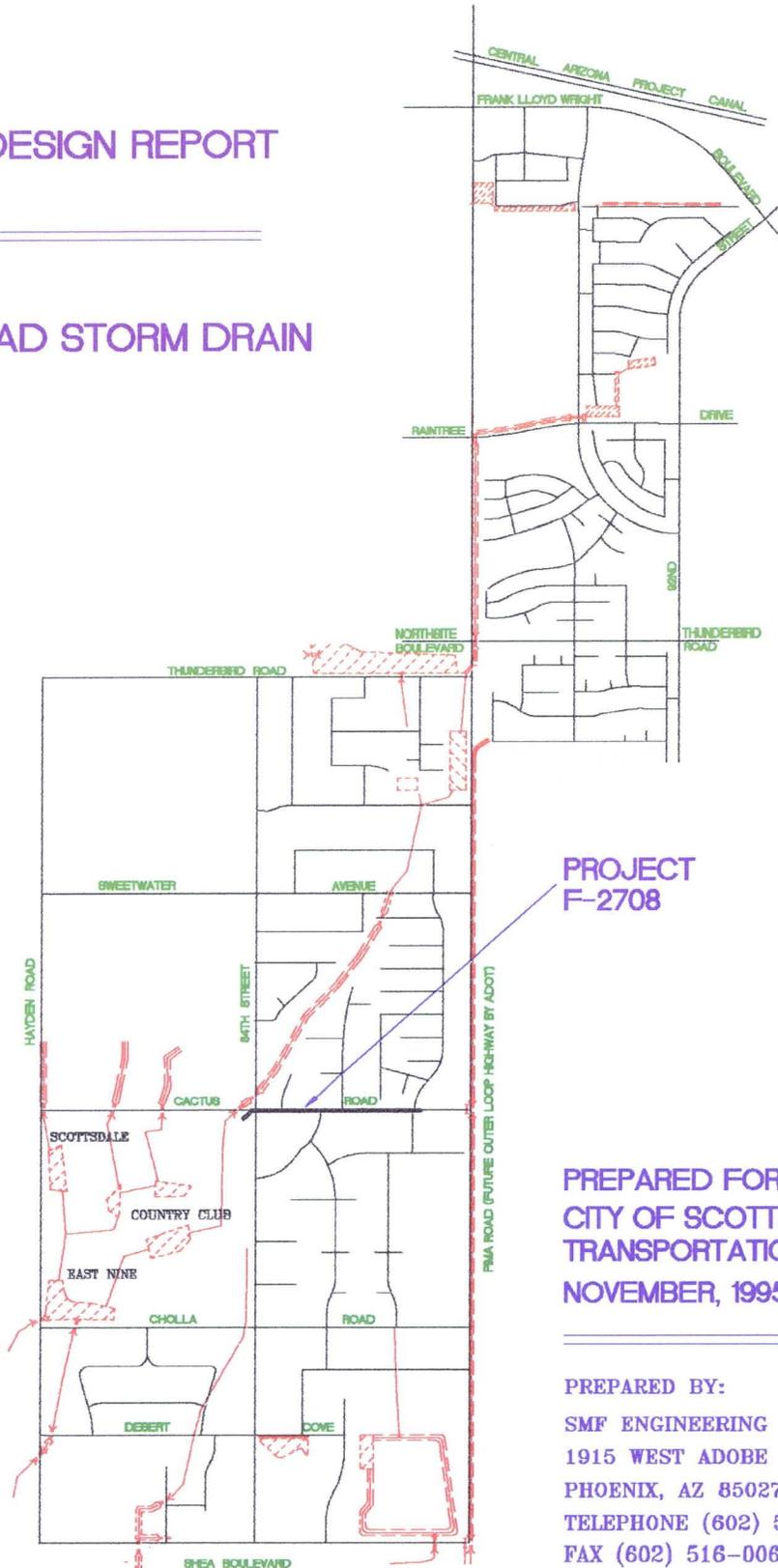


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DRAINAGE DESIGN REPORT

CACTUS ROAD STORM DRAIN



PROJECT
F-2708

PREPARED FOR:
CITY OF SCOTTSDALE
TRANSPORTATION DEPARTMENT
NOVEMBER, 1995

PREPARED BY:
SMF ENGINEERING CORPORATION
1915 WEST ADOBE DRIVE, SUITE D
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SECTION 1

October 26, 1995

I DESCRIPTION OF PROJECT

A. HYDROLOGY

Master Drainage Plan... The Master Drainage Plan¹ sets forth the various proposed major drainage components for both the Thunderbird watershed and the Cholla watershed. The Cactus Road Storm Drain is one of the proposed major drainage components. It is a diversion component; that is, it diverts runoff discharges from the Cholla watershed into the Thunderbird watershed. The storm drain outfalls into Thunderbird wash; south of Cactus Road this Thunderbird wash is generally known as the East Fairway channel of the Scottsdale Country Club (SCC) East Nine. The East Fairway channel and Lake 5 of the SCC are impacted by the additional flow which will be diverted into the channel at Cactus Road. Therefore, the proposed Pima Detention Basin must be constructed and in service prior to placing the Cactus Road Storm Drain into service.

Outer Loop Highway... ADOT's future, depressed, Outer Loop Highway corridor will follow the Pima Road alignment. ADOT's General Plan includes a channel to be constructed on the east side of the Outer Loop Highway. For future conditions, this ADOT channel will obviate the proposed, interim Pima/Sweetwater Detention Basin (see Proposed Improvements Map, Section II, page 3).

Design Periods... The Concept Design Report² considers three distinct periods, which are:

1. **Existing Conditions Period** - the period prior to construction of the COS proposed drainage improvements.
2. **Interim Conditions Period** - the period subsequent to construction of the COS proposed drainage improvement but prior to ADOT's Outer Loop Highway construction. COS proposed Drainage Improvements include all features shown on Section II, page 3 except the Desert Cove Storm Drain.
3. **Future Conditions Period** - the period subsequent to construction of both the COS's proposed drainage improvements including the Desert Cove Storm Drain and ADOT's Outer Loop Highway.

¹ SMF Engineering Corporation, Amendment to Volume II of II, Concept Design Report, March, 1995

² *ibid.*

Existing Conditions Hydrology... The Cholla Wash Basin hydrology for existing conditions is presented in "Volume I of II - EXISTING CONDITIONS HYDROLOGY REPORT" for this project. Volume I describes the Cholla sub-basins and existing drainage facilities in the study area; defines the study area; describes drainage patterns; and describes the source of data, criteria, and methodology. Runoff discharge values were calculated at numerous concentration points for the 2, 5, 10, 25, 50, and 100-year return frequency storms with a 6-hour duration. Concentration point numbers are shown on the Volume I Drainage Area Map and Table 4.6 lists the corresponding discharge values in cfs. The map and table of Volume I have been revised to include the Thunderbird Wash/sub-basins and are presented in the Master Drainage Plan³.

B. DESIGN STANDARDS AND CRITERIA

The design standards used for this project are City of Scottsdale Design Procedures and Criteria; Section 2 - Drainage Report Presentation; Section 2.2 - Hydrology (Revised March, 1994); Section 3 - Design of Facilities to Manage Storm Water Runoff; the City of Scottsdale code requirements; and the Design Criteria Summary prepared by SMF Engineering Corporation (included herein).

C. DRAINAGE BASINS AND DIVERSION CONCEPTS

Study Area... The study area is shown on the "Drainage Area Map" (Section II, pages 4 & 5). It consists of the Thunderbird Wash and Cholla Wash tributary sub-basins. The location of Thunderbird Wash and Cholla Wash are shown on the "Existing Drainage Facilities Map" (Section II, pages 1 & 2). Generally, the study area north of Thunderbird Road is located between Pima Road and 92nd Street; it is bordered on the north by the CAP canal. Between Shea Boulevard and Thunderbird Road, the study area is located between 82nd Street and Pima Road.

Planned Diversion Concept... If a planned diversion were to be considered, sufficient design/modeling would need to be performed to demonstrate that the affected, downstream areas are provided with at least the same level of flood protection as existed prior to the diversion.

Drainage Basin Overspillage... The study area is separated into two parts by Thunderbird channel; Cholla Basin lies south of it and Thunderbird Basin is located on the north side of it. Observation of storm events and calculations shows that overspillage from Thunderbird Basin occurs for existing conditions, during larger storms at:

³ *ibid.*

1. The Cactus Road / 84th Street existing box culverts (overspillage into the Cholla Drainage Basin)
2. Thunderbird Channel on the east side of Pima Road (overspillage into the Pima Road Channel)
3. Thunderbird channel on the west side of Pima Road (overspillage into the Cholla Drainage Basin)

The HEC-1 models developed in this final design study account for the overspillage at those three locations.

Pima Detention Basin... Pima Detention Basin is a planned, temporary, interim period facility and will be obviated by ADOT's future Outer Loop Channel. The location is shown on the Proposed Improvements Map (Section II, page 3). A part of the runoff discharge from the areas north of Thunderbird Road (700, 800 & 900 series sub-basins) will be detained in the Pima Detention Basin, thus reducing the downstream discharge in Thunderbird Wash.

The area north of Thunderbird Road is relatively large (435 acres) and is expected to contribute a significant discharge, for existing conditions, to the downstream Scottsdale Country Club (SCC) East Nine drainage facilities. The peak discharges and total volume of flow which reach those facilities will be reduced by the Pima Detention Basin.

Cactus Road Diversion Component... For existing conditions, Cactus Road from 84th Street to Pima Road collects flows from those areas north of Cactus Road and diverts those flows to 84th Street where it turns south and continues in 84th Street to Cholla Wash at Cortez Street. The hydraulic capacity of Cholla Wash is considerably less than the runoff flows which enter into it. Also, the surface runoff flows experienced in Cactus Road and 84th Street are considerably greater than the street's water conveyance capacity.

Therefore, a new storm sewer pipe is proposed in Cactus Road from about 87th Street to 84th Street. The storm sewer pipe outfalls into the SCC East Nine drainage facilities at the existing box culvert just west of 84th Street. The proposed Pima Detention Basin will reduce the flows reaching the outfall facilities at the SCC East Nine from Thunderbird Wash, and the Cactus Road storm sewer will increase those flows. Final design of the Cactus Road storm sewer includes modeling the SCC East Nine drainage facilities to ensure a proper balance with the Pima Detention Basin. This balance ultimately resulted in improved conditions at the SCC East Nine.

Scottsdale Country Club East Nine... For both the interim and future periods, post-construction impacts to this area will be beneficial. Essentially, runoff discharges flowing into the SCC East Nine drainage facilities will be reduced. The purpose of the proposed Pima Detention Basin is to reduce flows in Thunderbird channel, reduce the storage requirement for Lake 5 of the SCC East Nine, and reduce the outflow from Lake 2 of the SCC East Nine into those communities downstream.

II MAJOR DESIGN AND EXISTING COMPONENTS

A. PIMA DETENTION BASIN (See Map, Section II, page 1)

Design Period... "ADOT's future depressed Outer Loop Highway will follow the Pima Road alignment. ADOT's General Plan includes a channel to be constructed on the east side of the Outer Loop Highway."...⁴ The Pima Detention Basin planned for the interim period by the City of Scottsdale will be replaced by ADOT's Outer Loop Highway channel. Scottsdale's interim detention basin is planned for a ten (10) year life.

Detention Basin Site... The site is located along the west side of Pima Road between Sweetwater Avenue and Sutton Drive; The site is totally within the future Outer Loop Highway ROW. The total area of the site is about ten (10) acres. See Proposed Improvements Map, Section II, page 2.

Tributary Drainage Areas... The tributary area (0.68 sq mi) is bound by CAP canal on the north, Thunderbird Road on the south, Pima Road on the west and 92nd Street on the east. The area designation numbers are of the 700, 800, and 900 series. Runoff discharges from this area cross under Pima Road (east to west) in a box culvert located just south of Thunderbird Road; The flows continue south along the west side of Pima Road in an existing channel / wash to Sutton Drive where the proposed Pima Detention Basin is located.

Functional Parameters... The detention basin volumetric capacity and its outfall discharge have primary effects on the existing system function. The primary existing system components which this detention basin will have an impact on are Thunderbird channel, Cactus / 84th Street box culverts, the SCC East Nine east fairway channel, and the SCC East Nine Lake 5. The detention basin storage capacity and discharge rate is designed such that the peak flow at the Cactus / 84th Street box culverts do not exceed the box hydraulic capacity; and, that the Lake 5 water surface elevation is not increased beyond the existing conditions water surface elevation.

⁴ SMF Engineering Corporation, Hydrology Report 84th Street and Cholla Road Roadway Improvements and 83rd Place and Shea Boulevard Neighborhood Drainage Improvements, Volume I - Existing Conditions (June 21, 1993), section 3, p. 2.

The HEC-2 water surface profile computer run (see Section VIII) shows that the hydraulic capacity of the SCC East Nine fairway channel and Thunderbird channel is adequate and does not control the detention basin design.

Cactus / 84th Street Box Culverts... (See existing "Drainage Facilities Map", Section II, pages 1 and 2). An existing 2-barrel 10' x 2' box culvert is located in Thunderbird channel, under 84th Street, just north of Cactus Road; also, an existing 2-barrel 10' x 2' box culvert is located in Thunderbird channel, under Cactus Road, just west of 84th Street. For existing conditions the capacity of these box culverts is insufficient. However, the box culvert capacity is sufficient for interim and future conditions. Under future conditions, runoff discharges from that part of Thunderbird drainage basin, which lies east of Pima Road, will be intercepted by the Outer Loop Highway channel, thus reducing downstream flows in Thunderbird channel.

Under interim conditions, the runoff discharge flow at these box culverts will be reduced by the Pima Detention Basin when it is put into operation. The Pima Detention Basin is sized so that these culverts will have sufficient capacity and no improvements are necessary to carry the peak flows in Thunderbird channel.

However, some minor catchment facility improvement is recommended in 84th Street at the box culvert to direct street flows from north of Cactus Road into Thunderbird wash.

The following table presents a comparison of box culvert capacity versus expected peak runoff discharges in Thunderbird channel for each of the three periods.

Design Period	Box Culvert Capacity (CFS)	100-Year Event Runoff (CFS)
Existing Conditions	400	839
Interim Conditions	400	324
Future Conditions	400	307

Scottsdale Country Club East Nine, Lake 5... the Cactus Road / 84th Street box culverts are the critical design components of the Thunderbird Basin drainage system. The Pima Detention Basin storage volume, which is necessary to reduce runoff flows at the box culverts to a level equal to the culvert's capacity, also reduces the water surface elevation of the SCC East Nine, Lake 5 below that for existing conditions. Therefore, an improved condition is realized at Lake 5.

The following table presents a comparison of water surface elevations and volume in Lake 5 for each of the three periods.

Design Period	Water Surface Elevation	Storage Volume Acre-Feet	Peak Outflow CFS
Existing Conditions	1378.88	17.63	470
Interim Conditions	1378.53	16.02	361
Future Conditions	1378.46	15.70	340

Of the homes surrounding Lake 5, the lowest floor elevation is 1379.68.

B. CACTUS ROAD STORM DRAIN (See Map, Section II, page 3)

Purpose... The purpose of the Cactus Road planned diversion component (storm drain) is to: 1) divert runoff discharges from Cactus Road and 84th Street into the SCC East Nine drainage system (Thunderbird watershed). These flows enter Cholla Wash at about Cortez Street for existing conditions; 2) lower the water surface elevation in Cactus Road to eliminate road closures; and 3) lower the 100-year storm water surface elevation to eliminate flooding the house floor at the southeast corner of Cactus Road and 84th Street.

Existing Conditions... The Cactus Road roadway from Pima Road to 84th Street is improved with asphalt pavement, vertical curb, gutter and sidewalk. It carries surface flows from Pima Road to 84th Street. A small culvert is positioned on the west side of the Pima Road intersection to carry flows under Cactus Road; but, a portion of the larger storm flows are diverted west along Cactus Road. Those runoff discharges north of Cactus Road flow generally south/southwest; Cactus Road intercepts the flow and diverts the discharge to 84th Street where it turns south. The HEC-2 computer model for existing conditions demonstrates that for the 100-year return frequency storm, flows are not retained within the ROW and the depth of flow exceeds eight inches. Also, at the southeast corner of Cactus Road and 84th Street, the 100-year storm water surface elevation (1395.44) exceeds the floor elevation (1395.28).

Proposed Improvements... The Proposed Improvement Plan includes a storm sewer in Cactus Road to intercept the 50-year return frequency discharge and carry it to the SCC East Nine.

However, the 100-year event level of protection is desired; the difference between the 50-year and the 100-year events will surface flow in Cactus Road, and will be intercepted at 84th Street with catch basins. The 8'x4' box section storm drain outfalls into the SCC East Fairway channel.

HEC-1 Model... The Thunderbird Basin HEC-1 model was generated to ensure that an equal or better condition exists in Thunderbird channel and at the SCC East Nine subsequent to construction of drainage improvements.

For the Proposed Improvement Plan which includes the Cactus Road diversion component with an outfall into the SCC East Nine drainage swale, the effects were determined prior to considering the plan valid. See detailed discussion under "**A. PIMA DETENTION BASIN**".

Catchment Facilities... Usually, catch basins are designed to intercept flows for a 2-year storm in accordance with pavement drainage design criteria. "Catch basin or scupper inlets must be sized and located in series along a gutter grade to ensure that the estimated spread of longitudinal street flow will not exceed twelve feet (measured perpendicular to the curb face) during the peak runoff flow determined for a two-year frequency storm."⁵

Also, for the 100-year return frequency storm, ..."The inlets must also be sized and spaced to ensure that the longitudinal street flow at the peak runoff flow rates from a 100-year frequency storm is retained in the public right-of-way and is flowing at a depth no greater than eight inches above the gutter flow line."⁶

However, this proposed storm sewer is a flood control facility and the storm sewer design including catch basins will exceed the usual City criteria: the 100-year storm will be intercepted by the proposed system.

Existing ROW... The existing ROW is 80 feet along Cactus Road from 84th Street to 86th Street; the south half is 40 feet from 86th Street to Pima Road; and, the north half varies from 45 feet to 55 feet between 86th Street and Pima Road. No new ROW is required for this proposed storm sewer in Cactus Road, but a new Drainage Easement is required for the outlet structure at the SCC East Nine drainage swale.

Outfall Structure... For the Proposed Improvement Plan the outfall structure will be located near the existing box culvert under Cactus Road just west of 84th Street. The hydraulic profiles of the drainage swale and the proposed storm sewer have been carefully matched to ensure the proper hydraulic capacity of both systems.

⁵ City of Scottsdale, Design Procedures and Criteria, Section 3 - Design of Facilities to Manage Stormwater Runoff, P. 36.

⁶ Ibid.

C. **EIGHTY-FOURTH STREET (See Map, Section II, page 3)**

Existing Box Culvert... The existing box culvert located under 84th Street just north of Cactus Road in Thunderbird Wash has been observed to overflow and combine with the Cactus Road surface flow. Also, calculations confirm this. For existing conditions, that flow combines with the Cactus Road flow and continues south in 84th Street to Cholla Wash near Cortez Street.

The Proposed Improvement Plan HEC-1 model includes the Pima Detention Basin which eliminates overflow into Cactus Road and 84th Street.

D. **SCOTTSDALE COUNTRY CLUB EAST NINE (See Map, Section II, page 3)**

Initial Design... A HEC-1 model was prepared for the SCC East Nine development by Collar, Williams and White Engineering, Inc. (C W & W) in 1984. The improvements included five lakes with a ten-foot depth; the top three feet is for detention requirements. That system is shown on the "Existing Drainage Facilities" map. Thunderbird Wash flows discharge into Lake 5 and Lake 5 discharges into Lake 2 as do Lakes 1, 3, and 4.

The initial hydrology design was based on a 100-year return frequency 2-hour duration storm. Current City of Scottsdale criteria require a 6-hour duration.

The drainage areas shown on the C W & W Drainage Area Map agree very closely to that of this study; except, their drainage area 5 did not account for the detention site along Thunderbird Road which was constructed at a later date. Area 5 is tributary to Thunderbird Wash.

Existing Conditions... "The Scottsdale Country Club drainage facilities consist of a system of drainage swales and five lakes with detention capacity. The system intercepts flows from four major channels which cross Cactus Road between Hayden Road and 84th Street, including the Thunderbird Wash channel which borders this study area on the northwest side between the 84th Street / Cactus Road and the Pima Road / Thunderbird Road intersections."⁷

The Master Drainage Plan says... "Presently, there is a major flooding problem that occurs at the southwestern corner of the Scottsdale Country Club Second Nine. The lake at this location, Lake Number 2, has two culvert outlets, one under Cholla Road and one under Hayden Road. When a 10-year storm occurs on the watershed, water begins to spill out of Lake 2 onto Cholla and Hayden. Most of the water drains

⁷ SMF Engineering Corporation, Hydrology Report 84th Street and Cholla Road Roadway Improvements and 83rd Place and Shea Boulevard Neighborhood Drainage Improvements, Volume I - Existing Conditions (June 21, 1993), section 3, p. 4.

south on Hayden and some is captured by catch basins along Hayden. In a 100-year storm, over 2,000 cfs spills over into Hayden and Cholla."⁸

HEC-1 Model... The COS has a HEC-1 model for the SCC East Nine's basins and drainage facilities. This model originated with the Boyle Report. The Boyle Report says, "The proposed improvements for the Scottsdale Country Club Second Nine are based on data taken from the 'Grading and Drainage Plan for the Scottsdale Country Club Second Nine'. Further design of the proposed improvements would require more accurate data of the site".⁹ Consequently, Lake 5 was mapped and new volumetric calculations were performed for this study and report.

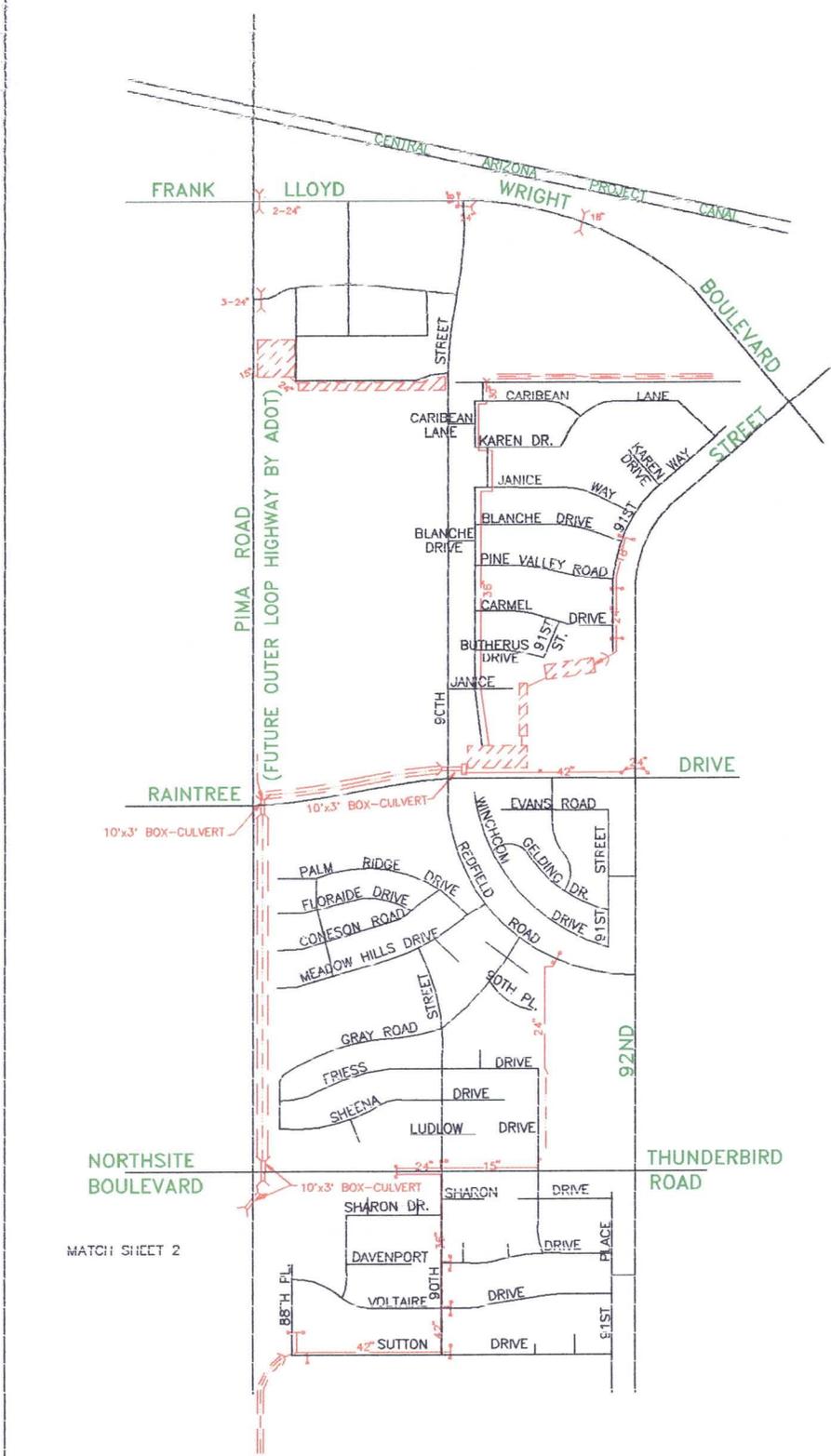
For this report, a new Thunderbird Basin HEC-1 model was generated to ensure that an equal or better condition exists in Thunderbird channel and at the SCC East Nine Lake 5 subsequent to construction of drainage improvements. For this new HEC-1 model, the upper limit of Thunderbird Basin is the CAP canal and the lower limit is the outfall at Lake 5. The system of drainage basins tributary to the other SCC East Nine lake network (Lakes 1, 2, 3, & 4) is not included in the new HEC-1 model.

HEC-2 Model Combined Discharges... For the Proposed Improvement Plan, the Thunderbird Wash channel and the new Cactus Road storm sewer discharges will combine and flow into the existing East Fairway swale to lake 5. The East Fairway HEC-2 water surface profile shows that this combined discharge does not exceed the capacity of the SCC East Nine drainage system which includes the East Fairway swale, the approach channel to Lake 5, and Lake 2. HEC-2 calculations show that the East Fairway swale has more than sufficient capacity.

⁸ Boyle Engineering Corporation. Hayden / Shea Area Master Drainage Plan, Pima/Doubletree Area Master Drainage Plan, Addendum No. 2, January 25, 1991, p. 2.

⁹ Boyle Engineering Corporation. Op. Cit., p. 9.





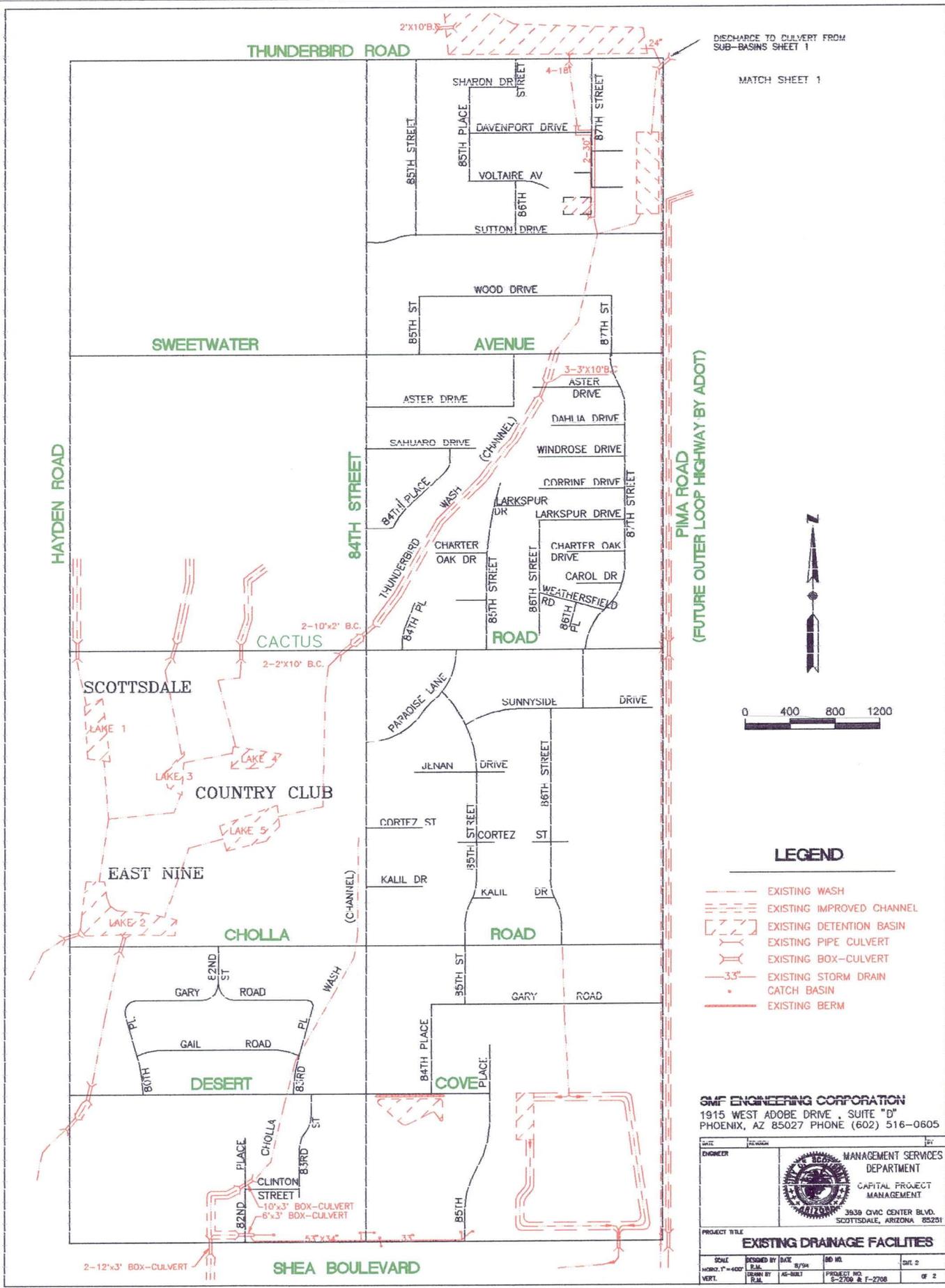
LEGEND

- EXISTING WASH
- EXISTING IMPROVED CHANNEL
- [] EXISTING DETENTION BASIN
- > < EXISTING PIPE CULVERT
- > < EXISTING BOX-CULVERT
- - -3.3' - EXISTING STORM DRAIN
- CATCH BASIN
- EXISTING BERM

MATCH SHEET 2

SMF ENGINEERING CORPORATION
 1915 WEST ADOBE DRIVE, SUITE "D"
 PHOENIX, AZ 85027 PHONE (602) 516-0605

PROJECT TITLE		EXISTING DRAINAGE FACILITIES	
SCALE	DESIGNED BY	DATE	DD NO.
HORIZ. 1"=400'	R.M.	05/94	
VERT.	DRONE BY	AS-BUILT	PROJECT NO.
	B.L.F.		5-2709 & T-2708
OWNER		MANAGEMENT SERVICES DEPARTMENT	
		CAPITAL PROJECT MANAGEMENT	
		3839 CIVIC CENTER BLVD. SCOTTSDALE, ARIZONA 85251	
		SHEET 1 OF 2	



DISCHARGE TO CULVERT FROM SUB-BASINS SHEET 1

MATCH SHEET 1



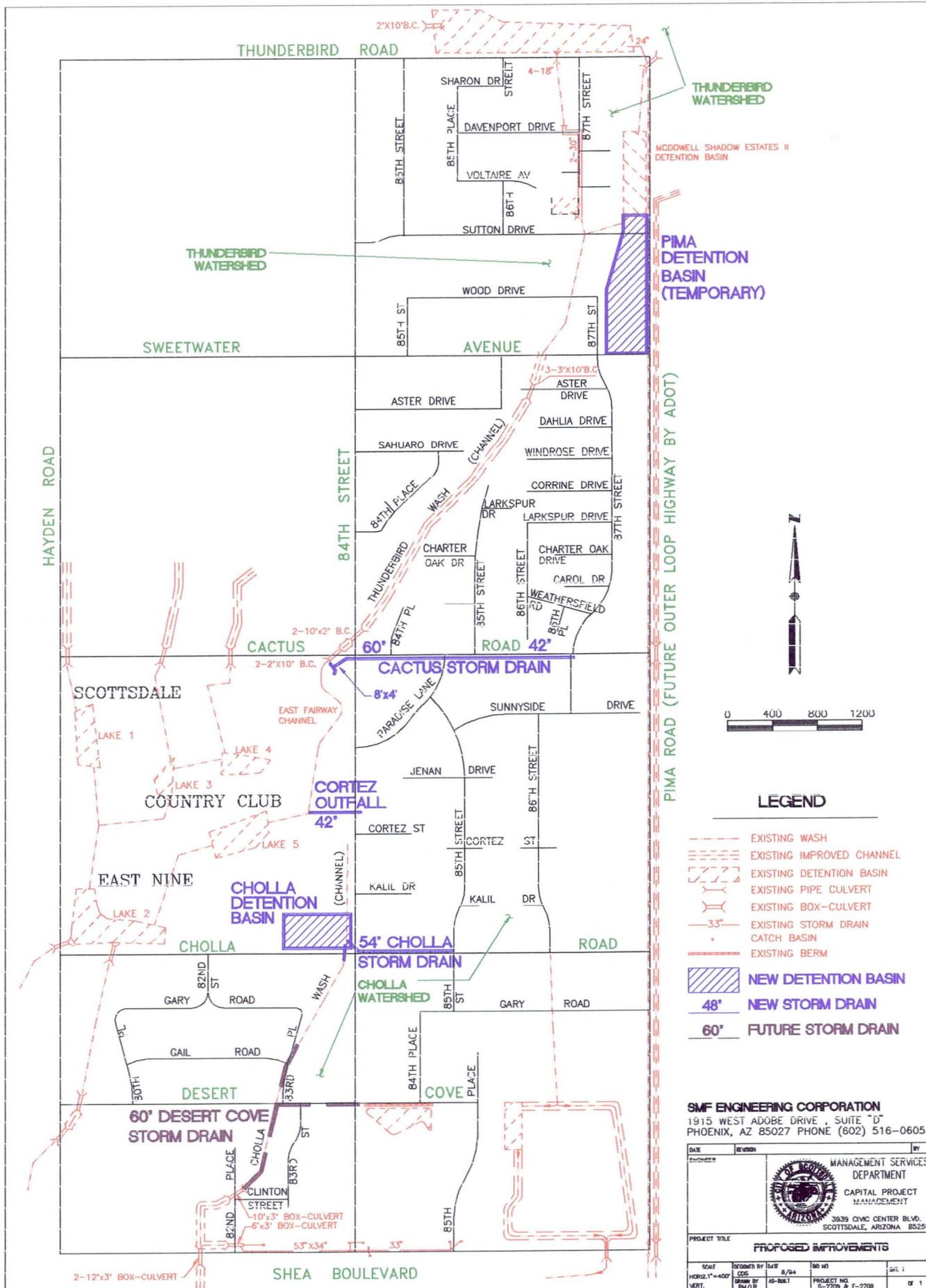
LEGEND

- EXISTING WASH
- == EXISTING IMPROVED CHANNEL
- ▭ EXISTING DETENTION BASIN
- C- EXISTING PIPE CULVERT
- ▭ EXISTING BOX-CULVERT
- S- EXISTING STORM DRAIN
- CATCH BASIN
- EXISTING BERM

SMF ENGINEERING CORPORATION
 1915 WEST ADOBE DRIVE, SUITE "D"
 PHOENIX, AZ 85027 PHONE (602) 516-0605

DATE	PROJECT	BY
ENGINEER		
		MANAGEMENT SERVICES DEPARTMENT
		CAPITAL PROJECT MANAGEMENT
3636 CIVIC CENTER BLVD. SCOTTSDALE, ARIZONA 85251		

PROJECT TITLE				
EXISTING DRAINAGE FACILITIES				
SCALE	DESIGNED BY	DATE	NO. OF	SHEET
HORIZ. 1"=400'	E.M.	8/94	10	2
VERT.	DESIGN BY	AS-BUILT	PROJECT NO.	OF 2
	E.M.		8-2706 & F-2708	



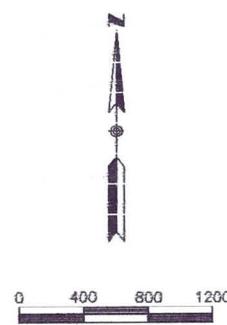
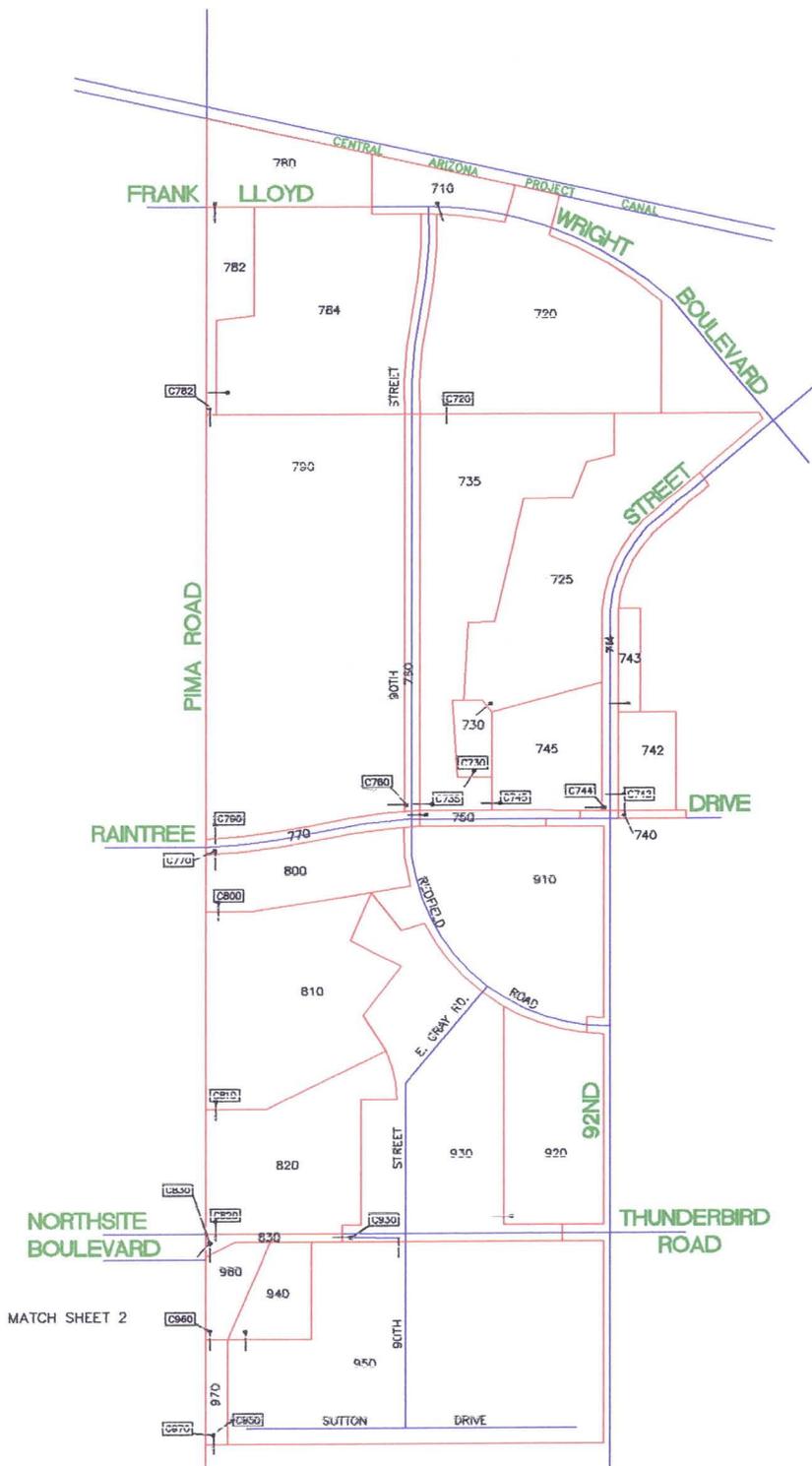
- LEGEND**
- EXISTING WASH
 - EXISTING IMPROVED CHANNEL
 - EXISTING DETENTION BASIN
 - EXISTING PIPE CULVERT
 - EXISTING BOX-CULVERT
 - EXISTING STORM DRAIN
 - EXISTING STORM DRAIN CATCH BASIN
 - EXISTING BERM
 - NEW DETENTION BASIN
 - 48" NEW STORM DRAIN
 - 60" FUTURE STORM DRAIN

SMF ENGINEERING CORPORATION
 1915 WEST ADOBE DRIVE, SUITE "D"
 PHOENIX, AZ 85027 PHONE (602) 516-0605

DATE	REVISION	BY

PROJECT TITLE: **PROPOSED IMPROVEMENTS**

SCALE	DRAWN BY	CHECKED BY	DATE	NO. OF	SHEET
HORIZ. 1"=400'	CSG	SM/ST	8/04	1	1
VERT.	SM/ST	AS-BUILT	PROJECT NO.	OF 1	
			8-2709 & T-2708		



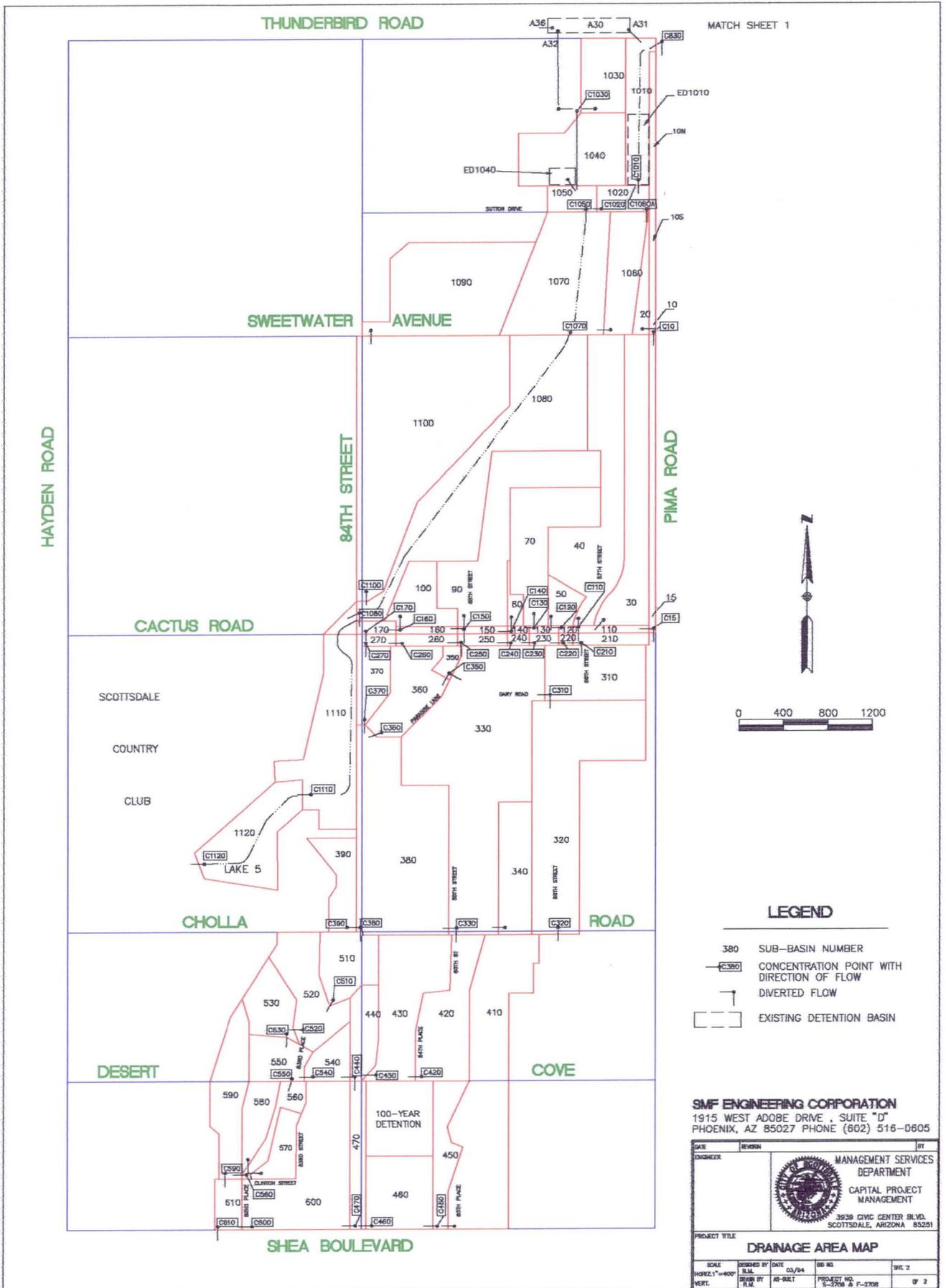
LEGEND

- 380 SUB-BASIN NUMBER
- C380 CONCENTRATION POINT WITH DIRECTION OF FLOW
- ↓ DIVERTED FLOW

MATCH SHEET 2

SMF ENGINEERING CORPORATION
 3915 WEST ADOBE DRIVE, SUITE 107
 PHOENIX, AZ 85027 PHONE (602) 516-0805

ENGINEER		DATE		JOB NO.	
		MANAGEMENT SERVICES DEPARTMENT		SHE. 1	
		CAPITAL PROJECT MANAGEMENT		OF 2	
PROJECT TITLE					
DRAINAGE AREA MAP					
SCALE	DESIGNED BY	DATE	JOB NO.	SHE. 1	
HORIZ. 1"=400'	R.M.	05/84	40-346		
VERT.	DRAWN BY	PROJECT NO.	S-2729 & F-2728		
	M.L.F.				



MATCH SHEET 1



LEGEND

- 380 SUB-BASIN NUMBER
- CONCENTRATION POINT WITH DIRECTION OF FLOW
- DIVERTED FLOW
- EXISTING DETENTION BASIN

SMF ENGINEERING CORPORATION
 1915 WEST ADOBE DRIVE, SUITE "D"
 PHOENIX, AZ 85027 PHONE (602) 516-0605

DATE	REVISION	BY
		MANAGEMENT SERVICES DEPARTMENT
		CAPITAL PROJECT MANAGEMENT
3939 CIVIC CENTER BLVD. SCOTTSDALE, ARIZONA 85251		
PROJECT TITLE		
DRAINAGE AREA MAP		
SCALE	DRAWN BY	DATE
HORIZ: 1"=400'	R.M.	03/94
VERT.	AP-DULT	
PROJECT NO.		SHEET NO.
S-2700 & P-2708		OF 2



Date: 11-2-95
By : Charles D. Scott
SMF Engineering Corporation

Drainage Design Criteria - FINAL

City of Scottsdale
84th Street & Cholla Road
Cholla and Cactus Storm Drain

1) Catch Basins:

- Calculate Peak Flows to Catch Basins with HEC-1. Use peak runoff of sub-basin. Add bypass from catch basin upstream. Assume sub-basin and bypass will peak at the same time.
- Use HEC-12 for catch basin inlet capacity, and pavement drainage spread and depth calculations.

For Cholla Road:

- Max Spread is 10.5 feet for a 2-year storm
- Spread shall be within Right-of-Way for a 100-year storm
- Max Depth is 8 inches for a 100-year storm

For 84th Street:

- Max Spread is 12 feet for a 2-year storm
- Spread shall be within Right-of-Way for a 100-year storm
- Max Depth is 8 inches for a 100-year storm

For Cactus Rd:

- Max Spread is 23 feet for a 50-year storm
- Max Depth is 6 inches for a 50-year storm
- Spread shall be within Right-of-Way for a 100-year storm
- Max Depth is 8 inches for a 100-year storm

Clogging Factors

- Curb Opening Inlet: 1.25 * required length
- Grate Inlet : 2.0 * required opening
- Combination Inlet : Curb - 1.25 * required length
Grate - 2.0 * required opening

- Approximately 90% of the total runoff will be intercepted by each Catch Basin.
- Catch Basins in 85th St (Cholla Storm Drain) are designed to intercept the 100-year storm.
- Catch Basins at 84th Street & Cactus Road are designed to intercept the 100-year storm.

2) Storm Drains:

- Hydraulic Gradient
 - Cactus - 50-year Storm, and 100-year from 84th Street to outlet structure (8'x4' Box Sections)
 - Cholla - 100-year Storm
- Assume that Catch Basins will intercept 100% of the design storm.
Use HEC-1 to calculate design flows. Combine hydrographs going downstream. Design the Hydraulic Gradient to be a minimum of 6 inches below the catch basin depression.
- Energy losses in main line from LA County (Street and Highway Drainage) as follows:
 - Catch Basin: Entrance Loss = $0.5 V^2/2g$
 - Manhole Shaft (no increase in flow): Loss = $0.05 V^2/2g$
 - Junction (increase in flow): Loss(Hj) = $\Delta H + H_{V1} - H_{V2}$
Where $\Delta H = Q_2V_2 - Q_1V_1 - Q_3V_3\cos(\alpha) / .5(A_1+A_2) * g$
 - Expansion: Loss = $(V_1-V_2)^2/2g$
 - Expansion (Outfall): Loss = $1.0 * V^2/2g$
 - Bend (Curve): Loss = $0.002 * \alpha * V^2/2g$
 - Bend (Angle): Loss = $0.0033 * \alpha * V^2/2g$
 - Friction: Loss = $29 * n^2 * L * V^2/(R^{4/3} * 2g)$
- Manning's n = 0.013 (For RGRCP)
Manning's n = 0.016 (For CIPCP)
- Minimum Velocity 3 ft/sec Flowing Full or Half Full
- Minimum pipe size is 18 inches
- Minimum cover is 3 feet
- Catch basin connector pipes are designed for the 100-year storm



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*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1)
* SEPTEMBER 1990
* VERSION 4.0
*
* RUN DATE 10/20/1994 TIME 11:52:18
*
*****

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*****
*
* U.S. ARMY CORPS OF ENGINEERS
* HYDROLOGIC ENGINEERING CENTER
* 609 SECOND STREET
* DAVIS, CALIFORNIA 95616
* (916) 756-1104
*
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X   X  XXXXXXXX  XXXXX      X
X   X X         X   X      XX
X   X X         X           X
XXXXXXXX XXXX   X           XXXXX X
X   X X         X           X
X   X X         X   X      X
X   X  XXXXXXXX  XXXXX      XXX

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THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE.
 THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION
 NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,
 DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION
 KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

```

LINE      ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
1         ID      84TH STREET AND CHOLLA ROAD
2         ID      2-5-10-25-50-100 yr STORM
3         ID      ULTIMATE CONDITION:
4         ID      --BOX CULVERTS IN CACTUS/84TH INTERSECTION ARE not IMPROVED
5         ID      --NEW STORM SEWER IN CACTUS (outfall at box-culvert)
6         ID      --INTERCEPTOR AT CORTEZ IN 84TH STREET
7         ID      --NO FLOW CROSSING PIMA ROAD AT TBIRD
8         ID      *****
9         ID      SCOTTSDALE COUNTRY CLUB LAKE 5
10        ID      *****
11        ID      FILE SCCULT.DAT
          *DIAGRAM
12        IT      2              300
13        IO      5
14        JR      PREC      .36      .53      .62      .76      .88      1.0
15        KK      A30      SUBBASIN A30 RUNOFF
16        PH              0.88      1.61      2.6      2.84      3      3.3
17        BA      0.4031
18        LS      0      77      11
19        UD      0.47

20        KK      DA30      DETENTION BASIN AT CPA30
21        KM              Outflow to A31 and A32 and A36
22        RS      1      STOR      0
23        SA      0      0.49      0.94      1.39      1.93
24        SE      34.99      35.00      37.00      39.00      41.40
25        SQ      0      40      137.4      268      361

26        KK      A31      SPLIT FLOW AT DETENTION BASIN DA30
27        KM              DI is Total Outflow from Detention Basin (A31+A32+A36)
28        KM              DQ is Split to A32 and A36
29        DT      A32
30        DI      0      40      137.4      268      361
31        DQ      0      40      124.4      242      326

32        KK      ED1010      ROUTE CA31 TO ED1010
33        RS      100      STOR      -1      0
34        RC      .060      .040      .060      600      .0086
35        RX      0      0.1      50      56      59      65      115      115.1
36        RY      105      100      99      95      95      99      100      105

37        KK      1010      SUBBASIN 1010 RUNOFF
38        BA      .01192
39        LS      0      77
40        UD      0.08

41        KK      C1010      COMBINE 1010 and CA31
42        HC      2
    
```

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

43	KK	ED1010	EXISTING DETENTION BASIN 1010						
44	RS	1	STOR	0					
45	SA	0	0.41	0.93	1.19	1.45	1.71	2.23	
46	SE	24.7	25.7	26.7	27.2	27.7	28.2	29.2	
47	SQ	0	7	17	21	69	240	1082	
48	KK	C1020	ROUTE DETENTION BASIN OUTFALL TO C1020						
49	RS	100	STOR	-1	0				
50	RC	.050	0.040	.050	220	.0086			
51	RX	0	0.1	50	56	59	65	115 115.1	
52	RY	105	100	99	95	95	99	100 105	
53	KK	1020	SUBBASIN 1020 RUNOFF						
54	BA	.00202							
55	LS	0	77	10					
56	UD	0.06							
57	KK	C1020	COMBINE C1010 AND 1020						
58	HC	2							
59	KK	A32	RETRIEVE SPLIT FLOW AT A32 (A36 and A32)						
60	DR	A32							
61	KK	A32	SPLIT FLOW AT DETENTION BASIN DA30						
62	KM		DI is Split to A32 and A36						
63	KM		DQ is Split to A36 (Box Culvert)						
64	DT	A36							
65	DI	0	40	124.4	242	326			
66	DQ	0	40	110	190	250			
67	KK	C1030	ROUTE A32 TO C1030						
68	RS	100	STOR	-1	0				
69	RC	.060	.040	.060	600	.0080			
70	RX	0	0.1	50	56	59	65	115 115.1	
71	RY	105	100	99	95	95	99	100 105	
72	KK	C1030	ROUTE A32 TO C1030						
73	RK	230	.0036	.012			CIRC	3.53	
74	KK	1030	SUBBASIN 1030 RUNOFF						
75	BA	.00985							
76	LS	0	77						
77	UD	.13							
78	KK	C1030	COMBINE C1030 AND A32						
79	HC	2							
80	KK	C1040	ROUTE C1030 TO C1040						
81	RK	524	0.0040	.012	0		CIRC	3.53	

LINE	ID	1	2	3	4	5	6	7	8	9	10
82	KK	1040	SUBBASIN 1040 RUNOFF								
83	BA	.01949									
84	LS	0	77	25							
85	UD	0.12									
86	KK	ED1040	EXISTING DETENTION BASIN 1040								
87	RS	1	STOR	-1	0						
88	SA	0	0.52	.597	.713	0.79	0.79				
89	SE	24.0	24.5	25.5	27.0	28	29				
90	SQ	0	1.5	6	13	16	19				
91	KK	C1040	COMBINE C1030 AND 1040								
92	HC	2									
93	KK	C1050	ROUTE C1040 TO C1050								
94	RS	100	STOR	-1	0						
95	RC	.050	0.040	.050	250	.0086					
96	RX	0	0.1	50	56	59	65	115	115.1		
97	RY	105	100	99	95	95	99	100	105		
98	KK	1050	SUBBASIN 1050 RUNOFF								
99	BA	.00387									
100	LS	0	77								
101	UD	0.07									
102	KK	C1050	COMBINE 1050 AND C1040								
103	HC	2									
104	KK	C1050	COMBINE C1050 AND C1020								
105	HC	2									
106	KK	C1070	ROUTE C1050 TO C1070								
107	RS	100	STOR	-1	0						
108	RC	.050	0.040	.050	1150	.0078					
109	RX	0	0.1	50	56	60	66	116	116.1		
110	RY	105	100	99	95	95	99	100	105		
111	KK	1060	SUBBASIN 1060 RUNOFF								
112	BA	.01174									
113	LS	0	77								
114	UD	0.20									
115	KK	C1070	ROUTE 1060 TO C1070								
116	RS	100	STOR	-1	0						
117	RC	.040	0.016	.040	380	.0100					
118	RX	0	0.1	21.5	21.6	60.5	60.6	72	72.1		
119	RY	105	100	99	98.86	98.86	99	100	105		
120	KK	1070	SUBBASIN 1070 RUNOFF								
121	BA	.02864									
122	LS	0	77	17							
123	UD	0.14									

LINE	ID	1	2	3	4	5	6	7	8	9	10
124	KK	C1070	COMBINE C1050 AND 1060 AND 1070								
125	HC	3									
126	KK	C1080	ROUTE C1070 TO C1080								
127	RS	100	STOR	-1	0						
128	RC	.050	0.040	.050	3100	.0066					
129	RX	0	0.1	30	41	49	60	90	90.1		
130	RY	108	100	99	95	95	99	100	108		
131	KK	1080	SUBBASIN 1080 RUNOFF								
132	BA	.04840									
133	LS	0	77	24							
134	UD	0.16									
135	KK	C1080	COMBINE 1080 AND C1070								
136	HC	2									
137	KK	1090	SUBBASIN 1090 RUNOFF								
138	BA	.03370									
139	LS	0	77	20							
140	UD	0.138									
141	KK	C1100	ROUTE 1090 TO C1100								
142	RS	100	STOR	-1	0						
143	RC	.040	0.016	.040	.0074	2340					
144	RX	0	0.1	20	20.1	60	60.1	80	80.1		
145	RY	105	100	99	98.75	98.75	99	100	105		
146	KK	1100	SUBBASIN 1100 RUNOFF								
147	BA	.07053									
148	LS	0	77	18							
149	UD	0.37									
150	KK	C1100	COMBINE 1100 AND 1090								
151	HC	2									
152	KK	C1080	COMBINE C1100 AND C1080								
153	HC	2									
154	KK	40	SUBBASIN 40 RUNOFF								
155	BA	.03122									
156	LS	0	77	45							
157	UD	.42									
158	KK	SD110	ROUTE C40 TO SD110								
159	RK	190	0.0010	0.012	CIRC	3					
160	KK	50	SUBBASIN 50 RUNOFF								
161	BA	.00659									
162	LS	0	77	35							
163	UD	.14									

LINE	ID	1	2	3	4	5	6	7	8	9	10
202	KK	220	SUBBASIN 220 RUNOFF								
203	BA	.00103									
204	LS		98								
205	UD	.06									
206	KK	C230	ROUTE C220 TO 230								
207	RS	100	STOR	-1	0						
208	RC	.016	.016	.040	380	.0030	120				
209	RX	0	0	31.8	33.8	33.8	38.8	55	80		
210	RY	100.41	98.41	97.95	97.87	98.37	98.49	99.0	99.9		
211	KK	230	SUBBASIN 230 RUNOFF								
212	BA	.00083									
213	LS		98								
214	UD	.06									
215	KK	C230	COMBINE C220 AND 230								
216	HC	2									
217	KK	SD230	COMBINE SD220 AND C130 AND C230								
218	HC	3									
219	KK	SD90	ROUTE SD230 TO SD90								
220	RK	205	0.0010	0.012		CIRC	4				
221	KK	90	SUBBASIN 90 RUNOFF								
222	BA	.02922									
223	LS		77	24							
224	UD	.23									
225	KK	SD90	COMBINE SD230 AND 90								
226	HC	2									
227	KK	SD240	ROUTE SD90 TO SD240								
228	RK	125	0.0010	0.012		CIRC	4				
229	KK	140	SUBBASIN 140 RUNOFF								
230	BA	.00081									
231	LS		98								
232	UD	.06									
233	KK	240	SUBBASIN 240 RUNOFF								
234	BA	.00150									
235	LS		98								
236	UD	.06									
237	KK	SD240	COMBINE SD90 AND 140 AND 240								
238	HC	3									

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

239 KK SD250 ROUTE SD240 TO SD250
 240 RK 350 0.0010 0.012 CIRC 4

241 KK 150 SUBBASIN 150 RUNOFF
 242 BA .00192
 243 LS 98
 244 UD .07

245 KK 250 SUBBASIN 250 RUNOFF
 246 BA .00134
 247 LS 98
 248 UD .06

249 KK SD250 COMBINE SD240 AND 150 AND 250
 250 HC 3

251 KK SD260 ROUTE SD250 TO SD260
 252 RK 336 0.0010 0.012 CIRC 5

253 KK 100 SUBBASIN 100 RUNOFF
 254 BA .00666
 255 LS 77 24
 256 UD .12

257 KK 160 SUBBASIN 160 RUNOFF
 258 BA .00058
 259 LS 98
 260 UD .06

261 KK C160 COMBINE 100 AND 160
 262 HC 2

263 KK 260 SUBBASIN 260 RUNOFF
 264 BA .00114
 265 LS 98
 266 UD .06

267 KK SD260 COMBINE SD250 AND C160 AND 260
 268 HC 3

269 KK SD270 ROUTE SD260 TO SD270
 270 RK 194 0.0010 0.012 CIRC 5

271 KK 170 SUBBASIN 170 RUNOFF
 272 BA .00047
 273 LS 77 35
 274 UD .06

275 KK 270 SUBBASIN 270 RUNOFF
 276 BA .00095
 277 LS 98
 278 UD .06

LINE	ID	1	2	3	4	5	6	7	8	9	10
279	KK	SD270	COMBINE SD260 AND 170 AND 270								
280	HC	3									
281	KK	SD270	DIVERT EXCESS OF 50YR STORMDRAIN TO 84TH ST SOUTH								
282	DT	ST270									
283	DI	0	131	200							
284	DQ	0	0	69							
285	KK	SDBOX	ROUTE SD270 TO SDBOX								
286	RK	270	0.0010	0.012	CIRC	5					
287	KK	C1080	COMBINE C1080 AND SDBOX								
288	HC	2									
289	KK	C1110N	ROUTE C1080 TO C1110N								
290	RS	100	STOR	-1	0						
291	RC	.040	0.030	.040	900	.0092					
292	RX	0	0.1	20	40	80	100	120	120.1		
293	RY	105	100	99	93	93	99	100	105		
294	KK	1110N	SUBBASIN 1110N RUNOFF								
295	BA	.00396									
296	LS	0	69	18							
297	UD	0.06									
298	KK	C1100N	COMBINE C1110N AND C1080								
299	HC	2									
300	KK	ST270	RETRIEVE ST270 (street flow in 84th street)								
301	DR	ST270									
302	KK	ST280	ROUTE ST270 TO ST280								
303	RS	100	STOR	-1	0						
304	RC	.040	.016	.040	400	.0077					
305	RX	0	24	24.1	40	40.1	56	56.1	80		
306	RY	101	98.93	98.61	98.97	98.97	98.62	98.92	101		
307	KK	SD280	DIVERT EXCESS OF DEPRESSED CURB ON WEST SIDE 84TH ST SOUTH (a11)								
308	DT	ST280									
309	DI	0	50								
310	DQ	0	50								
311	KK	C1110N	COMBINE C1110N AND ST280 (flow in channel and gutter 84th St)								
312	HC	2									
313	KK	C1110S	ROUTE C1110N TO C1110S								
314	RS	100	STOR	-1	0						
315	RC	.040	0.030	.040	1050	.0092					
316	RX	0	0.1	20	40	80	100	120	120.1		
317	RY	105	100	99	93	93	99	100	105		

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

318	KK	ST280	RETRIEVE ST280 (street flow in 84th street)						
319	DR	ST280							
320	KK	C370	ROUTE ST280 TO 370						
321	RS	100	STOR	-1	0				
322	RC	.040	.016	.040	370	.0077			
323	RX	0	24	24.1	40	40.1	56	56.1	80
324	RY	101	98.93	98.61	98.97	98.97	98.62	98.92	101
325	KK	350	SUBBASIN 350 RUNOFF						
326	BA	.00225							
327	LS		77	20					
328	UD	.06							
329	KK	C350	DIVERT C350 TO 330						
330	DT	D330							
331	DI	0	100						
332	DQ	0	50						
333	KK	C360	ROUTE C350 TO 360						
334	RS	100	STOR	-1	0				
335	RC	.040	.016	.040	850	.0040			
336	RX	0	24	24.1	40	40.1	56	56.1	80
337	RY	101	98.93	98.61	98.97	98.97	98.62	98.92	101
338	KK	360	SUBBASIN 360 RUNOFF						
339	BA	.01320							
340	LS		77	20					
341	UD	.14							
342	KK	370	SUBBASIN 370 RUNOFF						
343	BA	.00592							
344	LS		77	20					
345	UD	.11							
346	KK	C370	COMBINE D280 AND C350 AND 360 AND 370						
347	HC	4							
348	KK	C380N	ROUTE C370 TO 380N						
349	RS	100	STOR	-1	0				
350	RC	.040	.016	.040	620	.0054			
351	RX	0	20	20.1	40	40.1	60	60.1	80
352	RY	101	98.93	98.61	98.97	98.97	98.62	98.92	101
353	KK	380N	SUBBASIN 380N RUNOFF						
354	BA	.00588							
355	LS		77	20					
356	UD	.15							

LINE	ID	1	2	3	4	5	6	7	8	9	10
357	KK	C380N	COMBINE C370 AND 380N (street flow in 84th street at Kalil)								
358	HC	2									
359	KK	C1110S	ROUTE C380N TO C1110S								
360	RD	280	0.0030	0.012		CIRC	3				
361	KK	1110S	SUBBASIN 1110S RUNOFF								
362	BA	.01991									
363	LS	0	69	18							
364	UD	0.09									
365	KK	C1110S	COMBINE C1110S AND C380N AND 1110S (flow upstream of box-culvert)								
366	HC	3									
367	KK	C1120	ROUTE C1110S TO C1120								
368	RS	100	STOR	-1	0						
369	RC	.020	0.020	.020	200	.0080					
370	RX	0	0.1	0.2	0.3	24.3	24.4	24.5	24.6		
371	RY	110	110	110	100	100	110	110	110		
372	KK	1120	SUBBASIN 1120 RUNOFF								
373	BA	.01692									
374	LS	0	69	50							
375	UD	0.07									
376	KK	C1120	COMBINE 1120 AND C1110S								
377	HC	2									
378	KK	LAKE5	DETENTION BASIN AT LAKE 5								
379	RS	1	STOR	0							
380	SV	0	6.94	10.21	14	18.59	24.07	30.25			
381	SE	73.50	76.09	77.09	78.09	79.09	80.09	81.09			
382	SQ	0	0	49	225	535	960	1500			
383	ZZ										

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*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1)
* SEPTEMBER 1990
* VERSION 4.0
*
* RUN DATE 10/20/1994 TIME 11:52:18
*
*****

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*****
*
* U.S. ARMY CORPS OF ENGINEERS
* HYDROLOGIC ENGINEERING CENTER
* 609 SECOND STREET
* DAVIS, CALIFORNIA 95616
* (916) 756-1104
*
*****

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84TH STREET AND CHOLLA ROAD
2-5-10-25-50-100 yr STORM
ULTIMATE CONDITION:
--BOX CULVERTS IN CACTUS/84TH INTERSECTION ARE not IMPROVED
--NEW STORM SEWER IN CACTUS (outfall at box-culvert)
--INTERCEPTOR AT CORTEZ IN 84TH STREET
--NO FLOW CROSSING PIMA ROAD AT TBIRD
*****
SCOTTSDALE COUNTRY CLUB LAKE 5
*****
FILE SCCULT.DAT

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```

13 IO      OUTPUT CONTROL VARIABLES
          IPRNT      5  PRINT CONTROL
          IPLOT      0  PLOT CONTROL
          QSCAL      0. HYDROGRAPH PLOT SCALE

```

```

IT      HYDROGRAPH TIME DATA
        NMIN      2  MINUTES IN COMPUTATION INTERVAL
        IDATE     1  0  STARTING DATE
        ITIME     0000 STARTING TIME
        NQ        300 NUMBER OF HYDROGRAPH ORDINATES
        NDDATE    1  0  ENDING DATE
        NDTIME    0958 ENDING TIME
        ICENT     19  CENTURY MARK

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COMPUTATION INTERVAL .03 HOURS
TOTAL TIME BASE      9.97 HOURS

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ENGLISH UNITS
DRAINAGE AREA      SQUARE MILES
PRECIPITATION DEPTH INCHES
LENGTH, ELEVATION  FEET
FLOW               CUBIC FEET PER SECOND
STORAGE VOLUME    ACRE- FEET
SURFACE AREA      ACRES
TEMPERATURE       DEGREES FAHRENHEIT

```

```

JP      MULTI-PLAN OPTION
        NPLAN      1  NUMBER OF PLANS

```

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JR      MULTI-RATIO OPTION
        RATIOS OF PRECIPITATION
        .36      .53      .62      .76      .88      1.00

```

1

PEAK FLOW AND STAGE (END-OF-PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC COMPUTATIONS
 FLOWS IN CUBIC FEET PER SECOND, AREA IN SQUARE MILES
 TIME TO PEAK IN HOURS

RATIOS APPLIED TO PRECIPITATION

OPERATION	STATION	AREA	PLAN		RATIO 1	RATIO 2	RATIO 3	RATIO 4	RATIO 5	RATIO 6
					.36	.53	.62	.76	.88	1.00
HYDROGRAPH AT										
+	A30	.40	1	FLOW	50.	117.	163.	244.	321.	403.
				TIME	3.57	3.60	3.57	3.57	3.57	3.57
ROUTED TO										
+	DA30	.40	1	FLOW	47.	105.	144.	210.	271.	311.
				TIME	3.70	3.73	3.73	3.77	3.77	3.80
				*** PEAK STAGES IN FEET ***						
			1	STAGE	35.14	36.34	37.10	38.11	39.07	40.12
				TIME	3.70	3.73	3.73	3.77	3.77	3.80
DIVERSION TO										
+	A32	.40	1	FLOW	46.	97.	130.	190.	244.	281.
				TIME	3.70	3.73	3.73	3.77	3.77	3.80
HYDROGRAPH AT										
+	A31	.40	1	FLOW	1.	9.	14.	20.	26.	30.
				TIME	3.70	3.73	3.73	3.77	3.77	3.80
ROUTED TO										
+	ED1010	.40	1	FLOW	1.	9.	14.	20.	26.	30.
				TIME	3.80	3.80	3.80	3.80	3.80	3.83
				*** PEAK STAGES IN FEET ***						
			1	STAGE	95.12	95.80	96.07	96.29	96.49	96.61
				TIME	3.80	3.80	3.80	3.80	3.80	3.83
HYDROGRAPH AT										
+	1010	.01	1	FLOW	1.	6.	9.	15.	21.	27.
				TIME	3.20	3.13	3.13	3.13	3.13	3.13
2 COMBINED AT										
+	C1010	.42	1	FLOW	1.	9.	14.	21.	27.	32.
				TIME	3.20	3.80	3.73	3.80	3.77	3.80
ROUTED TO										
+	ED1010	.42	1	FLOW	1.	7.	10.	14.	18.	20.
				TIME	3.87	4.00	4.10	4.17	4.20	4.30
				*** PEAK STAGES IN FEET ***						
			1	STAGE	24.83	25.73	25.99	26.43	26.80	27.13
				TIME	3.87	4.00	4.10	4.17	4.20	4.30
ROUTED TO										
+	C1020	.42	1	FLOW	1.	7.	10.	14.	18.	20.
				TIME	3.90	4.00	4.10	4.17	4.20	4.30
				*** PEAK STAGES IN FEET ***						
			1	STAGE	95.13	95.72	95.87	96.09	96.21	96.30
				TIME	3.90	4.00	4.10	4.17	4.23	4.30

HYDROGRAPH AT
+ 1020 .00 1 FLOW TIME 1. 2. 2. 3. 4. 6.
3.10 3.10 3.10 3.10 3.10 3.10

2 COMBINED AT
+ C1020 .42 1 FLOW TIME 1. 7. 10. 14. 18. 21.
3.90 4.00 4.10 4.17 4.20 4.30

HYDROGRAPH AT
+ A32 .00 1 FLOW TIME 46. 97. 130. 190. 244. 281.
3.70 3.73 3.73 3.77 3.77 3.80

DIVERSION TO
+ A36 .00 1 FLOW TIME 45. 87. 114. 154. 192. 218.
3.70 3.73 3.73 3.77 3.77 3.80

HYDROGRAPH AT
+ A32 .00 1 FLOW TIME 1. 10. 16. 35. 53. 63.
3.70 3.73 3.73 3.77 3.77 3.80

ROUTED TO
+ C1030 .00 1 FLOW TIME 1. 10. 16. 35. 53. 63.
3.80 3.80 3.80 3.80 3.77 3.80

*** PEAK STAGES IN FEET ***
1 STAGE 95.14 95.88 96.18 96.76 97.16 97.35
TIME 3.80 3.80 3.80 3.80 3.77 3.80

ROUTED TO
+ C1030 .00 1 FLOW TIME 1. 10. 16. 35. 53. 63.
3.80 3.80 3.80 3.80 3.77 3.83

HYDROGRAPH AT
+ 1030 .01 1 FLOW TIME 1. 4. 6. 10. 14. 18.
3.27 3.20 3.20 3.20 3.17 3.17

2 COMBINED AT
+ C1030 .01 1 FLOW TIME 1. 10. 17. 36. 54. 65.
3.80 3.80 3.80 3.80 3.77 3.80

ROUTED TO
+ C1040 .01 1 FLOW TIME 1. 10. 17. 36. 54. 64.
3.80 3.80 3.80 3.80 3.77 3.83

HYDROGRAPH AT
+ 1040 .02 1 FLOW TIME 9. 17. 22. 32. 40. 49.
3.17 3.17 3.17 3.17 3.17 3.17

ROUTED TO
+ ED1040 .02 1 FLOW TIME 2. 4. 5. 6. 8. 9.
3.50 3.57 3.57 3.57 3.57 3.57

*** PEAK STAGES IN FEET ***
1 STAGE 24.68 25.02 25.23 25.58 25.87 26.18
TIME 3.50 3.57 3.57 3.57 3.57 3.57

2 COMBINED AT
+ C1040 .03 1 FLOW TIME 3. 14. 21. 42. 61. 73.
3.77 3.80 3.80 3.80 3.77 3.80

ROUTED TO
 + C1050 .03 1 FLOW 3. 14. 21. 42. 61. 73.
 TIME 3.80 3.80 3.80 3.80 3.80 3.83

*** PEAK STAGES IN FEET ***
 1 STAGE 95.46 96.07 96.33 96.89 97.28 97.49
 TIME 3.80 3.80 3.80 3.80 3.80 3.83

HYDROGRAPH AT
 + 1050 .00 1 FLOW 0. 2. 3. 5. 7. 9.
 TIME 3.17 3.13 3.13 3.10 3.10 3.10

2 COMBINED AT
 + C1050 .03 1 FLOW 3. 14. 22. 43. 62. 74.
 TIME 3.80 3.77 3.80 3.80 3.77 3.83

2 COMBINED AT
 + C1050 .45 1 FLOW 4. 21. 31. 55. 77. 92.
 TIME 3.83 3.83 3.83 3.83 3.83 3.83

ROUTED TO
 + C1070 .45 1 FLOW 4. 21. 31. 55. 77. 92.
 TIME 3.53 3.90 3.93 3.90 3.87 3.90

*** PEAK STAGES IN FEET ***
 1 STAGE 95.48 96.20 96.48 97.01 97.39 97.62
 TIME 3.53 3.90 3.93 3.90 3.87 3.90

HYDROGRAPH AT
 + 1060 .01 1 FLOW 1. 4. 6. 10. 14. 18.
 TIME 3.37 3.30 3.30 3.27 3.27 3.27

ROUTED TO
 + C1070 .01 1 FLOW 1. 4. 6. 10. 14. 17.
 TIME 3.40 3.33 3.30 3.30 3.30 3.30

*** PEAK STAGES IN FEET ***
 1 STAGE 98.87 98.88 98.89 98.92 98.94 98.96
 TIME 3.40 3.33 3.30 3.30 3.30 3.30

HYDROGRAPH AT
 + 1070 .03 1 FLOW 9. 19. 26. 38. 50. 62.
 TIME 3.20 3.20 3.20 3.20 3.17 3.17

3 COMBINED AT
 + C1070 .49 1 FLOW 10. 31. 44. 68. 91. 116.
 TIME 3.20 3.27 3.23 3.23 3.23 3.23

ROUTED TO
 + C1080 .49 1 FLOW 10. 33. 46. 78. 98. 121.
 TIME 3.67 3.47 3.43 3.40 3.37 3.37

*** PEAK STAGES IN FEET ***
 1 STAGE 95.49 96.06 96.31 96.71 96.95 97.17
 TIME 3.67 3.47 3.43 3.40 3.37 3.37

HYDROGRAPH AT
 + 1080 .05 1 FLOW 18. 36. 48. 68. 87. 106.
 TIME 3.20 3.20 3.20 3.20 3.20 3.20

2 COMBINED AT
+ C1080 .54 1 FLOW 20. 49. 69. 114. 149. 183.
TIME 3.20 3.47 3.43 3.40 3.37 3.37

HYDROGRAPH AT
+ 1090 .03 1 FLOW 12. 24. 33. 48. 62. 76.
TIME 3.17 3.20 3.20 3.17 3.17 3.17

ROUTED TO
+ C1100 .03 1 FLOW 12. 24. 33. 48. 62. 76.
TIME 3.17 3.20 3.20 3.17 3.17 3.17

** PEAK STAGES IN FEET **

1 STAGE 98.75 98.75 98.75 98.75 98.75 98.75
TIME 3.17 3.20 3.17 3.17 3.17 3.17

HYDROGRAPH AT
+ 1100 .07 1 FLOW 14. 29. 39. 56. 72. 90.
TIME 3.43 3.47 3.47 3.43 3.43 3.43

2 COMBINED AT
+ C1100 .10 1 FLOW 20. 41. 55. 79. 102. 126.
TIME 3.27 3.30 3.30 3.30 3.27 3.27

2 COMBINED AT
+ C1080 .64 1 FLOW 39. 87. 121. 190. 249. 307.
TIME 3.23 3.47 3.43 3.40 3.37 3.37

HYDROGRAPH AT
+ 40 .03 1 FLOW 12. 20. 25. 33. 40. 47.
TIME 3.47 3.47 3.47 3.47 3.47 3.47

ROUTED TO
+ SD110 .03 1 FLOW 12. 20. 25. 33. 40. 47.
TIME 3.47 3.47 3.47 3.47 3.47 3.47

HYDROGRAPH AT
+ 50 .01 1 FLOW 4. 7. 8. 11. 14. 17.
TIME 3.17 3.17 3.17 3.17 3.17 3.17

HYDROGRAPH AT
+ 110 .00 1 FLOW 1. 1. 2. 2. 2. 3.
TIME 3.07 3.07 3.07 3.07 3.07 3.07

2 COMBINED AT
+ C110 .01 1 FLOW 4. 7. 9. 13. 16. 19.
TIME 3.17 3.17 3.17 3.17 3.17 3.17

HYDROGRAPH AT
+ 210 .00 1 FLOW 2. 3. 4. 5. 5. 6.
TIME 3.07 3.07 3.07 3.07 3.07 3.07

3 COMBINED AT
+ SD210 .04 1 FLOW 14. 23. 28. 37. 46. 54.
TIME 3.43 3.43 3.43 3.43 3.43 3.43

ROUTED TO
+ SD220 .04 1 FLOW 14. 23. 28. 37. 45. 54.
TIME 3.43 3.43 3.43 3.43 3.43 3.43

HYDROGRAPH AT
+ 70 .01 1 FLOW 5. 9. 12. 16. 20. 25.
TIME 3.23 3.23 3.23 3.23 3.23 3.23

HYDROGRAPH AT
+ 120 .00 1 FLOW 1. 1. 1. 2. 2. 2.
TIME 3.07 3.07 3.07 3.07 3.07 3.07

2 COMBINED AT
+ C120 .01 1 FLOW 6. 10. 13. 17. 21. 25.
TIME 3.20 3.23 3.23 3.23 3.23 3.23

2 COMBINED AT
+ SD220 .05 1 FLOW 18. 30. 37. 49. 60. 72.
TIME 3.30 3.30 3.30 3.30 3.30 3.30

ROUTED TO
+ SD230 .05 1 FLOW 18. 30. 37. 49. 60. 72.
TIME 3.30 3.30 3.30 3.30 3.30 3.30

HYDROGRAPH AT
+ 80 .00 1 FLOW 1. 2. 3. 4. 4. 5.
TIME 3.13 3.13 3.13 3.13 3.13 3.13

HYDROGRAPH AT
+ 130 .00 1 FLOW 1. 1. 1. 1. 2. 2.
TIME 3.07 3.07 3.07 3.07 3.07 3.07

2 COMBINED AT
+ C130 .00 1 FLOW 2. 3. 3. 5. 6. 7.
TIME 3.10 3.10 3.13 3.13 3.13 3.13

HYDROGRAPH AT
+ 220 .00 1 FLOW 2. 3. 3. 4. 5. 6.
TIME 3.07 3.07 3.07 3.07 3.07 3.07

ROUTED TO
+ C230 .00 1 FLOW 2. 3. 3. 4. 5. 6.
TIME 3.10 3.10 3.10 3.10 3.10 3.10

*** PEAK STAGES IN FEET ***

1 STAGE 97.88 97.89 97.90 97.90 97.91 97.91
TIME 3.10 3.10 3.10 3.10 3.10 3.10

HYDROGRAPH AT
+ 230 .00 1 FLOW 1. 2. 3. 3. 4. 4.
TIME 3.07 3.07 3.07 3.07 3.07 3.07

2 COMBINED AT
+ C230 .00 1 FLOW 3. 5. 6. 8. 9. 10.
TIME 3.10 3.10 3.10 3.10 3.10 3.10

3 COMBINED AT
+ SD230 .05 1 FLOW 20. 33. 41. 54. 66. 79.
TIME 3.17 3.20 3.23 3.23 3.23 3.23

ROUTED TO
+ SD90 .05 1 FLOW 20. 33. 41. 54. 66. 79.
TIME 3.20 3.23 3.23 3.23 3.23 3.23

3 COMBINED AT
+ SD260 .10 1 FLOW TIME 38. 62. 78. 104. 129. 155.
3.17 3.20 3.20 3.20 3.23 3.23

ROUTED TO
+ SD270 .10 1 FLOW TIME 37. 62. 78. 104. 129. 154.
3.17 3.20 3.20 3.23 3.23 3.23

HYDROGRAPH AT
+ 170 .00 1 FLOW TIME 0. 1. 1. 1. 1. 2.
3.10 3.10 3.10 3.10 3.10 3.10

HYDROGRAPH AT
+ 270 .00 1 FLOW TIME 2. 3. 3. 4. 4. 5.
3.07 3.07 3.07 3.07 3.07 3.07

3 COMBINED AT
+ SD270 .10 1 FLOW TIME 39. 64. 79. 106. 131. 157.
3.17 3.17 3.20 3.20 3.20 3.23

DIVERSION TO
+ ST270 .10 1 FLOW TIME 0. 0. 0. 0. 0. 26.
.03 .03 .03 .03 .03 3.23

HYDROGRAPH AT
+ SD270 .10 1 FLOW TIME 39. 64. 79. 106. 131. 131.
3.17 3.17 3.20 3.20 3.20 3.13

ROUTED TO
+ SDBOX .10 1 FLOW TIME 39. 64. 79. 106. 131. 131.
3.17 3.20 3.20 3.23 3.23 3.17

2 COMBINED AT
+ C1080 .74 1 FLOW TIME 78. 141. 186. 282. 368. 438.
3.20 3.23 3.43 3.40 3.37 3.37

ROUTED TO
+ C1110N .74 1 FLOW TIME 78. 147. 185. 275. 364. 443.
3.27 3.27 3.23 3.43 3.40 3.40

*** PEAK STAGES IN FEET ***
1 STAGE 93.54 93.81 93.93 94.21 94.42 94.59
TIME 3.27 3.27 3.23 3.43 3.40 3.40

HYDROGRAPH AT
+ 1110N .00 1 FLOW TIME 1. 2. 3. 5. 7. 9.
3.07 3.10 3.10 3.10 3.10 3.10

2 COMBINED AT
+ C1100N .75 1 FLOW TIME 78. 148. 187. 276. 366. 445.
3.27 3.27 3.23 3.43 3.40 3.40

HYDROGRAPH AT
+ ST270 .00 1 FLOW TIME 0. 0. 0. 0. 0. 26.
.03 .03 .03 .03 .03 3.23

ROUTED TO
+ ST280 .00 1 FLOW TIME 0. 0. 0. 0. 0. 28.
.03 .03 .03 .03 .03 3.20

*** PEAK STAGES IN FEET ***

1	STAGE	98.61	98.61	98.61	98.61	98.61	99.05
	TIME	.00	.00	.00	.00	.00	3.20

DIVERSION TO

+	ST280	.00	1	FLOW	0.	0.	0.	0.	0.	28.
				TIME	.03	.03	.03	.03	.03	3.20

HYDROGRAPH AT

+	SD280	.00	1	FLOW	0.	0.	0.	0.	0.	0.
				TIME	.03	.03	.03	.03	.03	.03

2 COMBINED AT

+	C1110N	.75	1	FLOW	78.	148.	187.	276.	366.	445.
				TIME	3.27	3.27	3.23	3.43	3.40	3.40

ROUTED TO

+	C1110S	.75	1	FLOW	78.	156.	196.	280.	367.	449.
				TIME	3.37	3.27	3.23	3.50	3.43	3.43

*** PEAK STAGES IN FEET ***

1	STAGE	93.55	93.84	93.97	94.23	94.43	94.60
	TIME	3.37	3.27	3.23	3.50	3.43	3.43

HYDROGRAPH AT

+	ST280	.00	1	FLOW	0.	0.	0.	0.	0.	28.
				TIME	.03	.03	.03	.03	.03	3.20

ROUTED TO

+	C370	.00	1	FLOW	0.	0.	0.	0.	0.	29.
				TIME	.03	.03	.03	.03	.03	3.23

*** PEAK STAGES IN FEET ***

1	STAGE	98.61	98.61	98.61	98.61	98.61	99.06
	TIME	.00	.00	.00	.00	.00	3.23

HYDROGRAPH AT

+	350	.00	1	FLOW	1.	2.	3.	4.	6.	7.
				TIME	3.10	3.10	3.10	3.10	3.10	3.10

DIVERSION TO

+	D330	.00	1	FLOW	1.	1.	1.	2.	3.	3.
				TIME	3.10	3.10	3.10	3.10	3.10	3.10

HYDROGRAPH AT

+	C350	.00	1	FLOW	1.	1.	1.	2.	3.	3.
				TIME	3.10	3.10	3.10	3.10	3.10	3.10

ROUTED TO

+	C360	.00	1	FLOW	0.	1.	2.	2.	3.	3.
				TIME	3.37	3.27	3.27	3.23	3.23	3.27

*** PEAK STAGES IN FEET ***

1	STAGE	98.71	98.76	98.78	98.80	98.82	98.84
	TIME	3.37	3.27	3.27	3.23	3.23	3.27

HYDROGRAPH AT

+	360	.01	1	FLOW	5.	10.	13.	19.	24.	30.
				TIME	3.17	3.20	3.20	3.20	3.17	3.17

HYDROGRAPH AT										
+	370	.01	1	FLOW	2.	5.	6.	9.	12.	15.
				TIME	3.13	3.17	3.17	3.13	3.13	3.13

4 COMBINED AT										
+	C370	.02	1	FLOW	7.	14.	19.	28.	37.	71.
				TIME	3.17	3.17	3.17	3.20	3.17	3.23

ROUTED TO										
+	C380N	.02	1	FLOW	7.	14.	20.	28.	37.	69.
				TIME	3.23	3.27	3.23	3.20	3.23	3.30

*** PEAK STAGES IN FEET ***

1	STAGE	98.88	98.95	99.00	99.04	99.09	99.23
	TIME	3.23	3.27	3.23	3.20	3.23	3.30

HYDROGRAPH AT										
+	380N	.01	1	FLOW	2.	4.	6.	8.	10.	13.
				TIME	3.20	3.20	3.20	3.20	3.20	3.20

2 COMBINED AT										
+	C380N	.03	1	FLOW	9.	18.	25.	36.	47.	79.
				TIME	3.23	3.23	3.23	3.20	3.23	3.30

ROUTED TO										
+	C1110S	.03	1	FLOW	9.	18.	25.	36.	47.	78.
				TIME	3.23	3.27	3.23	3.20	3.23	3.30

HYDROGRAPH AT										
+	1110S	.02	1	FLOW	6.	11.	15.	22.	30.	39.
				TIME	3.10	3.13	3.13	3.13	3.13	3.13

3 COMBINED AT										
+	C1110S	.79	1	FLOW	87.	180.	231.	308.	402.	501.
				TIME	3.37	3.27	3.23	3.30	3.27	3.43

ROUTED TO										
+	C1120	.79	1	FLOW	87.	189.	235.	313.	402.	506.
				TIME	3.37	3.27	3.23	3.30	3.27	3.43

*** PEAK STAGES IN FEET ***

1	STAGE	100.68	101.14	101.30	101.57	101.83	102.13
	TIME	3.37	3.27	3.23	3.30	3.27	3.43

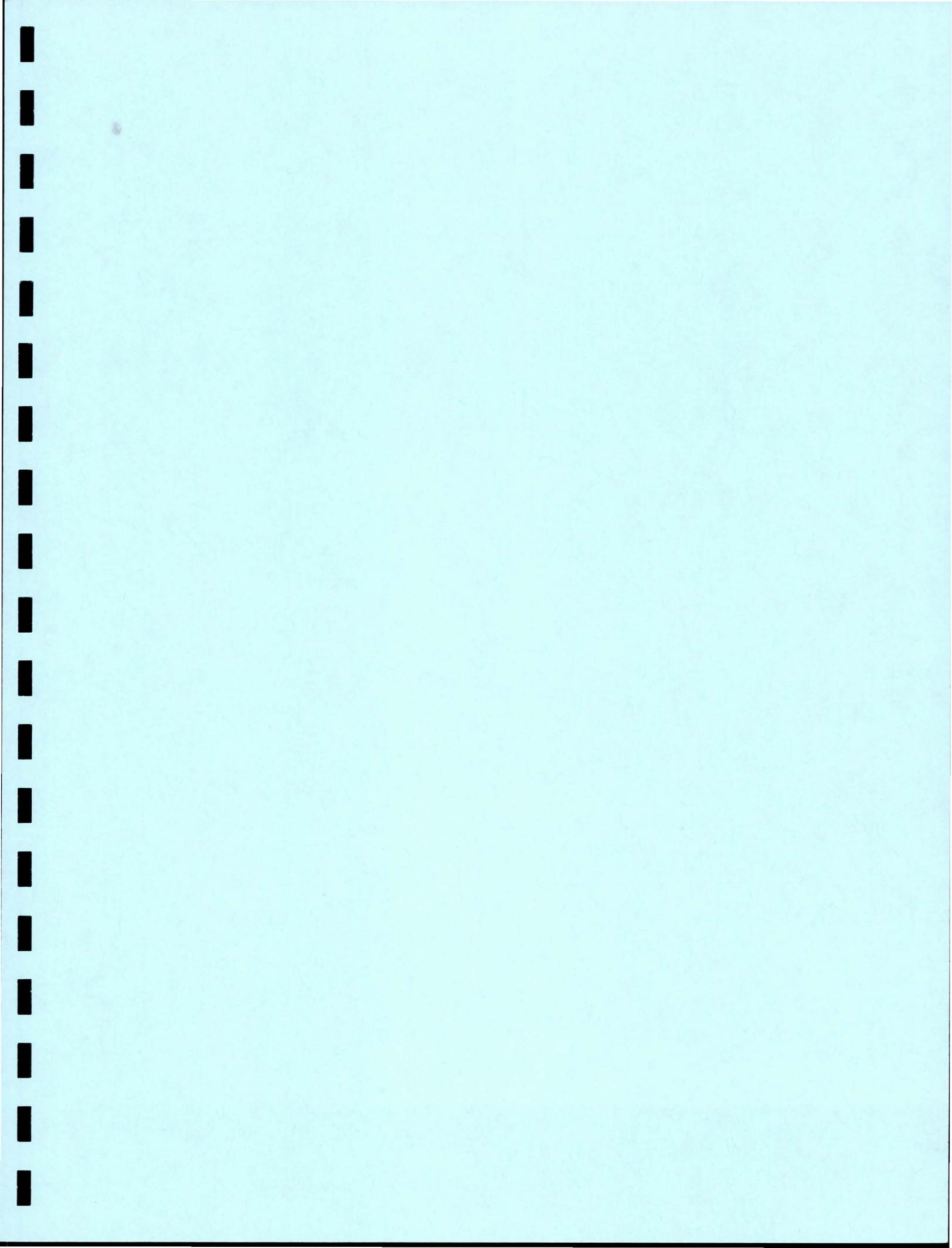
HYDROGRAPH AT										
+	1120	.02	1	FLOW	16.	24.	30.	39.	48.	57.
				TIME	3.10	3.10	3.10	3.10	3.10	3.10

2 COMBINED AT										
+	C1120	.81	1	FLOW	90.	198.	248.	324.	419.	515.
				TIME	3.33	3.27	3.23	3.30	3.27	3.43

ROUTED TO										
+	LAKE5	.81	1	FLOW	4.	44.	86.	168.	248.	340.
				TIME	5.97	4.33	4.03	3.77	3.70	3.63

*** PEAK STAGES IN FEET ***

1	STAGE	76.18	76.99	77.30	77.77	78.16	78.46
	TIME	5.97	4.33	4.03	3.77	3.70	3.63



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*
* FLOOD HYDROGRAPH PACKAGE (HEC-1)
* SEPTEMBER 1990
* VERSION 4.0
*
* RUN DATE 06/28/1995 TIME 16:40:38
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*
* U.S. ARMY CORPS OF ENGINEERS
* HYDROLOGIC ENGINEERING CENTER
* 609 SECOND STREET
* DAVIS, CALIFORNIA 95616
* (916) 756-1104
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THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE.
 THE DEFINITION OF -AMSK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION
 NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,
 DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION
 KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

1 ID 84TH STREET AND CHOLLA ROAD
 2 ID 2-5-10-25-50-100 yr STORM
 3 ID INTERIM CONDITION:
 4 ID FINAL DESIGN ***** SCC BASIN*****
 5 ID --ASSUME NO SPLIT IN CACTUS/84TH INTERSECTION
 6 ID --100-YR NEW STORM SEWER IN CACTUS (INclude ADOT R/W FOR INTERIM)
 7 ID --no bypass into 84th st south. all flows go to scc.
 8 ID --CACTUS SD TO OUTFALL AT BOX-CULVERT
 9 ID --NO INTERCEPTOR AT CORTEZ IN 84TH STREET
 10 ID --No NEW PIMA CHANNEL
 11 ID --FLOW SPLIT AT NORTH END OF PIMA DETENTION BASINS (1060A)
 12 ID --NEW INTERIM DETENTION BASINS (2) WEST OF PIMA & NORTH OF SWEETWATER
 13 ID --36" PIPE TO EAST PIMA.
 14 ID --3 DETENTION BASINS AT PIMA-LAYOUT UPDATED FOR LANDSCAPING (5-17-95)
 15 ID --FILE SCCSW7.DAT
 16 ID *****

*DIAGRAM

17 IT 2 300
 18 IO 5
 19 JR PREC .36 .53 .62 .76 .88 1.0
 20 ID JR PREC 1.0

21 KK 710 SUBBASIN 710 RUNOFF
 22 PH 0.88 1.61 2.6 2.84 3 3.3
 23 BA 0.0090
 24 LS 0 77 50
 25 UD 0.07

26 KK C720 ROUTE 710 TO C720
 27 RS 100 STOR -1 0
 28 RC .060 0.040 0.060 850 .0100
 29 RX 0 .1 100 101 104 105 205 205.1
 30 RY 105 100 99 96 96 99 100 105
 31 RS 100 STOR -1 0
 32 RC .060 0.040 .060 460 .0100
 33 RX 0 .1 100 101 106 107 207 207.1
 34 RY 105 100 99 95 95 99 100 105
 35 RS 100 STOR -1 0
 36 RC .050 0.030 .050 350 .0034
 37 RX 0 .1 100 109 109.1 118.1 120 120.1
 38 RY 105 100 99 96 96 99 99 105

39 KK 720 SUBBASIN 720 RUNOFF
 40 BA 0.0655
 41 LS 0 77
 42 UD 0.21

43 KK C720 COMBINE 710 AND 720
 44 HC 2

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

45	KK	C720	ROUTE C720 TO C735						
46	RS	100	STOR	-1	0				
47	RC	.040	0.020	.040	130	.0150			
48	RX	0	.1	1	5	15	19	19.1	20
49	RY	105	100	100	99	99	100	100	105
50	RC	.040	0.016	.040	400	.0060			
51	RX	0	.1	9	9.1	37	37.1	46	46.1
52	RY	105	100	100	99.75	99.75	100	100	105
53	RC	.040	0.016	.040	650	.0080			
54	RX	0	.1	9	9.1	37	37.1	46	46.1
55	RY	105	100	100	99.75	99.75	100	100	105
56	RX	0	.1	1	5	15	19	19.1	20
57	RC	.040	0.016	.040	1400	.0100			
58	RX	0	.1	9	9.1	37	37.1	46	46.1
59	RY	105	100	100	99.75	99.75	100	100	105

60	KK	725	SUBBASIN 725 RUNOFF						
61	BA	0.0680							
62	LS	0	77	42					
63	UD	0.20							

64	KK	ED725	EXISTING DETENTION BASIN 725						
65	RS	1	STOR	-1	0				
66	SA	0.78	1.14	1.17	1.2	1.24	1.24	1.24	1.24
67	SE	1468.5	1472	1472.3	1472.6	1473	1473.5	1474	
68	SQ	0	0	10.45	31.23	72.0	100	200	

69	KK	730	SUBBASIN 730 RUNOFF						
70	BA	0.0053							
71	LS	0	77	42					
72	UD	0.05							

73	KK	C730	COMBINE C725 AND 730						
74	HC	2							

75	KK	ED730	EXISTING DETENTION BASIN 730						
76	RS	1	STOR	-1	0				
77	SA	0.76	1.12	1.15	1.18	1.22	1.22		
78	SE	1464.5	1468	1468.3	1468.6	1469	1469.5		
79	SQ	0	0	5.52	17.29	42.0	150		

80	KK	735	SUBBASIN 735 RUNOFF						
81	BA	.05147							
82	LS	0	77	42					
83	UD	0.29							

84	KK	C735	COMBINE C725 AND C730 AND 735						
85	HC	3							

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

86 KK ED735 EXISTING DETENTION BASIN 735
 87 RS 1 STOR -1 0
 88 SA 1.04 1.40 1.45 1.51 1.56 1.61 1.61 1.61
 89 SE 1461.9 1465.4 1465.9 1466.4 1466.9 1467.4 1468 1468.5
 90 SQ 0 0 3.2 18.0 49.6 101.8 200 500

91 KK 740 SUBBASIN 740 RUNOFF
 92 BA .00055
 93 LS 0 98
 94 UD 0.08

95 KK 742 SUBBASIN 742 RUNOFF
 96 BA .00836
 97 LS 77
 98 UD .11

99 KK C742 COMBINE 740 AND 742
 100 HC 2

101 KK C744 ROUTE C742 TO C744
 102 RK 95 .0044 .012 CIRC 2

103 KK 743 SUBBASIN 743 RUNOFF
 104 BA .00373
 105 LS 0 77 47
 106 UD 0.07

107 KK C744 ROUTE 743 TO C744
 108 RS 100 STOR -1 0
 109 RC .030 0.016 .030 580 .0085
 110 RX 0 .1 11 11.1 79 79.1 90 90.1
 111 RY 105 100 99 99.82 99.82 99 100 105

112 KK 744 SUBBASIN 744 RUNOFF
 113 BA .00661
 114 LS 0 98
 115 UD 0.14

116 KK C744 COMBINE C742 AND 743 AND 744
 117 HC 3

118 KK C745 ROUTE C744 TO C745
 119 RK 638 .0029 .012 CIRC 3.5

120 KK 745 SUBBASIN 745 RUNOFF
 121 BA .01783
 122 LS 0 77
 123 UD 0.17

LINE	ID	1	2	3	4	5	6	7	8	9	10
124	KK	C745	COMBINE C744 AND 745								
125	HC	2									
126	KK	C735	ROUTE C745 TO C735								
127	RK	510	.0024	.012		CIRC	4				
128	KK	C735	COMBINE C745 AND 735								
129	HC	2									
130	KK	C760	ROUTE C735 TO C760								
131	RK	130	.0030	.012		TRAP	10	.001			
132	KK	760	SUBBASIN 760 RUNOFF								
133	BA	.01266									
134	LS	0	98								
135	UD	0.19									
136	KK	C760	COMBINE C735 AND 760								
137	HC	2									
138	KK	C790	ROUTE C760 TO C790								
139	RS	100	STOR	-1	0						
140	RC	.050	0.012	.020	900	.0019					
141	RX	0	.1	28	32	37	42	100	100.1		
142	RY	105	100	99	95	95	100	101	105		
143	RC	.050	0.012	.020	250	.0019					
144	RX	0	.1	28	28.1	37.5	37.6	49	49.1		
145	RY	105	100	99	95	95	99	100	105		
146	KK	780	SUBBASIN 780 RUNOFF								
147	BA	.01686									
148	LS	0	77	20							
149	UD	0.13									
150	KK	C782	ROUTE C780 TO C782								
151	RS	100	STOR	-1	0						
152	RC	.020	.025	.050	1210	.010					
153	RX	2	2	30	40	50	60	80	100		
154	RY	105	100.52	100	99.5	98	100	100.5	101		
155	KK	782	SUBBASIN 782 RUNOFF								
156	BA	.01080									
157	LS		77								
158	UD	.18									
159	KK	784	SUBBASIN 784 RUNOFF								
160	BA	.04764									
161	LS		77	42							
162	UD	.19									

LINE	ID	1	2	3	4	5	6	7	8	9	10
163	KK	ED784	EXISTING DETENTION BASIN 784								
164	RS	1	STOR	-1	0						
165	SA	0	1.09	2.02	2.02						
166	SE	1389.0	1389.5	1392.5	1393.0						
167	SQ	0	1.4	58	768						
168	KK	C782	COMBINE 780 AND C782 AND 784								
169	HC	3									
170	KK	C790	ROUTE C782 TO C790								
171	RS	100	STOR	-1	0						
172	RC	.020	.025	.050	2800	.010					
173	RX	2	2	30	40	50	60	80	100		
174	RY	105	100.52	100	99.5	98	100	100.5	101		
175	KK	790	SUBBASIN 790 RUNOFF								
176	BA	.11345									
177	LS		77								
178	UD	.23									
179	KK	C790	COMBINE 782 AND C760 AND 790								
180	HC	3									
181	KK	750	SUBBASIN 750 RUNOFF								
182	BA	.00313									
183	LS	0	98								
184	UD	0.07									
185	KK	C770	ROUTE C750 TO C770								
186	RS	100	STOR	-1	0						
187	RC	.050	0.016	.016	1100	.0040					
188	RX	0	.1	.2	5	5.1	29.1	29.2	29.3		
189	RY	105	100.5	100.5	100	99.5	100	105	105		
190	KK	770	SUBBASIN 770 RUNOFF								
191	BA	.00505									
192	LS	0	98								
193	UD	0.09									
194	KK	C770	COMBINE C770 AND 770								
195	HC	2									
196	KK	C770	COMBINE C770 AND C790								
197	HC	2									
198	KK	C800	ROUTE C770 TO C800								
199	RS	100	STOR	-1	0						
200	RC	.050	0.020	.050	380	.0037					
201	RX	0	.1	20	36	46	62	82	102		
202	RY	110	106.5	106	100	100	106	106.5	107		

LINE	ID	1	2	3	4	5	6	7	8	9	10
203	KK	800									
204	BA	.01719									
205	LS	0	77								
206	UD	0.16									
207	KK	C800									
208	HC	2									
209	KK	C810									
210	RS	100	STOR	-1	0						
211	RC	.050	0.020	.050	1170	.0037					
212	RX	0	.1	20	36	60	76	96	116		
213	RY	110	105	104.5	100	100	104.5	105	105.5		
214	KK	810									
215	BA	.04392									
216	LS	0	77	42							
217	UD	0.23									
218	KK	C810									
219	HC	2									
220	KK	C820									
221	RS	100	STOR	-1	0						
222	RC	.050	0.020	.050	790	.0037					
223	RX	0	.1	20	36	60	76	96	116		
224	RY	110	105	104.5	100	100	104.5	105	105.5		
225	KK	820									
226	BA	.03645									
227	LS	0	77	38							
228	UD	0.16									
229	KK	C820									
230	HC	2									
231	KK	C830									
232	RS	100	STOR	-1	0						
233	RC	.012	0.012	.012	97	.0104					
234	RX	0	.1	.2	.3	.4	.5	20	20.1		
235	RY	106	100	100	100	100	100	100	106		
236	KK	910									
237	BA	.04977									
238	LS	0	77	65							
239	UD	0.20									
240	KK	C920									
241	RK	660	.050	.012		CIRC	2				
242	RK	680	.0060	.025		TRAP	1	1			

LINE	ID	1	2	3	4	5	6	7	8	9	10
243	KK	920	SUBBASIN 920 RUNOFF								
244	BA	.02748									
245	LS	0	69	49							
246	UD	0.26									
247	KK	C920	COMBINE 910 AND 920								
248	HC	2									
249	KK	C930	ROUTE C920 TO C930								
250	RS	100	STOR	-1	0						
251	RC	.050	0.016	.016	680	.0040					
252	RX	0	.1	15	20.5	20.6	44.5	44.6	44.7		
253	RY	105	100	99.5	99.4	98.9	99.4	100	105		
254	KK	930	SUBBASIN 930 RUNOFF								
255	BA	.05831									
256	LS	0	77	38							
257	UD	0.25									
258	KK	C930	COMBINE C920 AND 930								
259	HC	2									
260	KK	C930	DIVERT FLOW TO C950								
261	DT	D930									
262	DI	0	51	400							
263	DQ	0	51	51							
264	KK	C830	ROUTE C930 TO C830								
265	RS	100	STOR	-1	0						
266	RC	.050	0.016	.016	640	.0028					
267	RX	0	.1	7.5	7.6	34.5	34.6	40.5	50.0		
268	RY	105	100	100	99.5	99.0	99.5	99.7	100		
269	KK	830	SUBBASIN 830 RUNOFF								
270	BA	.00148									
271	LS	0	98								
272	UD	0.07									
273	KK	C830	COMBINE 830 AND C820 AND 930 (Downstream Box-Culvert T-bird)								
274	HC	3									
275	KK	C830	DIVERT FLOW TO C960 (EXISTING DIVERSION)								
276	DT	D830									
277	DI	0	520	718	1045						
278	DQ	0	0	138	445						
279	KK	A30	SUBBASIN A30 RUNOFF								
280	BA	0.4031									
281	LS	0	77	11							
282	UD	0.47									

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

283	KK	DA30	DETENTION BASIN AT CPA30						
284	KM		Outflow to A31 and A32 and A36						
285	RS	1	STOR	0					
286	SA	0	0.49	0.94	1.39	1.93			
287	SE	34.99	35.00	37.00	39.00	41.40			
288	SQ	0	40	137.4	268	361			
289	KK	A31	SPLIT FLOW AT DETENTION BASIN DA30						
290	KM		DI is Total Outflow from Detention Basin (A31+A32+A36)						
291	KM		DQ is Split to A32 and A36						
292	DT	A32							
293	DI	0	40	137.4	268	361			
294	DQ	0	40	124.4	242	326			
295	KK	CA31	COMBINE C830 AND A31						
296	HC	2							
297	KK	ED1010	ROUTE CA31 TO ED1010						
298	RS	100	STOR	-1	0				
299	RC	.060	.040	.060	600	.0086			
300	RX	0	0.1	50	56	59	65	115 115.1	
301	RY	105	100	99	95	95	99	100 105	
302	KK	1010	SUBBASIN 1010 RUNOFF						
303	BA	.01192							
304	LS	0	77						
305	UD	0.08							
306	KK	C1010	COMBINE 1010 and CA31						
307	HC	2							
308	KK	ED1010	EXISTING DETENTION BASIN 1010 (McDowell Shadow Estates II)						
309	RS	1	STOR	0					
310	SA	0	0.41	0.93	1.19	1.45	1.71	2.23	
311	SE	24.7	25.7	26.7	27.2	27.7	28.2	29.2	
312	SQ	0	7	17	21	69	240	1082	
313	KK	1060A	SUBBASIN 1060A RUNOFF						
314	BA	.00198							
315	LS	0	77						
316	UD	0.06							
317	KK	10N	SUBBASIN 10N RUNOFF						
318	BA	.00236							
319	LS	0	89						
320	UD	0.06							
321	KK	C1060A	COMBINE ED1010 AND 1060A AND 10N						
322	HC	3							

LINE	ID	1	2	3	4	5	6	7	8	9	10
323	KK	CPIMAA	ROUTE NEW DETENTION BASIN PIMA-A(Box-Culvert 12'x3' to Basin B)								
324	RS	1	STOR	0							
325	SV	0	0.33	0.71	1.14	1.90	2.17	2.57	2.77	2.97	3.17
326	SE	19	20	21	22	23.5	24	25	25.5	26	27
327	SQ	36	102	192	252	348	361	446	489	547	743
328	KK	C1060A	SPLIT FLOW WITH EXISTING WASH-WEST SPILLWAY (WASH FL=1423.5)								
329	DT	D1060A									
330	DI	0	348	361	405	446	489	547	647	743	
331	DQ	0	0	1	9	26	57	103	167	251	
332	KK	1060B	SUBBASIN 1060B RUNOFF								
333	BA	.00440									
334	LS	0	77								
335	UD	0.06									
336	KK	1060C	SUBBASIN 1060C RUNOFF								
337	BA	.00487									
338	LS	0	77								
339	UD	0.06									
340	KK	C1060C	COMBINE 1060B AND 1060C AND PIMA-A								
341	HC	3									
342	KK	CPIMAB	ROUTE NEW DETENTION BASIN PIMA-B (SPILLWAY ELEV=1421)								
343	RS	1	STOR	0							
344	SV	0	2.01	4.13	6.38	8.74	11.22	13.84	15.22	16.59	
345	SE	16	17	18	19	20	21	22	22.5	23	
346	SQ	0	4	13	21	26	32	235	386	617	
347	KK	1060D	SUBBASIN 1060D RUNOFF								
348	BA	.00488									
349	LS	0	77								
350	UD	0.06									
351	KK	C1060D	COMBINE PIMA-B AND 1060D								
352	HC	2									
353	KK	CPIMAC	ROUTE NEW DETENTION BASIN PIMA-C (36" PIPE TO PIMA ROAD)								
354	RS	1	STOR	0							
355	SV	0	3.60	7.35	11.13	14.99	19.13	23.43			
356	SE	15	16	17	18	19	20	21			
357	SQ	0	10	20	35	50	60	70			
358	KK	A32	RETRIEVE SPLIT FLOW AT A32 (A36 and A32)								
359	DR	A32									
360	KK	A32	SPLIT FLOW AT DETENTION BASIN DA30								
361	KM		DI is Split to A32 and A36								
362	KM		DQ is Split to A36 (Box Culvert)								
363	DT	A36									
364	DI	0	40	124.4	242	326					
365	DQ	0	40	110	190	250					

LINE	ID	1	2	3	4	5	6	7	8	9	10
405	KK	1020	SUBBASIN 1020 RUNOFF								
406	BA	.00198									
407	LS	0	77	10							
408	UD	0.06									
409	KK	C1050	COMBINE C1050 AND C1020 AND D1060A								
410	HC	3									
411	KK	C1070	ROUTE C1050 TO C1070								
412	RS	100	STOR	-1	0						
413	RC	.050	0.040	.050	1150	.0078					
414	RX	0	0.1	50	56	60	66	116	116.1		
415	RY	105	100	99	95	95	99	100	105		
416	KK	1070	SUBBASIN 1070 RUNOFF								
417	BA	.02864									
418	LS	0	77	17							
419	UD	0.14									
420	KK	C1070	COMBINE C1050 AND 1070								
421	HC	2									
422	KK	C1080	ROUTE C1070 TO C1080								
423	RS	100	STOR	-1	0						
424	RC	.050	0.040	.050	3100	.0066					
425	RX	0	0.1	30	41	49	60	90	90.1		
426	RY	108	100	99	95	95	99	100	108		
427	KK	1080	SUBBASIN 1080 RUNOFF								
428	BA	.04840									
429	LS	0	77	24							
430	UD	0.16									
431	KK	C1080	COMBINE 1080 AND C1070								
432	HC	2									
433	KK	1090	SUBBASIN 1090 RUNOFF								
434	BA	.03370									
435	LS	0	77	20							
436	UD	0.138									
437	KK	C1100	ROUTE 1090 TO C1100								
438	RS	100	STOR	-1	0						
439	RC	.040	0.016	.040	.0074	2340					
440	RX	0	0.1	20	20.1	60	60.1	80	80.1		
441	RY	105	100	99	98.75	98.75	99	100	105		
442	KK	1100	SUBBASIN 1100 RUNOFF								
443	BA	.07053									
444	LS	0	77	18							
445	UD	0.37									

LINE	ID	1	2	3	4	5	6	7	8	9	10
446	KK	C1100	COMBINE 1100 AND 1090								
447	HC	2									
448	KK	C1080	COMBINE C1100 AND C1080								
449	HC	2									
450	KK	40	SUBBASIN 40 RUNOFF								
451	BA	.03122									
452	LS		77	45							
453	UD	.42									
454	KK	SD110	ROUTE C40 TO SD110								
455	RK	190	0.0010	0.012		CIRC	3				
456	KK	10	SUBBASIN 10 RUNOFF								
457	BA	.00536									
458	PH		0.88	1.61	2.6	2.84	3.0	3.3			
459	LS		89								
460	UD	.10									
461	KK	20	SUBBASIN 20 RUNOFF								
462	BA	.00273									
463	LS		77								
464	UD	.20									
465	KK	C10	COMBINE 10 AND 20								
466	HC	2									
467	KK	C15	ROUTE C10 TO C15								
468	RS	100	STOR	-1	0						
469	RC	0.016	0.025	0.040	2605	0.0070					
470	RX	0	20	40	49	51	60	80	100		
471	RY	100	99.6	99.2	97	97	99.2	99.6	100		
472	KK	15	SUBBASIN 15 RUNOFF								
473	BA	.00559									
474	LS		89								
475	UD	.08									
476	KK	C15	COMBINE C10 AND 15								
477	HC	2									
478	KK	C15	DIVERT C15 TO SOUTH PIMA ROAD								
479	DT	D15									
480	DI	0	19	30	40						
481	DQ	0	19	19	29						
482	KK	C110	ROUTE C15 TO 110								
483	RS	100	STOR	-1	0						
484	RC	.040	0.016	.016	680	.0030					
485	RX	20	40	65	70	70	72	100	100		
486	RY	103.1	102.9	101.75	101.74	101.27	101.35	101.63	103.63		

LINE	ID	1	2	3	4	5	6	7	8	9	10
527	KK	C130	COMBINE 80 AND 130								
528	HC	2									
529	KK	220	SUBBASIN 220 RUNOFF								
530	BA	.00103									
531	LS		98								
532	UD	.06									
533	KK	C230	ROUTE C220 TO 230								
534	RS	100	STOR	-1	0						
535	RC	.016	.016	.040	380	.0030	120				
536	RX	0	0	31.8	33.8	33.8	38.8	55	80		
537	RY	100.41	98.41	97.95	97.87	98.37	98.49	99.0	99.9		
538	KK	230	SUBBASIN 230 RUNOFF								
539	BA	.00083									
540	LS		98								
541	UD	.06									
542	KK	C230	COMBINE C220 AND 230								
543	HC	2									
544	KK	SD230	COMBINE SD220 AND C130 AND C230								
545	HC	3									
546	KK	SD90	ROUTE SD230 TO SD90								
547	RK	205	0.0010	0.012		CIRC	4				
548	KK	90	SUBBASIN 90 RUNOFF								
549	BA	.02922									
550	LS		77	24							
551	UD	.23									
552	KK	SD90	COMBINE SD230 AND 90								
553	HC	2									
554	KK	SD240	ROUTE SD90 TO SD240								
555	RK	125	0.0010	0.012		CIRC	4				
556	KK	140	SUBBASIN 140 RUNOFF								
557	BA	.00081									
558	LS		98								
559	UD	.06									
560	KK	240	SUBBASIN 240 RUNOFF								
561	BA	.00150									
562	LS		98								
563	UD	.06									

LINE	ID	1	2	3	4	5	6	7	8	9	10
602	KK	270	SUBBASIN 270 RUNOFF								
603	BA	.00095									
604	LS		98								
605	UD	.06									
606	KK	SD270	COMBINE SD260 AND 170 AND 270								
607	HC	3									
608	KK	SDBOX	ROUTE SD270 TO SDBOX								
609	RK	270	0.0010	0.012		CIRC	5				
610	KK	C1080	COMBINE C1080 AND SDBOX								
611	HC	2									
612	KK	C1110N	ROUTE C1080 TO C1110N								
613	RS	100	STOR	-1	0						
614	RC	.040	0.030	.040	900	.0092					
615	RX	0	0.1	20	40	80	100	120	120.1		
616	RY	105	100	99	93	93	99	100	105		
617	KK	1110N	SUBBASIN 1110N RUNOFF								
618	BA	.00396									
619	LS	0	69	18							
620	UD	0.06									
621	KK	C1110N	COMBINE C1110N AND C1080								
622	HC	2									
623	KK	C1110S	ROUTE C1110N TO C1110S								
624	RS	100	STOR	-1	0						
625	RC	.040	0.030	.040	1050	.0092					
626	RX	0	0.1	20	40	80	100	120	120.1		
627	RY	105	100	99	93	93	99	100	105		
628	KK	1110S	SUBBASIN 1110S RUNOFF								
629	BA	.01991									
630	LS	0	69	18							
631	UD	0.09									
632	KK	C1110S	COMBINE C1110N AND C1110S								
633	HC	2									
634	KK	C1120	ROUTE C1110S TO C1120								
635	RS	100	STOR	-1	0						
636	RC	.020	0.020	.020	200	.0080					
637	RX	0	0.1	0.2	0.3	24.3	24.4	24.5	24.6		
638	RY	110	110	110	100	100	110	110	110		
639	KK	1120	SUBBASIN 1120 RUNOFF								
640	BA	.01692									
641	LS	0	69	50							
642	UD	0.07									

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

643	KK	C1120	COMBINE 1120 AND C1110S					
644	HC	2						
645	KK	LAKE5	DETENTION BASIN AT LAKE 5					
646	RS	1	STOR	0				
647	SV	0	6.94	10.21	14	18.59	24.07	30.25
648	SE	73.50	76.09	77.09	78.09	79.09	80.09	81.09
649	SQ	0	0	49	225	535	960	1500
650	ZZ							

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*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1)
* SEPTEMBER 1990
* VERSION 4.0
*
* RUN DATE 06/28/1995 TIME 16:40:38
*
*****

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*****
*
* U.S. ARMY CORPS OF ENGINEERS
* HYDROLOGIC ENGINEERING CENTER
* 609 SECOND STREET
* DAVIS, CALIFORNIA 95616
* (916) 756-1104
*
*****

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84TH STREET AND CHOLLA ROAD
2-5-10-25-50-100 yr STORM
INTERIM CONDITION:
FINAL DESIGN ***** SCC BASIN*****
--ASSUME NO SPLIT IN CACTUS/84TH INTERSECTION
--100-YR NEW STORM SEWER IN CACTUS (INclude ADOT R/W FOR INTERIM)
--no bypass into 84th st south. all flows go to scc.
--CACTUS SD TO OUTFALL AT BOX-CULVERT
--NO INTERCEPTOR AT CORTEZ IN 84TH STREET
--No NEW PIMA CHANNEL
--FLOW SPLIT AT NORTH END OF PIMA DETENTION BASINS (1060A)
--NEW INTERIM DETENTION BASINS (2) WEST OF PIMA & NORTH OF SWEETWATER
--36" PIPE TO EAST PIMA.
--3 DETENTION BASINS AT PIMA-LAYOUT UPDATED FOR LANDSCAPING (5-17-95)
--FILE SCCSW7.DAT
*****

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18 10

OUTPUT CONTROL VARIABLES

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IPRNT      5  PRINT CONTROL
IPLOT      0  PLOT CONTROL
QSCAL      0.  HYDROGRAPH PLOT SCALE
JR  PREC   1.0

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IT

HYDROGRAPH TIME DATA

```

NMIN      2  MINUTES IN COMPUTATION INTERVAL
IDATE     1  0  STARTING DATE
ITIME     0000  STARTING TIME
NQ        300  NUMBER OF HYDROGRAPH ORDINATES
NDDATE    1  0  ENDING DATE
NDTIME    0958  ENDING TIME
ICENT     19  CENTURY MARK

```

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COMPUTATION INTERVAL   .03 HOURS
TOTAL TIME BASE       9.97 HOURS

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ENGLISH UNITS

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DRAINAGE AREA      SQUARE MILES
PRECIPITATION DEPTH  INCHES
LENGTH, ELEVATION  FEET
FLOW               CUBIC FEET PER SECOND
STORAGE VOLUME     ACRE-FEET
SURFACE AREA       ACRES
TEMPERATURE        DEGREES FAHRENHEIT

```

JP

MULTI-PLAN OPTION

```

NPLAN      1  NUMBER OF PLANS

```

JR

MULTI-RATIO OPTION

```

RATIOS OF PRECIPITATION
.36   .53   .62   .76   .88   1.00

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PEAK FLOW AND STAGE (END-OF-PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC COMPUTATIONS
 FLOWS IN CUBIC FEET PER SECOND, AREA IN SQUARE MILES
 TIME TO PEAK IN HOURS

OPERATION	STATION	AREA	PLAN	RATIOS APPLIED TO PRECIPITATION						
				RATIO 1	RATIO 2	RATIO 3	RATIO 4	RATIO 5	RATIO 6	
				.36	.53	.62	.76	.88	1.00	
HYDROGRAPH AT										
+	710	.01	1	FLOW	9.	15.	18.	24.	29.	34.
				TIME	3.10	3.10	3.10	3.10	3.10	3.10
ROUTED TO										
+	C720	.01	1	FLOW	9.	15.	19.	24.	29.	34.
				TIME	3.13	3.13	3.13	3.13	3.13	3.13
				*** PEAK STAGES IN FEET ***						
			1	STAGE	97.16	97.45	97.56	97.72	97.87	97.99
				TIME	3.13	3.13	3.13	3.13	3.13	3.13
HYDROGRAPH AT										
+	720	.07	1	FLOW	5.	21.	32.	53.	73.	95.
				TIME	3.37	3.30	3.30	3.30	3.27	3.27
2 COMBINED AT										
+	C720	.07	1	FLOW	10.	27.	40.	64.	86.	111.
				TIME	3.13	3.23	3.23	3.27	3.23	3.23
ROUTED TO										
+	C720	.07	1	FLOW	10.	27.	42.	65.	88.	113.
				TIME	3.27	3.33	3.27	3.33	3.30	3.27
				*** PEAK STAGES IN FEET ***						
			1	STAGE	99.84	99.99	100.07	100.15	100.24	100.32
				TIME	3.27	3.33	3.27	3.33	3.30	3.27
HYDROGRAPH AT										
+	725	.07	1	FLOW	38.	64.	80.	107.	132.	157.
				TIME	3.23	3.23	3.23	3.23	3.23	3.23
ROUTED TO										
+	ED725	.07	1	FLOW	25.	47.	61.	79.	92.	119.
				TIME	3.40	3.37	3.37	3.37	3.37	3.37
				*** PEAK STAGES IN FEET ***						
			1	STAGE	1472.52	1472.76	1472.89	1473.12	1473.37	1473.59
				TIME	3.40	3.37	3.37	3.37	3.37	3.37
HYDROGRAPH AT										
+	730	.01	1	FLOW	5.	8.	10.	14.	17.	21.
				TIME	3.07	3.07	3.07	3.07	3.07	3.07
2 COMBINED AT										
+	C730	.07	1	FLOW	26.	49.	62.	81.	95.	122.
				TIME	3.40	3.37	3.37	3.37	3.37	3.37
ROUTED TO										
+	ED730	.07	1	FLOW	17.	35.	49.	75.	90.	112.
				TIME	3.67	3.60	3.53	3.50	3.47	3.43

*** PEAK STAGES IN FEET ***

1	STAGE	1468.60	1468.88	1469.03	1469.15	1469.22	1469.32
	TIME	3.67	3.60	3.53	3.50	3.47	3.43

HYDROGRAPH AT

+	735	.05	1	FLOW	23.	40.	49.	66.	81.	96.
				TIME	3.33	3.33	3.33	3.33	3.33	3.33

3 COMBINED AT

+	C735	.20	1	FLOW	42.	91.	122.	188.	242.	303.
				TIME	3.40	3.40	3.37	3.40	3.37	3.37

ROUTED TO

+	ED735	.20	1	FLOW	26.	66.	94.	153.	204.	288.
				TIME	3.83	3.67	3.63	3.57	3.50	3.43

*** PEAK STAGES IN FEET ***

1	STAGE	1466.52	1467.05	1467.32	1467.71	1468.01	1468.15
	TIME	3.83	3.67	3.63	3.57	3.50	3.43

HYDROGRAPH AT

+	740	.00	1	FLOW	1.	1.	2.	2.	2.	3.
				TIME	3.10	3.10	3.10	3.10	3.10	3.10

HYDROGRAPH AT

+	742	.01	1	FLOW	1.	4.	6.	9.	13.	17.
				TIME	3.23	3.17	3.17	3.17	3.17	3.17

2 COMBINED AT

+	C742	.01	1	FLOW	1.	5.	7.	11.	15.	19.
				TIME	3.17	3.17	3.17	3.17	3.13	3.13

ROUTED TO

+	C744	.01	1	FLOW	1.	5.	7.	11.	15.	19.
				TIME	3.17	3.17	3.17	3.17	3.17	3.13

HYDROGRAPH AT

+	743	.00	1	FLOW	3.	6.	7.	10.	12.	14.
				TIME	3.10	3.10	3.10	3.10	3.10	3.10

ROUTED TO

+	C744	.00	1	FLOW	3.	6.	7.	10.	12.	14.
				TIME	3.13	3.17	3.17	3.17	3.17	3.17

*** PEAK STAGES IN FEET ***

1	STAGE	99.39	99.49	99.55	99.64	99.66	99.67
	TIME	3.13	3.17	3.17	3.17	3.17	3.17

HYDROGRAPH AT

+	744	.01	1	FLOW	9.	14.	16.	20.	24.	27.
				TIME	3.17	3.17	3.17	3.17	3.17	3.17

3 COMBINED AT

+	C744	.02	1	FLOW	14.	24.	31.	41.	50.	60.
				TIME	3.17	3.17	3.17	3.17	3.17	3.17

ROUTED TO

+	C745	.02	1	FLOW	14.	24.	30.	40.	49.	59.
				TIME	3.17	3.20	3.17	3.17	3.17	3.17

HYDROGRAPH AT
 + 745 .02 1 FLOW 2. 6. 10. 16. 22. 29.
 TIME 3.33 3.27 3.23 3.23 3.23 3.23

2 COMBINED AT
 + C745 .04 1 FLOW 14. 29. 39. 55. 70. 85.
 TIME 3.20 3.20 3.20 3.20 3.20 3.20

ROUTED TO
 + C735 .04 1 FLOW 14. 29. 38. 55. 70. 85.
 TIME 3.20 3.20 3.20 3.20 3.20 3.20

2 COMBINED AT
 + C735 .24 1 FLOW 27. 72. 103. 169. 227. 324.
 TIME 3.77 3.63 3.60 3.53 3.50 3.43

ROUTED TO
 + C760 .24 1 FLOW 27. 72. 103. 169. 227. 323.
 TIME 3.80 3.63 3.60 3.53 3.50 3.43

HYDROGRAPH AT
 + 760 .01 1 FLOW 15. 23. 27. 33. 39. 44.
 TIME 3.23 3.20 3.20 3.20 3.20 3.20

2 COMBINED AT
 + C760 .25 1 FLOW 32. 77. 110. 180. 241. 345.
 TIME 3.23 3.63 3.60 3.53 3.50 3.43

ROUTED TO
 + C790 .25 1 FLOW 32. 77. 110. 180. 240. 350.
 TIME 3.23 3.63 3.60 3.53 3.50 3.43

*** PEAK STAGES IN FEET ***
 1 STAGE 95.78 96.41 96.80 97.52 98.08 99.00
 TIME 3.23 3.63 3.60 3.53 3.50 3.43

HYDROGRAPH AT
 + 780 .02 1 FLOW 6. 13. 17. 25. 32. 39.
 TIME 3.17 3.17 3.17 3.17 3.17 3.17

ROUTED TO
 + C782 .02 1 FLOW 6. 13. 17. 24. 33. 40.
 TIME 3.27 3.23 3.23 3.27 3.23 3.23

*** PEAK STAGES IN FEET ***
 1 STAGE 98.58 98.81 98.89 99.03 99.15 99.23
 TIME 3.27 3.23 3.23 3.27 3.23 3.23

HYDROGRAPH AT
 + 782 .01 1 FLOW 1. 4. 6. 10. 13. 17.
 TIME 3.33 3.27 3.27 3.23 3.23 3.23

HYDROGRAPH AT
 + 784 .05 1 FLOW 27. 46. 58. 77. 95. 113.
 TIME 3.23 3.23 3.23 3.23 3.23 3.23

ROUTED TO
 + ED784 .05 1 FLOW 9. 15. 18. 24. 29. 35.
 TIME 3.57 3.60 3.60 3.60 3.60 3.60

*** PEAK STAGES IN FEET ***

1	STAGE	1389.88	1390.20	1390.38	1390.70	1390.98	1391.27
	TIME	3.57	3.60	3.60	3.60	3.60	3.60

3 COMBINED AT

+	C782	.08	1	FLOW	13.	26.	35.	50.	63.	77.
				TIME	3.33	3.27	3.30	3.27	3.27	3.23

ROUTED TO

+	C790	.08	1	FLOW	14.	27.	37.	50.	63.	77.
				TIME	3.47	3.47	3.40	3.37	3.37	3.40

*** PEAK STAGES IN FEET ***

1	STAGE	98.83	99.07	99.20	99.35	99.49	99.61
	TIME	3.47	3.47	3.40	3.37	3.37	3.40

HYDROGRAPH AT

+	790	.11	1	FLOW	9.	34.	53.	87.	121.	156.
				TIME	3.40	3.33	3.33	3.30	3.30	3.30

3 COMBINED AT

+	C790	.44	1	FLOW	49.	123.	177.	287.	390.	547.
				TIME	3.47	3.57	3.43	3.47	3.40	3.43

HYDROGRAPH AT

+	750	.00	1	FLOW	5.	8.	10.	12.	14.	16.
				TIME	3.10	3.10	3.10	3.10	3.10	3.10

ROUTED TO

+	C770	.00	1	FLOW	6.	9.	10.	12.	15.	16.
				TIME	3.20	3.17	3.17	3.20	3.20	3.20

*** PEAK STAGES IN FEET ***

1	STAGE	99.84	99.88	99.89	99.93	99.97	100.00
	TIME	3.20	3.17	3.17	3.20	3.20	3.20

HYDROGRAPH AT

+	770	.01	1	FLOW	8.	12.	15.	18.	21.	24.
				TIME	3.10	3.10	3.10	3.10	3.10	3.10

2 COMBINED AT

+	C770	.01	1	FLOW	12.	19.	22.	27.	31.	36.
				TIME	3.20	3.17	3.17	3.13	3.13	3.17

2 COMBINED AT

+	C770	.45	1	FLOW	53.	127.	183.	293.	398.	555.
				TIME	3.47	3.47	3.43	3.47	3.40	3.43

ROUTED TO

+	C800	.45	1	FLOW	53.	127.	183.	293.	399.	557.
				TIME	3.47	3.47	3.43	3.47	3.43	3.43

*** PEAK STAGES IN FEET ***

1	STAGE	101.03	101.66	102.03	102.60	103.03	103.59
	TIME	3.47	3.47	3.43	3.47	3.43	3.43

HYDROGRAPH AT

+	800	.02	1	FLOW	2.	6.	10.	16.	22.	29.
				TIME	3.30	3.23	3.23	3.23	3.23	3.20

2 COMBINED AT
+ C800 .46 1 FLOW 54. 130. 189. 301. 410. 571.
TIME 3.47 3.47 3.43 3.47 3.43 3.43

ROUTED TO
+ C810 .46 1 FLOW 55. 132. 189. 300. 412. 564.
TIME 3.30 3.50 3.47 3.50 3.47 3.47

*** PEAK STAGES IN FEET ***
1 STAGE 100.63 101.08 101.32 101.72 102.07 102.45
TIME 3.30 3.50 3.47 3.50 3.47 3.47

HYDROGRAPH AT
+ 810 .04 1 FLOW 23. 38. 48. 64. 79. 94.
TIME 3.27 3.27 3.27 3.27 3.27 3.27

2 COMBINED AT
+ C810 .51 1 FLOW 77. 155. 220. 342. 464. 622.
TIME 3.30 3.47 3.47 3.43 3.43 3.47

ROUTED TO
+ C820 .51 1 FLOW 77. 156. 222. 347. 468. 622.
TIME 3.37 3.47 3.43 3.47 3.43 3.50

*** PEAK STAGES IN FEET ***
1 STAGE 100.76 101.18 101.45 101.87 102.22 102.60
TIME 3.37 3.47 3.43 3.47 3.43 3.50

HYDROGRAPH AT
+ 820 .04 1 FLOW 21. 36. 45. 61. 76. 91.
TIME 3.20 3.20 3.20 3.20 3.20 3.20

2 COMBINED AT
+ C820 .54 1 FLOW 88. 176. 242. 370. 501. 652.
TIME 3.37 3.37 3.43 3.47 3.43 3.50

ROUTED TO
+ C830 .54 1 FLOW 88. 176. 242. 370. 500. 653.
TIME 3.37 3.30 3.43 3.47 3.43 3.50

*** PEAK STAGES IN FEET ***
1 STAGE 100.52 100.81 100.99 101.29 101.56 101.84
TIME 3.37 3.30 3.43 3.47 3.43 3.50

HYDROGRAPH AT
+ 910 .05 1 FLOW 41. 65. 78. 99. 118. 138.
TIME 3.23 3.23 3.23 3.23 3.23 3.23

ROUTED TO
+ C920 .05 1 FLOW 41. 64. 77. 98. 117. 137.
TIME 3.23 3.23 3.23 3.23 3.23 3.23

HYDROGRAPH AT
+ 920 .03 1 FLOW 15. 22. 27. 35. 43. 51.
TIME 3.27 3.30 3.30 3.30 3.30 3.30

2 COMBINED AT
+ C920 .08 1 FLOW 55. 86. 104. 133. 159. 186.
TIME 3.27 3.27 3.27 3.27 3.27 3.27

ROUTED TO

+	C930	.08	1	FLOW	56.	86.	103.	133.	159.	187.
				TIME	3.27	3.30	3.27	3.30	3.30	3.27

*** PEAK STAGES IN FEET ***

1	STAGE	99.69	99.86	99.93	100.04	100.13	100.22
	TIME	3.27	3.30	3.27	3.30	3.30	3.27

HYDROGRAPH AT

+	930	.06	1	FLOW	26.	46.	57.	77.	96.	115.
				TIME	3.30	3.30	3.30	3.30	3.30	3.30

2 COMBINED AT

+	C930	.14	1	FLOW	82.	132.	161.	211.	254.	300.
				TIME	3.27	3.30	3.30	3.30	3.30	3.27

DIVERSION TO

+	D930	.14	1	FLOW	51.	51.	51.	51.	51.	51.
				TIME	3.17	3.10	3.07	3.03	3.03	3.00

HYDROGRAPH AT

+	C930	.14	1	FLOW	31.	81.	110.	160.	203.	249.
				TIME	3.27	3.30	3.30	3.30	3.30	3.27

ROUTED TO

+	C830	.14	1	FLOW	31.	83.	114.	161.	203.	252.
				TIME	3.30	3.33	3.30	3.33	3.30	3.30

*** PEAK STAGES IN FEET ***

1	STAGE	99.66	99.97	100.09	100.27	100.39	100.53
	TIME	3.30	3.33	3.30	3.33	3.30	3.30

HYDROGRAPH AT

+	830	.00	1	FLOW	3.	4.	5.	6.	7.	8.
				TIME	3.10	3.10	3.10	3.10	3.10	3.10

3 COMBINED AT

+	C830	.68	1	FLOW	118.	256.	347.	509.	676.	861.
				TIME	3.37	3.30	3.33	3.37	3.37	3.40

DIVERSION TO

+	D830	.68	1	FLOW	0.	0.	0.	0.	109.	272.
				TIME	.03	.03	.03	.03	3.37	3.40

HYDROGRAPH AT

+	C830	.68	1	FLOW	118.	256.	347.	509.	567.	589.
				TIME	3.37	3.30	3.33	3.37	3.37	3.40

HYDROGRAPH AT

+	A30	.40	1	FLOW	50.	117.	163.	244.	321.	403.
				TIME	3.57	3.60	3.57	3.57	3.57	3.57

ROUTED TO

+	DA30	.40	1	FLOW	47.	105.	144.	210.	271.	311.
				TIME	3.70	3.73	3.73	3.77	3.77	3.80

*** PEAK STAGES IN FEET ***

1	STAGE	35.14	36.34	37.10	38.11	39.07	40.12
	TIME	3.70	3.73	3.73	3.77	3.77	3.80

DIVERSION TO
 + A32 .40 1 FLOW 46. 97. 130. 190. 244. 281.
 TIME 3.70 3.73 3.73 3.77 3.77 3.80

HYDROGRAPH AT
 + A31 .40 1 FLOW 1. 9. 14. 20. 26. 30.
 TIME 3.70 3.73 3.73 3.77 3.77 3.80

2 COMBINED AT
 + CA31 1.08 1 FLOW 118. 256. 350. 519. 580. 610.
 TIME 3.37 3.30 3.33 3.40 3.37 3.50

ROUTED TO
 + ED1010 1.08 1 FLOW 119. 257. 355. 519. 583. 611.
 TIME 3.37 3.40 3.37 3.40 3.40 3.53

*** PEAK STAGES IN FEET ***
 1 STAGE 98.14 99.32 99.76 100.17 100.31 100.36
 TIME 3.37 3.40 3.37 3.40 3.40 3.53

HYDROGRAPH AT
 + 1010 .01 1 FLOW 1. 6. 9. 15. 21. 27.
 TIME 3.20 3.13 3.13 3.13 3.13 3.13

2 COMBINED AT
 + C1010 1.10 1 FLOW 120. 259. 359. 524. 588. 616.
 TIME 3.37 3.40 3.37 3.40 3.40 3.53

ROUTED TO
 + ED1010 1.10 1 FLOW 74. 240. 345. 520. 585. 614.
 TIME 3.63 3.47 3.43 3.43 3.43 3.53

*** PEAK STAGES IN FEET ***
 1 STAGE 27.71 28.20 28.33 28.53 28.61 28.64
 TIME 3.63 3.47 3.43 3.43 3.43 3.53

HYDROGRAPH AT
 + 1060A .00 1 FLOW 0. 1. 2. 3. 4. 5.
 TIME 3.17 3.13 3.10 3.10 3.10 3.10

HYDROGRAPH AT
 + 10N .00 1 FLOW 2. 4. 5. 7. 8. 10.
 TIME 3.10 3.10 3.10 3.10 3.10 3.10

3 COMBINED AT
 + C1060A 1.10 1 FLOW 74. 241. 347. 522. 587. 616.
 TIME 3.63 3.47 3.40 3.43 3.43 3.53

ROUTED TO
 + CPIMAA 1.10 1 FLOW 72. 222. 315. 499. 591. 616.
 TIME 3.67 3.57 3.57 3.53 3.47 3.53

*** PEAK STAGES IN FEET ***
 1 STAGE 19.54 21.51 22.99 25.59 26.23 26.35
 TIME 3.67 3.57 3.57 3.53 3.47 3.53

DIVERSION TO
 + D1060A 1.10 1 FLOW 0. 0. 0. 65. 131. 147.
 TIME .03 .03 .03 3.53 3.47 3.53

HYDROGRAPH AT
 + C1060A 1.10 1 FLOW 72. 222. 315. 434. 460. 469.
 TIME 3.67 3.57 3.57 3.53 3.47 3.53

HYDROGRAPH AT
 + 1060B .00 1 FLOW 1. 2. 4. 6. 8. 11.
 TIME 3.17 3.13 3.10 3.10 3.10 3.10

HYDROGRAPH AT
 + 1060C .00 1 FLOW 1. 3. 4. 7. 9. 12.
 TIME 3.17 3.13 3.10 3.10 3.10 3.10

3 COMBINED AT
 + C1060C 1.11 1 FLOW 72. 223. 316. 436. 463. 473.
 TIME 3.67 3.53 3.57 3.53 3.47 3.43

ROUTED TO
 + CPIMAB 1.11 1 FLOW 36. 140. 234. 379. 429. 447.
 TIME 9.37 3.93 3.83 3.77 3.77 3.73

*** PEAK STAGES IN FEET ***
 1 STAGE 21.02 21.53 22.00 22.48 22.59 22.63
 TIME 9.47 3.93 3.83 3.77 3.77 3.73

HYDROGRAPH AT
 + 1060D .00 1 FLOW 1. 3. 4. 7. 9. 12.
 TIME 3.17 3.13 3.10 3.10 3.10 3.10

2 COMBINED AT
 + C1060D 1.11 1 FLOW 36. 140. 234. 379. 429. 448.
 TIME 9.37 3.93 3.83 3.77 3.77 3.73

ROUTED TO
 + CPIMAC 1.11 1 FLOW 29. 36. 51. 68. 78. 86.
 TIME 9.97 9.97 5.13 5.00 5.03 5.07

*** PEAK STAGES IN FEET ***
 1 STAGE 17.58 18.05 19.06 20.81 21.81 22.60
 TIME 9.97 9.97 5.13 5.00 5.03 5.07

HYDROGRAPH AT
 + A32 .00 1 FLOW 46. 97. 130. 190. 244. 281.
 TIME 3.70 3.73 3.73 3.77 3.77 3.80

DIVERSION TO
 + A36 .00 1 FLOW 45. 87. 114. 154. 192. 218.
 TIME 3.70 3.73 3.73 3.77 3.77 3.80

HYDROGRAPH AT
 + A32 .00 1 FLOW 1. 10. 16. 35. 53. 63.
 TIME 3.70 3.73 3.73 3.77 3.77 3.80

ROUTED TO
 + C1030 .00 1 FLOW 1. 10. 16. 35. 53. 63.
 TIME 3.80 3.80 3.80 3.80 3.77 3.80

*** PEAK STAGES IN FEET ***
 1 STAGE 95.14 95.88 96.18 96.76 97.16 97.35
 TIME 3.80 3.80 3.80 3.80 3.77 3.80

ROUTED TO
+ C1030 .00 1 FLOW TIME 1. 10. 16. 35. 53. 63.
3.80 3.80 3.80 3.80 3.77 3.83

HYDROGRAPH AT
+ 1030 .01 1 FLOW TIME 1. 4. 6. 10. 14. 18.
3.27 3.20 3.20 3.20 3.17 3.17

2 COMBINED AT
+ C1030 .01 1 FLOW TIME 1. 10. 17. 36. 54. 65.
3.80 3.80 3.80 3.80 3.77 3.80

ROUTED TO
+ C1040 .01 1 FLOW TIME 1. 10. 17. 36. 54. 64.
3.80 3.80 3.80 3.80 3.77 3.83

HYDROGRAPH AT
+ 1040 .02 1 FLOW TIME 9. 17. 22. 32. 40. 49.
3.17 3.17 3.17 3.17 3.17 3.17

ROUTED TO
+ ED1040 .02 1 FLOW TIME 2. 4. 5. 6. 8. 9.
3.50 3.57 3.57 3.57 3.57 3.57

*** PEAK STAGES IN FEET ***
1 STAGE 24.68 25.02 25.23 25.58 25.87 26.18
TIME 3.50 3.57 3.57 3.57 3.57 3.57

2 COMBINED AT
+ C1040 .03 1 FLOW TIME 3. 14. 21. 42. 61. 73.
3.77 3.80 3.80 3.80 3.77 3.80

ROUTED TO
+ C1050 .03 1 FLOW TIME 3. 14. 21. 42. 61. 73.
3.80 3.80 3.80 3.80 3.80 3.83

*** PEAK STAGES IN FEET ***
1 STAGE 95.46 96.07 96.33 96.89 97.28 97.49
TIME 3.80 3.80 3.80 3.80 3.80 3.83

HYDROGRAPH AT
+ 1050 .00 1 FLOW TIME 0. 2. 3. 5. 7. 9.
3.17 3.13 3.13 3.10 3.10 3.10

2 COMBINED AT
+ C1050 .03 1 FLOW TIME 3. 14. 22. 43. 62. 74.
3.80 3.77 3.80 3.80 3.77 3.83

HYDROGRAPH AT
+ D1060A .00 1 FLOW TIME 0. 0. 0. 65. 131. 147.
.03 .03 .03 3.53 3.47 3.53

HYDROGRAPH AT
+ 1020 .00 1 FLOW TIME 1. 1. 2. 3. 4. 5.
3.10 3.10 3.10 3.10 3.10 3.10

3 COMBINED AT
+ C1050 .04 1 FLOW TIME 4. 14. 22. 93. 167. 213.
3.33 3.77 3.80 3.53 3.57 3.60

ROUTED TO
+ C1070 .04 1 FLOW 4. 14. 22. 93. 170. 212.
TIME 3.50 3.90 3.87 3.57 3.53 3.63

*** PEAK STAGES IN FEET ***
1 STAGE 95.40 95.96 96.22 97.65 98.53 98.89
TIME 3.50 3.90 3.87 3.57 3.53 3.63

HYDROGRAPH AT
+ 1070 .03 1 FLOW 9. 19. 26. 38. 50. 62.
TIME 3.20 3.20 3.20 3.20 3.17 3.17

2 COMBINED AT
+ C1070 .06 1 FLOW 10. 26. 37. 103. 184. 224.
TIME 3.20 3.27 3.23 3.57 3.53 3.60

ROUTED TO
+ C1080 .06 1 FLOW 10. 29. 39. 107. 204. 239.
TIME 3.63 3.50 3.43 3.77 3.70 3.67

*** PEAK STAGES IN FEET ***
1 STAGE 95.47 95.98 96.17 97.06 97.83 98.05
TIME 3.63 3.50 3.43 3.77 3.70 3.67

HYDROGRAPH AT
+ 1080 .05 1 FLOW 18. 36. 48. 68. 87. 106.
TIME 3.20 3.20 3.20 3.20 3.20 3.20

2 COMBINED AT
+ C1080 .11 1 FLOW 20. 43. 62. 115. 217. 258.
TIME 3.20 3.50 3.43 3.77 3.70 3.67

HYDROGRAPH AT
+ 1090 .03 1 FLOW 12. 24. 33. 48. 62. 76.
TIME 3.17 3.20 3.20 3.17 3.17 3.17

ROUTED TO
+ C1100 .03 1 FLOW 12. 24. 33. 48. 62. 76.
TIME 3.17 3.20 3.20 3.17 3.17 3.17

*** PEAK STAGES IN FEET ***
1 STAGE 98.75 98.75 98.75 98.75 98.75 98.75
TIME 3.17 3.20 3.17 3.17 3.17 3.17

HYDROGRAPH AT
+ 1100 .07 1 FLOW 14. 29. 39. 56. 72. 90.
TIME 3.43 3.47 3.47 3.43 3.43 3.43

2 COMBINED AT
+ C1100 .10 1 FLOW 20. 41. 55. 79. 102. 126.
TIME 3.27 3.30 3.30 3.30 3.27 3.27

2 COMBINED AT
+ C1080 .22 1 FLOW 39. 79. 114. 172. 273. 338.
TIME 3.23 3.50 3.43 3.40 3.70 3.63

HYDROGRAPH AT
+ 40 .03 1 FLOW 12. 20. 25. 33. 40. 47.
TIME 3.47 3.47 3.47 3.47 3.47 3.47

ROUTED TO
+ SD110 .03 1 FLOW 12. 20. 25. 33. 40. 47.
TIME 3.47 3.47 3.47 3.47 3.47 3.47

HYDROGRAPH AT
+ 10 .01 1 FLOW 3. 7. 10. 13. 16. 19.
TIME 3.13 3.13 3.13 3.13 3.13 3.13

HYDROGRAPH AT
+ 20 .00 1 FLOW 0. 1. 1. 2. 3. 4.
TIME 3.37 3.30 3.30 3.27 3.27 3.27

2 COMBINED AT
+ C10 .01 1 FLOW 4. 8. 10. 14. 18. 22.
TIME 3.13 3.13 3.13 3.13 3.13 3.13

ROUTED TO
+ C15 .01 1 FLOW 5. 9. 11. 15. 19. 23.
TIME 3.43 3.37 3.33 3.33 3.30 3.30

*** PEAK STAGES IN FEET ***
1 STAGE 97.49 97.67 97.75 97.85 97.95 98.03
TIME 3.43 3.37 3.33 3.33 3.30 3.30

HYDROGRAPH AT
+ 15 .01 1 FLOW 4. 8. 11. 15. 18. 22.
TIME 3.13 3.10 3.10 3.10 3.10 3.10

2 COMBINED AT
+ C15 .01 1 FLOW 6. 11. 15. 20. 25. 30.
TIME 3.43 3.37 3.33 3.30 3.30 3.30

DIVERSION TO
+ D15 .01 1 FLOW 6. 11. 15. 19. 19. 19.
TIME 3.43 3.37 3.33 3.30 3.27 3.30

HYDROGRAPH AT
+ C15 .01 1 FLOW 0. 0. 0. 1. 6. 11.
TIME .03 .03 .03 3.30 3.30 3.30

ROUTED TO
+ C110 .01 1 FLOW 0. 0. 0. 0. 6. 13.
TIME .03 .03 .03 3.57 3.43 3.40

*** PEAK STAGES IN FEET ***
1 STAGE 101.27 101.27 101.27 101.40 101.60 101.70
TIME .00 .00 .00 3.57 3.43 3.40

HYDROGRAPH AT
+ 50 .01 1 FLOW 4. 7. 8. 11. 14. 17.
TIME 3.17 3.17 3.17 3.17 3.17 3.17

HYDROGRAPH AT
+ 110 .00 1 FLOW 2. 3. 3. 4. 5. 6.
TIME 3.10 3.10 3.10 3.10 3.10 3.10

2 COMBINED AT
+ C110 .01 1 FLOW 5. 9. 11. 14. 18. 21.
TIME 3.13 3.13 3.13 3.17 3.17 3.17

HYDROGRAPH AT
 + 210 .00 1 FLOW 4. 6. 7. 9. 10. 12.
 TIME 3.10 3.10 3.10 3.10 3.10 3.10

4 COMBINED AT
 + SD210 .05 1 FLOW 14. 24. 29. 38. 53. 68.
 TIME 3.40 3.43 3.43 3.43 3.43 3.40

ROUTED TO
 + SD220 .05 1 FLOW 14. 24. 29. 38. 52. 67.
 TIME 3.40 3.43 3.43 3.43 3.43 3.40

HYDROGRAPH AT
 + 70 .01 1 FLOW 5. 9. 12. 16. 20. 25.
 TIME 3.23 3.23 3.23 3.23 3.23 3.23

HYDROGRAPH AT
 + 120 .00 1 FLOW 1. 1. 1. 2. 2. 2.
 TIME 3.07 3.07 3.07 3.07 3.07 3.07

2 COMBINED AT
 + C120 .01 1 FLOW 6. 10. 13. 17. 21. 25.
 TIME 3.20 3.23 3.23 3.23 3.23 3.23

2 COMBINED AT
 + SD220 .07 1 FLOW 19. 32. 39. 52. 64. 83.
 TIME 3.20 3.23 3.23 3.23 3.23 3.40

ROUTED TO
 + SD230 .07 1 FLOW 19. 32. 39. 52. 64. 83.
 TIME 3.23 3.23 3.27 3.27 3.27 3.40

HYDROGRAPH AT
 + 80 .00 1 FLOW 1. 2. 3. 4. 4. 5.
 TIME 3.13 3.13 3.13 3.13 3.13 3.13

HYDROGRAPH AT
 + 130 .00 1 FLOW 1. 1. 1. 1. 2. 2.
 TIME 3.07 3.07 3.07 3.07 3.07 3.07

2 COMBINED AT
 + C130 .00 1 FLOW 2. 3. 3. 5. 6. 7.
 TIME 3.10 3.10 3.13 3.13 3.13 3.13

HYDROGRAPH AT
 + 220 .00 1 FLOW 2. 3. 3. 4. 5. 6.
 TIME 3.07 3.07 3.07 3.07 3.07 3.07

ROUTED TO
 + C230 .00 1 FLOW 2. 3. 3. 4. 5. 6.
 TIME 3.10 3.10 3.10 3.10 3.10 3.10

*** PEAK STAGES IN FEET ***
 1 STAGE 97.88 97.89 97.90 97.90 97.91 97.91
 TIME 3.10 3.10 3.10 3.10 3.10 3.10

HYDROGRAPH AT
 + 230 .00 1 FLOW 1. 2. 3. 3. 4. 4.
 TIME 3.07 3.07 3.07 3.07 3.07 3.07

HYDROGRAPH AT
 + 160 .00 1 FLOW TIME 1. 2. 2. 2. 3. 3.
 3.07 3.07 3.07 3.07 3.07 3.07

2 COMBINED AT
 + C160 .01 1 FLOW TIME 4. 7. 9. 12. 15. 19.
 3.13 3.13 3.13 3.13 3.13 3.13

HYDROGRAPH AT
 + 260 .00 1 FLOW TIME 2. 3. 4. 5. 5. 6.
 3.07 3.07 3.07 3.07 3.07 3.07

3 COMBINED AT
 + SD260 .11 1 FLOW TIME 40. 66. 82. 110. 135. 162.
 3.17 3.17 3.20 3.20 3.20 3.20

ROUTED TO
 + SD270 .11 1 FLOW TIME 40. 66. 82. 110. 135. 161.
 3.17 3.20 3.20 3.20 3.20 3.20

HYDROGRAPH AT
 + 170 .00 1 FLOW TIME 0. 1. 1. 1. 1. 2.
 3.10 3.10 3.10 3.10 3.10 3.10

HYDROGRAPH AT
 + 270 .00 1 FLOW TIME 2. 3. 3. 4. 4. 5.
 3.07 3.07 3.07 3.07 3.07 3.07

3 COMBINED AT
 + SD270 .12 1 FLOW TIME 41. 68. 84. 112. 138. 165.
 3.17 3.17 3.20 3.20 3.20 3.20

ROUTED TO
 + SDBOX .12 1 FLOW TIME 41. 68. 84. 112. 137. 164.
 3.17 3.20 3.20 3.20 3.20 3.20

2 COMBINED AT
 + C1080 .33 1 FLOW TIME 80. 145. 187. 265. 351. 436.
 3.20 3.20 3.20 3.40 3.37 3.37

ROUTED TO
 + C1110N .33 1 FLOW TIME 80. 150. 191. 260. 346. 438.
 3.27 3.27 3.23 3.23 3.40 3.40

*** PEAK STAGES IN FEET ***
 1 STAGE 93.56 93.82 93.95 94.17 94.38 94.58
 TIME 3.27 3.27 3.23 3.23 3.40 3.40

HYDROGRAPH AT
 + 1110N .00 1 FLOW TIME 1. 2. 3. 5. 7. 9.
 3.07 3.10 3.10 3.10 3.10 3.10

2 COMBINED AT
 + C1110N .34 1 FLOW TIME 81. 151. 193. 263. 347. 440.
 3.27 3.27 3.23 3.23 3.40 3.40

ROUTED TO
 + C1110S .34 1 FLOW TIME 81. 156. 198. 271. 349. 440.
 3.37 3.27 3.23 3.30 3.43 3.43

*** PEAK STAGES IN FEET ***

1	STAGE	93.57	93.84	93.97	94.20	94.39	94.58
	TIME	3.37	3.27	3.23	3.30	3.43	3.43

HYDROGRAPH AT

+	1110S	.02	1	FLOW	6.	11.	15.	22.	30.	39.
				TIME	3.10	3.13	3.13	3.13	3.13	3.13

2 COMBINED AT

+	C1110S	.36	1	FLOW	83.	162.	208.	281.	364.	450.
				TIME	3.37	3.27	3.23	3.30	3.27	3.43

ROUTED TO

+	C1120	.36	1	FLOW	83.	174.	215.	285.	366.	453.
				TIME	3.37	3.27	3.23	3.30	3.27	3.43

*** PEAK STAGES IN FEET ***

1	STAGE	100.67	101.09	101.23	101.47	101.73	101.98
	TIME	3.37	3.27	3.23	3.30	3.27	3.43

HYDROGRAPH AT

+	1120	.02	1	FLOW	16.	24.	30.	39.	48.	57.
				TIME	3.10	3.10	3.10	3.10	3.10	3.10

2 COMBINED AT

+	C1120	.37	1	FLOW	86.	183.	229.	297.	383.	463.
				TIME	3.37	3.27	3.23	3.30	3.27	3.43

ROUTED TO

+	LAKE5	.37	1	FLOW	2.	36.	70.	160.	265.	355.
				TIME	6.40	4.33	4.07	3.93	3.90	3.80

*** PEAK STAGES IN FEET ***

1	STAGE	76.14	76.83	77.21	77.72	78.22	78.51
	TIME	6.40	4.33	4.07	3.93	3.90	3.80



HYDRAULIC GRADIENT WORKSHEET

SMF Engineering Corporation

Client : City of Scottsdale
 Project : 84th Street and Cholla Road
 Comments : New Storm Drain in Cactus Road
 Final Design
 Main Line (50 yr storm), Outfall at Box-culvert (100 yr storm)

By: RM/LR
 Checked: CDS
 10/27/95 09:57 AM

Station	Structure	Pipe Length [ft]	Diam [ft]	Design Q [cfs]	Velocity Head		Energy Losses										Change Hydr Grad Hv2+Ht-Hv1	Hydr Grad Elevation Up Stream	Hydr Grad Elevation Dn Stream			
					Up Strm Hv1	Dn Strm Hv2	Pipe Frict	Angle [Degr]	Bend/ Curve	MH	Contr/ Exp	Angle [Degr]	D3 Q3	Angle [Degr]	D4 Q4	Junction				Total Ht		
29+75	Catch Basin					0.63					0.31							0.31	0.94	G=1399.99	1398.83	1397.89
	Pipe	38.0	2.00	20.00	0.63	0.63	0.29						2.00		2.00		0.29	0.29		1397.89	1397.59	
29+93	Manhole				0.63	0.27				0.03	0.08	45.00	20.00	45.00	20.00	-0.07	0.04	-0.32		1397.59	1397.91	
	Pipe	203.0	3.50	40.00	0.27	0.27	0.32	90.00	0.05				2.50		1.50		0.37	0.37		1397.91	1397.55	
27+90	PrefabCross				0.27	0.35						90.00	4.40	90.00	1.60	0.17	0.17	0.26		1397.55	1397.29	
	Pipe	255.0	3.50	46.00	0.35	0.35	0.53						2.50				0.53	0.53		1397.29	1396.76	
25+35	Manhole				0.35	0.35				0.02	0.00	90.00	14.00			0.19	0.20	0.20		1396.76	1396.55	
	Pipe	255.0	4.00	60.00	0.35	0.35	0.44						1.50		2.00		0.44	0.44		1396.55	1396.11	
22+80	PrefabCross				0.35	0.43						90.00	2.70	90.00	3.30	0.15	0.15	0.22		1396.11	1395.89	
	Pipe	188.0	4.00	66.00	0.43	0.43	0.39	30.70	0.03				2.50				0.42	0.42		1395.89	1395.47	
20+94	Manhole				0.35	0.31				0.02	0.01	90.00	21.50			0.08	0.11	0.07		1395.47	1395.40	
	Pipe	34.0	5.00	87.50	0.31	0.31	0.04						2.50				0.04	0.04		1395.40	1395.36	
20+60	PrefabTee				0.43	0.48						90.00	21.50			0.34	0.34	0.39		1395.36	1394.97	
	Pipe	110.0	5.00	109.00	0.48	0.48	0.19						1.50		1.50		0.19	0.19		1394.97	1394.78	
19+50	Prefab Cross				0.48	0.50						90.00	1.00	90.00	2.00	0.05	0.05	0.08		1394.78	1394.70	
	Pipe	350.0	5.00	112.00	0.50	0.50	0.64						1.50		1.50		0.64	0.64		1394.70	1394.06	
16+00	Manhole				0.50	0.54				0.03		90.00	2.50	90.00	1.60	0.07	0.10	0.14		1394.06	1393.92	
	Pipe	337.0	5.00	116.00	0.54	0.54	0.66						2.00		1.50		0.66	0.66		1393.92	1393.26	
12+63	Prefab Cross				0.54	0.67						90.00	10.00	90.00	3.00	0.26	0.26	0.39		1393.26	1392.87	
	Pipe	178.0	5.00	129.00	0.67	0.67	0.43						1.50		2.50		0.43	0.43		1392.87	1392.44	
10+85	Junction Structure				0.67	0.41					0.03	90.00	19.50	90.00	16.50	0.00	0.04	-0.22		1392.44	1392.66	
	8'x4' Box	276.0	6.10	165.00	0.41	0.41	0.38	36.35	0.05								0.43	0.43		1392.66	1392.23	
8+09	Headwall Outlet				0.41						0.41						0.41			1392.23	1392.23	

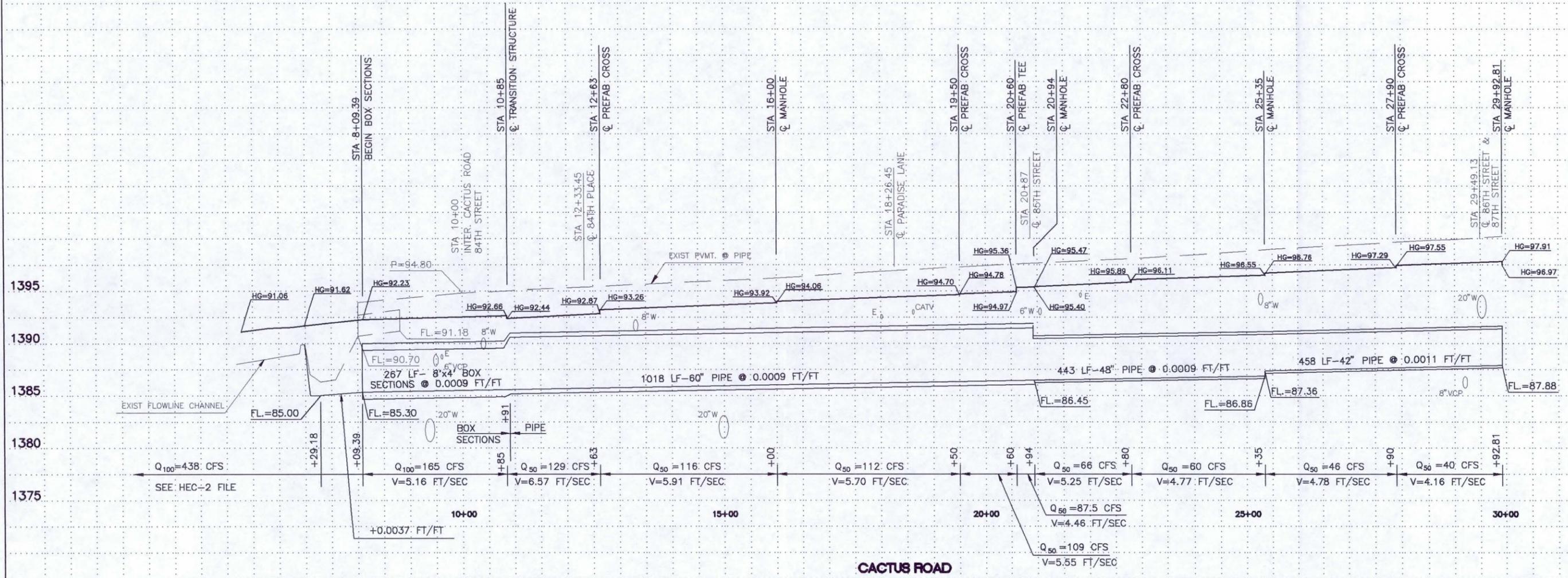
HYDRAULIC GRADIENT WORKSHEET

SMF Engineering Corporation

Client : City of Scottsdale
 Project : 84th Street and Cholla Road
 Comments : New Storm Drain in Cactus Road
 Final Design
 Main Line (100 yr storm), Outfall at Box-culvert (100 yr storm)

By: RM/LR
 Checked: CDS
 10/27/95 09:57 AM

Station	Structure	Pipe Length [ft]	Pipe Diam [ft]	Design Q [cfs]	Velocity Head		Energy Losses										Change Hydr Grad Hv2+Ht-Hv1	Hydr Grad Elevation Up Stream	Hydr Grad Elevation Dn Stream	
					Up Strm Hv1	Dn Strm Hv2	Pipe Frict	Angle [Degr]	Bend/ Curve	MH	Contr/ Exp	Angle [Degr]	D3 Q3	Angle [Degr]	D4 Q4	Junction				Total Ht
29+75	Catch Basin				0.00	0.87					0.43						0.43	1.30	G=1399.99 1400.88	1399.57
	Pipe	38.0	2.00	23.50	0.87	0.87	0.41						2.00		2.00		0.41	0.41	1399.57	1399.17
29+93	Manhole				0.87	0.37				0.04	0.10	45.00	23.50	45.00	23.50	-0.09	0.06	-0.44	1399.17	1399.61
	Pipe	203.0	3.50	47.00	0.37	0.37	0.44	90.00	0.07				2.50		1.50		0.51	0.51	1399.61	1399.10
27+90	PrefabCross				0.37	0.49						90.00	5.10	90.00	1.90	0.24	0.24	0.36	1399.10	1398.75
	Pipe	255.0	3.50	54.00	0.49	0.49	0.73						2.50				0.73	0.73	1398.75	1398.02
25+35	Manhole				0.49	0.51				0.02	0.00	90.00	18.00			0.31	0.33	0.35	1398.02	1397.66
	Pipe	255.0	4.00	72.00	0.51	0.51	0.64						1.50		2.00		0.64	0.64	1397.66	1397.03
22+80	PrefabCross				0.51	0.61						90.00	3.10	90.00	3.90	0.21	0.21	0.31	1397.03	1396.72
	Pipe	188.0	4.00	79.00	0.61	0.61	0.57	30.70					2.50				0.57	0.57	1396.72	1396.15
20+94	Manhole				0.51	0.45				0.03	0.01	90.00	26.50			0.14	0.17	0.11	1396.15	1396.04
	Pipe	34.0	5.00	105.50	0.45	0.45	0.06						2.50				0.06	0.06	1396.04	1395.98
20+60	PrefabTee				0.61	0.69				0.00		90.00	26.50			0.49	0.49	0.56	1395.98	1395.42
	Pipe	110.0	5.00	131.00	0.69	0.69	0.28						1.50		1.50		0.28	0.28	1395.42	1395.14
19+50	Prefab Cross				0.69	0.72						90.00	1.00	90.00	2.00	0.06	0.06	0.10	1395.14	1395.05
	Pipe	350.0	5.00	134.00	0.72	0.72	0.92						1.50		1.50		0.92	0.92	1395.05	1394.12
16+00	Manhole				0.72	0.78				0.04		90.00	3.00	90.00	2.00	0.11	0.15	0.20	1394.12	1393.92
	Pipe	337.0	5.00	139.00	0.78	0.78	0.95						2.00		1.50		0.95	0.95	1393.92	1392.97
12+63	Prefab Cross				0.78	0.97						90.00	12.30	90.00	3.70	0.38	0.38	0.57	1392.97	1392.40
	Pipe	178.0	5.00	155.00	0.97	0.97	0.63						1.50		2.50		0.63	0.63	1392.40	1391.77
10+85	Junction Structure				0.97	0.41		0.00	0.00		0.12	90.00	5.40	90.00	4.60	-0.45	-0.33	-0.89	1391.77	1392.66
	8'x4' Box	276.0	6.10	165.00	0.41	0.41	0.38	36.35	0.05								0.43	0.43	1392.66	1392.23
8+09	Headwall Outlet				0.41	0.00					0.41						0.41	0.00	1392.23	1392.23



**CACTUS STORM DRAIN
 50/100 YEAR - HYDRAULIC PROFILE**

DATE	REVISION		
ENGINEER			
			
		MUNICIPAL S DEPARTM CAPITAL PI MANAGER 3939 CIVIC CENT SCOTTSDALE, ARIZ	
PROJECT TITLE			
CACTUS ROAD STORM DRAIN			
SCALE	DESIGNED BY	CHECKED BY	BID NO.
HORIZ. 1"=100'	CDS	CDS	96-
VERT. 1"=5'	DRAWN BY	AS-BUILT	PROJECT NO.
	MC		F2708



Licensed to: SMF Engineering Corporation, Phoenix, AZ

Project : Cactus Road Left 50-Yr Return Frequency

Sta 29+75

INPUT

Intens.= 0.00 C1=0.00 A1= 0.00 Qadd = 20.0 Slope1=99.9999 Gutter= 1.42 Area = 0.00
 CB ID = 1 C2=0.00 A2= 0.00 Qrunoff= 20.0 Slope2= 0.0587 a = 2.00 Perim = 0.00
 Curb Opening C3=0.00 A3= 0.00 Grade = 0.0055 Slope3= 0.0160 W = 1.42 Length=34.00

OUTPUT

Flowby= 0.0 Qtotal= 20.0 Qint= 19.8 Flowby dn= 0.2 Depth=0.50 Spread= 27.15 Veloc= 3.37

INPUT

End of this reach of Catch Basins
 Flowby dn flows to Catch Basin 4

OUTPUT

Flowby dn= 0.2

Sta 29+34

INPUT

Intens.= 0.00 C1=0.00 A1= 0.00 Qadd = 20.0 Slope1=99.9999 Gutter= 1.42 Area = 0.00
 CB ID = 2 C2=0.00 A2= 0.00 Qrunoff= 20.0 Slope2= 0.0587 a = 2.00 Perim = 0.00
 Curb Opening C3=0.00 A3= 0.00 Grade = 0.0054 Slope3= 0.0060 W = 1.42 Length=34.00

OUTPUT

Flowby= 0.0 Qtotal= 20.0 Qint= 17.2 Flowby dn= 2.8 Depth=0.38 Spread= 51.53 Veloc= 2.49

Sta 27+90

INPUT

Intens.= 0.00 C1=0.00 A1= 0.00 Qadd = 2.0 Slope1=99.9999 Gutter= 1.42 Area = 0.00
 CB ID = 4 C2=0.00 A2= 0.00 Qrunoff= 2.0 Slope2= 0.0587 a = 3.25 Perim = 0.00
 Curb Opening C3=0.00 A3= 0.00 Grade = 0.0034 Slope3= 0.0173 W = 2.50 Length= 9.88

OUTPUT

Flowby= 3.0 Qtotal= 5.0 Qint= 5.0 Flowby dn= 0.1 Depth=0.35 Spread= 16.54 Veloc= 2.08

Sta 25+35

INPUT

Intens.= 0.00 C1=0.00 A1= 0.00 Qadd = 2.0 Slope1=99.9999 Gutter= 1.42 Area = 0.00
 CB ID = 6 C2=0.00 A2= 0.00 Qrunoff= 2.0 Slope2= 0.0587 a = 3.25 Perim = 0.00
 Curb Opening C3=0.00 A3= 0.00 Grade = 0.0033 Slope3= 0.0217 W = 2.50 Length= 9.88

OUTPUT

Flowby= 0.1 Qtotal= 2.1 Qint= 2.1 Flowby dn= 0.0 Depth=0.27 Spread= 10.02 Veloc= 1.82

Sta 22+80

INPUT

Intens.= 0.00 C1=0.00 A1= 0.00 Qadd = 6.0 Slope1=99.9999 Gutter= 1.42 Area = 0.00
 CB ID = 7 C2=0.00 A2= 0.00 Qrunoff= 6.0 Slope2= 0.0587 a = 2.00 Perim = 0.00
 Curb Opening C3=0.00 A3= 0.00 Grade = 0.0080 Slope3= 0.0200 W = 1.42 Length=13.00

OUTPUT

Flowby= 0.0 Qtotal= 6.0 Qint= 5.4 Flowby dn= 0.6 Depth=0.33 Spread= 13.65 Veloc= 3.15

INPUT

End of this reach of Catch Basins
 Flowby dn flows to Catch Basin 10

OUTPUT

Flowby dn= 0.6

Licensed to: SMF Engineering Corporation, Phoenix, AZ

Project : Cactus Road Left 50-Yr Return Frequency

Sta 20+95 INPUT
 Intens.= 0.00 C1=0.00 A1= 0.00 Qadd = 21.5 Slope1=99.9999 Gutter= 1.42 Area = 0.00
 CB ID = 8 C2=0.00 A2= 0.00 Qrunoff= 21.5 Slope2= 0.0587 a = 2.00 Perim = 0.00
 Curb Opening C3=0.00 A3= 0.00 Grade = 0.0072 Slope3= 0.0100 W = 1.42 Length=37.00

.....
 OUTPUT
 Flowby= 0.0 Qtotal= 21.5 Qint= 20.1 Flowby dn= 1.4 Depth=0.43 Spread= 35.98 Veloc= 3.30

INPUT
 End of this reach of Catch Basins
 Flowby dn flows to Catch Basin 10

.....
 OUTPUT
 Flowby dn= 1.4

Sta 20+60 INPUT
 Intens.= 0.00 C1=0.00 A1= 0.00 Qadd = 21.5 Slope1=99.9999 Gutter= 1.42 Area = 0.00
 CB ID = 9 C2=0.00 A2= 0.00 Qrunoff= 21.5 Slope2= 0.0587 a = 2.00 Perim = 0.00
 Curb Opening C3=0.00 A3= 0.00 Grade = 0.0072 Slope3= 0.0100 W = 1.42 Length=37.00

.....
 OUTPUT
 Flowby= 0.0 Qtotal= 21.5 Qint= 20.1 Flowby dn= 1.4 Depth=0.43 Spread= 35.98 Veloc= 3.30

Sta 19+50 INPUT
 Intens.= 0.00 C1=0.00 A1= 0.00 Qadd = 4.0 Slope1=99.9999 Gutter= 1.42 Area = 0.00
 CB ID = 10 C2=0.00 A2= 0.00 Qrunoff= 4.0 Slope2= 0.0587 a = 2.00 Perim = 0.00
 Curb Opening C3=0.00 A3= 0.00 Grade = 0.0037 Slope3= 0.0159 W = 1.42 Length=13.00

.....
 OUTPUT
 Flowby= 3.5 Qtotal= 7.5 Qint= 6.6 Flowby dn= 0.9 Depth=0.38 Spread= 20.14 Veloc= 2.30

Sta 16+00 INPUT
 Intens.= 0.00 C1=0.00 A1= 0.00 Qadd = 9.0 Slope1=99.9999 Gutter= 1.42 Area = 0.00
 CB ID = 11 C2=0.00 A2= 0.00 Qrunoff= 9.0 Slope2= 0.0587 a = 2.00 Perim = 0.00
 Curb Opening C3=0.00 A3= 0.00 Grade = 0.0021 Slope3= 0.0165 W = 1.42 Length=13.00

.....
 OUTPUT
 Flowby= 0.9 Qtotal= 9.9 Qint= 8.5 Flowby dn= 1.4 Depth=0.46 Spread= 24.43 Veloc= 2.00

Sta 12+63 INPUT
 Intens.= 0.00 C1=0.00 A1= 0.00 Qadd = 15.0 Slope1=99.9999 Gutter= 1.42 Area = 0.00
 CB ID = 12 C2=0.00 A2= 0.00 Qrunoff= 15.0 Slope2= 0.0587 a = 2.00 Perim = 0.00
 Curb Opening C3=0.00 A3= 0.00 Grade = 0.0030 Slope3= 0.0160 W = 1.42 Length=20.00

.....
 OUTPUT
 Flowby= 1.4 Qtotal= 16.4 Qint= 14.4 Flowby dn= 2.0 Depth=0.51 Spread= 28.27 Veloc= 2.55

Sta 10+85 INPUT
 Intens.= 0.00 C1=0.00 A1= 0.00 Qadd = 4.7 Slope1=99.9999 Gutter= 1.42 Area = 0.00
 CB ID = 13 C2=0.00 A2= 0.00 Qrunoff= 4.7 Slope2= 0.0587 a = 2.00 Perim = 0.00
 Curb Opening C3=0.00 A3= 0.00 Grade = 0.0010 Slope3= 0.0140 W = 1.42 Length=13.00

.....
 OUTPUT
 Flowby= 2.0 Qtotal= 6.7 Qint= 6.6 Flowby dn= 0.1 Depth=0.44 Spread= 27.04 Veloc= 1.30

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Project : Cactus Road Left 50-Yr Return Frequency

INPUT

End of this reach of Catch Basins
Flowby dn flows to Catch Basin

OUTPUT

Flowby dn= 0.1

Sta 25+35

INPUT

Intens.= 0.00 C1=0.00 A1= 0.00 Qadd = 20.0 Slope1= 0.0100 Gutter= 2.00 Area =11.00
CB ID = 3 C2=0.00 A2= 0.00 Qrunoff= 20.0 Slope2= 0.0100 a = 0.00 Perim =19.40
Grt P-1-7/8 C3=0.00 A3= 0.00 Grade = 0.0000 Slope3= 0.0100 W = 0.00 Length=10.00

OUTPUT

Flowby= 0.0 Qtotal= 20.0 Qint= 20.0 Flowby dn= 0.0 Depth=0.78 Spread= 77.88 Veloc= 0.00

CRITERIA

Runoff computed by Rational Method Manning`s n Gutter=0.012 Manning`s n Pavement=0.016
Clogging Factors in Sag Location:
----- Curb Opening= 1.25 Grate= 2.00 Slotted Drain= 1.25 Comb-Curb= 1.25 Comb-Grate= 2.00
Clogging Factors on Continuous Grade:
----- Curb Opening= 1.25 Grate= 2.00 Slotted Drain= 1.25 Comb-Curb= 1.25 Comb-Grate= 2.00

Prepared by: Date:10/27/95 Time:13:21:44 Checked by: Date:
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Project : Cactus Road Right 50-Yr Return Frequency

Sta 27+90

INPUT

Intens.= 0.00 C1=0.00 A1= 0.00 Qadd = 5.0 Slope1=99.9999 Gutter= 1.42 Area = 0.00
 CB ID = 1 C2=0.00 A2= 0.00 Qrunoff= 5.0 Slope2= 0.0587 a = 3.25 Perim = 0.00
 Curb Opening C3=0.00 A3= 0.00 Grade = 0.0034 Slope3= 0.0173 W = 2.50 Length= 9.88

OUTPUT

Flowby= 0.0 Qtotal= 5.0 Qint= 5.0 Flowby dn= 0.0 Depth=0.35 Spread= 16.54 Veloc= 2.07

Sta 22+80

INPUT

Intens.= 0.00 C1=0.00 A1= 0.00 Qadd = 9.0 Slope1=99.9999 Gutter= 1.42 Area = 0.00
 CB ID = 2 C2=0.00 A2= 0.00 Qrunoff= 9.0 Slope2= 0.0587 a = 3.25 Perim = 0.00
 Curb Opening C3=0.00 A3= 0.00 Grade = 0.0037 Slope3= 0.0159 W = 2.50 Length= 9.88

OUTPUT

Flowby= 0.0 Qtotal= 9.0 Qint= 7.4 Flowby dn= 1.6 Depth=0.41 Spread= 21.65 Veloc= 2.40

Sta 19+50

INPUT

Intens.= 0.00 C1=0.00 A1= 0.00 Qadd = 7.0 Slope1=99.9999 Gutter= 1.42 Area = 0.00
 CB ID = 3 C2=0.00 A2= 0.00 Qrunoff= 7.0 Slope2= 0.0587 a = 3.25 Perim = 0.00
 Curb Opening C3=0.00 A3= 0.00 Grade = 0.0021 Slope3= 0.0165 W = 2.50 Length= 9.88

OUTPUT

Flowby= 1.6 Qtotal= 8.6 Qint= 7.7 Flowby dn= 0.9 Depth=0.44 Spread= 23.10 Veloc= 1.94

Sta 16+00

INPUT

Intens.= 0.00 C1=0.00 A1= 0.00 Qadd = 6.0 Slope1=99.9999 Gutter= 1.42 Area = 0.00
 CB ID = 4 C2=0.00 A2= 0.00 Qrunoff= 6.0 Slope2= 0.0587 a = 3.25 Perim = 0.00
 Curb Opening C3=0.00 A3= 0.00 Grade = 0.0030 Slope3= 0.0160 W = 2.50 Length= 9.88

OUTPUT

Flowby= 0.9 Qtotal= 6.9 Qint= 6.4 Flowby dn= 0.5 Depth=0.38 Spread= 20.21 Veloc= 2.08

Sta 12+63

INPUT

Intens.= 0.00 C1=0.00 A1= 0.00 Qadd = 5.0 Slope1=99.9999 Gutter= 1.42 Area = 0.00
 CB ID = 5 C2=0.00 A2= 0.00 Qrunoff= 5.0 Slope2= 0.0587 a = 3.25 Perim = 0.00
 Curb Opening C3=0.00 A3= 0.00 Grade = 0.0030 Slope3= 0.0160 W = 2.50 Length= 9.88

OUTPUT

Flowby= 0.5 Qtotal= 5.5 Qint= 5.4 Flowby dn= 0.1 Depth=0.36 Spread= 18.52 Veloc= 1.97

Sta 10+85

INPUT

Intens.= 0.00 C1=0.00 A1= 0.00 Qadd = 29.3 Slope1=99.9999 Gutter= 1.42 Area = 0.00
 CB ID = 6 C2=0.00 A2= 0.00 Qrunoff= 29.3 Slope2= 0.0587 a = 3.25 Perim = 0.00
 Curb Opening C3=0.00 A3= 0.00 Grade = 0.0010 Slope3= 0.0140 W = 2.50 Length=30.50

OUTPUT

Flowby= 0.1 Qtotal= 29.4 Qint= 29.4 Flowby dn= 0.0 Depth=0.73 Spread= 47.47 Veloc= 1.86

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Project : Cactus Road Right 50-Yr Return Frequency

CRITERIA

Runoff computed by Rational Method Manning`s n Gutter=0.012 Manning`s n Pavement=0.016

Clogging Factors in Sag Location:

----- Curb Opening= 1.25 Grate= 2.00 Slotted Drain= 1.25 Comb-Curb= 1.25 Comb-Grate= 2.00

Clogging Factors on Continuous Grade:

----- Curb Opening= 1.25 Grate= 2.00 Slotted Drain= 1.25 Comb-Curb= 1.25 Comb-Grate= 2.00

Prepared by: Date:10/27/95 Time:13:21:01 Checked by: Date:
Pavement Drainage Program (C), 1991 Copyright by SMF Engineering Corporation, Phoenix, AZ

PAVEMENT DRAINAGE PROGRAM

SMF Pavement Drainage Program - HEC 12

Version 2.11

Introduction

This program "Pavement Drainage" was developed by SMF Engineering Corporation. With this program, it is possible to calculate interception and bypass of a series of catch basins. The methodology and equations as published in the Federal Highway Administration's Hydraulic Engineering Circular No. 12 (HEC-12) is the basis of this program for the calculation of catch basin interception and flowby rates. The spread and depth calculations use the modified Manning Equations for composite channel sections. If your agency does not use the HEC-12 methodology for catch basins, you can still use the program for spread and depth.

This program is quite simple to use and we hope that the manual we are providing is sufficient to get you a quick start. This manual should be used in conjunction with the FHWA HEC-12, "Drainage of Highway Pavements (order number PB84 215003). You can order a copy of the FHWA HEC-12 circular from the National Technical Information Service, Springfield, VA 22161. Phone (703) 487-4650.

If you have any questions or suggestions about the program, please call:

Charles D. Scott, PE & RLS or Lynn Ruskin
SMF Engineering Corporation
1915 West Adobe Drive, Suite D
Phoenix, AZ 85027
(602) 516-0605 (voice)
(602) 516-0068 (fax)

To Start:

Copy the contents of the disk into the directory you will be using (e.g. HEC12). To start the program, enter HEC12. To familiarize yourself with the program enter the name of the sample file:

```
Enter Drive and Directory: C:\HEC12
Enter Filename           : [Return]
```

This provides a listing of all files in the directory. You can move through your directory with the arrows keys. Pressing return will select the file highlighted. If you press Esc, you will return to "Enter Filename".

or, you can enter:

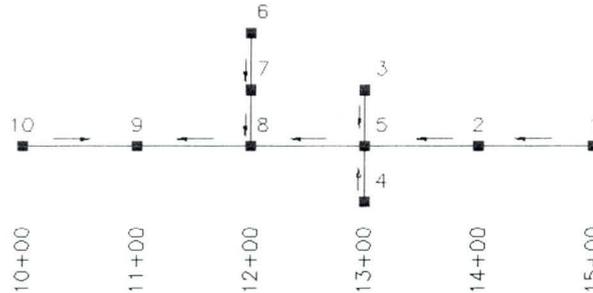
```
Enter Drive and Directory: C:\HEC12
Enter Filename           : SAMPLE1
```

The screen will now show the main menu with the first catch basin, which is located at the upstream terminal.

To start a new file just enter a new filename. The program will then take you directly to the criteria menu.

Main Menu:

It is very important to place the catch basins in the right order. We suggest that you always start your project by drawing up a diagram showing all catch basins, for example:



The first catch basin (number 1) should be the one at the farthest upstream end of the reach. Then add the next catch basin (number 2) downstream, which accepts the bypass. When you have several subreaches, as shown above, you have to add an imaginary catch basin to save the bypass. For this imaginary catch basin, you can enter the ID number of the catch basin that the bypass flows to and enter an 'x' at the "Type of Inlet".

From the Main Menu, you can choose to Add, Insert, Delete or Edit the worksheet that is currently shown (further description follows). You can also Page Up and Page Down through your reach.

F-5 - Criteria:

When you start the program, it will check for the filename you entered. If it exists, it will continue to the main menu. If it can not find the path and filename, it creates the path and file and brings you to the criteria screen. You can enter your project name with up to 45 characters.

Printouts: All printout is configured for a printer with at least 12 characters per inch (cpi). A laser printer will have to be set to a 12 cpi font for good results.

You can select the following printers for output, entering any page length:

- 1 - IBM Proprinter
- 2 - Hewlett Packard
- 3 - Other (Epson FX-80, etc)

Clogging Factors: Please note that you have to add all clogging factors for all catch basins listed before you can run the program. When calculating interception rates, the program will divide the length or area of the catch basin by the clogging factor. If you have entered a curb opening length of 10' and a clogging factor of 1.25', the program will calculate an interception rate for an 8' catch basin. For example, if you have a catch basin that is 20% clogged (80% open), the clogging factor will be $100/80 = 1.25$ and if the clogging is 50% (50% open), the clogging factor will be $100/50 = 2$. Therefore, most likely your clogging factor will vary between 1.0 and 2.0.

F-10

F-10 will save your input data and return you to the first catch basin worksheet. There are no provisions in this program for changing a file name or saving an edited file to a different name. To save an edited file as a different name, you will need to copy the unedited file to its new name first, outside of HEC-12, then call up the new file and edit it.

F-1 - Add

This feature will add catch basin data for a new worksheet at the most downstream end of the reach. Note the worksheet counter in the bottom right hand corner. If you enter the first three parameters, "Station", "Catch Basin ID nr" and "Type of Inlet", and then press F-10, the program will bring forward the remaining parameters from the previous catch basin. If you get an "Incomplete Worksheet", you have not entered all of the information necessary or are copying a parameter from the previous catch basin which is not compatible with the one you are creating. The "Incomplete Worksheet" only works in the "Add", "Insert" or "Edit" mode.

For Type of Inlet, enter;

- "1" for curb opening inlet
- "2.1" through "2.8" for grate inlet
- "3" for slotted drain
- "4.1" through "4.8" for combination inlet

The following Grate Type can be entered;

2.1 or 4.1	P - 1-7/8	Figure 8, HEC-12
2.2 or 4.2	P - 1-7/8 - 4	Figure 8, HEC-12
2.3 or 4.3	P - 1-1/8	Figure 9, HEC-12
2.4 or 4.4	CV - 3-1/4 - 4-1/4	Figure 10, HEC-12
2.5 or 4.5	45 - 2-1/4 - 4	Figure 11, HEC-12
2.6 or 4.6	45 - 3-1/4 - 4	Figure 12, HEC-12
2.7 or 4.7	30 - 3-1/4 - 4	Figure 11, HEC-12
2.8 or 4.8	Reticuline	Figure 13, Hec-12

You can either press **Esc** to quit or press **F-10** to save your worksheet. **F-10** will only work if there are no input errors.

F-2 - Insert

This feature works the same as the "Add" feature but inserts a new catch basin before the one displayed. Please note the sheet counter in the bottom right hand corner of the screen.

F-3 - Delete

"Delete" will delete the catch basin that is shown on the screen.

F-4 - Edit

This feature will allow you to edit any parameter. Use the arrow keys and instructions at the top of the screen. Saving an edited file overwrites the previous file; see **F-10** for instructions on how to save an edited file under a different name.

F-6 - Run

If you run the program and it aborts, it means that you have made an error and you will have to go into the "Edit" mode to find it. If the program runs successfully, you will find yourself at the first catch basin with the output parameters on the bottom of the screen. You can "Page Up" and "Page Down" through your reach.

F-7 - Print:

Make sure the number of lines in the criteria section is the same as for the printer you have selected.

Catch Basin Types

1. Curb Opening Inlet:

You will have to enter only the length of the curb opening.

On Grade - Like the FHWA HEC-12, this program does not limit the depth at the curb for which the equation is applicable. However, when you review your output, you should try to maintain depth below curb (See paragraph 7.2, FHWA HEC-12).

In Sag - When the depth calculated with a weir equation is larger than h (= 4-inch + depression) the orifice equation will be used. Minimum depth will then be h . Enter 0 for the longitudinal grade (See paragraph 8.2, FHWA HEC-12).

2. Grate Inlet:

You will have to enter the area, perimeter, and length of the catch basin.

On Grade - The grate type used for splash-over velocity is different for each grate type as shown on Chart 7, FHWA HEC-12. This chart has been incorporated into this program (See paragraph 7.1, FHWA HEC-12).

In Sag - For depth smaller than 0.8', the weir equation is used and for depth greater than 0.8', the orifice equation is used. Enter 0 for the longitudinal grade (See Paragraph 8.2, FHWA HEC-12).

3. Slotted Drain:

You will have to enter both area and length.

On Grade - The slotted drain equation assumes a weir will occur on one side only (See paragraph 7.3, FHWA HEC-12).

In Sag - For depths smaller than 0.4' the weir equation is used. For depths greater than 0.4', the orifice equation is used. Enter 0 for the longitudinal grade (See paragraph 8.3, FHWA HEC-12).

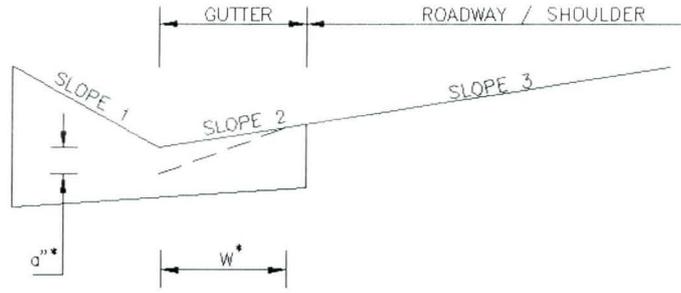
4. Combination Inlets:

When you enter "4.1" - "4.8" for "Type of Inlet" you also will need to enter the area of the grate, the length of the grate, and the length of the upstream curb opening. If you have a combination inlet without an upstream curb opening, you essentially have a grate. In that case, either enter a "2.1" through "2.8" for inlet type, or enter "0.01" for the length of the upstream curb opening with "4.1" - "4.8" for inlet type. A "0" entered for length would cause an "Incomplete Worksheet".

On Grade - With an upstream curb opening, the program first calculates the interception for a curb opening and then calculates the interception for a grate (See paragraph 7.4, FHWA HEC-12).

In Sag - The program uses the weir equations for both grate and curb opening upstream, unless the depth calculated is greater than h (= 4-inch + depression). For depths greater than h , the grate will be calculated with the weir equation and the curb opening upstream with the orifice equation. Enter 0 for the longitudinal grade (See paragraph 8.4, FHWA HEC-12).

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TYPICAL X-SECTION

Design Terms and Abbreviations used in SMF - HEC 12 program
 (Also read the "Glossary of Design Terms" in HEC-12, p. XIII & XIV)

<u>Parameter</u>	<u>: Description</u>	<u>Limitations</u>
Sta	: Station	8 characters
CBID	: Identification Number for Catch Basins	3 characters
C1, C2, C3	: Coefficient of Runoff	$0 \leq C1 \leq 1$
A1, A2, A3	: Drainage Area (acres)	$0 \leq A1 < 100$
Intensity	: Rainfall Intensity (inches/hour)	$0 \leq \text{Intens} \leq 20$
Qadd	: Additional Runoff (cfs)	$0 \leq Q_{add} \leq 100$
Grade	: Longitudinal Gutter Grade (ft/ft)	$0 < \text{Grade} \leq 0.200$
Slope1	: Cross-Slope Face of Curb (ft/ft)	$0 < \text{Slope1} < 100$
Slope2	: Cross-Slope of Gutter (ft/ft)	$0 < \text{Slope2} < 1$
Slope3	: Cross-Slope Roadway Pavement or shoulder (ft/ft)	$0 < \text{Slope3} < 1$
Gutter	: Width of Gutter (ft)	$0 < \text{Gutter} < 90$
a	: Catch Basin Depression below normal gutter line (inch)	$0 \leq A < 10$
W	: Width of Depression (ft)	$0 \leq W < 10$
Area	: Area of Grate excluding the steel bars (sf)	$0 \leq \text{Area} < 100$
Perim	: Length of Weir excluding the steel bars (ft)	$0 \leq \text{Perim} < 100$
Lgrate	: Length grate for combination inlet (ft)	$0 < \text{Lgrate} < 100$
Length	: Length of Catch Basin (ft) (if combination inlet, length upstream of grate)	$0 < \text{Length} < 100$
Flowby	: Flow received as bypass from upstream string of Catch Basin(s) (cfs)	
Qrunoff	: Total Runoff contributed by this area (cfs)	
Qtotal	: Total Flow contributing to this Catch Basin (cfs)	$\{(C1 \cdot A1) + (C2 \cdot A2) + (C3 \cdot A3)\} rli + Q_{add} \neq 0$
Qint	: Flow intercepted by this Catch Basin (cfs)	
Flowby dn	: Flow Bypassed (cfs)	
Depth	: Depth of Flow in Gutter, upstream of Catch Basin (ft)	
Spread	: Width of Flow from gutter line, upstream of CB (ft)	
Veloc	: Velocity in gutter upstream of CB (ft/sec)	
Manning's n Gutter	: Coefficient for roughness	$0 < n < 1$
Manning's n Pavement	: Coefficient for roughness	$0 < n < 1$
Printer Emulation	: Type of printer	1, 2, or 3
Clogging Factor (CF)	: Ratio of CB opening / unclogged opening	$0 < CF < 100$



HYDRAULIC GRADIENT WORKSHEET

SMF Engineering Corporation

Client : City of Scottsdale
 Project : 84th Street and Cholla Road
 Comments : New Storm Drain in Cactus Road
 Trunk Final Design - 50 Yr Storm
 Connector Pipes on North Side of Cactus Road (100 yr storm)

By: RM/LR
 Checked: CDS
 10/27/95 08:21 AM

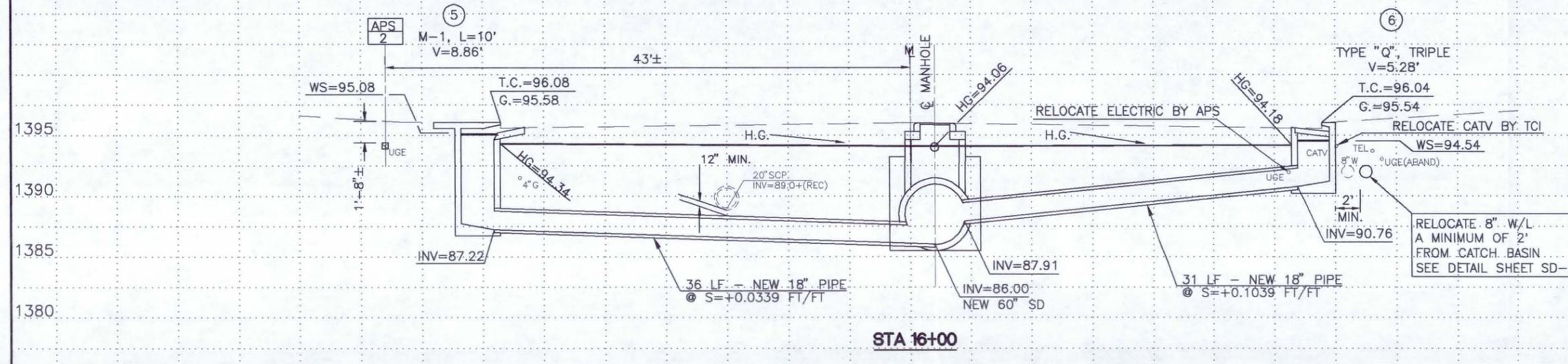
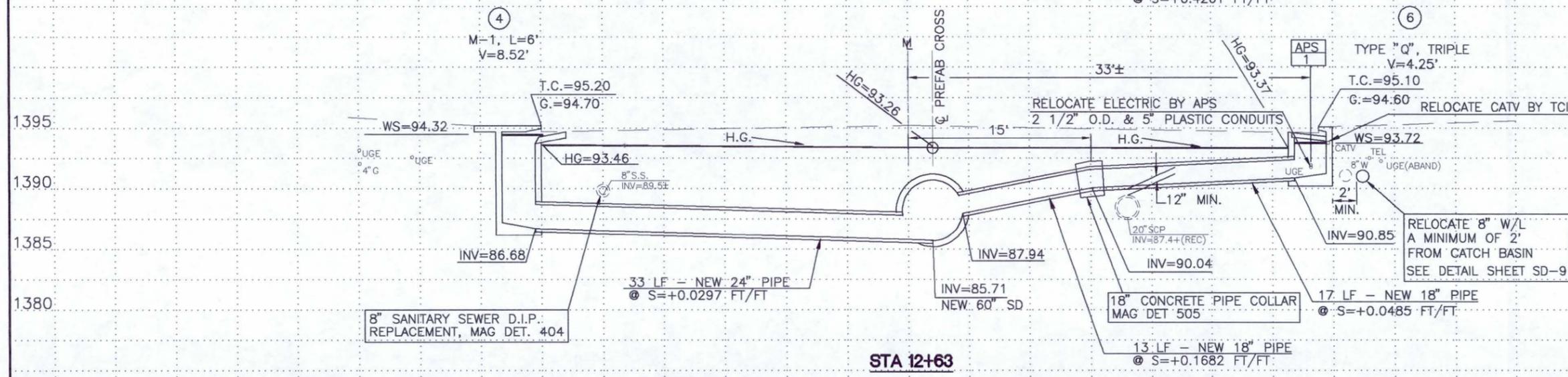
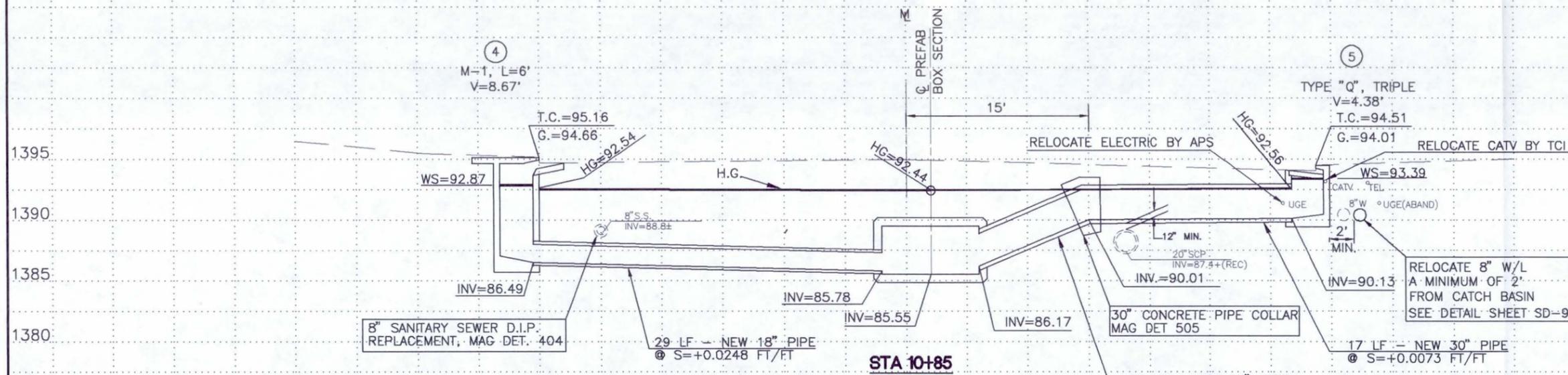
Station	Structure	Pipe Length [ft]	Diam [ft]	Design Q [cfs]	Velocity Head		Energy Losses										Change Hydr Grad Hv2+Ht-Hv1	Hydr Grad Elevation Up Stream	Hydr Grad Elevation Dn Stream	
					Up Strm Hv1	Dn Strm Hv2	Pipe Frict	Angle [Degr]	Bend/ Curve	MH	Contr/ Exp	Angle [Degr]	Q3 [cfs]	Angle [Degr]	Q4 [cfs]	Junction				Total Ht
29+75	CB					0.87						0.43							G=1399.99	
	Pipe	38.0	2.00	23.50	0.87	0.87	0.35									0.43	1.30	1399.24	1397.94	
29+46	Manhole				0.87											0.35	0.35	1397.94	1397.59	
																		1397.59		
29+75	CB					0.87						0.43						G=1399.99		
	Pipe	23.0	2.00	23.50	0.87	0.87	0.21									0.43	1.30	1399.10	1397.80	
29+46	Manhole				0.87											0.21	0.21	1397.80	1397.59	
																		1397.59		
27+90	CB					0.45						0.23						G=1399.00		
	Pipe	8.0	2.00	17.00	0.45	0.45	0.04									0.23	0.68	1398.26	1397.58	
27+90	CB				0.45	0.23						0.12				0.04	0.04	1397.58	1397.54	
	Pipe	55.0	2.50	19.00	0.23	0.23	0.10									0.12	-0.11	1397.54	1397.65	
27+90	Prefab X				0.23											0.10	0.10	1397.65	1397.55	
																		1397.55		
25+35	CB					0.26						0.13						G=1398.20	T.C.=1398.7	
	Pipe	8.0	2.50	20.00	0.26	0.26	0.02									0.13	0.39	1397.68	1397.29	
25+35	CB				0.26	0.40						0.20				0.02	0.02	1397.29	1397.28	
	Pipe	55.0	2.50	25.00	0.40	0.40	0.17									0.20	0.35	1397.28	1396.93	
25+35	Manhole				0.40											0.17	0.17	1396.93	1396.76	
																		1396.76		
22+80	CB					0.24						0.12						G=1397.40		
	Pipe	62.0	1.50	7.00	0.24	0.24	0.23									0.12	0.37	1396.71	1396.34	
22+80	Manhole				0.24											0.23	0.23	1396.34	1396.11	
																		1396.11		

HYDRAULIC GRADIENT WORKSHEET

SMF Engineering Corporation

Client : City of Scottsdale
 Project : 84th Street and Cholla Road
 Comments : New Storm Drain in Cactus Road
 Trunk Final Design - 50 Yr Storm
 Connector Pipes on South Side of Cactus Road (100 yr storm)

Station	Structure	Pipe Lenght [ft]	Diam [ft]	Design Q [cfs]	Velocity Head		Energy Losses										Change Hydr Grad Hv2+Ht-Hv1	Hydr Grad Elevation Up Stream	Hydr Grad Elevation Dn Stream	
					Up Strm	Dn Strm	Pipe	Angle	Bend/	MH	Contr/	Angle	Q3	Angle	Q4	Junction				Total
					Hv1	Hv2	Frict	[Degr]	Curve		Exp	[Degr]	[cfs]	[Degr]	[cfs]	Ht				
27+90	CB					0.18						0.09						G=1399.06		
	Pipe	8.0	1.50	6.00	0.18	0.18	0.02												1397.84	1397.57
27+90	Prefab X				0.18														1397.57	1397.55
																			1397.55	
22+80	CB					0.16						0.08						G=1397.50		
	Pipe	8.0	2.00	10.00	0.16	0.16	0.01												1396.36	1396.12
22+80	Prefab X				0.16														1396.12	1396.11
																			1396.11	
19+50	CB					0.37						0.18						G=1396.60		
	Pipe	31.0	1.50	8.60	0.37	0.37	0.18												1395.51	1394.96
19+50	Prefab X				0.37														1394.96	1394.78
																			1394.78	
16+00	CB					0.24						0.12						G=1395.50		
	Pipe	31.0	1.50	7.00	0.24	0.24	0.12												1394.54	1394.18
16+00	Manhole				0.24														1394.18	1394.06
																			1394.06	
12+63	CB					0.24						0.12						G=1394.60		
	Pipe	30.0	1.50	6.90	0.24	0.24	0.11												1393.72	1393.37
12+63	Prefab X				0.24														1393.37	1393.26
																			1393.26	
10+85	CB					0.56						0.28						G=1394.10		
	Pipe	27.0	2.50	29.40	0.56	0.56	0.12												1393.39	1392.56
10+85	Prefab Junc.				0.56														1392.56	1392.44
																			1392.44	

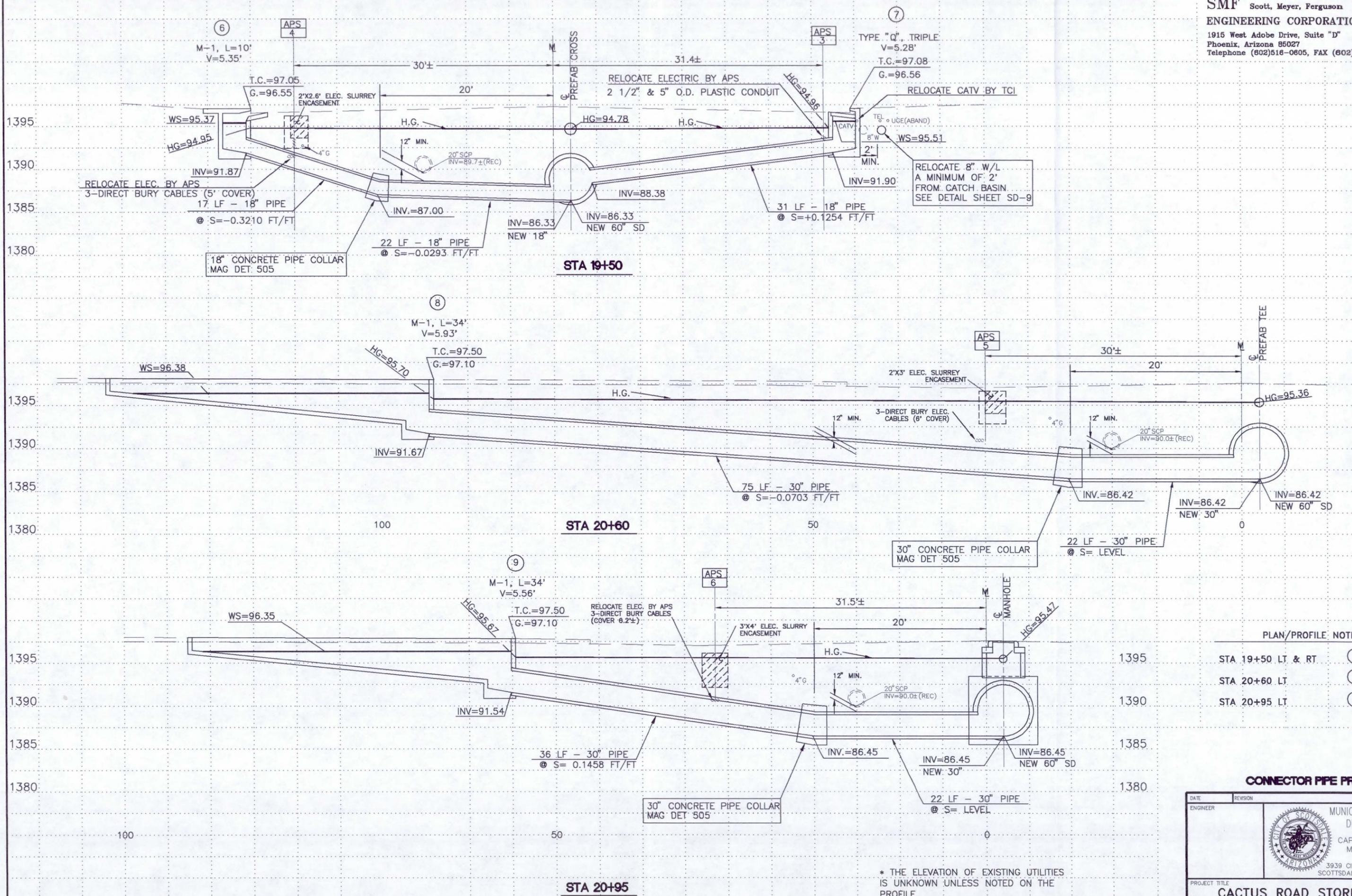


PLAN/PROFILE NOTE	
STA 10+85 LT & RT	④
STA 12+63 LT & RT	④
STA 16+00 LT & RT	⑤

* THE ELEVATION OF EXISTING UTILITIES IS UNKNOWN UNLESS NOTED ON THE PROFILE.

CONNECTOR PIPE PROFILE

DATE	REVISION
ENGINEER	
	
MUNICIPAL S DEPART CAPITAL P MANAGE 3939 CIVIC CEN SCOTTSDALE, ARIZ	
PROJECT TITLE	
CACTUS ROAD STORM DF	
SCALE	DESIGNED BY
HORIZ. 1"=5'	CDS
VERT. 1"=5'	DR
CHECKED BY	BID NO.
MC	96-55
AS-BUILT	PROJECT NO.
	F2708



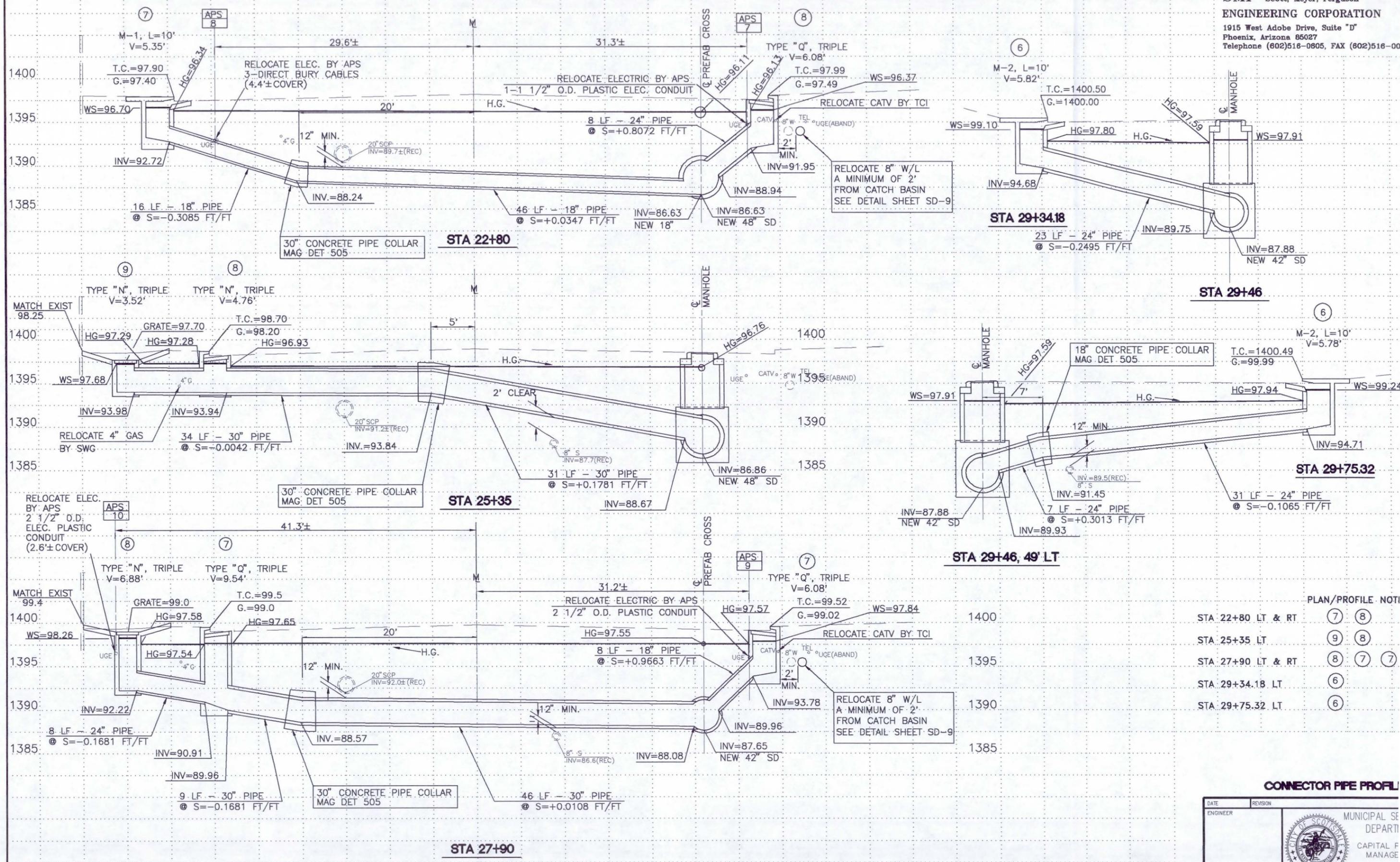
PLAN/PROFILE NOTE

STA 19+50 LT & RT	⑥
STA 20+60 LT	⑧
STA 20+95 LT	⑨

* THE ELEVATION OF EXISTING UTILITIES IS UNKNOWN UNLESS NOTED ON THE PROFILE.

CONNECTOR PIPE PROFILE

DATE	REVISION		MUNICIPAL S DEPARTM CAPITAL PR MANAGEM 3939 CIVIC CENT SCOTTSDALE, ARIZO
ENGINEER			
PROJECT TITLE CACTUS ROAD STORM DP			
SCALE	DESIGNED BY	CHECKED BY	BD NO.
HORIZ. 1"=5'	CDS	MC	96-55
VERT. 1"=5'	DRAWN	AS-BUILT	PROJECT NO.
	TR		F2708



PLAN/PROFILE	NOTI
STA 22+80 LT & RT	(7) (8)
STA 25+35 LT	(9) (8)
STA 27+90 LT & RT	(8) (7) (7)
STA 29+34.18 LT	(6)
STA 29+75.32 LT	(6)

* THE ELEVATION OF EXISTING UTILITIES IS UNKNOWN UNLESS NOTED ON THE PROFILE.

CONNECTOR PIPE PROFILE

DATE	REVISION	 MUNICIPAL SE DEPARTI CAPITAL F MANAGE 3939 CIVIC CEN SCOTTSDALE, ARIZ
ENGINEER		
PROJECT TITLE		
CACTUS ROAD STORM D		
SCALE	DESIGNED BY	CHECKED BY
HORIZ. 1"=5'	CDS	MC
VERT. 1"=5'	LR	AS-BUILT
	BID NO.	96-55
	PROJECT NO.	F2708



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*****
1 * HEC-2 WATER SURFACE PROFILES *
* *
* Version 4.6.2; May 1991 *
* *
* RUN DATE 23FEB95 TIME 10:10:22 *
*****
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*****
* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET, SUITE D *
* DAVIS, CALIFORNIA 95616-4687 *
* (916) 756-1104 *
*****
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THIS RUN EXECUTED 23FEB95 10:10:22

HEC-2 WATER SURFACE PROFILES

Version 4.6.2; May 1991

T1 84TH STREET AND CACTUS ROAD DRAINAGE IMPROVEMENT PROJECT
T2 SUBCRITICAL FLOW IN FAIRWAY SOUTH OF CACTUS - FILE FAIRULS.DAT
T3 ULTIMATE CONDITION-STORM DRAIN OUTFALL AT BOX-CULVERT
T4 NO CORTEZ CONNECTOR

J1 ICHECK INQ NINV IDIR STRT METRIC HVINS Q WSEL FQ
0 2 0 0 0 0 0 0 1378.46 1

J2 NPROF IPLIT PRFVS XSECV XSECH FN ALLDC IBW CHNIM ITRACE
0 0 -1

J3 VARIABLE CODES FOR SUMMARY PRINTOUT

38 43 13 14 15 42 53 54 8 1
2 17

QT 1 515
NC .04 .04 .030 .1 .3
X1 10.00 3 9930 10060
GR 1379 9930 1373.53 10000 1382 10060

X1 11.00 6 9918 10070 46 47 45
GR 1384 9918 1379 9940 1379 9974 1376 10000 1381.5 10070
GR 1383.7 10100

X1 12.00 5 9951 10065 50 48 51
GR 1384 9951 1378 9983 1377.2 10000 1378 10015 1383 10065

X1 13.00 4 9952 10045 50 42 46
GR 1386 9952 1378 9987 1377 10000 1384 10045

X1 14.00 4 9940 10060 61 51 57
GR 1386 9940 1379 9977 1378 10000 1387 10060

X1 15.00 4 9935 10070 16 15 16
GR 1386 9935 1379 9978 1378 10000 1387 10070

X1	16.00	8	9945	10075	42	58	50			
GR	1386	9931	1384	9945	1383	9954	1380	9965	1379	9978
GR	1377.5	10000	1379	10030	1383	10075				

X1	17.00	8	9942	10050	42	56	47			
GR	1387	9942	1382	9968	1380	9978	1379	9994	1378.1	10000
GR	1379	10010	1380	10020	1385	10050				

QT	1	501								
NC	.040	.040	.012							
X1	18.00	4	9986.9	10013.1	32	58	44			
GR	1386	9986.9	1378	9987	1378	10013	1386	10013.1		

X1	19.00	4	9986.9	10013.1	56	66	60			
GR	1386	9986.9	1378.5	9987	1378.5	10013	1386	10013.1		

X1	20.00	4	9986.9	10013.1	57	57	57			
GR	1386	9986.9	1378.9	9987	1378.9	10013	1386	10013.1		

X1	21.00	4	9986.9	10013.1	44	44	44			
GR	1386	9986.9	1379.1	9987	1379	10013	1386	10013.1		

X1	22.00	4	9986.9	10013.1	52	52	52			
GR	1386	9986.9	1379.4	9987	1379.4	10013	1386	10013.1		

NC	.040	.040	.030							
X1	23.00	4	9986.9	10013.1	54	54	54			
GR	1386	9986.9	1380	9987	1380	10013	1386	10013.1		

X1	24.00	33	9965.9	10044.2	39	1	22			
GR	1394.4	9781.4	1394.1	9787.7	1392.6	9795.2	1391.0	9797.9	1391.0	9804.4
GR	1391.6	9810.0	1391.3	9819.1	1389.1	9832.1	1388.8	9844.9	1389.6	9856.7
GR	1389.3	9867.7	1386.9	9881.9	1385.1	9891.5	1383.1	9903.7	1382.4	9914.3
GR	1382.3	9927.2	1382.5	9941.2	1383.2	9948.1	1384.5	9956.5	1385.0	9963.0
GR	1384.8	9965.9	1381.9	9974.3	1381.4	9979.3	1380.4	9989.9	1380.2	9999.2
GR	1380.2	10000.0	1380.1	10007.5	1380.6	10016.3	1381.9	10027.0	1382.4	10029.7
GR	1386.2	10044.2	1386.6	10053.4	1386.4	10059.5				

X1	25.00	62	9933.8	10044.2	26	1	15			
GR	1384.8	9690.2	1385.2	9697.2	1386.0	9703.4	1386.7	9708.1	1386.6	9710.5
GR	1385.4	9716.6	1384.9	9722.5	1385.4	9732.4	1386.1	9737.7	1386.8	9745.4
GR	1388.0	9753.2	1388.9	9757.7	1389.5	9764.8	1389.6	9769.6	1389.6	9777.4
GR	1389.3	9786.8	1388.7	9787.7	1388.6	9792.7	1388.4	9799.1	1388.5	9802.2
GR	1388.9	9803.5	1388.8	9808.4	1388.7	9815.9	1388.4	9824.9	1388.2	9833.4
GR	1388.3	9836.2	1388.3	9842.2	1388.5	9852.1	1388.5	9860.5	1388.3	9866.9
GR	1388.0	9875.2	1387.0	9882.4	1386.6	9888.9	1386.2	9894.4	1386.7	9899.1
GR	1387.2	9905.1	1387.7	9911.1	1387.9	9915.7	1387.6	9921.5	1386.4	9925.9
GR	1384.5	9933.8	1383.7	9939.5	1383.6	9942.9	1384.6	9947.6	1385.0	9951.6
GR	1385.1	9957.5	1382.2	9966.5	1381.1	9972.5	1380.9	9975.7	1381.1	9984.1
GR	1381.0	9994.4	1380.8	9999.3	1380.5	10000.0	1380.1	10002.5	1380.6	10006.4
GR	1380.8	10014.1	1381.6	10021.9	1382.4	10031.5	1382.5	10034.7	1386.2	10044.2
GR	1386.6	10053.4	1386.4	10059.5	0.0	0.0	0.0	0.0	0.0	0.0

X1	44.00	24	9953.8	10031.0	53	46	50			
GR	1390.9	9920.8	1390.9	9921.8	1391.5	9926.8	1391.5	9934.7	1391.2	9944.8
GR	1390.6	9953.8	1389.3	9969.4	1388.1	9980.6	1387.4	9988.7	1386.5	9992.4
GR	1386.2	9996.4	1387.2	10000.0	1387.1	10004.9	1388.3	10014.3	1389.7	10021.7
GR	1391.6	10031.0	1392.4	10037.7	1392.4	10045.0	1392.0	10057.7	1391.3	10066.2
GR	1391.0	10068.5	1391.2	10077.7	1391.1	10088.5	1391.1	10090.1	0.0	0.0

X1	45.00	21	9960.3	10040.7	52	44	49			
GR	1391.6	9938.4	1393.3	9939.9	1394.6	9947.1	1394.8	9952.4	1393.9	9960.3
GR	1391.1	9973.2	1388.5	9984.7	1387.1	9992.7	1386.5	9997.5	1387.2	10000.0
GR	1387.6	10006.0	1388.0	10014.2	1389.3	10024.1	1390.7	10031.8	1391.6	10040.7
GR	1391.4	10051.7	1391.5	10063.6	1391.5	10075.1	1391.8	10083.6	1392.4	10090.3
GR	1392.6	10094.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0

X1	46.00	26	9968.0	10040.3	56	25	51			
GR	1391.8	9946.8	1392.8	9948.8	1393.0	9953.2	1393.0	9958.9	1391.4	9968.0
GR	1388.2	9979.6	1388.0	9986.8	1387.5	9993.0	1386.7	9999.0	1387.1	10000.0
GR	1387.7	10006.2	1387.9	10011.6	1388.1	10019.7	1389.4	10027.3	1391.0	10035.0
GR	1392.5	10040.3	1393.0	10042.1	1393.1	10044.4	1393.2	10055.5	1393.3	10067.6
GR	1393.1	10074.8	1392.0	10079.8	1392.1	10085.8	1392.2	10091.6	1392.5	10100.3
GR	1392.5	10104.5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0

QT	1	438								
X1	47.00	31	9969.4	10036.4	68	11	47			
GR	1392.5	9926.3	1392.5	9928.4	1393.3	9929.3	1393.5	9934.3	1393.5	9943.0
GR	1393.7	9953.0	1393.4	9960.0	1392.0	9969.4	1390.0	9978.8	1388.3	9985.0
GR	1388.2	9991.6	1388.2	9994.2	1387.3	9998.4	1387.4	10000.0	1387.5	10003.3
GR	1388.3	10009.4	1388.3	10014.2	1388.6	10022.0	1389.9	10027.5	1391.0	10032.5
GR	1392.0	10036.4	1392.9	10039.8	1393.3	10045.3	1393.3	10052.6	1393.3	10056.3
GR	1393.4	10073.0	1392.3	10079.4	1392.2	10081.9	1392.2	10092.7	1392.7	10106.4
GR	1392.8	10109.8	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0

X1	48.00	30	9935.5	10054.0	58	28	46			
GR	1392.6	9875.3	1394.5	9877.4	1394.8	9881.6	1394.6	9887.9	1393.8	9894.4
GR	1393.2	9902.9	1392.5	9907.6	1393.2	9915.7	1394.2	9922.7	1395.0	9928.3
GR	1394.0	9935.5	1393.0	9944.8	1392.0	9955.2	1390.4	9964.5	1389.2	9971.9
GR	1388.3	9980.7	1387.8	9994.0	1387.7	10000.0	1388.0	10008.4	1388.8	10017.6
GR	1389.6	10023.9	1390.2	10033.5	1391.4	10042.9	1391.9	10048.3	1392.2	10054.0
GR	1392.9	10062.6	1393.0	10070.7	1392.6	10078.7	1392.4	10087.7	1392.6	10093.0

X1	49.00	33	9956.1	10042.2	53	45	52			
GR	1392.7	9826.6	1392.7	9830.2	1393.1	9833.6	1392.9	9840.1	1393.0	9847.7
GR	1394.1	9855.7	1394.9	9862.1	1395.8	9870.4	1396.2	9877.9	1396.3	9886.1
GR	1396.6	9894.3	1396.5	9901.0	1396.2	9905.6	1395.9	9915.4	1394.8	9922.4
GR	1394.5	9932.2	1394.0	9941.5	1392.5	9948.4	1392.1	9956.1	1389.9	9967.8
GR	1388.2	9975.8	1387.8	9986.0	1387.4	9994.3	1387.3	10000.0	1387.6	10009.1
GR	1388.8	10017.6	1390.2	10026.6	1391.3	10033.4	1392.0	10042.2	1392.5	10052.1
GR	1392.4	10060.9	1392.5	10069.6	1392.5	10076.7	0.0	0.0	0.0	0.0

X1	50.00	38	9971.8	10054.9	46	51	49			
GR	1392.8	9791.1	1393.0	9797.7	1393.5	9806.4	1394.3	9814.1	1395.1	9822.4
GR	1395.4	9831.2	1395.7	9841.2	1397.1	9848.3	1397.9	9856.0	1398.2	9863.6
GR	1397.5	9872.4	1397.2	9882.7	1396.5	9892.2	1395.6	9903.3	1396.5	9913.9
GR	1396.6	9914.1	1395.7	9923.3	1394.0	9932.7	1392.5	9941.3	1392.7	9952.8
GR	1392.5	9962.4	1393.1	9971.8	1392.5	9977.1	1390.7	9983.4	1388.8	9990.3
GR	1387.7	9996.8	1387.4	10000.0	1387.5	10004.9	1388.3	10011.2	1389.2	10021.0
GR	1390.5	10027.6	1391.4	10035.9	1392.0	10043.3	1392.6	10051.4	1393.1	10054.9
GR	1393.2	10059.9	1392.7	10064.7	1392.6	10070.3	0.0	0.0	0.0	0.0

X1	51.00	41	9953.2	10092.0	39	65	50			
GR	1392.8	9772.5	1393.6	9780.6	1394.0	9786.4	1395.2	9792.4	1395.6	9798.1
GR	1395.1	9807.1	1394.6	9812.7	1395.7	9820.8	1396.1	9828.9	1396.2	9837.9
GR	1396.5	9848.6	1396.7	9857.4	1397.0	9868.2	1397.5	9874.2	1397.0	9880.6
GR	1396.4	9890.1	1395.9	9898.7	1394.8	9901.5	1394.4	9911.4	1393.3	9920.8
GR	1394.2	9930.3	1395.4	9938.0	1395.6	9946.7	1394.6	9953.2	1393.1	9960.2
GR	1391.8	9969.7	1390.1	9979.0	1388.5	9988.8	1387.6	9999.2	1387.4	10000.0
GR	1387.5	10006.2	1388.7	10013.8	1389.3	10019.5	1390.2	10026.7	1390.7	10033.7
GR	1390.8	10042.4	1391.0	10053.2	1391.6	10064.4	1392.2	10076.8	1392.9	10092.0
GR	1393.2	10099.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0

X1	52.00	38	9948.2	10036.5	38	67	50			
GR	1393.0	9763.1	1393.0	9765.1	1393.5	9768.7	1393.7	9776.3	1394.6	9790.3
GR	1395.7	9801.4	1397.0	9808.7	1397.4	9814.2	1396.9	9827.4	1396.8	9836.2
GR	1397.0	9849.5	1397.4	9859.4	1397.8	9867.9	1396.4	9878.3	1394.4	9882.1
GR	1394.8	9889.5	1394.8	9897.1	1394.2	9915.4	1393.8	9931.4	1393.6	9948.2
GR	1393.1	9958.8	1392.8	9968.5	1391.1	9976.4	1388.9	9987.8	1387.8	9993.1
GR	1387.9	10000.0	1388.4	10009.0	1389.8	10017.6	1391.4	10024.8	1392.4	10031.4
GR	1392.9	10036.5	1392.8	10043.7	1392.5	10056.7	1392.9	10068.1	1394.3	10079.6
GR	1395.5	10088.7	1396.2	10093.5	1396.3	10096.8	0.0	0.0	0.0	0.0

X1	53.00	40	9927.1	10116.8	38	69	50			
GR	1393.1	9761.0	1393.6	9765.0	1393.6	9772.6	1394.5	9783.3	1395.4	9793.8
GR	1396.4	9804.7	1397.0	9814.7	1397.5	9824.8	1398.3	9829.0	1398.5	9837.6
GR	1397.3	9845.3	1395.1	9851.1	1394.6	9862.9	1394.7	9873.2	1394.6	9886.2
GR	1394.6	9901.1	1393.7	9927.1	1393.1	9947.1	1392.0	9961.5	1390.7	9970.5
GR	1389.3	9980.3	1388.5	9987.4	1388.1	9994.2	1388.5	10000.0	1389.1	10012.3
GR	1389.6	10021.7	1390.0	10027.1	1390.8	10036.6	1391.3	10049.6	1391.5	10061.7
GR	1391.8	10079.2	1392.0	10090.6	1392.4	10104.5	1393.0	10116.8	1393.0	10128.3
GR	1392.7	10141.8	1393.0	10157.6	1393.2	10174.7	1393.4	10195.6	1393.4	10199.0

X1	54.00	60	9951.2	10092.4	38	64	47			
GR	1393.3	9764.2	1393.4	9767.3	1393.9	9771.0	1393.9	9776.5	1393.8	9785.0
GR	1395.0	9791.0	1396.2	9799.6	1397.4	9805.8	1398.5	9810.3	1399.6	9815.9
GR	1400.0	9820.8	1399.8	9825.6	1398.2	9834.4	1397.5	9848.0	1395.8	9859.3
GR	1393.8	9869.0	1395.3	9880.5	1394.6	9887.5	1395.8	9894.9	1394.6	9898.5
GR	1395.0	9905.2	1394.9	9911.8	1394.3	9919.8	1394.3	9920.2	1394.1	9938.3
GR	1393.6	9951.2	1393.4	9962.8	1390.8	9974.7	1388.8	9981.2	1388.5	9986.8
GR	1387.7	9990.7	1388.1	9995.1	1388.6	9998.3	1388.6	10000.0	1389.0	10007.3
GR	1389.6	10013.5	1389.8	10020.0	1390.6	10027.5	1391.3	10034.7	1392.1	10041.6
GR	1393.0	10047.4	1392.8	10052.2	1392.3	10059.7	1391.5	10067.0	1391.3	10076.4
GR	1391.8	10086.3	1393.0	10092.4	1394.4	10100.0	1395.0	10105.7	1394.6	10112.1
GR	1394.1	10113.4	1393.5	10122.2	1393.7	10129.7	1393.9	10136.6	1394.9	10141.1

HEC-2 WATER SURFACE PROFILES

Version 4.6.2; May 1991

NOTE- ASTERISK (*) AT LEFT OF CROSS-SECTION NUMBER INDICATES MESSAGE IN SUMMARY OF ERRORS LIST

ULTIMATE CONDITION-STORM

SUMMARY PRINTOUT

SECNO	Q	QLOB	QCH	QROB	ELMIN	SSTA	ENDST	DEPTH	CWSEL	CRIWS	K* XNCH
10.000	515.00	.00	515.00	.00	1373.53	9936.91	10034.92	4.93	1378.46	.00	30.00
* 11.000	515.00	.00	515.00	.00	1376.00	9976.69	10034.24	2.69	1378.69	1378.69	30.00
* 12.000	515.00	.00	515.00	.00	1377.20	9975.21	10029.61	2.26	1379.46	1379.46	30.00
* 13.000	515.00	.00	515.00	.00	1377.00	9978.37	10019.11	2.97	1379.97	1379.97	30.00
14.000	515.00	.00	515.00	.00	1378.00	9967.28	10018.93	2.84	1380.84	.00	30.00
15.000	515.00	.00	515.00	.00	1378.00	9965.08	10024.14	3.10	1381.10	.00	30.00
* 16.000	515.00	.00	515.00	.00	1377.50	9959.62	10057.77	3.97	1381.47	.00	30.00
* 17.000	515.00	.00	515.00	.00	1378.10	9971.44	10027.87	3.20	1381.30	.00	30.00
* 18.000	501.00	.00	501.00	.00	1378.00	9986.96	10013.04	3.27	1381.27	.00	12.00
19.000	501.00	.00	501.00	.00	1378.50	9986.96	10013.04	2.61	1381.11	.00	12.00
* 20.000	501.00	.00	501.00	.00	1378.90	9986.97	10013.03	2.25	1381.15	1381.15	12.00
* 21.000	501.00	.00	501.00	.00	1379.00	9986.97	10013.03	2.31	1381.31	1381.31	12.00
* 22.000	501.00	.00	501.00	.00	1379.40	9986.97	10013.03	2.25	1381.65	1381.65	12.00
* 23.000	501.00	.00	501.00	.00	1380.00	9986.96	10013.04	2.25	1382.25	1382.25	30.00
* 24.000	501.00	47.01	453.99	.00	1380.10	9901.81	10033.55	3.32	1383.42	.00	30.00
25.000	501.00	.00	501.00	.00	1380.10	9962.71	10037.06	3.32	1383.42	.00	30.00
26.000	445.00	.00	445.00	.00	1381.10	9957.72	10031.31	2.35	1383.45	.00	30.00

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	SECNO	Q	QLOB	QCH	QROB	ELMIN	SSTA	ENDST	DEPTH	CWSEL	CRIWS	K* XNCH
*	27.000	445.00	.00	445.00	.00	1381.30	9969.11	10028.00	2.20	1383.50	.00	30.00
	28.000	445.00	.00	445.00	.00	1381.40	9967.36	10031.17	2.36	1383.76	.00	30.00
*	29.000	445.00	.09	444.91	.00	1381.60	9907.19	10030.02	2.43	1384.03	.00	30.00
	30.000	445.00	.00	445.00	.00	1381.80	9959.22	10032.86	2.26	1384.06	.00	30.00
	31.000	445.00	.61	444.39	.00	1381.90	9964.73	10029.65	2.23	1384.13	.00	30.00
	32.000	445.00	.00	445.00	.00	1382.10	9949.75	10027.85	2.23	1384.33	.00	30.00
	33.000	445.00	1.18	443.82	.00	1382.20	9944.80	10029.74	2.25	1384.45	.00	30.00
	34.000	445.00	.00	445.00	.00	1382.30	9957.53	10025.48	2.23	1384.53	.00	30.00
*	35.000	445.00	.00	445.00	.00	1382.60	9964.76	10025.59	2.02	1384.62	.00	30.00
*	36.000	445.00	.00	445.00	.00	1382.30	9956.42	10029.84	2.75	1385.05	.00	30.00
	37.000	445.00	3.70	441.30	.00	1383.20	9922.02	10031.08	1.99	1385.19	.00	30.00
*	38.000	445.00	.00	445.00	.00	1383.70	9960.34	10025.21	1.59	1385.29	1385.29	30.00
	39.000	445.00	.00	445.00	.00	1383.90	9969.81	10022.53	1.98	1385.88	.00	30.00
*	40.000	445.00	.00	445.00	.00	1384.70	9976.33	10029.14	1.79	1386.49	1386.49	30.00
*	41.000	445.00	.00	445.00	.00	1385.30	9984.12	10027.60	1.84	1387.14	1387.14	30.00
*	42.000	445.00	.00	445.00	.00	1385.60	9976.08	10028.71	2.46	1388.06	1388.06	30.00
*	43.000	445.00	.00	445.00	.00	1385.50	9977.78	10018.68	3.25	1388.75	1388.75	30.00
*	44.000	445.00	.00	445.00	.00	1386.20	9966.26	10020.97	3.36	1389.56	.00	30.00
	45.000	445.00	.00	445.00	.00	1386.50	9979.10	10026.66	3.27	1389.77	.00	30.00
*	46.000	445.00	.00	445.00	.00	1386.70	9972.35	10031.16	3.50	1390.20	.00	30.00
	47.000	438.00	.00	438.00	.00	1387.30	9977.64	10029.07	2.95	1390.25	.00	30.00
	48.000	438.00	.00	438.00	.00	1387.70	9963.54	10036.36	2.86	1390.56	.00	30.00
	49.000	438.00	.00	438.00	.00	1387.30	9963.60	10029.63	3.39	1390.69	.00	30.00
*	50.000	438.00	.00	438.00	.00	1387.40	9983.72	10028.63	3.21	1390.61	.00	30.00
	51.000	438.00	.00	438.00	.00	1387.40	9974.07	10053.21	3.60	1391.00	.00	30.00
	52.000	438.00	.00	438.00	.00	1387.80	9976.59	10023.29	3.26	1391.06	.00	30.00

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SECNO	Q	QLOB	QCH	QROB	ELMIN	SSTA	ENDST	DEPTH	CWSEL	CRIWS	K* XNCH
53.000	438.00	.00	438.00	.00	1388.10	9965.71	10055.14	3.29	1391.39	.00	30.00
54.000	438.00	.00	438.00	.00	1387.70	9971.65	10079.72	3.77	1391.47	.00	30.00
* 54.100	438.00	16.72	421.28	.00	1389.90	9936.20	10019.87	1.72	1391.62	1391.62	30.00
* 55.000	438.00	.00	438.00	.00	1386.00	9975.50	10061.17	6.23	1392.23	.00	30.00